

Variational Nonlocal Regularization in Finite-Deformation Inelasticity

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COMPLAS XI

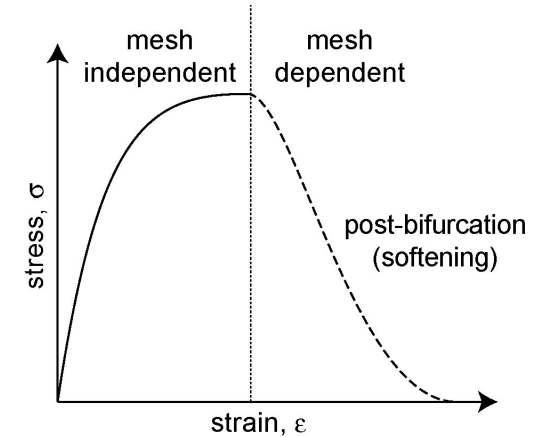
Barcelona, Spain, 7-9 September 2011

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Loss of Ellipticity

Softening behavior

Stress-strain curve has one or more peaks.



Loss of ellipticity

Governing partial differential equation changes character.

$$\text{Div } \mathbf{P} + \mathbf{B} = \mathbf{0}$$

Loss of convexity

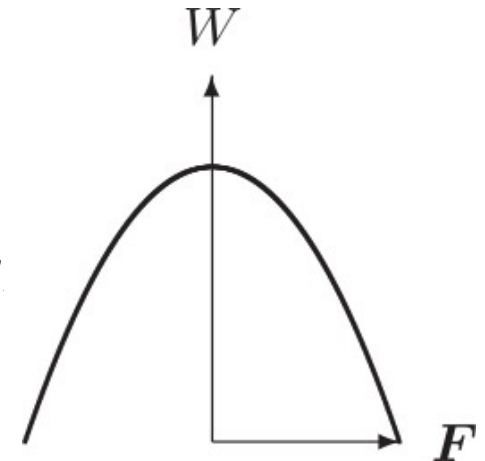
Stored energy function becomes non-convex.

$$\Phi[\varphi] = \int_B W(\mathbf{F}, \mathbf{Z}, T) dV - \int_B \mathbf{B} \cdot \varphi dV - \int_{\partial_T B} \bar{\mathbf{T}} \cdot \varphi dS$$

Non-positive-definite Hessian

Tangent modulus becomes non-positive definite (singular acoustic tensor).

$$\mathbb{C} = 4 \frac{\partial^2 W}{\partial \mathbf{C}^2}$$



Non-positive-definite stiffness

Stiffness has one or more null or negative eigenvalues.

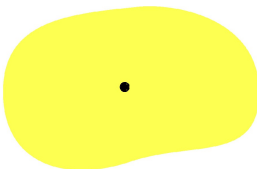
Regularization Methods

Gradient Formulations

$$\Phi[\varphi] = \int_B A(\mathbf{F}, \mathcal{K}, \mathbf{Z}, T) dV + \Phi^{\text{ext}}[\varphi]$$

$$\bar{\mathbf{Z}} = \mathbf{Z}_0 + \nabla^2 \mathbf{Z}(\mathbf{X}_0) : \mathbf{H}(D) + \dots$$

- ✓ By-passes loss of ellipticity entirely.
- ✓ Capable of modeling post-peak behavior.
- ✗ Special boundary considerations.
- ✗ Constitutive models require modifications.

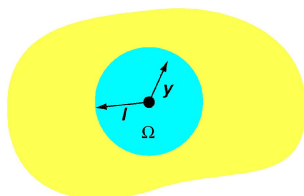


Nonlocal FE Formulations

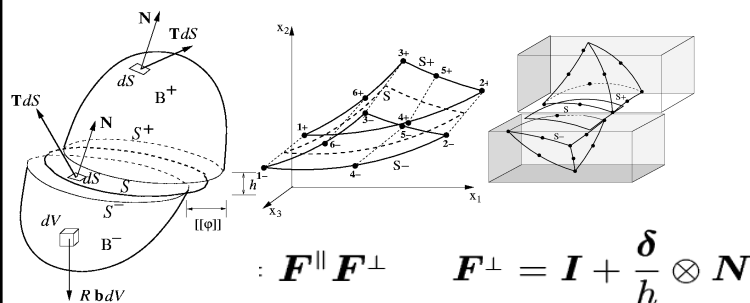
$$\bar{\mathbf{F}}(\mathbf{X}) := \frac{1}{\Psi(\mathbf{X})} \int_D \psi(\mathbf{X}, \mathbf{Y}) \mathbf{F}(\mathbf{Y}) dV$$

$$\Psi(\mathbf{X}) := \int_D \psi(\mathbf{X}, \mathbf{Y}) dV$$

- ✓ Confine localization to nonlocal domain.
- ✓ Use constitutive behavior as-is.
- ✗ Special boundary considerations.
- ✗ Requires “cut off” approaches.

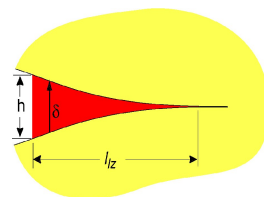


Localization Elements



- ✓ Use constitutive behavior as-is.
- ✓ Accurate and efficient.
- ✗ Failure follows mesh geometry.
- ✗ Requires robust adaptive insertion.

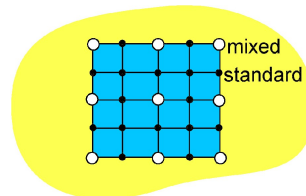
(Yang, Mota, Ortiz; IJNME 2005)



Variational Nonlocal Method

$$\begin{aligned} \Phi[\varphi, \bar{\mathbf{Z}}, \bar{\mathbf{Y}}] := & \int_B W(\mathbf{F}, \bar{\mathbf{Z}}, \mathbf{Q}, T) dV + \int_B \bar{\mathbf{Y}} \cdot (\bar{\mathbf{Z}} - \mathbf{Z}) dV \\ & - \int_B \rho_0 \mathbf{B} \cdot \varphi dV - \int_{\partial_T B} \mathbf{T} \cdot \varphi dS \end{aligned}$$

- ✓ Nonlocality defined naturally.
- ✓ Use constitutive behavior as-is.



Motivation for Variational Methods

- Begin from fundamental physical principles.
- Governing equations from optimization.
- Allow better analysis for uniqueness of solutions.
- Lead to robust numerical methods.
- Help identify correct conjugate fields.
- Et cetera.

Variational Nonlocal Method

Three-Field Mixed Finite Element Formulation:

$$\Phi[\varphi, \bar{\mathbf{Z}}, \bar{\mathbf{Y}}] := \int_B W(\mathbf{F}, \bar{\mathbf{Z}}, \mathbf{Q}, T) dV + \int_B \bar{\mathbf{Y}} \cdot (\bar{\mathbf{Z}} - \mathbf{Z}) dV - \int_B \rho_0 \mathbf{B} \cdot \varphi dV - \int_{\partial_T B} \mathbf{T} \cdot \varphi dS$$

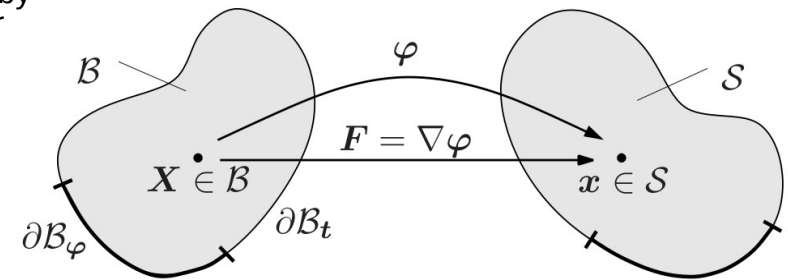
Deformation
Mapping

Helmholtz Free
Energy

Nonlocal
Internal
Variable

Constraint Enforced by
Lagrange Multiplier

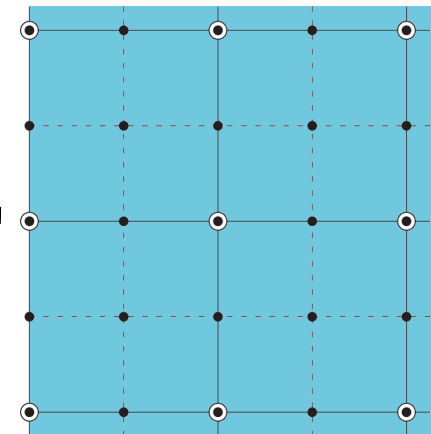
- Motivated through studies of non-locality
- Fully variational approach.
- Entirely by-passes ad hoc approaches.
- Does not require any modifications to constitutive models.
- Nonlocal domain is defined naturally by support of mixed interpolation functions.
- Natural parallelization by domain decomposition of coarse discretization.
- Does not require cut-off approaches at boundary.
- Weight functions are unit interpolation functions.



Deformation Mapping

Natural
boundary for
both levels

- Standard node
fine level
- Mixed node
coarse level



Finite Element Formulation

Three-Field Mixed Finite Element Formulation:

$$\Phi[\boldsymbol{\varphi}, \bar{\mathbf{Z}}, \bar{\mathbf{Y}}] := \int_B W(\mathbf{F}, \bar{\mathbf{Z}}, \mathbf{Q}, T) dV + \int_B \bar{\mathbf{Y}} \cdot (\bar{\mathbf{Z}} - \mathbf{Z}) dV - \int_B \rho_0 \mathbf{B} \cdot \boldsymbol{\varphi} dV - \int_{\partial_T B} \mathbf{T} \cdot \boldsymbol{\varphi} dS$$

Variations:

$$\boldsymbol{\varphi} \in V_\varphi := (W_2^1(B))^3, \bar{\mathbf{Z}} \in V_Z := (W_2^1(B))^q \text{ and } \bar{\mathbf{Y}} \in V_Y := (W_2^1(B))^q$$

$$\boldsymbol{\eta} \in V_\varphi, \boldsymbol{\zeta} \in V_Z \text{ and } \boldsymbol{\xi} \in V_Y$$

$$D\Phi[\boldsymbol{\varphi}, \bar{\mathbf{Z}}, \bar{\mathbf{Y}}](\boldsymbol{\eta}) = \int_B \mathbf{P} : \text{Grad } \boldsymbol{\eta} dV - \int_B \rho_0 \mathbf{B} \cdot \boldsymbol{\eta} dV - \int_{\partial_T B} \mathbf{T} \cdot \boldsymbol{\eta} dS = 0,$$

$$D\Phi[\boldsymbol{\varphi}, \bar{\mathbf{Z}}, \bar{\mathbf{Y}}](\boldsymbol{\zeta}) = \int_B (\bar{\mathbf{Y}} - \mathbf{Y}) \cdot \boldsymbol{\zeta} dV = 0,$$

$$D\Phi[\boldsymbol{\varphi}, \bar{\mathbf{Z}}, \bar{\mathbf{Y}}](\boldsymbol{\xi}) = \int_B (\bar{\mathbf{Z}} - \mathbf{Z}) \cdot \boldsymbol{\xi} dV = 0,$$

$$\mathbf{P} := \partial W / \partial \mathbf{F} \quad \mathbf{Y} := -\partial W / \partial \bar{\mathbf{Z}}$$

Regularization

Discrete Statement of Equilibrium,
Internal Variables and Conjugate Forces:

$$\int_B \mathbf{P} \cdot \text{Grad } N_a \, dV - \int_B \rho_0 \mathbf{B} N_a \, dV - \int_{\partial_T B} \mathbf{T} N_a \, dS = \mathbf{0},$$

$$\bar{\mathbf{Y}} = \lambda_\alpha \left(\int_B \lambda_\alpha \lambda_\beta \, dV \right)^{-1} \int_B \lambda_\beta \mathbf{Y} \, dV,$$

$$\bar{\mathbf{Z}} = \lambda_\alpha \left(\int_B \lambda_\alpha \lambda_\beta \, dV \right)^{-1} \int_B \lambda_\beta \mathbf{Z} \, dV,$$

Unit Interpolation, Regularized Variables:

$$\lambda_\alpha = 1, \lambda_\beta = 1 \quad \longrightarrow \quad \begin{aligned} \bar{\mathbf{Y}} &= \frac{1}{\text{vol}(D)} \int_D \mathbf{Y} \, dV, \\ \bar{\mathbf{Z}} &= \frac{1}{\text{vol}(D)} \int_D \mathbf{Z} \, dV, \\ \text{vol}(\bullet) &:= \int_{(\bullet)} dV, \end{aligned}$$

Connection to Gradients

Expansion in Taylor Series:

$$\mathbf{Z} = \mathbf{Z}_0 + \frac{\partial \mathbf{Z}}{\partial \mathbf{X}}(\mathbf{X}_0) \cdot (\mathbf{X} - \mathbf{X}_0) + \frac{1}{2}(\mathbf{X} - \mathbf{X}_0) \cdot \frac{\partial^2 \mathbf{Z}}{\partial \mathbf{X}^2}(\mathbf{X}_0) \cdot (\mathbf{X} - \mathbf{X}_0) + \dots$$

Apply to Regularized Variables:

$$\bar{\mathbf{Z}} = \mathbf{Z}_0 + \frac{1}{2 \text{vol}(D)} \frac{\partial^2 \mathbf{Z}}{\partial \mathbf{X}^2}(\mathbf{X}_0) : \int_D (\mathbf{X} - \mathbf{X}_0) \otimes (\mathbf{X} - \mathbf{X}_0) dV + \dots$$

Obtain Gradient Regularization:

$$\bar{\mathbf{Z}} = \mathbf{Z}_0 + \nabla^2 \mathbf{Z}(\mathbf{X}_0) : \mathbf{H}(D) + \dots$$

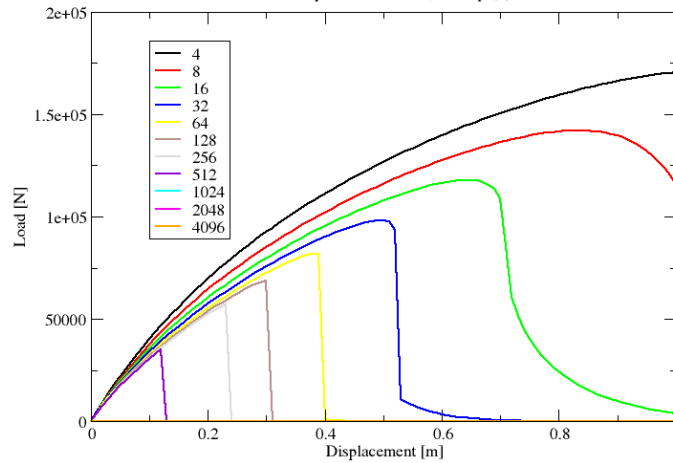
1D Problem – Stretching of Bar

- Proof of concept problem.
- Area proportional to square root of length.
- Strong singularity on left end of bar.
- Simple hyperelastic model with damage.
- Code written in Matlab.
- Two interpolation schemes.

Constant Unit Interpolation

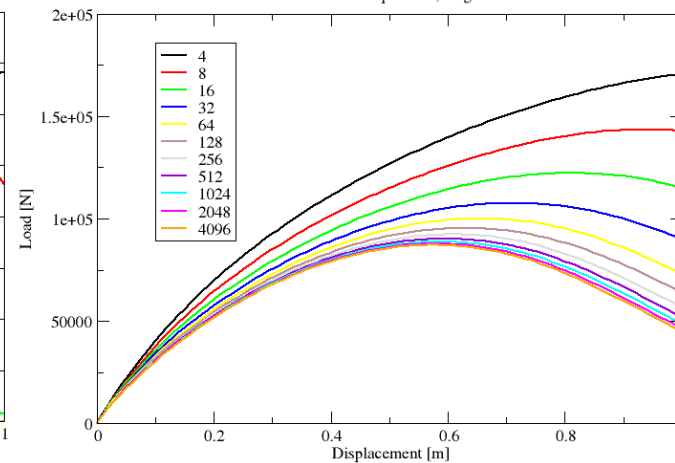
Stretching of Tapered Bar

Mesh-dependent solutions, $A = \sqrt{x}$



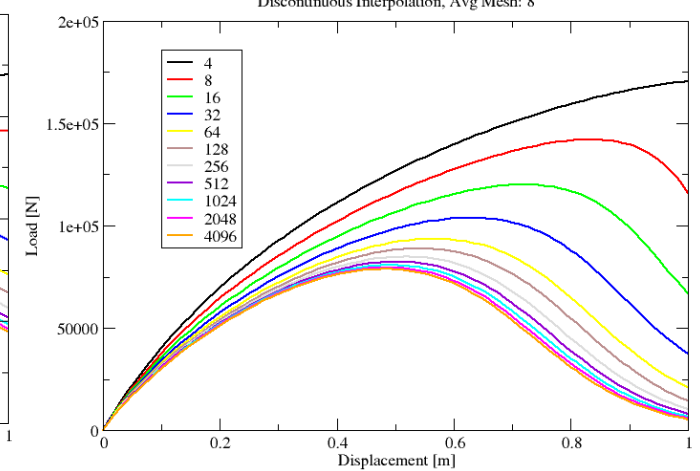
Stretching of Tapered Bar

Discontinuous Interpolation, Avg Mesh: 4



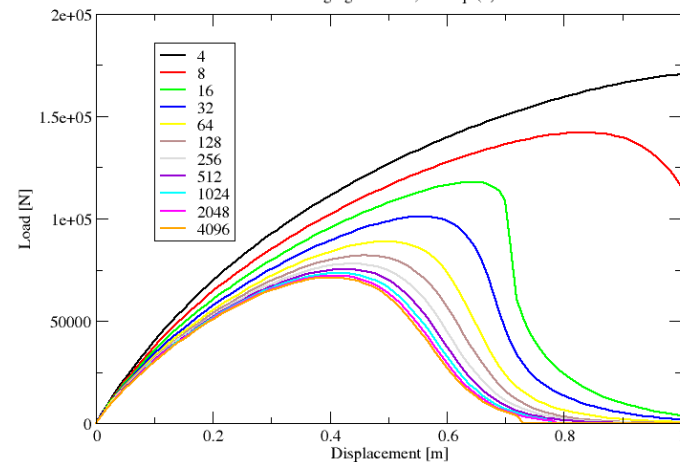
Stretching of Tapered Bar

Discontinuous Interpolation, Avg Mesh: 8



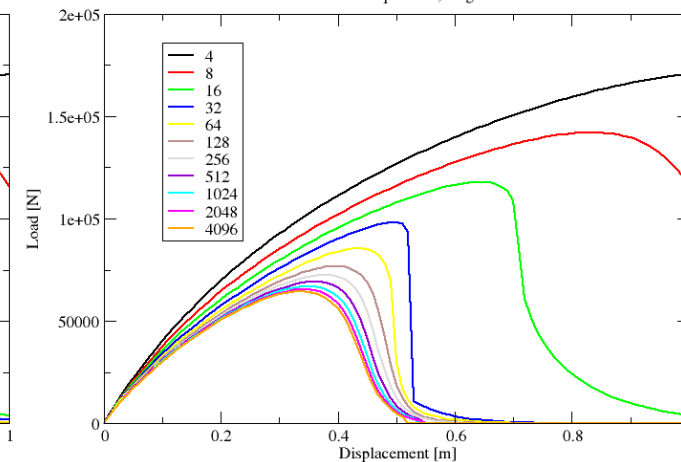
Stretching of Tapered Bar

Averaging level = 3, $A = \sqrt{x}$



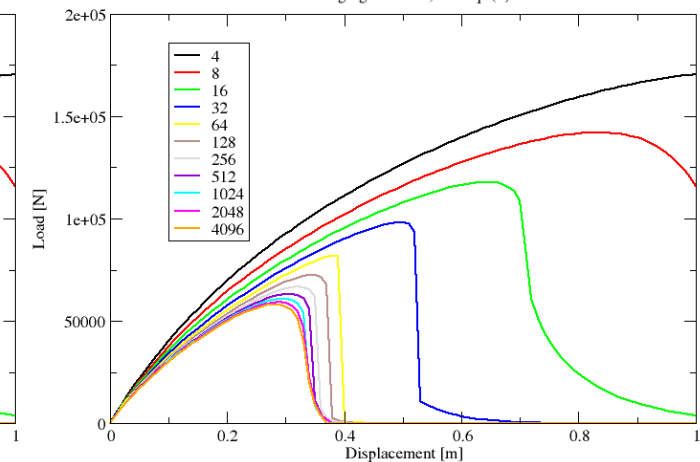
Stretching of Tapered Bar

Discontinuous Interpolation, Avg Mesh: 32



Stretching of Tapered Bar

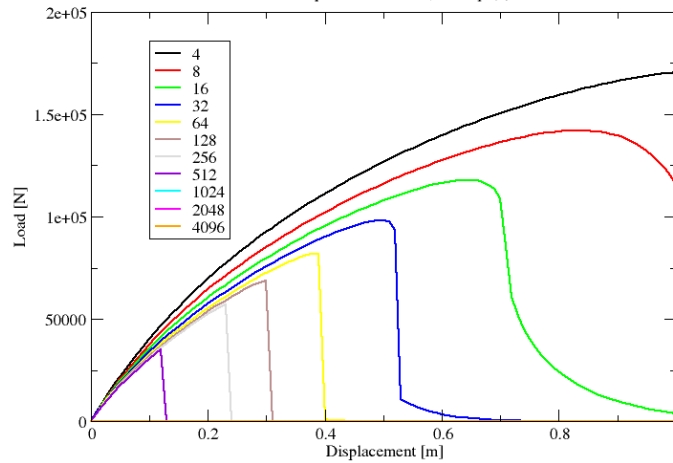
Averaging level = 5, $A = \sqrt{x}$



Linear Interpolation

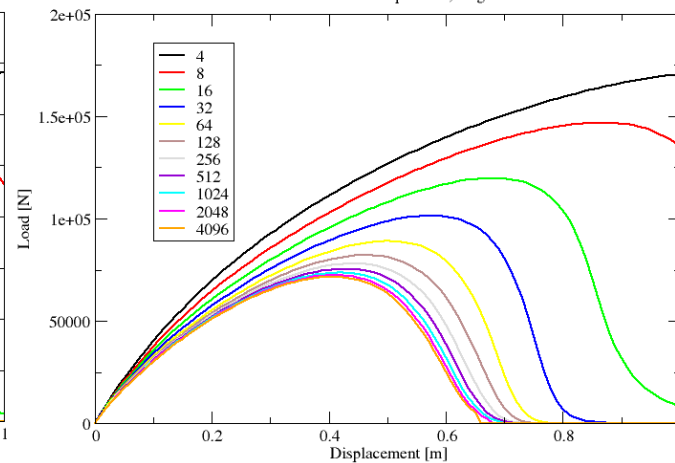
Stretching of Tapered Bar

Mesh-dependent solutions, $A = \sqrt{x}$



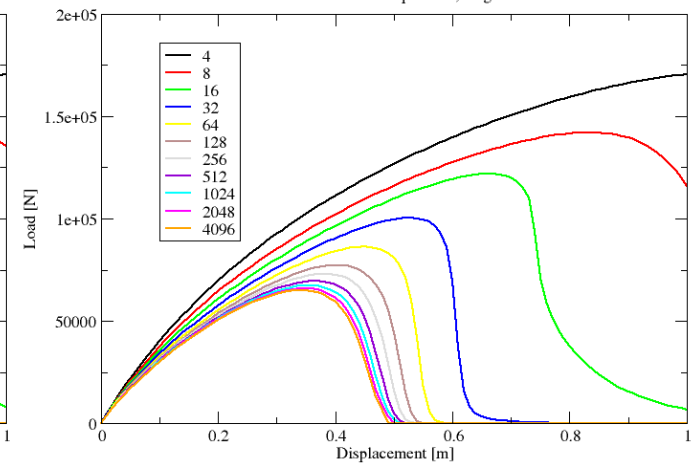
Stretching of Tapered Bar

Piecewise-linear C^0 Interpolation, Avg. Mesh: 4



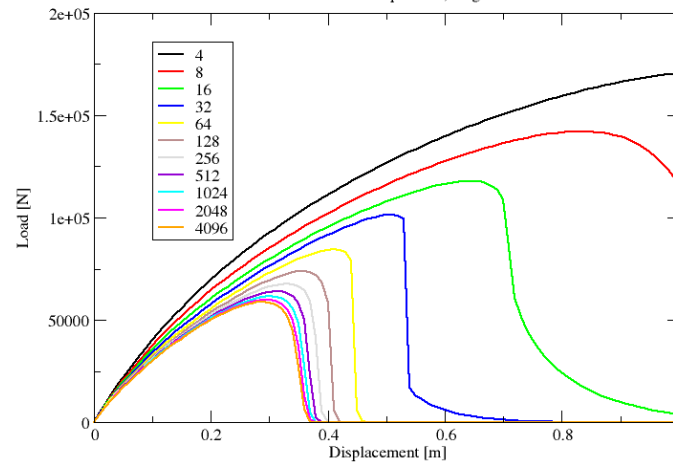
Stretching of Tapered Bar

Piecewise-linear C^0 Interpolation, Avg. Mesh: 8



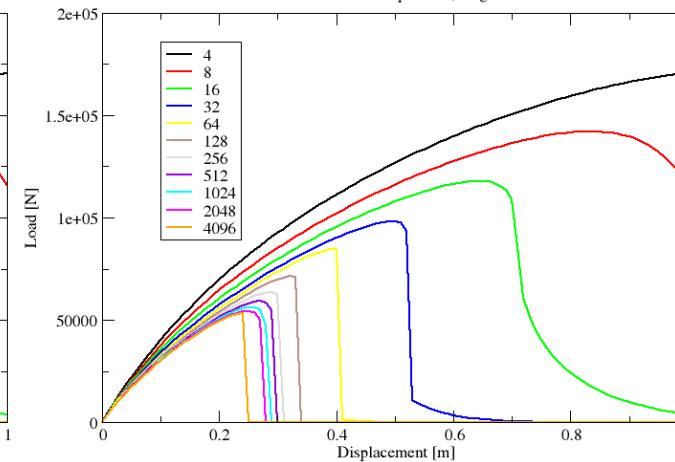
Stretching of Tapered Bar

Piecewise-linear C^0 Interpolation, Avg. Mesh: 16



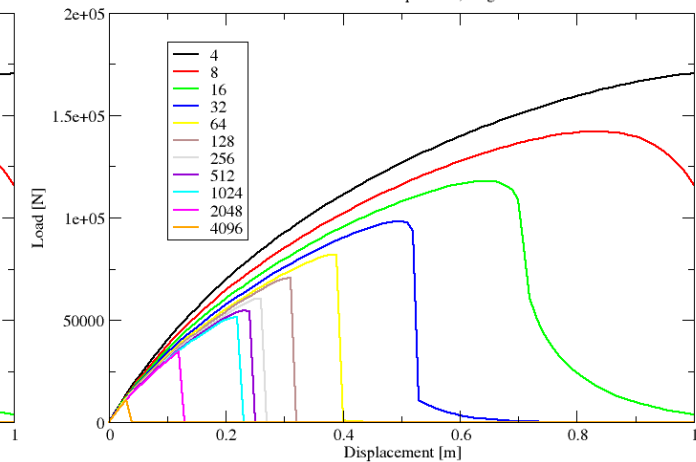
Stretching of Tapered Bar

Piecewise-linear C^0 Interpolation, Avg. Mesh: 32



Stretching of Tapered Bar

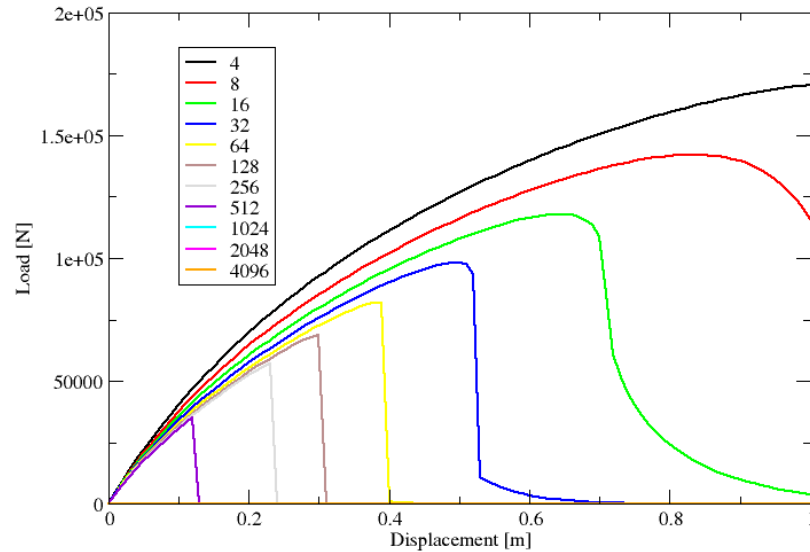
Piecewise-linear C^0 Interpolation, Avg. Mesh: 64



Avg Mesh 4, Unit Interpolation

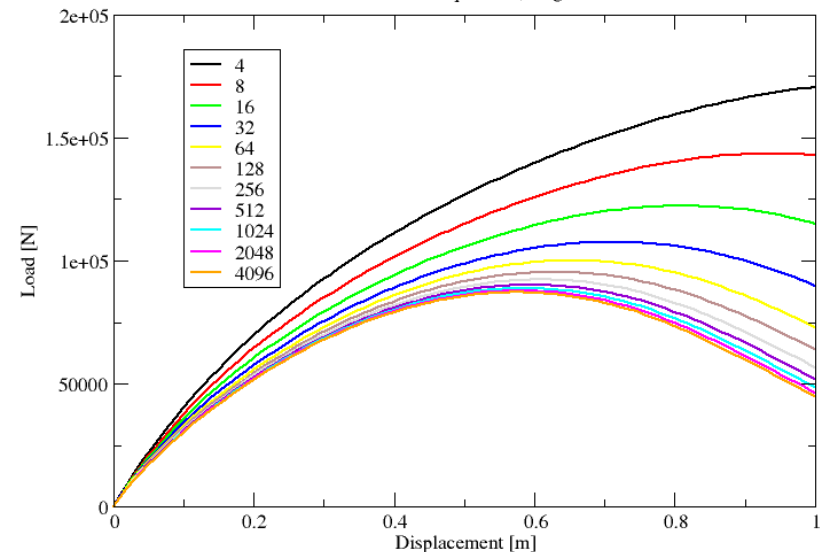
Stretching of Tapered Bar

Mesh-dependent solutions, $A = \sqrt{x}$



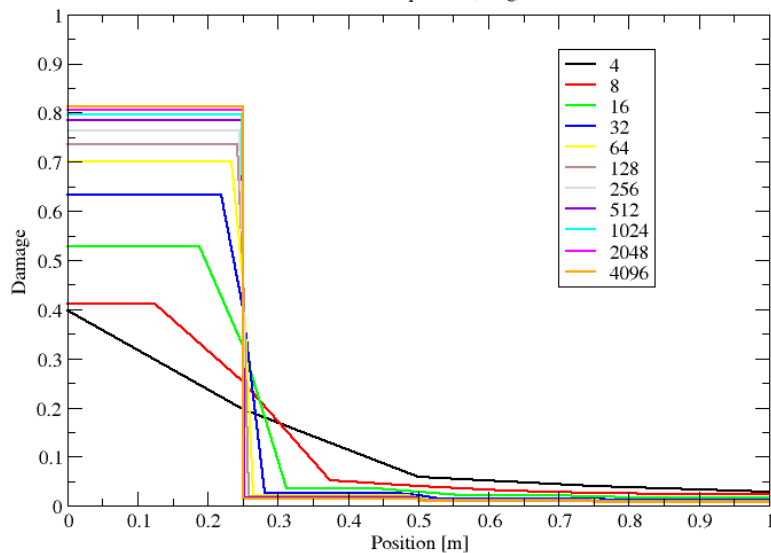
Stretching of Tapered Bar

Discontinuous Interpolation, Avg Mesh: 4



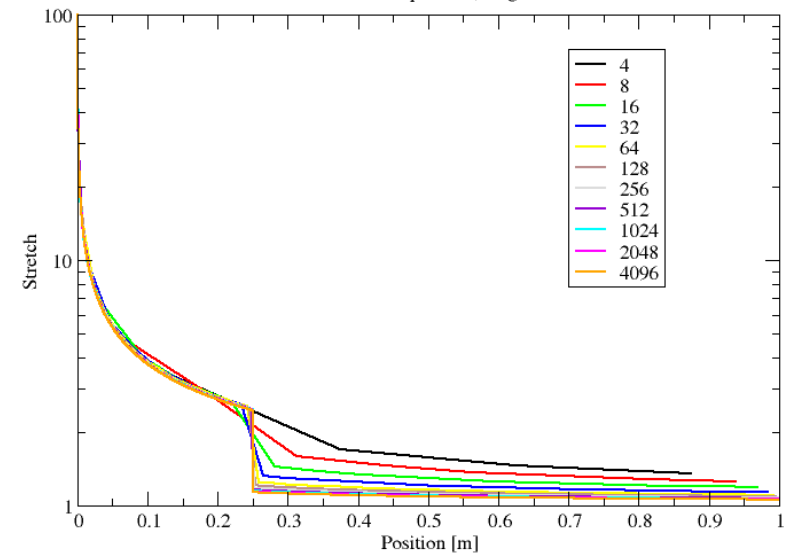
Stretching of Tapered Bar

Discontinuous Interpolation, Avg Mesh: 4

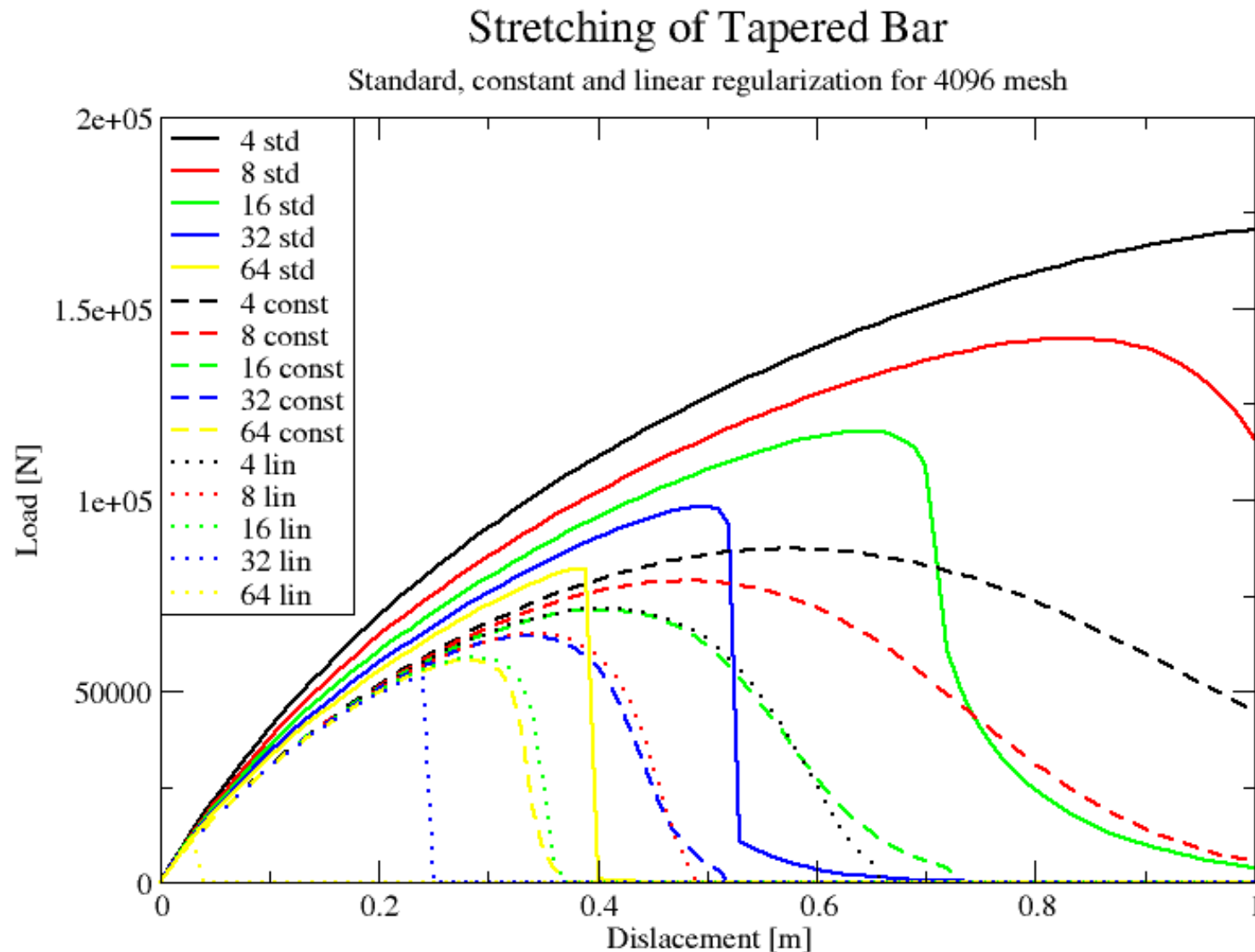


Stretching of Tapered Bar

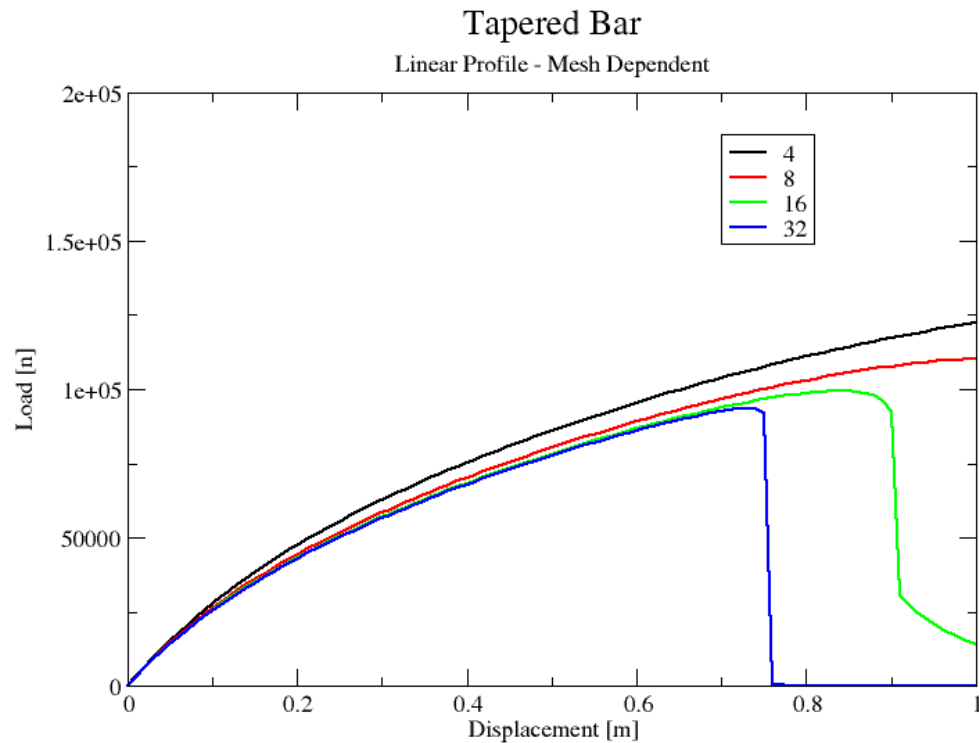
Constant C^{-1} Interpolation, Avg. Mesh: 4



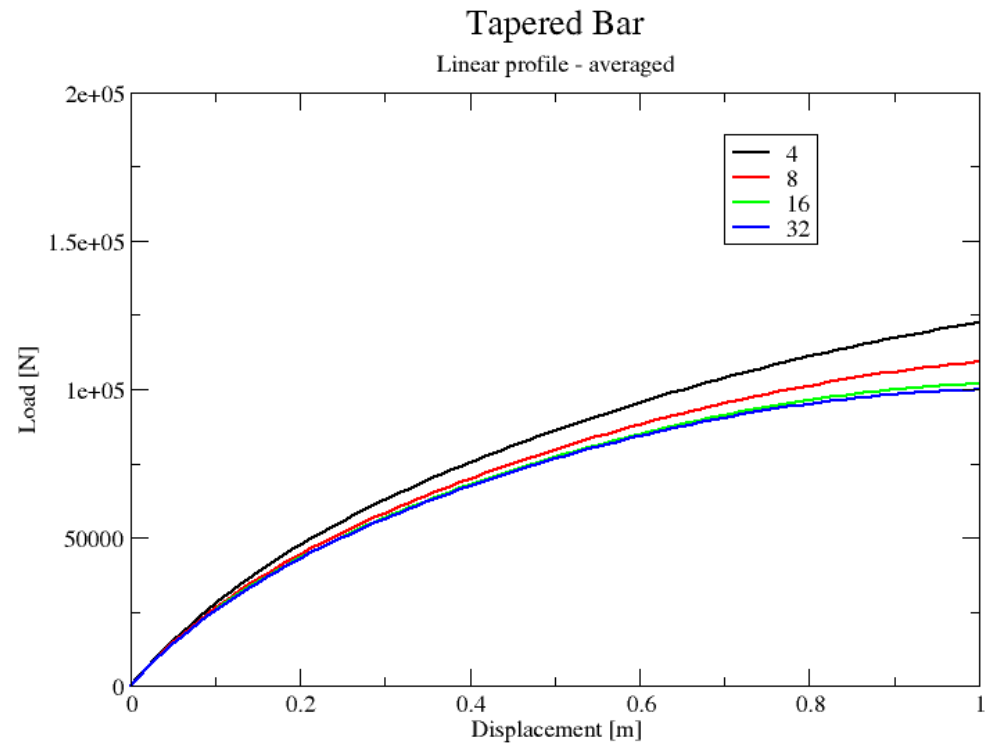
Effect of Order of Interpolation



Weaker Defect – V Profile Bar



Mesh Dependent



Regularized

Mesh Dependence

Simple finite-deformation elastic model with damage:

$$W(\mathbf{C}, \zeta) = (1 - \zeta)W_0(\mathbf{C})$$

$$W_0(\mathbf{C}) = W_0^{\text{vol}}(\theta) + W_0^{\text{dev}}(\bar{\epsilon}),$$

$$\zeta(\alpha) := \zeta_\infty [1 - \exp(-\alpha/\iota)]$$

$$\epsilon = \frac{1}{2} \log(\mathbf{C})$$

$$W_0^{\text{vol}}(\theta) = \frac{\kappa}{4} [\exp(2\theta) - 1 - 2\theta],$$

$$\alpha(t) := \max_{s \in [0, t]} W_0(s)$$

$$\bar{\epsilon} = \text{dev}(\epsilon), \quad \theta = \text{tr}(\epsilon),$$

$$W_0^{\text{dev}}(\bar{\epsilon}) = \frac{\mu}{2} [\text{tr}(\exp \bar{\epsilon}) - 3].$$

ζ_∞ : maximum possible damage
 ι : damage saturation parameter

$$E = 200 \text{ GPa}$$

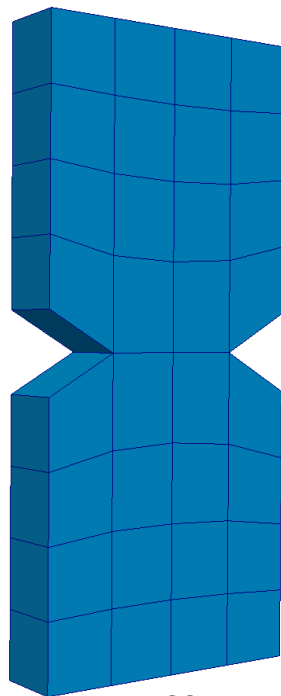
$$\nu = 0.25$$

$$\kappa = 133 \text{ GPa}$$

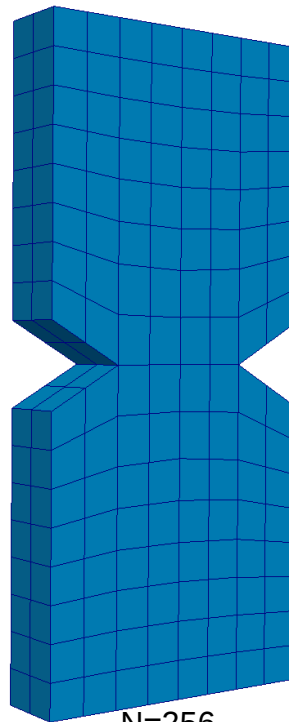
$$\mu = 67 \text{ GPa}$$

$$\zeta_\infty = 1.0$$

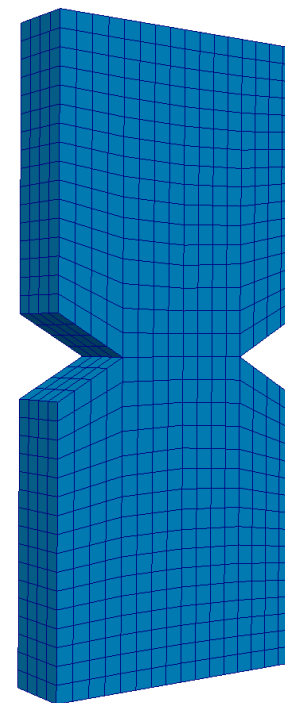
$$\iota = 100 \text{ GJm}^{-3}$$



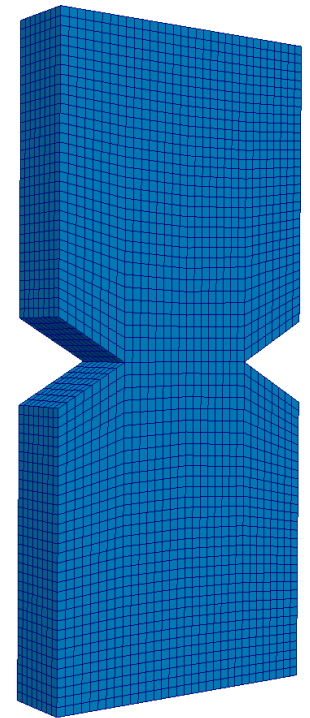
N=32
h~1mm



N=256
h~0.5mm

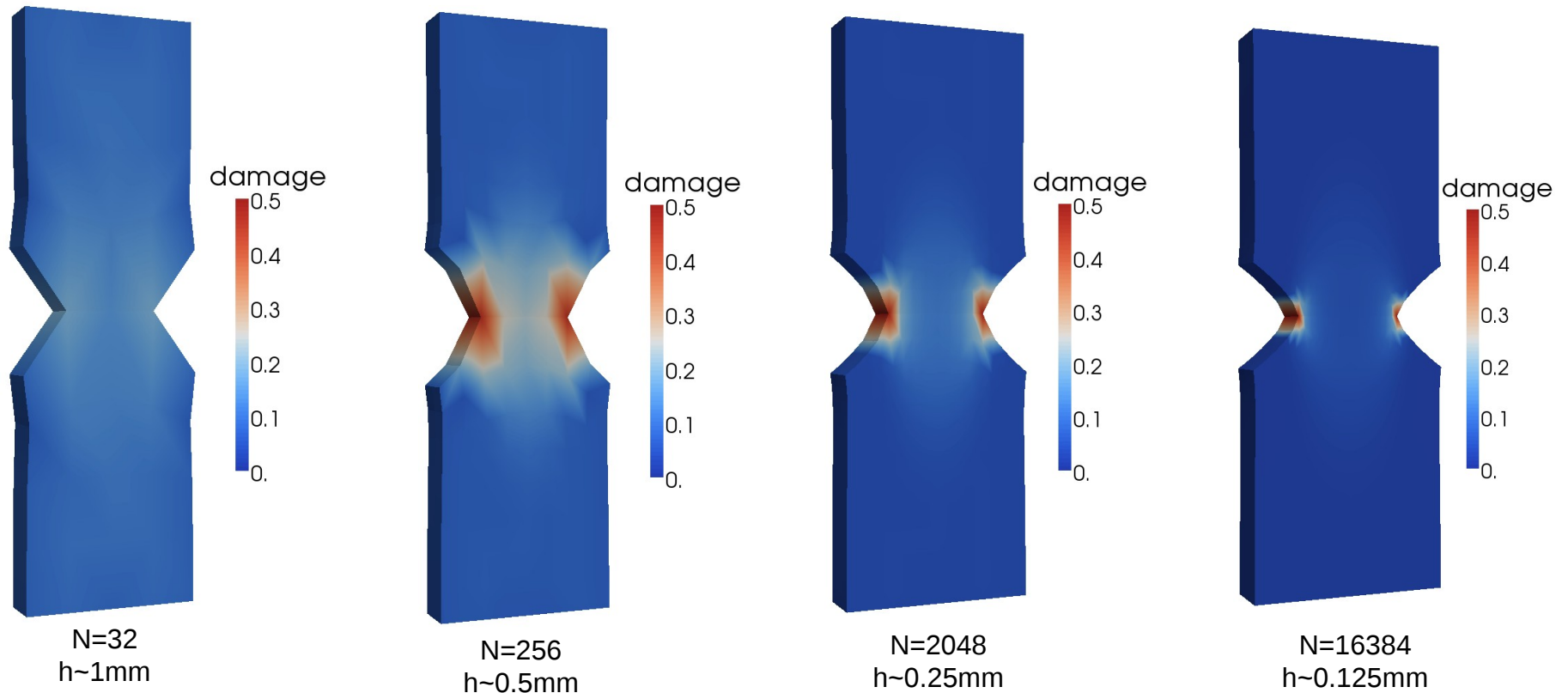


N=2048
h~0.25mm



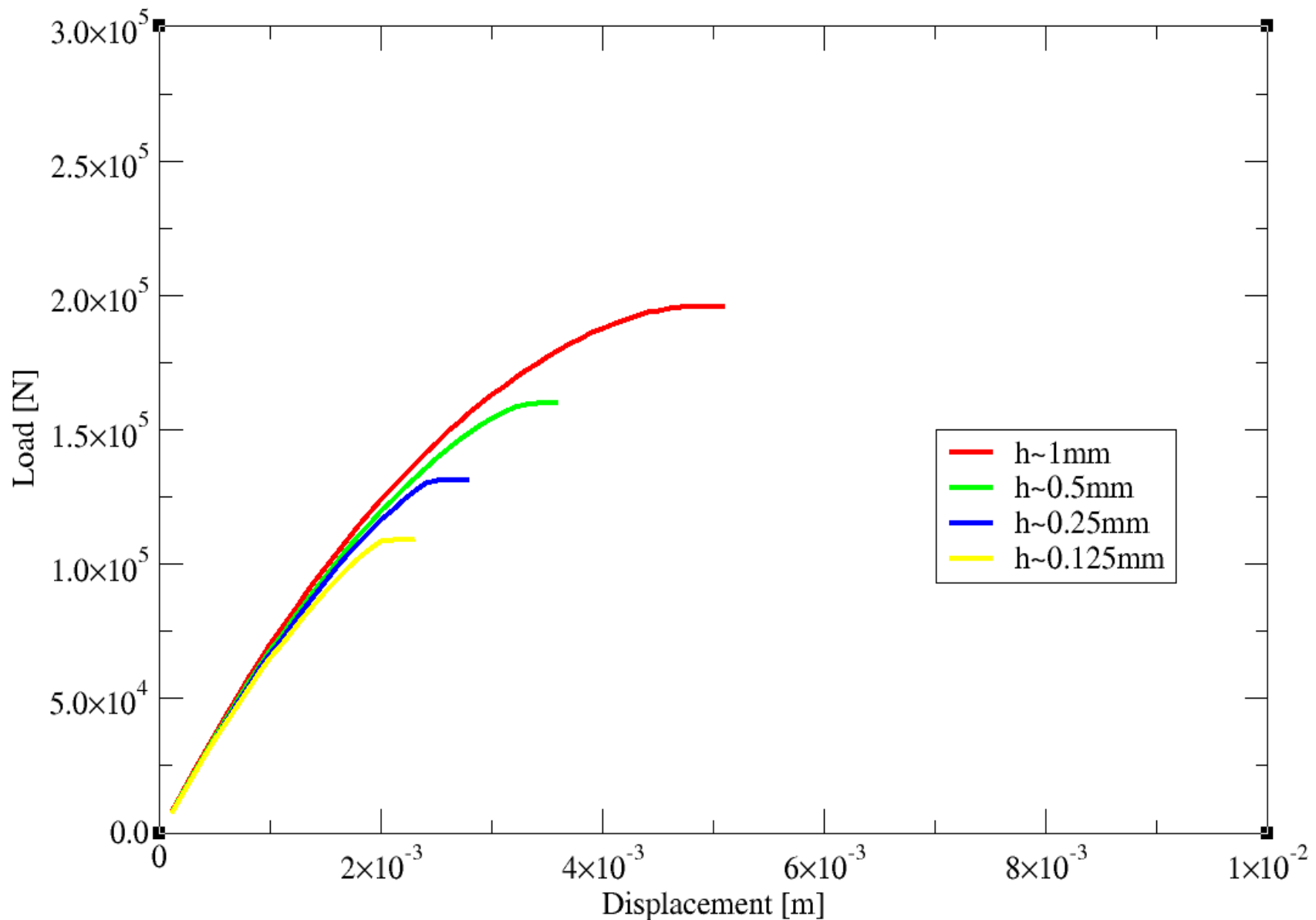
N=16384
h~0.125mm
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Mesh Dependence



Damage

Mesh Dependence



Load - Displacement

Implementation

$$\bar{\mathbf{Y}} = \frac{1}{\text{vol}(D)} \int_D \mathbf{Y} \, dV,$$

$$\bar{\mathbf{Z}} = \frac{1}{\text{vol}(D)} \int_D \mathbf{Z} \, dV,$$

$$\text{vol}(\bullet) := \int_{(\bullet)} dV,$$

Constant interpolation leads to simple averaging:

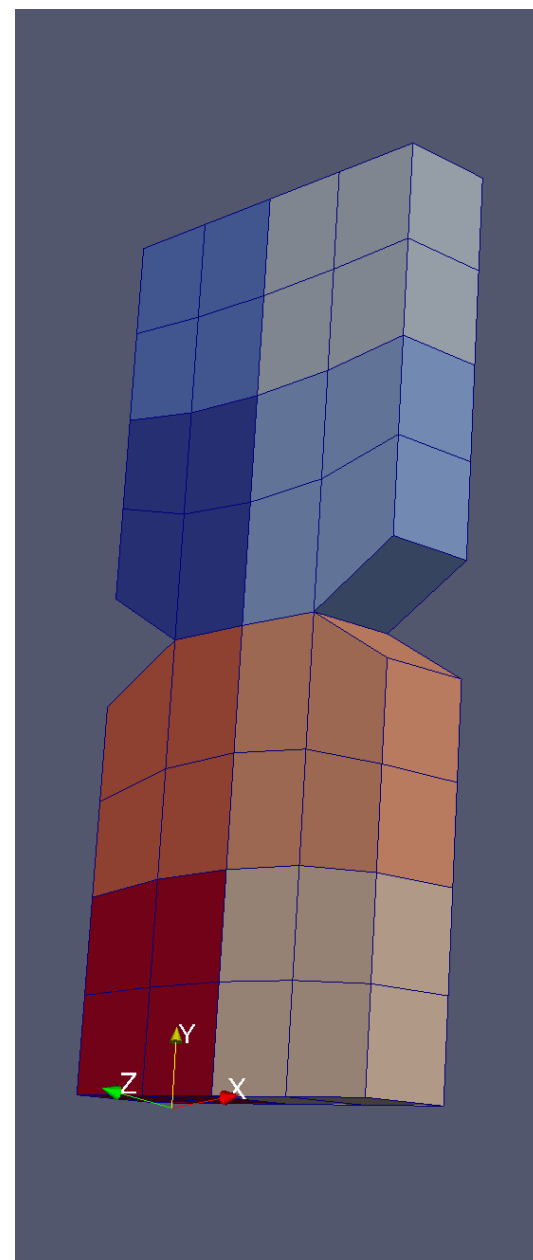
$$\text{vol}(D) = \sum_{i=0}^n \text{vol}(E_i),$$

$$\int_D \mathbf{Y} \, dV = \sum_{i=0}^n \int_{E_i} \mathbf{Y} \, dV,$$

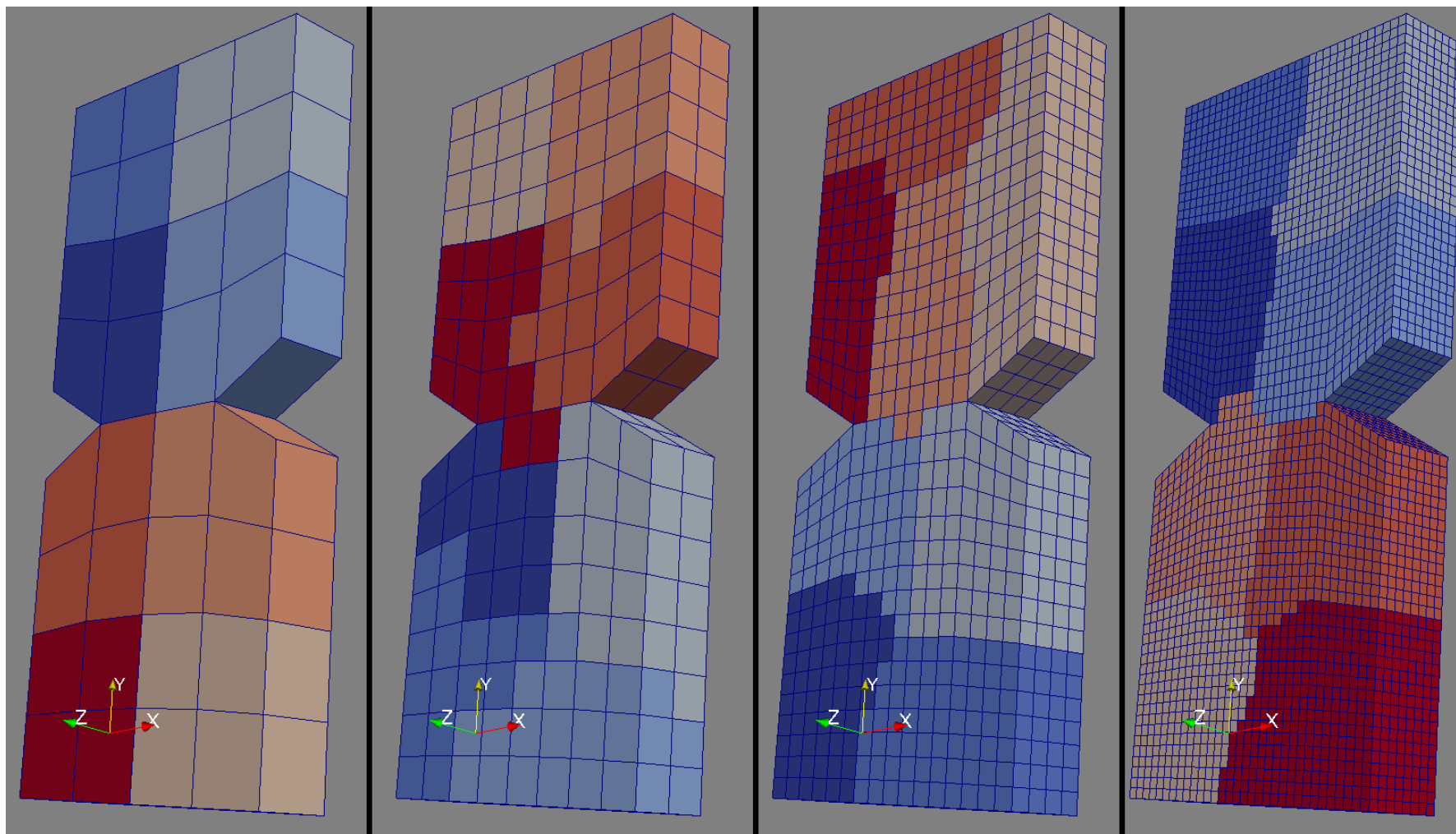
$$\int_D \mathbf{Z} \, dV = \sum_{i=0}^n \int_{E_i} \mathbf{Z} \, dV.$$

Use METIS to create domains D

$$\text{vol}(D) = (\text{length scale})^3 = (1.6\text{mm})^3$$



Partitions



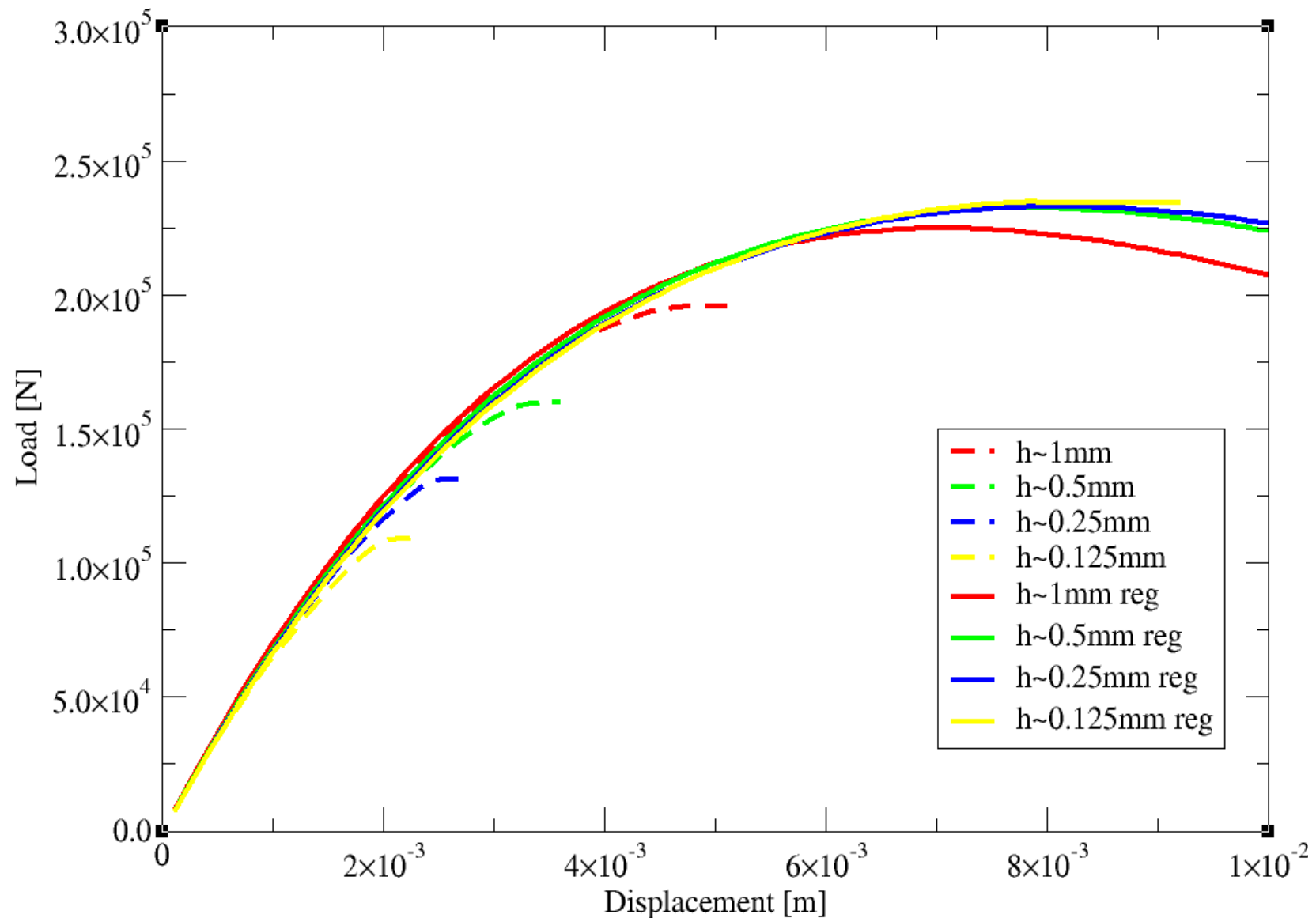
N=32
h~1mm

N=256
h~0.5mm

N=2048
h~0.25mm

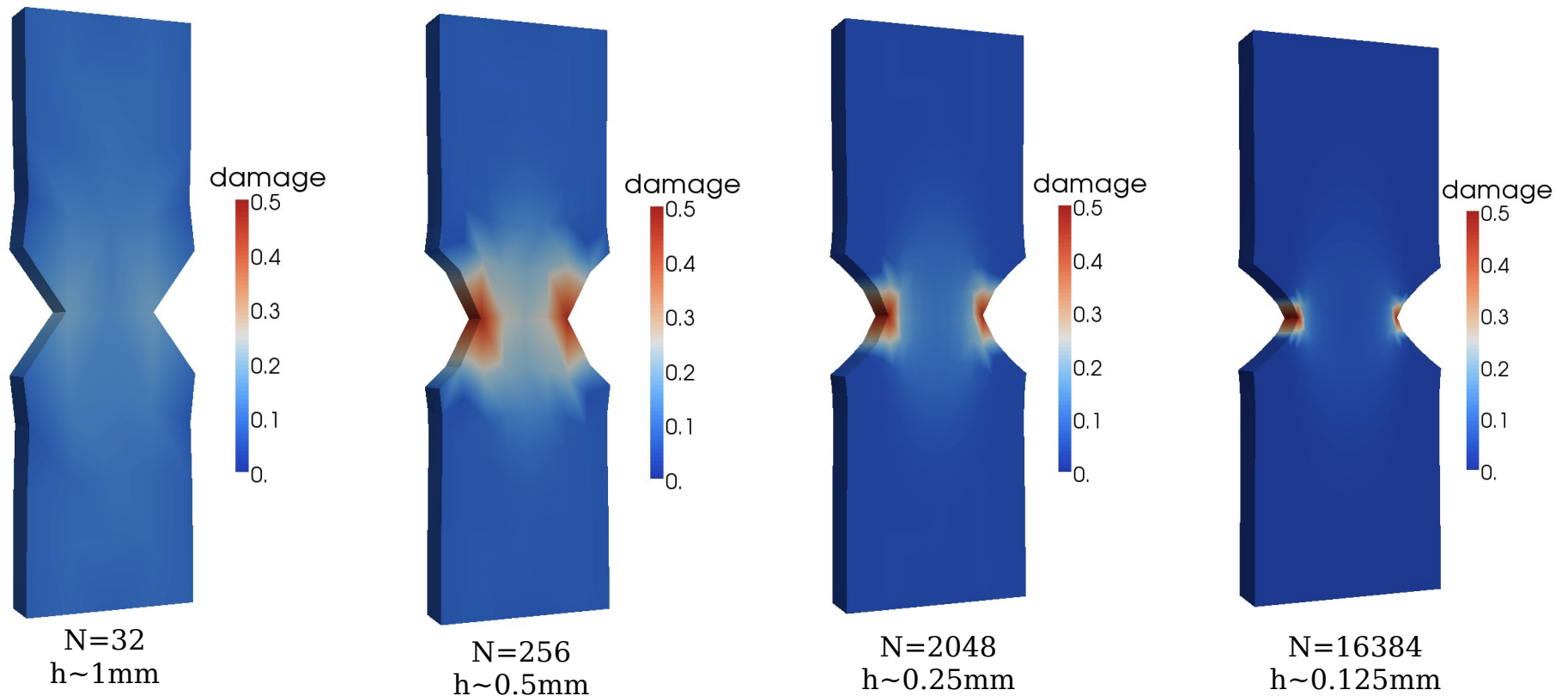
N=16384
h~0.125mm

Regularized Solution



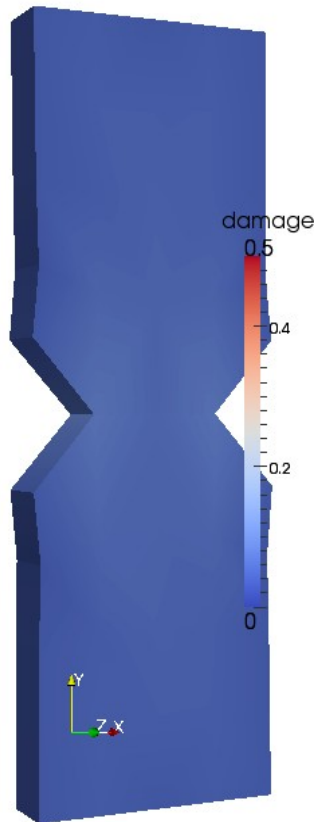
Load - Displacement

Mesh Dependence

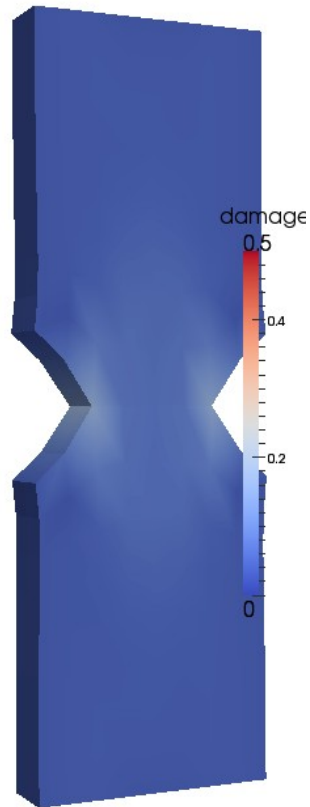


Damage

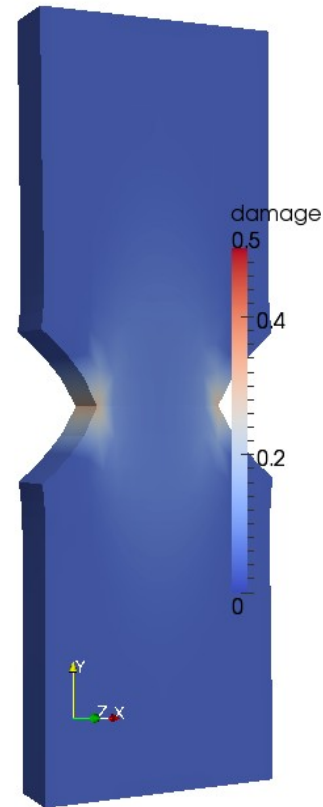
Regularized Solution



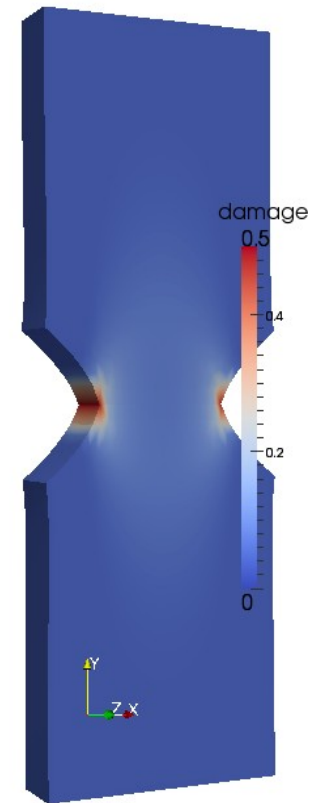
N=32
h~1mm



N=256
h~0.5mm



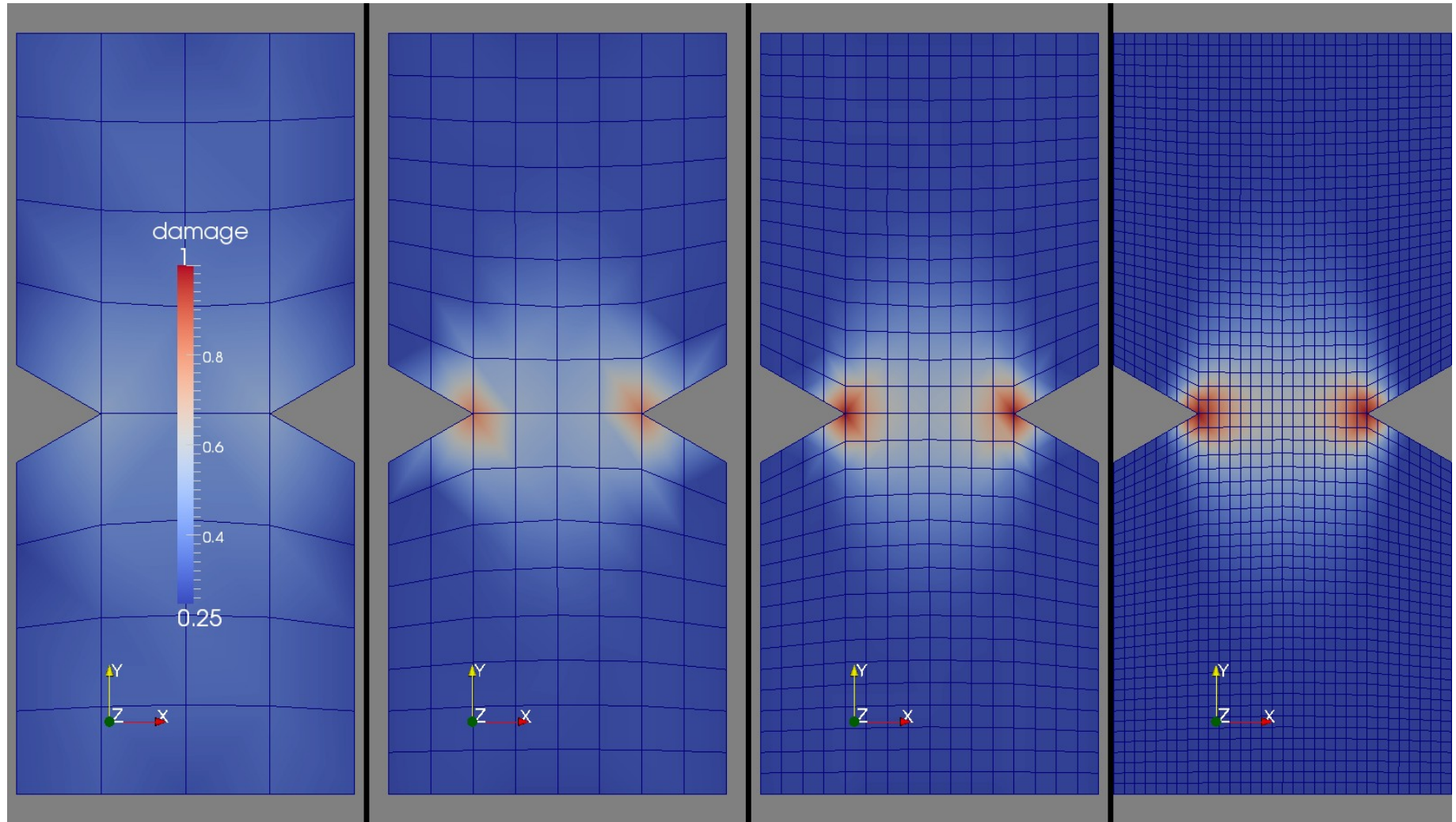
N=2048
h~0.25mm



N=16384
h~0.125mm

Damage

Regularized Solution (reference)



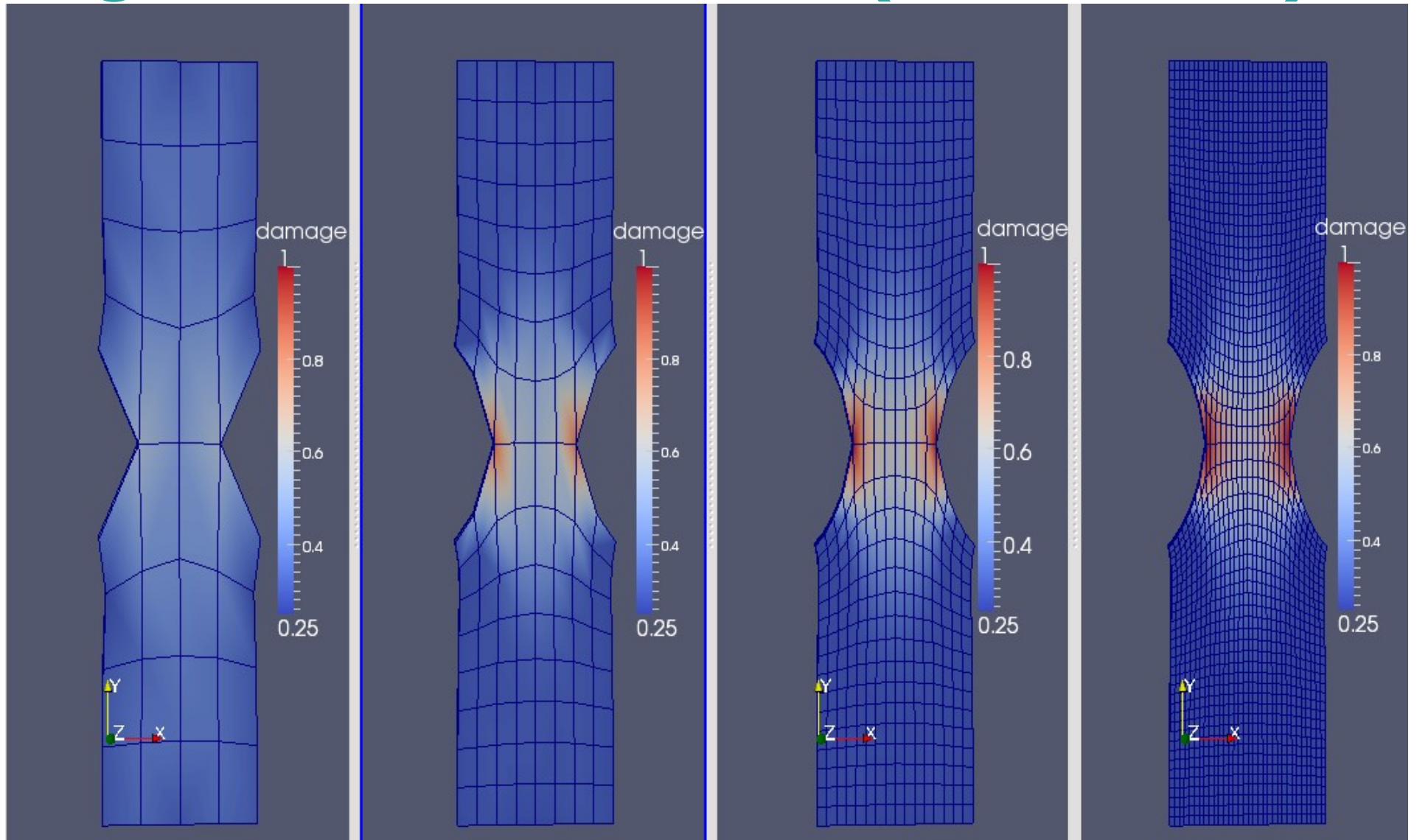
$N=32$
 $h \sim 1\text{mm}$

$N=256$
 $h \sim 0.5\text{mm}$

$N=2048$
 $h \sim 0.25\text{mm}$

$N=16384$
 $h \sim 0.125\text{mm}$

Regularized Solution (deformed)



$N=32$
 $h \sim 1\text{mm}$

$N=256$
 $h \sim 0.5\text{mm}$

$N=2048$
 $h \sim 0.25\text{mm}$

$N=16384$
 $h \sim 0.125\text{mm}$

Conclusions

- Regularization effective.
- Derived naturally from variational principle.
- Strong connection to gradient methods.
- No special boundary considerations.
- Simple form with unit interpolation functions.

Work in Progress

- Test in large 3D problems.
- Use same variational principle for mapping of internal variables.

Acknowledgments

This work was supported in part through the Joint US DoD/DOE Munitions Technology Development Program.