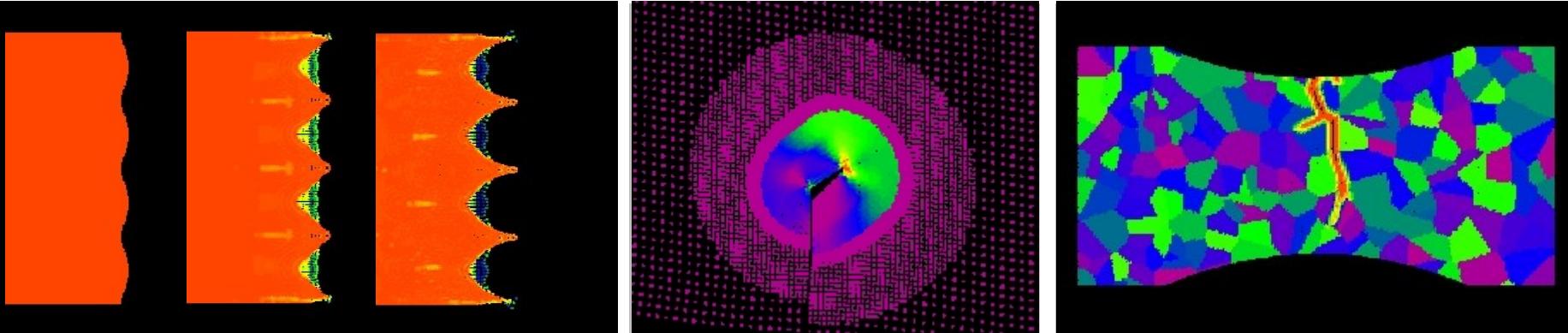


Exceptional service in the national interest



Variable length scale in a peridynamic body

Stewart Silling, David Littlewood

Sandia National Laboratories

Pablo Seleson

University of Texas, Austin

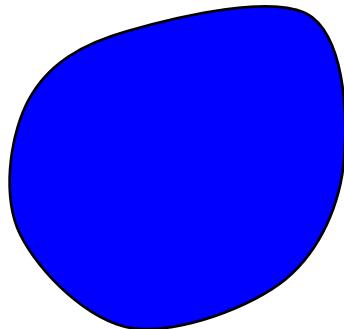
SIAM Conference on Mathematical Aspects of Materials Science, Philadelphia, PA, June 12, 2013



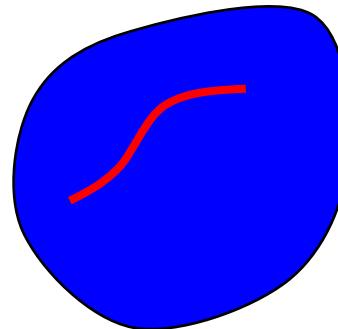
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Purpose of peridynamics

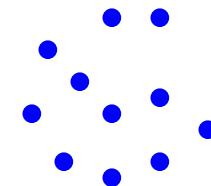
- To unify the mechanics of continuous and discontinuous media within a single, consistent set of equations.



Continuous body



Continuous body
with a defect



Discrete particles

- Why do this? Develop a mathematical framework that help in modeling...
 - Discrete-to-continuum coupling
 - Cracking, including complex fracture patterns
 - Communication across length scales.

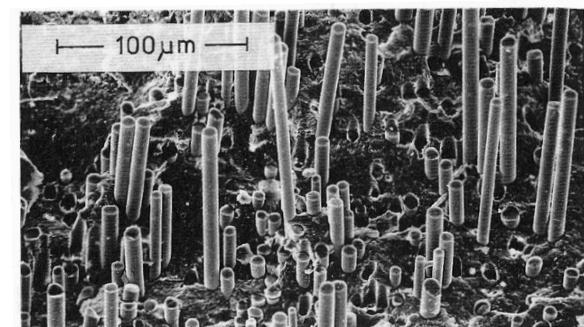


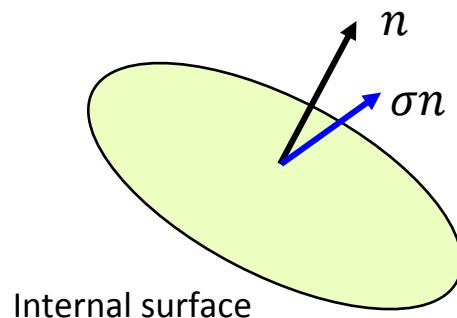
Figure 11.20 Pull-out: (a) schematic diagram; (b) fracture surface of 'Silceram' glass-ceramic reinforced with SiC fibres. (Courtesy H. S. Kim, P. S. Rogers and R. D. Rawlings.)

Peridynamics basics:

The nature of internal forces

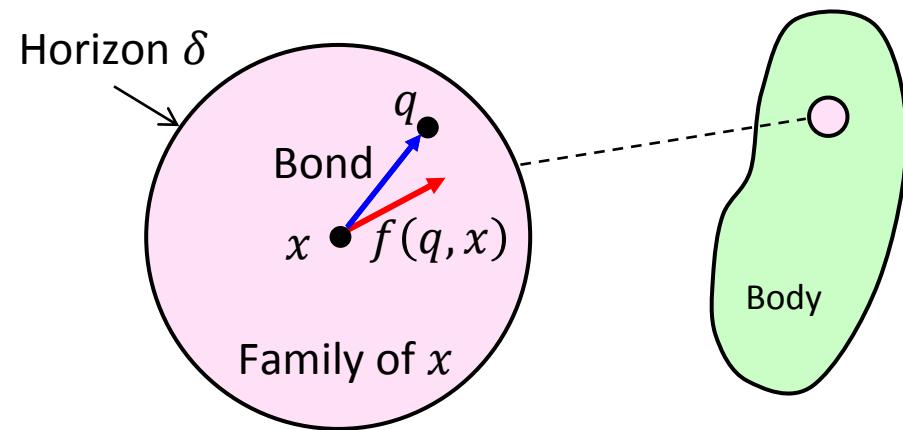
Standard theory

Stress tensor field
(assumes contact forces and
smooth deformation)



Peridynamics

Bond forces within small neighborhoods
(allow discontinuity)



$$\rho \ddot{u}(x, t) = \nabla \cdot \sigma(x, t) + b(x, t)$$

Differentiation of contact forces

$$\rho \ddot{u}(x, t) = \int_{H_x} f(q, x) dV_q + b(x, t)$$

Summation over bond forces

Peridynamics basics:

Deformation state and force state

- The deformation state maps each bond to its deformed image.

$$Y[x]\langle q - x \rangle = y(q) - y(x)$$

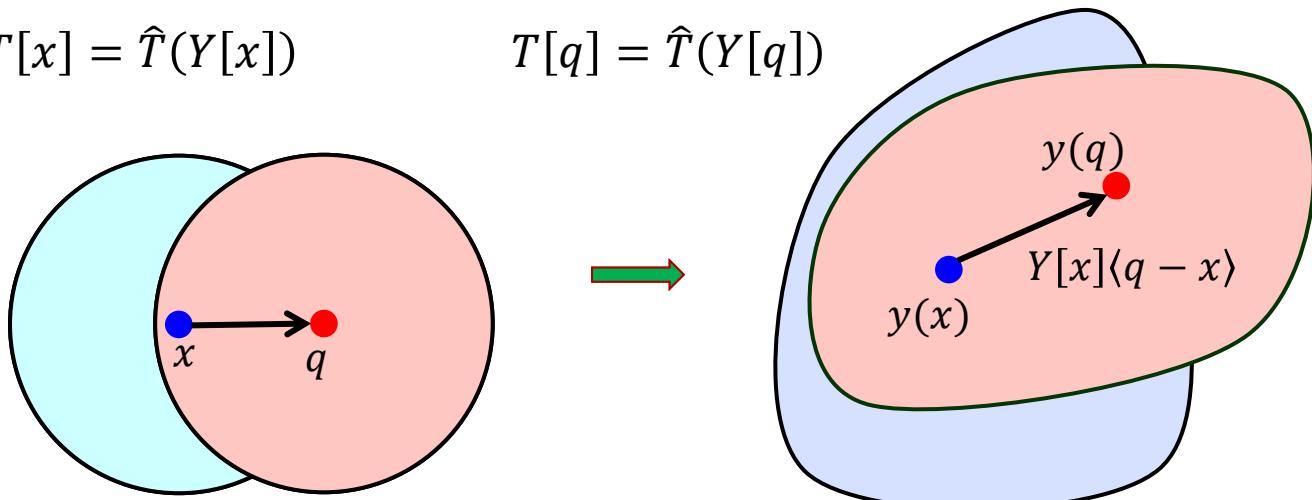
- The force state maps bonds to bond forces according to the constitutive model.

$$f(q, x) = T[x]\langle q - x \rangle - T[q]\langle x - q \rangle$$

- The constitutive model maps deformation states to force states.

$$T[x] = \hat{T}(Y[x])$$

$$T[q] = \hat{T}(Y[q])$$



Peridynamic vs. local equations

State notation: State \langle bond \rangle = vector

<i>Relation</i>	<i>Peridynamic theory</i>	<i>Standard theory</i>
Kinematics	$\underline{\mathbf{Y}}\langle \mathbf{q} - \mathbf{x} \rangle = \mathbf{y}(\mathbf{q}) - \mathbf{y}(\mathbf{x})$	$\mathbf{F}(\mathbf{x}) = \frac{\partial \mathbf{y}}{\partial \mathbf{x}}(\mathbf{x})$
Linear momentum balance	$\rho \ddot{\mathbf{y}}(\mathbf{x}) = \int_{\mathcal{H}} \left(\mathbf{t}(\mathbf{q}, \mathbf{x}) - \mathbf{t}(\mathbf{x}, \mathbf{q}) \right) dV_{\mathbf{q}} + \mathbf{b}(\mathbf{x})$	$\rho \ddot{\mathbf{y}}(\mathbf{x}) = \nabla \cdot \boldsymbol{\sigma}(\mathbf{x}) + \mathbf{b}(\mathbf{x})$
Constitutive model	$\mathbf{t}(\mathbf{q}, \mathbf{x}) = \underline{\mathbf{T}}\langle \mathbf{q} - \mathbf{x} \rangle, \quad \underline{\mathbf{T}} = \hat{\underline{\mathbf{T}}}(\underline{\mathbf{Y}})$	$\boldsymbol{\sigma} = \hat{\boldsymbol{\sigma}}(\mathbf{F})$
Angular momentum balance	$\int_{\mathcal{H}} \underline{\mathbf{Y}}\langle \mathbf{q} - \mathbf{x} \rangle \times \underline{\mathbf{T}}\langle \mathbf{q} - \mathbf{x} \rangle dV_{\mathbf{q}} = \mathbf{0}$	$\boldsymbol{\sigma} = \boldsymbol{\sigma}^T$
Elasticity	$\underline{\mathbf{T}} = W_{\underline{\mathbf{Y}}}$ (Fréchet derivative)	$\boldsymbol{\sigma} = W_{\mathbf{F}}$ (tensor gradient)
First law	$\dot{\varepsilon} = \underline{\mathbf{T}} \bullet \dot{\underline{\mathbf{Y}}} + q + r$	$\dot{\varepsilon} = \boldsymbol{\sigma} \cdot \dot{\mathbf{F}} + q + r$

$$\underline{\mathbf{T}} \bullet \dot{\underline{\mathbf{Y}}} := \int_{\mathcal{H}} \underline{\mathbf{T}}\langle \xi \rangle \cdot \dot{\underline{\mathbf{Y}}}\langle \xi \rangle dV_{\xi}$$

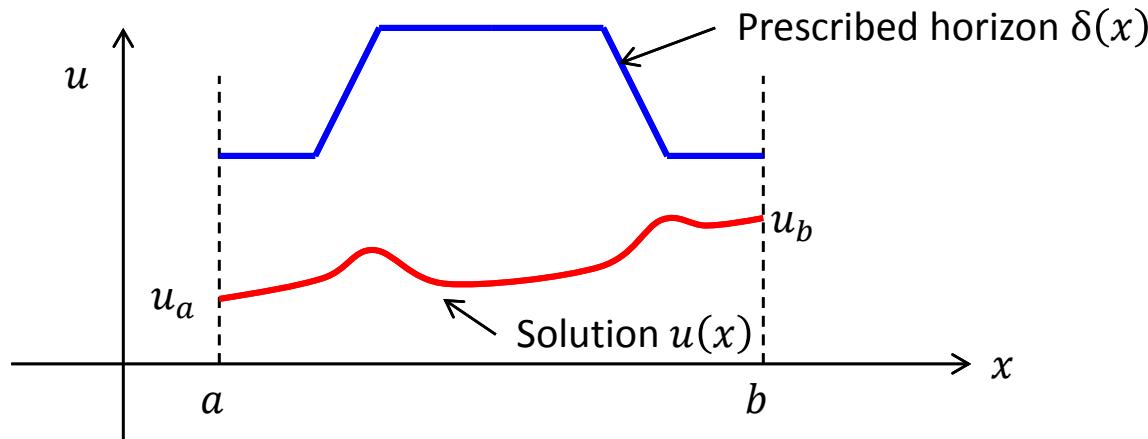
Mixed blessing of nonlocality

- Nonlocality is necessary to achieve the goals of peridynamics , but it entails some practical difficulties.
- Example: nonuniform horizon in a bar with “homogeneous bulk properties”.
- We know how to scale a material model so the Young’s modulus is independent of horizon.

$$T_\delta(\xi) = \delta^{-2} Z(\xi/\delta)$$

where Z is a reference force state that depends only on strain.

- But when you use this to model equilibrium of a bar with variable horizon, you get a “wrong” result:

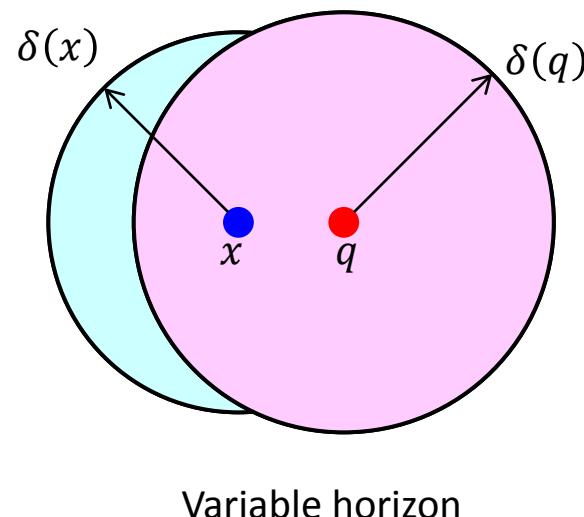


Origin of artifacts

- The peridynamic force density operator $L(x)$ involves the force state not only at x but also the force states at all points within the horizon.

$$0 = L(x) + b, \quad L(x) = \int_{-\infty}^{\infty} \{T_{\delta(x)}[x]\langle q - x \rangle - \textcolor{blue}{T_{\delta(q)}[q]\langle x - q \rangle}\} dq$$

so simply scaling the material model at x is not sufficient.



Variable horizon

“Patch test” requirement for a coupling method

- In a deformation of the form

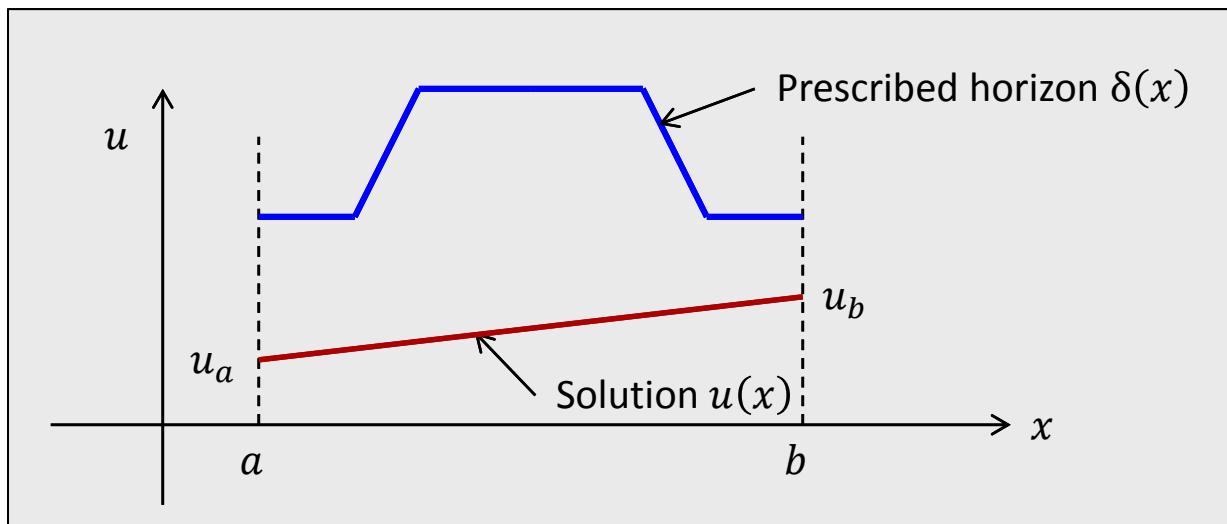
$$u(x) = a + Hx$$

where H is a constant and the material model is of the form

$$T[x]\langle\xi\rangle = \delta^{-2}(x)Z\langle\xi/\delta(x)\rangle$$

where $\delta(x)$ is a prescribed function and Z is a state that depends only on H , we require

$$L(x) = 0 \text{ for all } x.$$



Peridynamic stress tensor

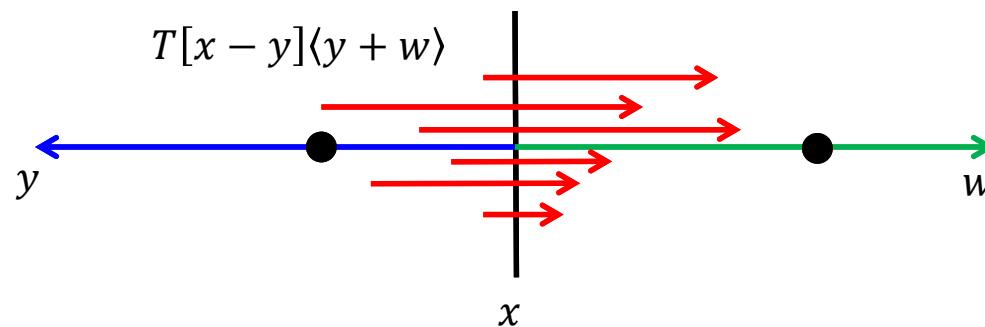
- Define the peridynamic stress tensor field by

$$v(x) = \int_0^\infty \int_0^\infty \{T[x-y]\langle y+w \rangle - T[x+y]\langle -y-w \rangle\} dy dz$$

- Identity:

$$\frac{dv}{dx} = \int_{-\infty}^\infty \{T[x]\langle q-x \rangle - T[q]\langle x-q \rangle\} dq$$

- $v(x)$ is the force per unit area carried by all the bonds that cross x .



Partial stress field

- Under our assumption that

$$T[x]\langle\xi\rangle = \delta^{-2}(x)Z\langle\xi/\delta(x)\rangle$$

one finds directly that

$$v_0(x) := \int_{-\infty}^{\infty} \xi T[x]\langle\xi\rangle d\xi = \int_{-\infty}^{\infty} \xi Z\langle\xi\rangle d\xi$$

which is independent of x , so $dv_0/dx = 0$.

- v_0 is called the ***partial stress*** field.
- Clearly the internal force density field computed from

$$L_0(x) := dv_0/dx$$

passes the “patch test.”

- This observation leads to the following idea...

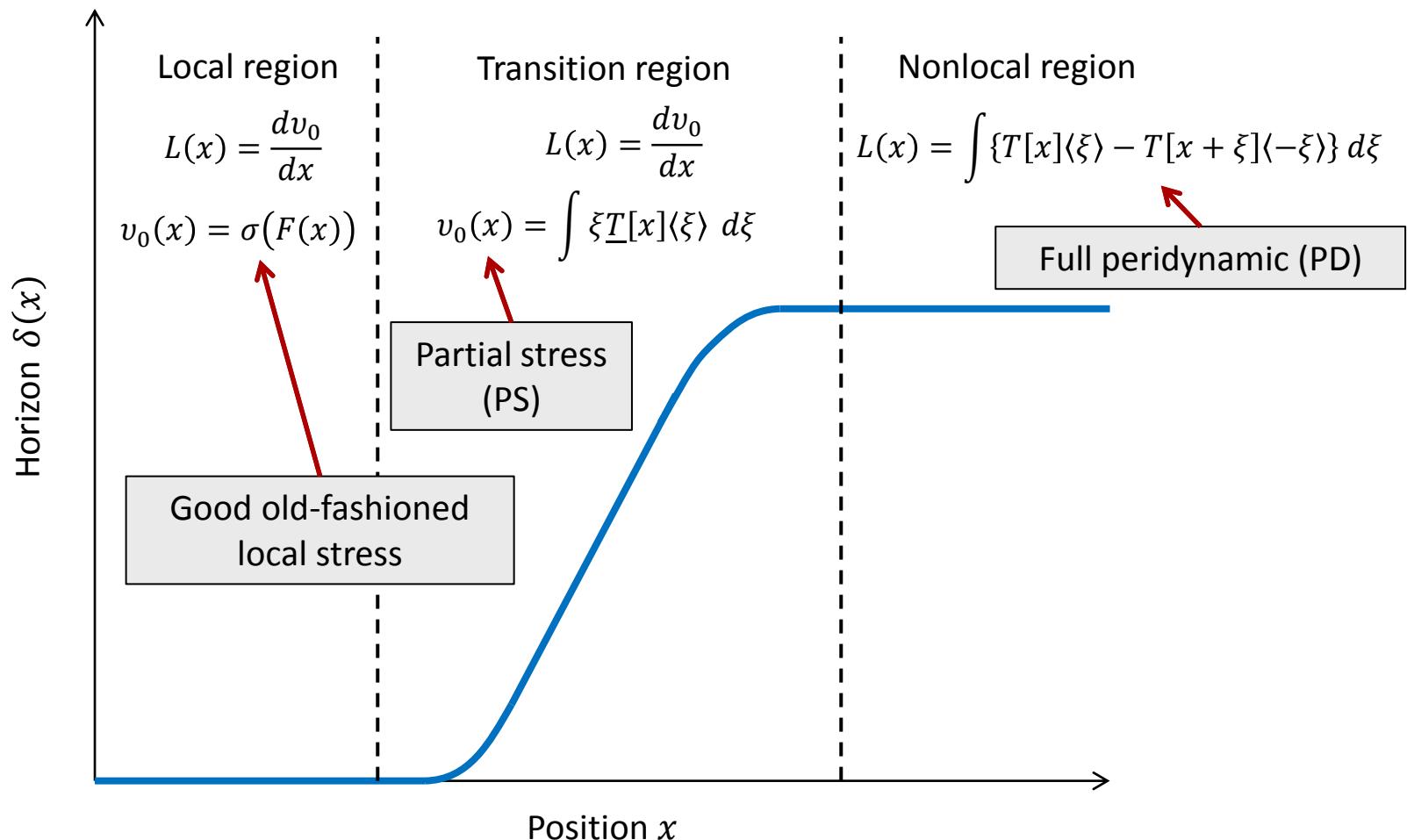
Concept for coupling method

- Idea: within a coupling region in which δ is changing, compute the internal force density from

$$L(x) = \frac{dv_0}{dx}(x), \quad v_0(x) := \int_{-\infty}^{\infty} \xi T[x](\xi) d\xi$$

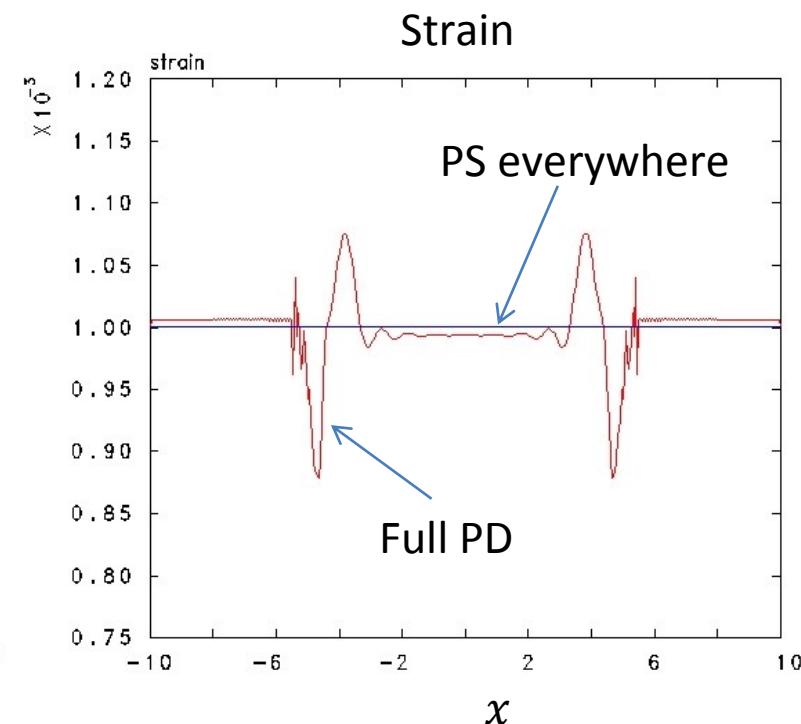
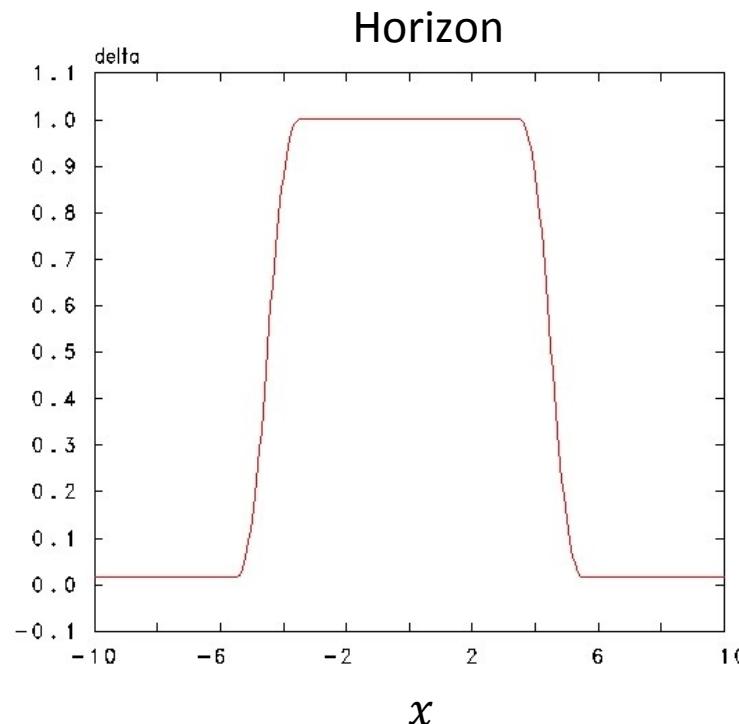
- Here, Tx is determined from whatever the deformation happens to be near x .
 - Z is no longer involved.
 - The material model has not changed from full PD, but the way of computing L has.

Local-nonlocal coupling idea



Continuum patch test results

- Full PD shows artifacts, as expected.
- PS shows no artifacts, as promised.

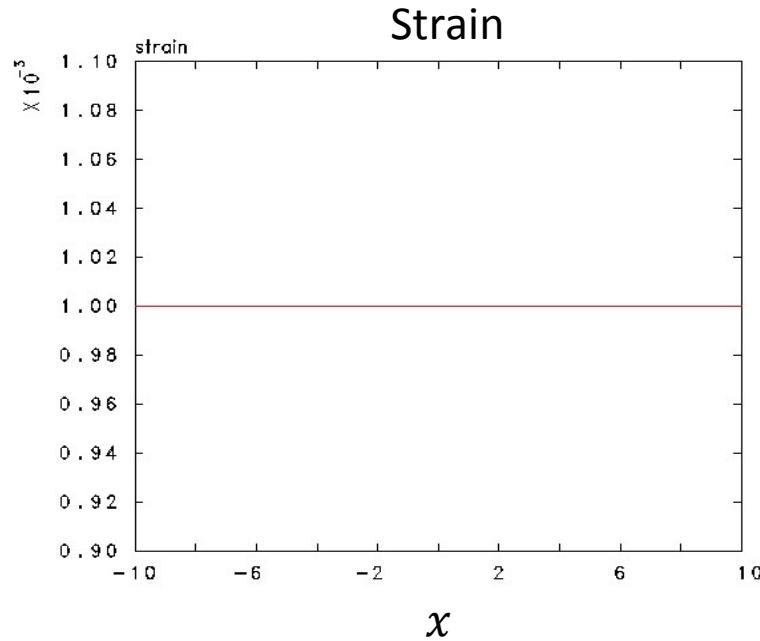
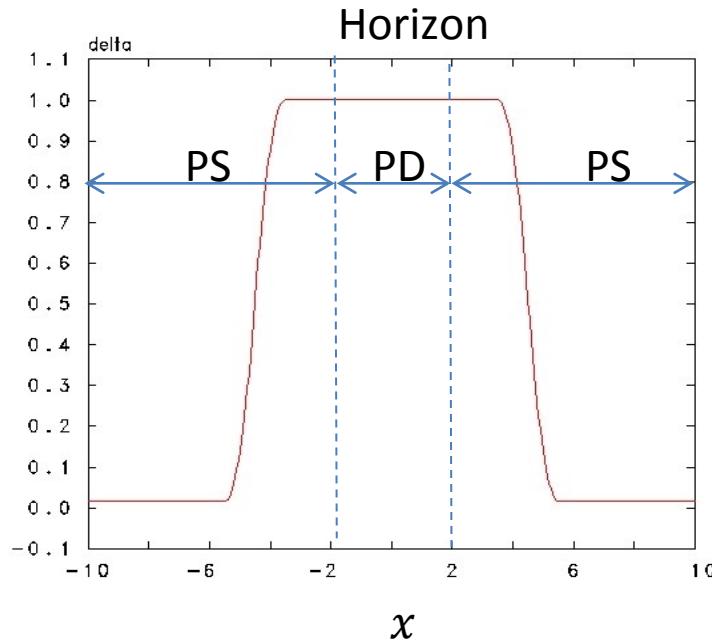


$$u = 0$$

$$u = 0.02$$

Continuum patch test with coupling

- No artifacts with PD-PS coupling (this was hoped for but not guaranteed).

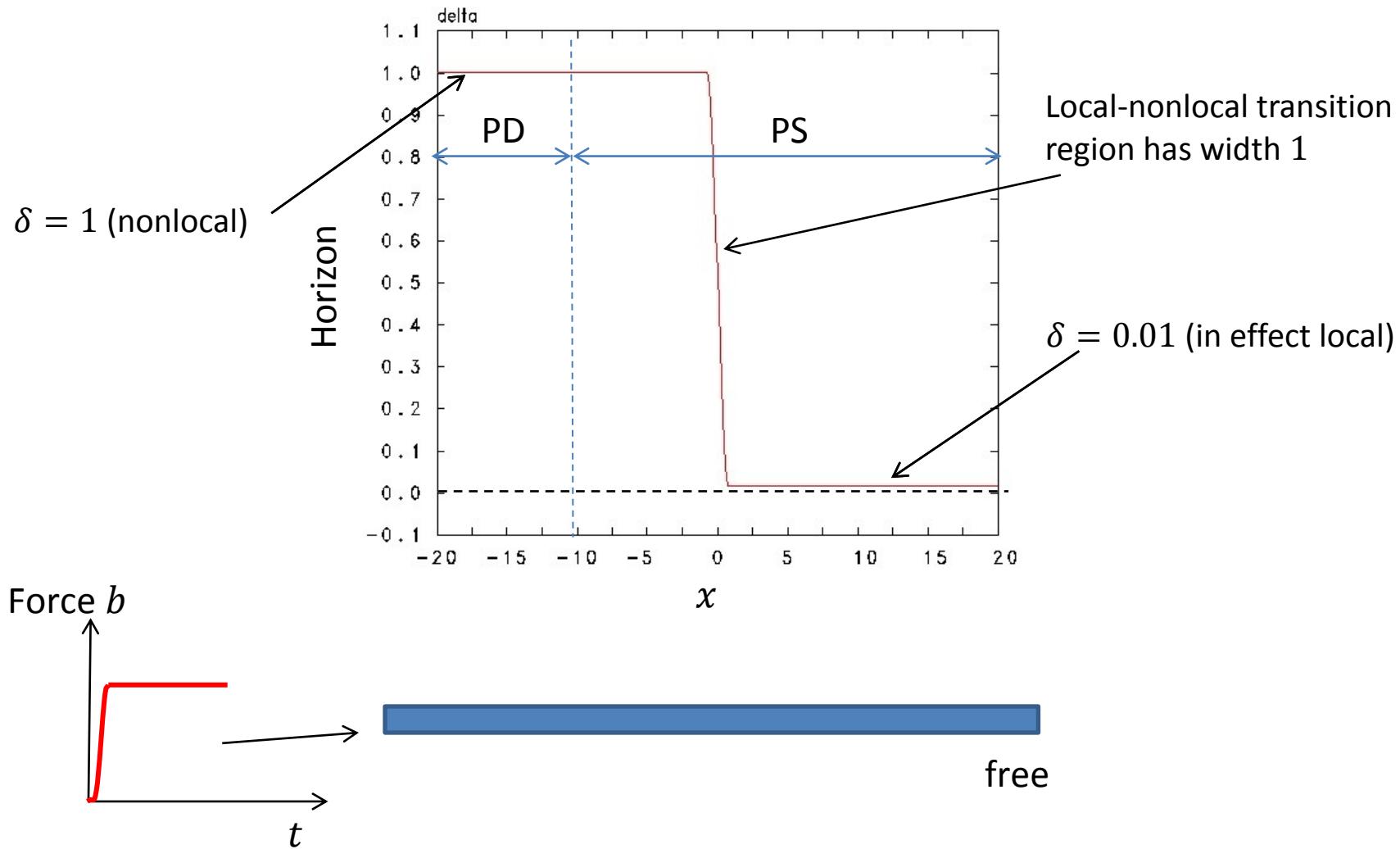


$$u = 0$$

$$u = 0.02$$

Pulse propagation test problem

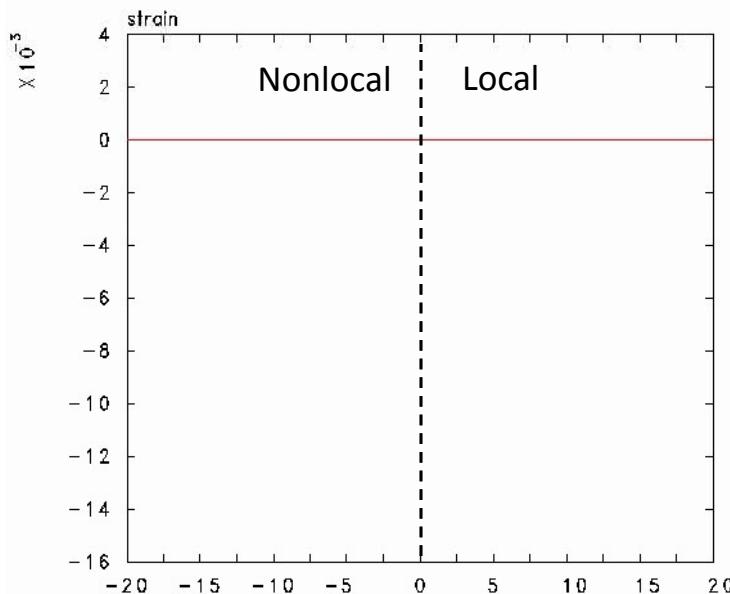
- Does our coupling method work for dynamics as well as statics with variable horizon?



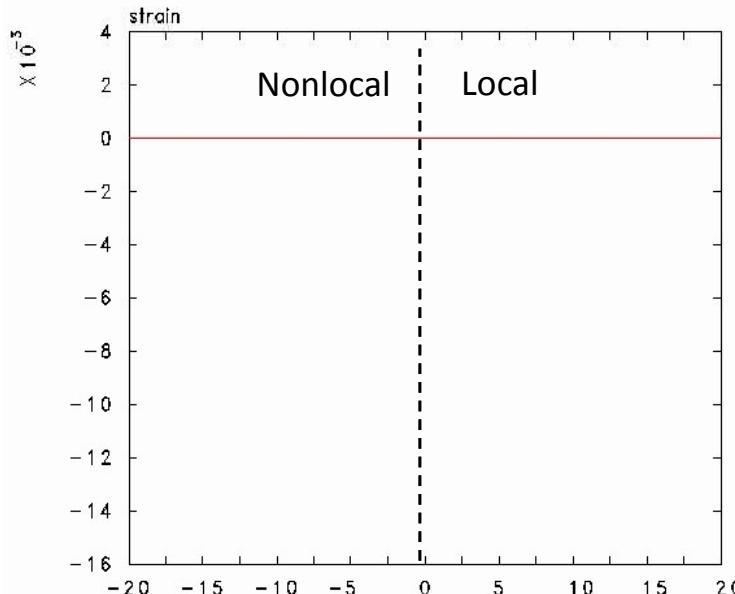
Pulse propagation test results

- Movies of strain field evolution

Full PD everywhere

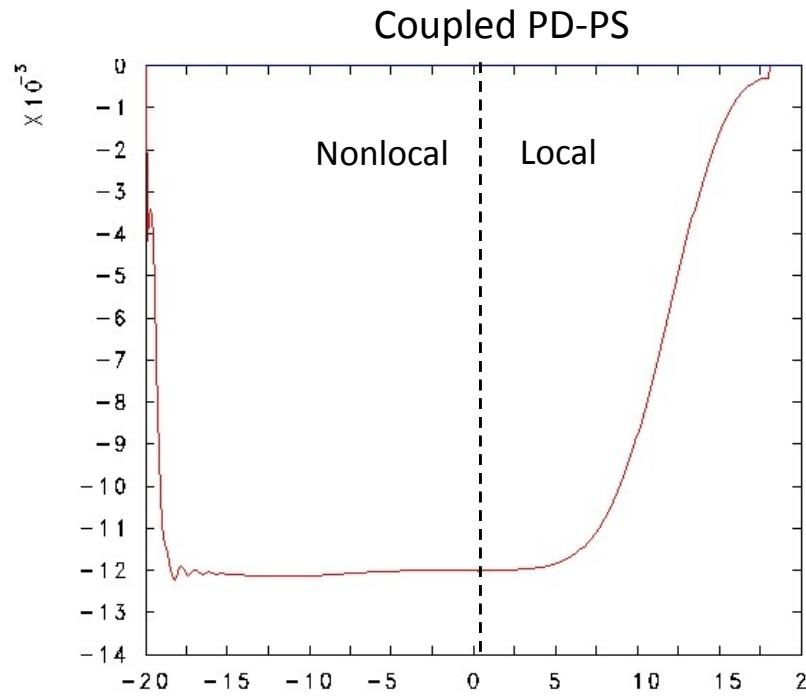
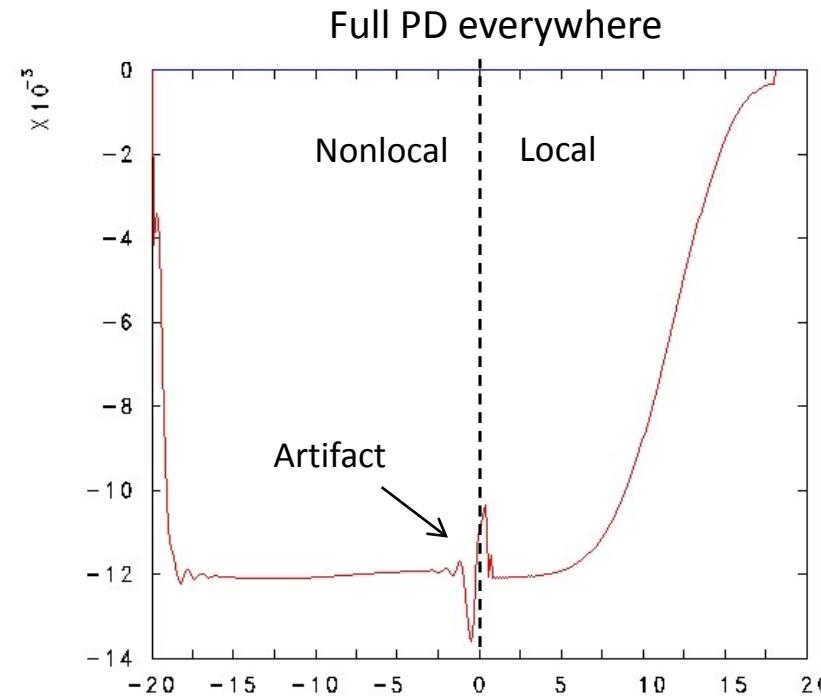


Coupled PD-PS



Pulse propagation test results

- Strain field: no artifacts appear in the coupled model the local-nonlocal transition.



Discussion

- The partial stress approach may provide a means for local-nonlocal coupling within the continuum equations.
 - Uses the underlying peridynamic material model but modifies the way internal force density is computed.
 - Expected to work in 2D and 3D too (but not yet tested).
 - No assumption of linear material response (but nonlinear not yet tested).
- PS is inconsistent from an energy minimization point of view.
 - Not suitable for a full-blown theory of mechanics (as PD is).
 - Not yet clear what implications this may have in practice.
 - We still need to use full PD for crack progression.
- Some similarities between PS and the Virtual Internal Bond method (Gao & Klein, Jmps, 1998).