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11-04286

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Title: Influence of Grain Boundary Structure and Distribution on
Dynamic (Shock) Response of Materials

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Intended for: Presentation at Gordon Research Conference on Physical
Metallurgy.



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GRC Abstract

Influence of Grain Boundary Structure and Distribution on Dynamic (Shock) Response of Materials

Juan P. Escobedo-Diaz, Ellen K. Cerreta, Darcie Dennis-Koller, Curt A. Bronkhorst, Saryu Fensin, Ricardo A. Lebensohn and Davis Tonks.

Plate impact experiments were conducted to examine the influence of defect density, in this case grain boundary distribution, on the dynamic tensile response of Cu. Grain boundary distribution was altered through heat treatment, which altered grain size. The peak compressive stress was maintained at ~ 1.5 GPa for all experiments, low enough to cause an early stage of incipient spall damage that can be correlated to the surrounding. The quantitative post-impact metallographic analyses of recovered samples showed that for the materials with grain sizes larger than $30\text{ }\mu\text{m}$ the void volume fraction and the average void size increased with increasing grain size. In the 30 and $200\text{ }\mu\text{m}$ samples, void growth and coalescence was observed to dominate the damage behavior, whereas in 60 and $100\text{ }\mu\text{m}$ sized grains samples, most of the damage was restricted to individual, isolated voids. Electron backscatter diffraction (EBSD) observations showed that voids preferentially nucleate and grow at grain boundaries with high angle misorientation. However, special boundaries corresponding to $\Sigma 1$ (low angle, $<5^\circ$) and $\Sigma 3$ ($\sim 60^\circ$ $\langle 111 \rangle$ misorientation) type were more resistant to void formation.

Influence of Grain Boundary Structure and Distribution on Dynamic (Shock) Response of Materials

J. Pablo Escobedo

Collaborators:

Ellen Cerreta, Darcie Dennis-Koller, Curt Bronkhorst, Saryu Fensin, Ricardo Lebensohn and Davis Tonks

GRC Seminar

July 31st, 2011



Operated by Los Alamos National Security, LLC for the U.S. Department of Energy's NNSA

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Motivation: why dynamic (shock) response?

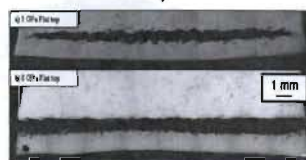
Damage due to dynamic failure (shock phenomena)



Vulnerability



Crash worthiness



Lab tested

Identifying the physical mechanisms responsible for dynamic material failure during shock loading provides a capability of designing and predicting material response to extreme conditions.

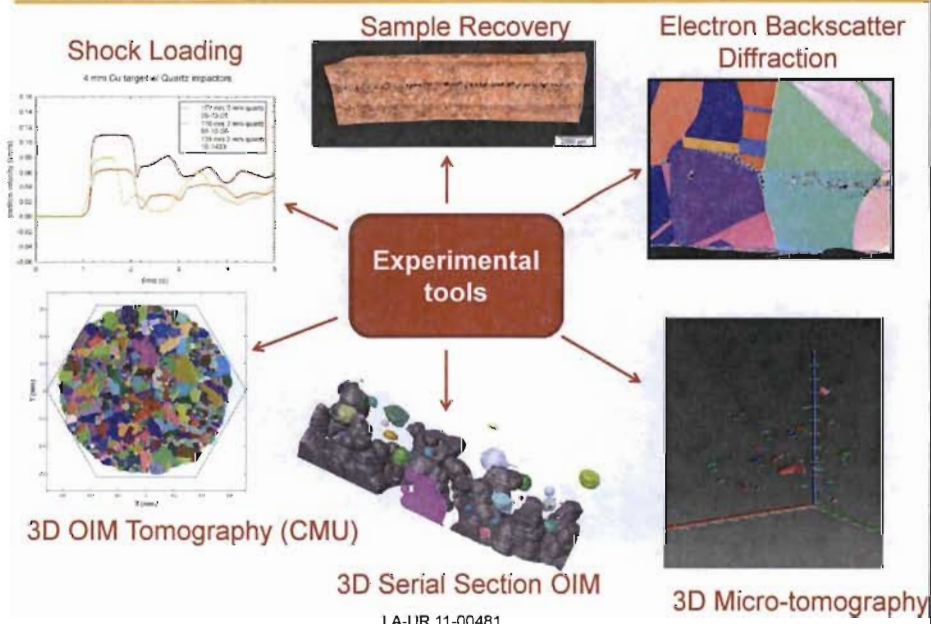
We attempt to address some key questions

1. Can we partition deterministic processes (controllable) vs. stochastic (random) processes?
2. Can we develop a multi-scale understanding of these processes?
3. **Can we capture the essential physics in our models?**
4. **Can we control these behaviors through**

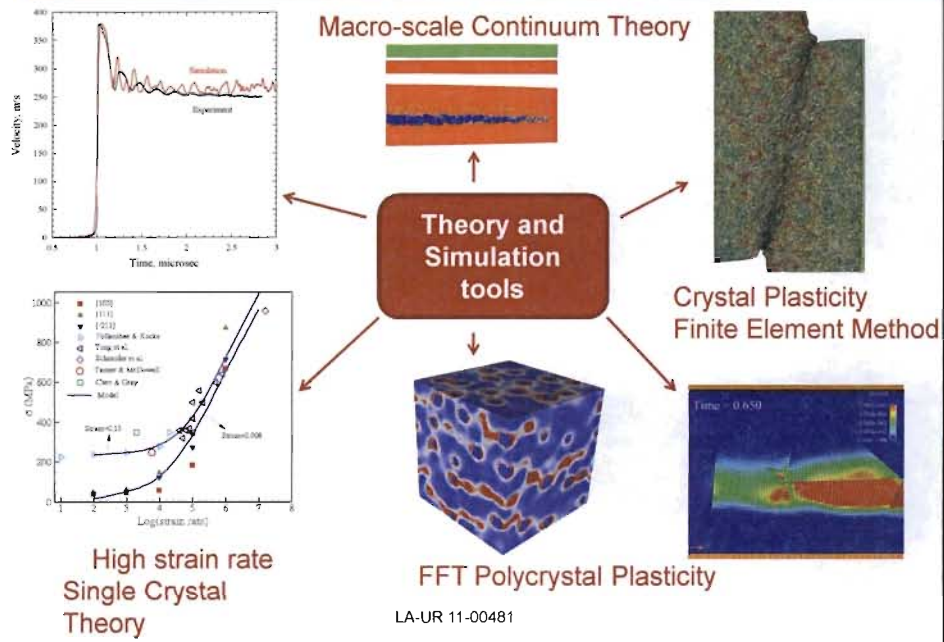


To do this, we want to understand the connections between loading environment and the characteristics of a material

Isolating Kinetic and Spatial Effects - I



Isolating Kinetic and Spatial Effects - II



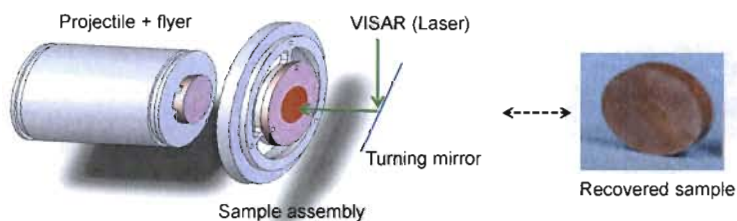
Experimental Observations

Experimental configuration

In the lab: A gas gun platform can be utilized to study shock wave interactions within materials.

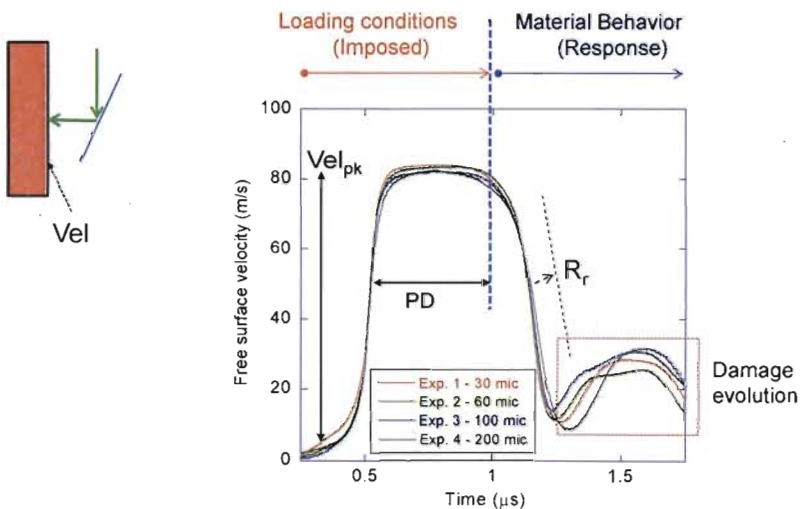


Plate impact technique



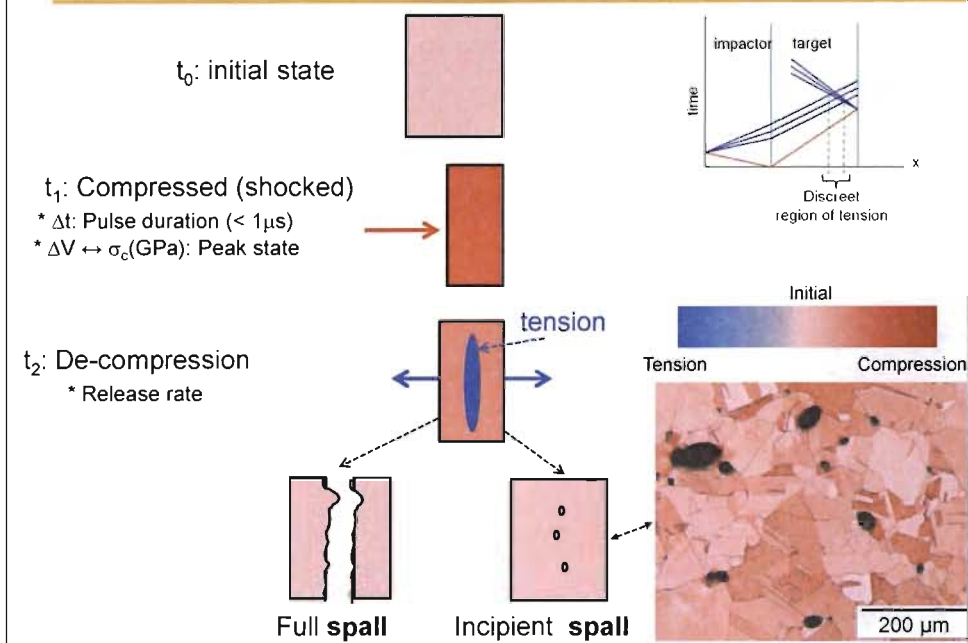
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Real-time response: Free surface velocities.

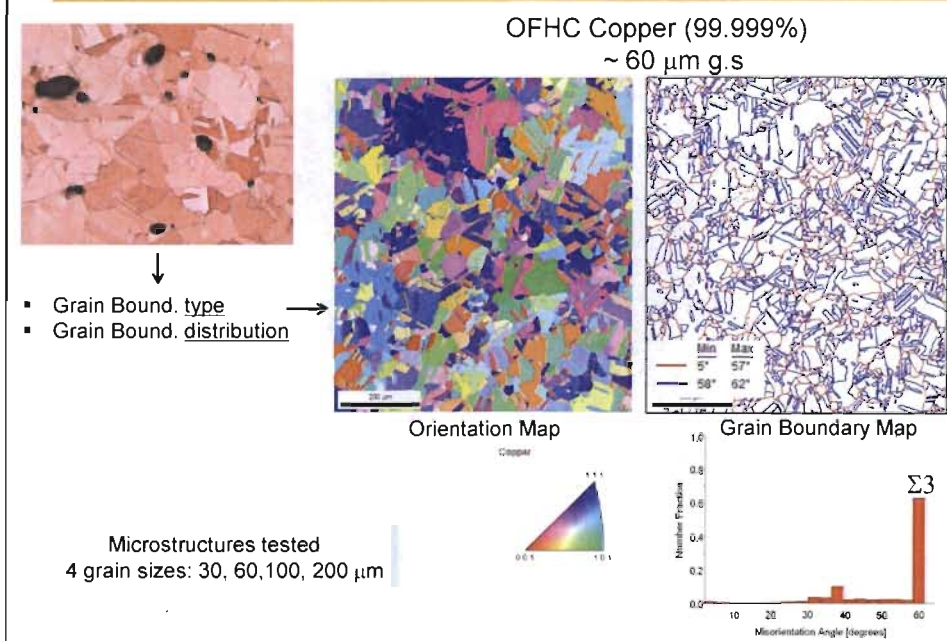


Similar loading conditions: peak velocity (Vel_{pk}), pulse duration(PD) and release rate(R_r).

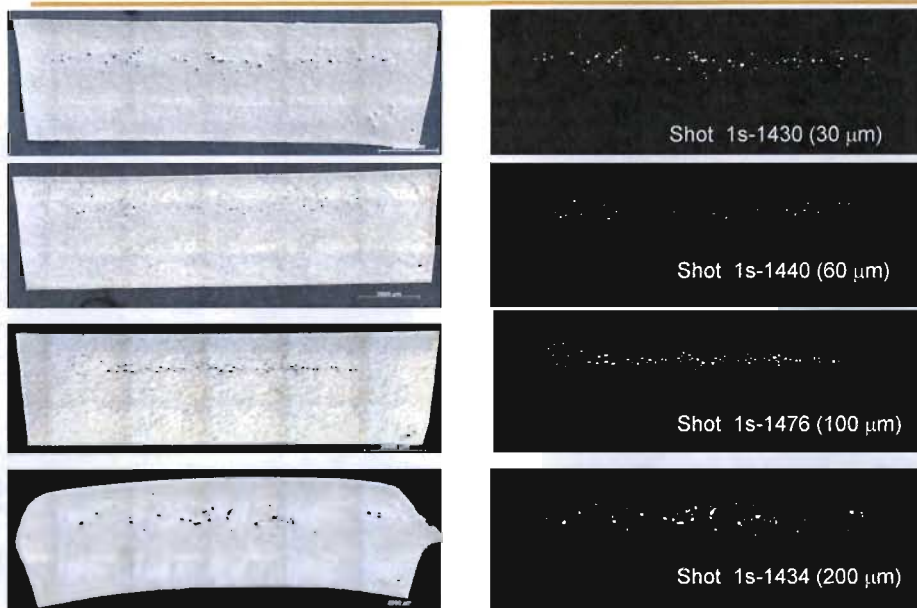
Material response in a dynamic tensile experiment (spall)



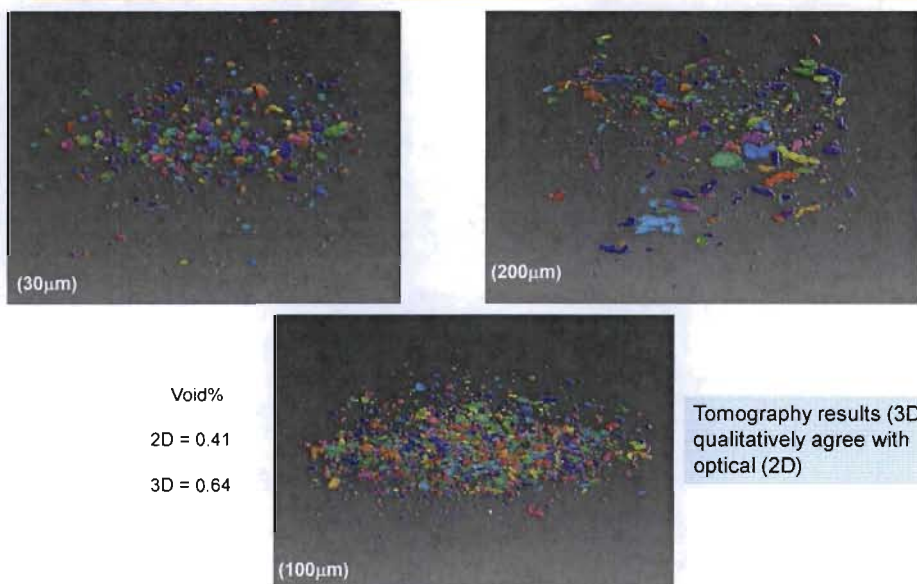
Dynamic Response vs. Grain Boundary (defects) distribution



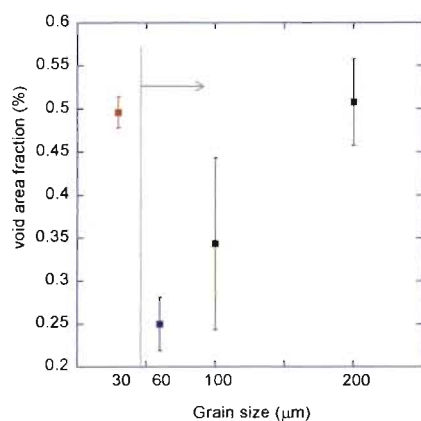
Optical analysis



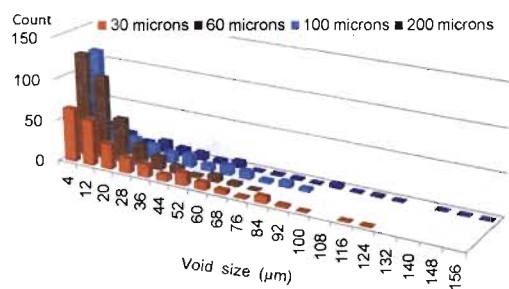
Micro x-ray tomography



Damage quantification



Void area fraction as function of the grain size

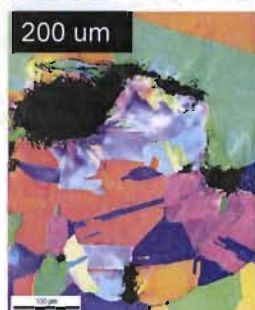
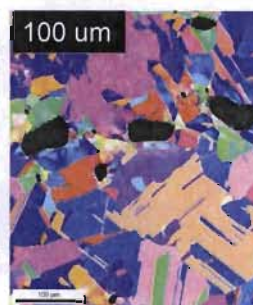
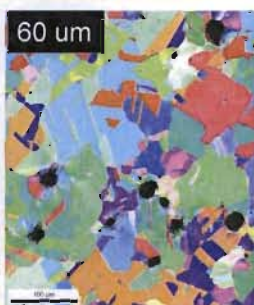
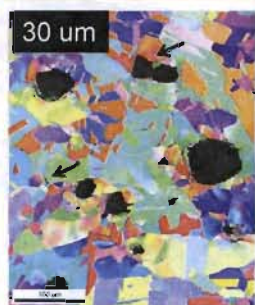


Void size distribution.

Void area fraction does not show linear trend

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Damage characteristics

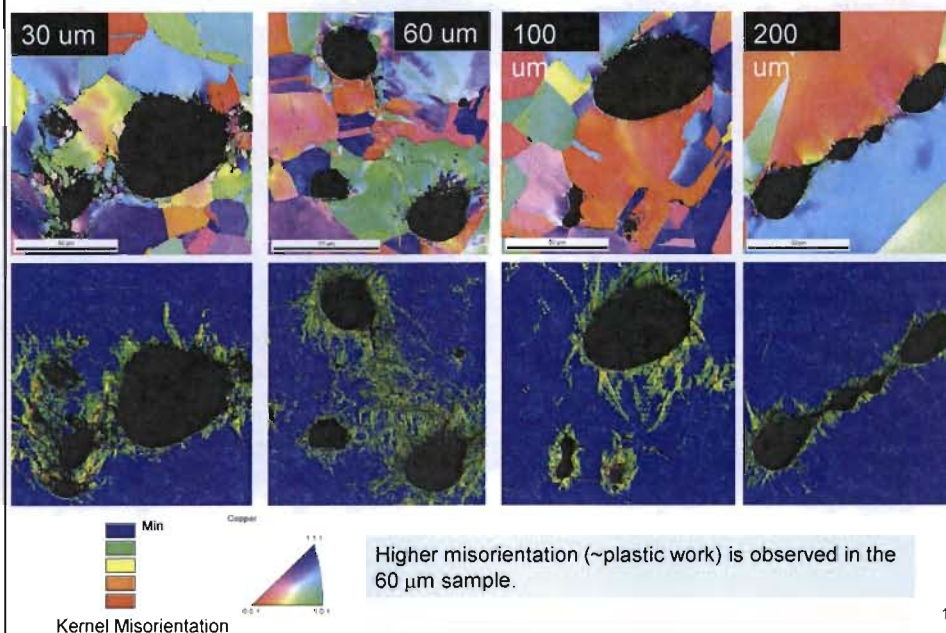


Experiment	Grain size	Number of voids	Void area fraction (%)	Avg Void diameter (μm)
1s-1430	30 μm	236	0.496	38.1
1s-1440	60 μm	343	0.249	22.7
1s-1476	100 μm	267	0.416	33.0
1s-1434	200 μm	111	0.507	55.1

Damage Statistics from 2D optical analysis

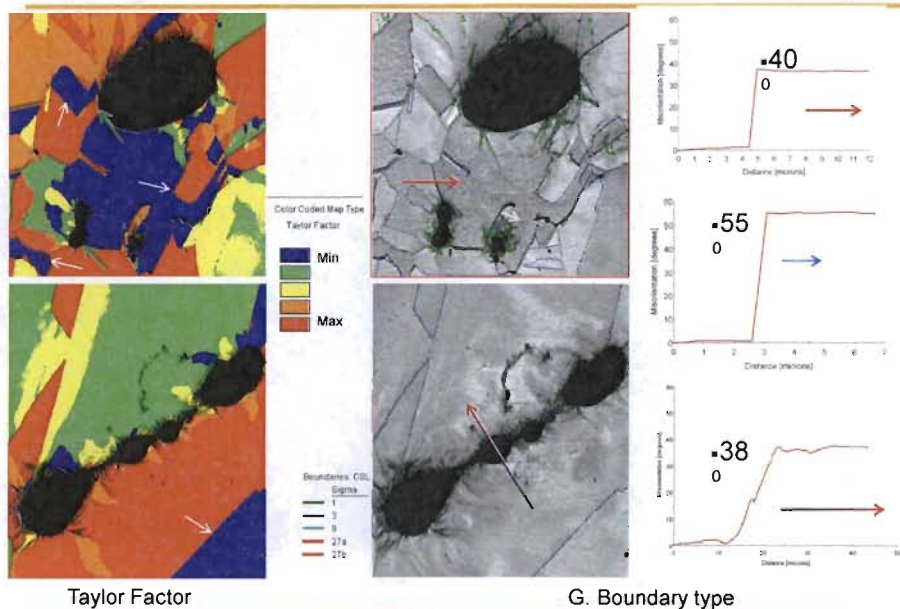
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Void growth/coalescence vs. grain size



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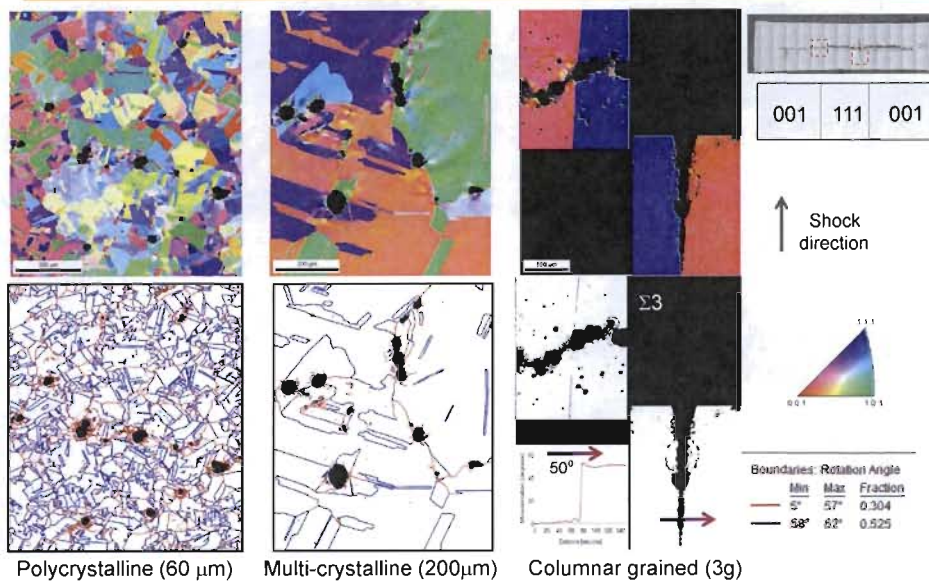
Properties from EBSD data: Taylor Factor and boundary type



Grain boundary structure as the determining factor for preferred void nucleation location.

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Grain boundary type



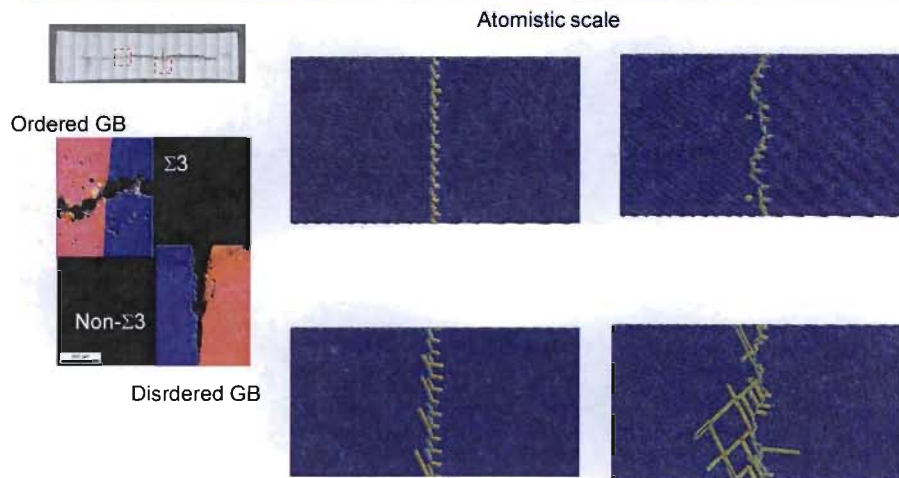
Grain boundary $\neq \Sigma 3$ as the determining factor for preferred void nucleation location.

Main experimental findings

- The special $\Sigma 3$ ($\sim 60^\circ$) grain boundaries resistant to void nucleation, indicating that lattice coincidence may be important to damage mitigation.
- Grain size determines the spatial distribution and size of the defects (i.e. grain boundaries), inherently dictating the preferred mechanism for damage evolution:
 - Individual void growth with accompanying plastic dissipation in intermediate grain sized samples (60 μm).
 - Coalescence more dominant in the 200 (and 30) μm samples due to the proximity of interacting growing voids.

Modeling Efforts

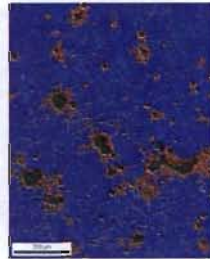
Response to Shock Grain Boundary Structure.



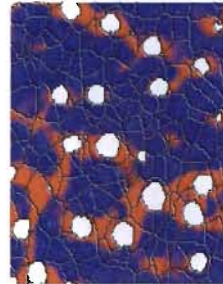
Higher generation of defects at disordered grain boundaries.

Plastic flow and void interaction

Mesoscale

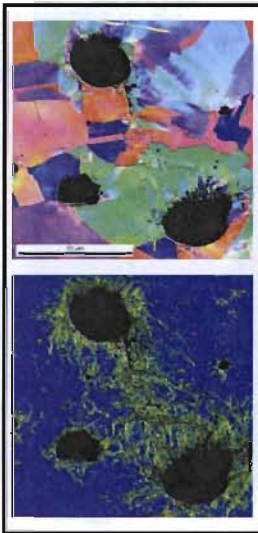


EBSD
Misorientation



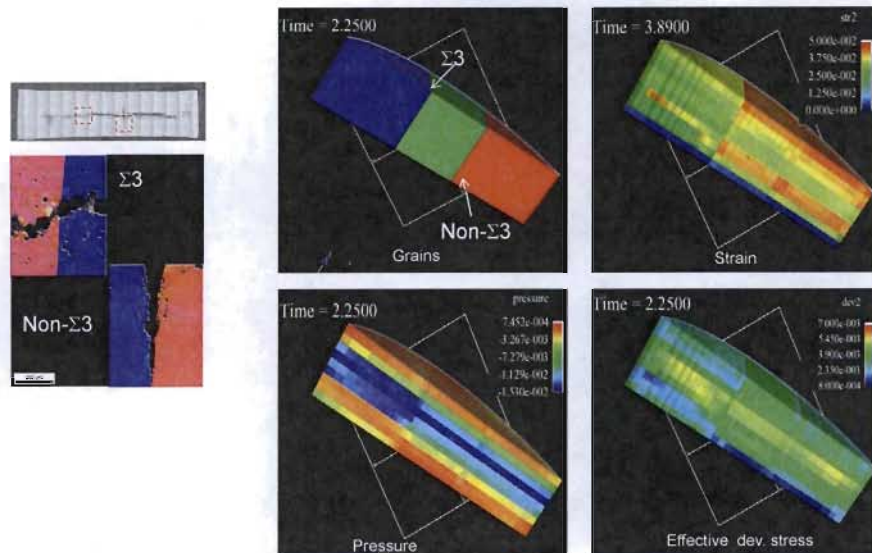
Plastic flow and void interaction

FFT



Plastic fields between voids determine damage behavior: void growth vs. coalescence.

Boundary Response to stress state



The highest calculated stress, strain and pressure gradients $\Sigma 3$ boundary indicating its higher strength.

Experimental Observations

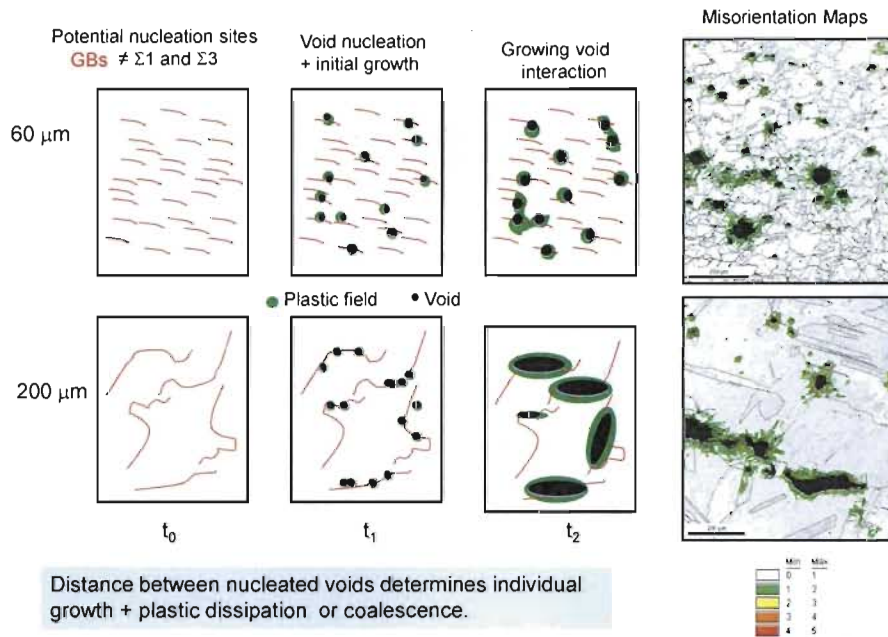
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Modeling Efforts



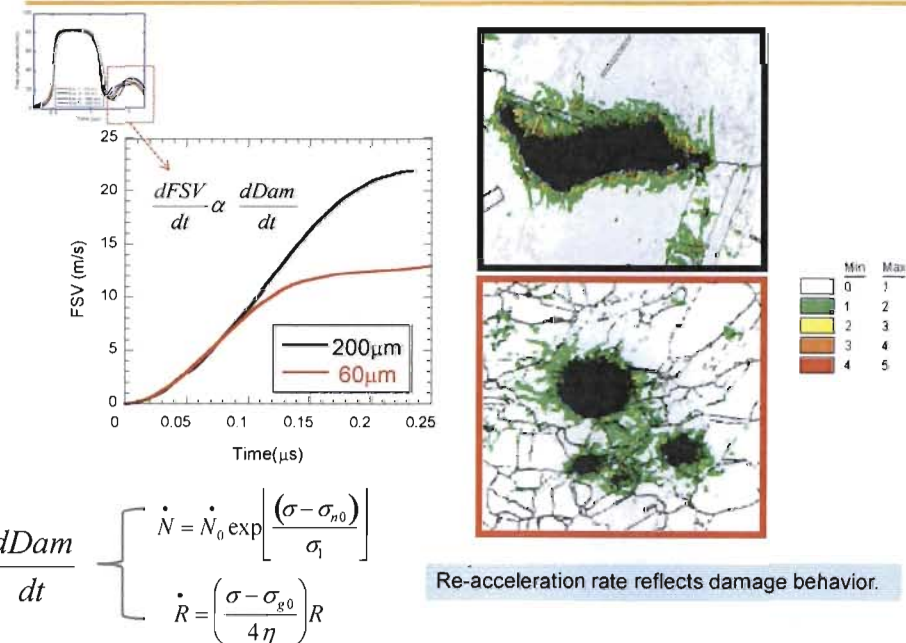
Damage mechanism

Mechanism for damage evolution



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Real time response \leftrightarrow damage characteristics



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Summary

- Shock loading and microstructure are intimately connected to the dynamic material response.
- A critical length scale exists where mechanisms of ductile damage formation transition from individual void growth to coalescence dominated.
- An understanding of mechanisms dominating damage regimes is necessary to quantitatively interpret velocimetry results.