

The Relationship Between Crack-Tip Strain and Subcritical Cracking Thresholds for Steels in High-Pressure Hydrogen Gas

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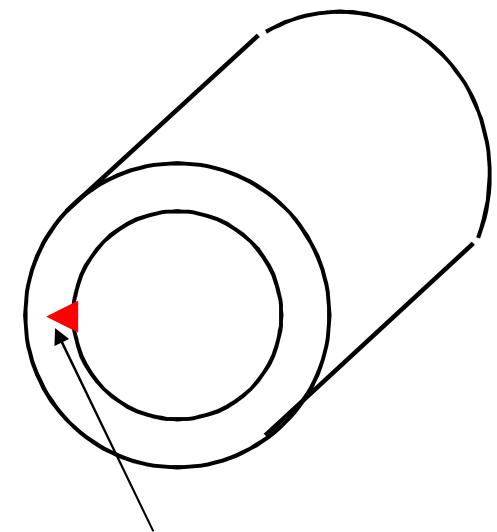
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Subcritical cracking threshold (K_{TH}) measurement methods needed for H_2 pressure systems

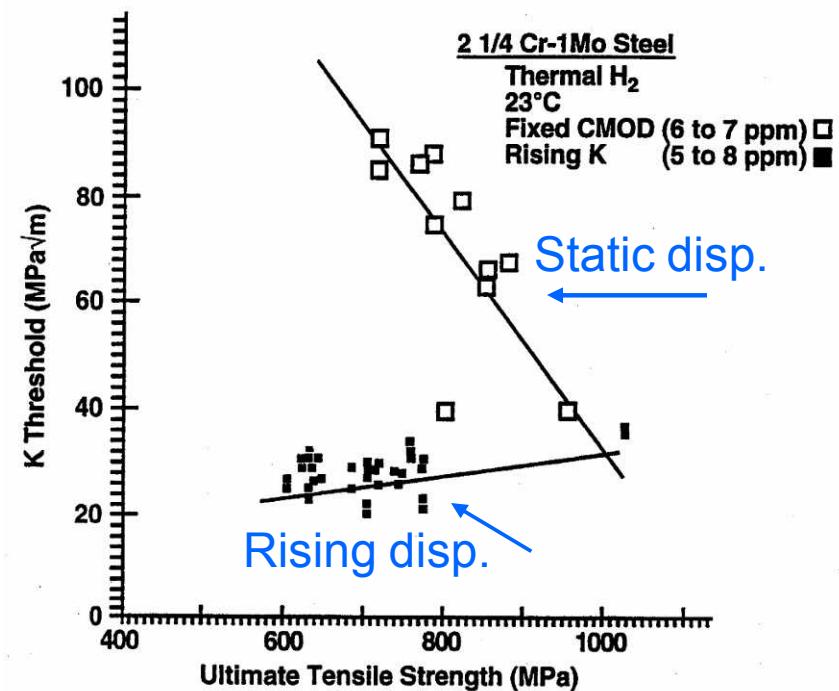
- New applications are considering low-strength, low-alloy steels for flaw tolerant designs
 - Pressure vessels, pipelines
 - Hydrogen gas pressure up to 100 MPa
 - Designs require fracture and fatigue properties
- **Conservative and reliable methods for measuring cracking threshold (K_{TH}) needed for low strength steel in H_2**



K_{TH} is stress intensity factor above which subcritical crack growth proceeds under quasi-static loading

K_{TH} testing originates from stress-corrosion cracking methods

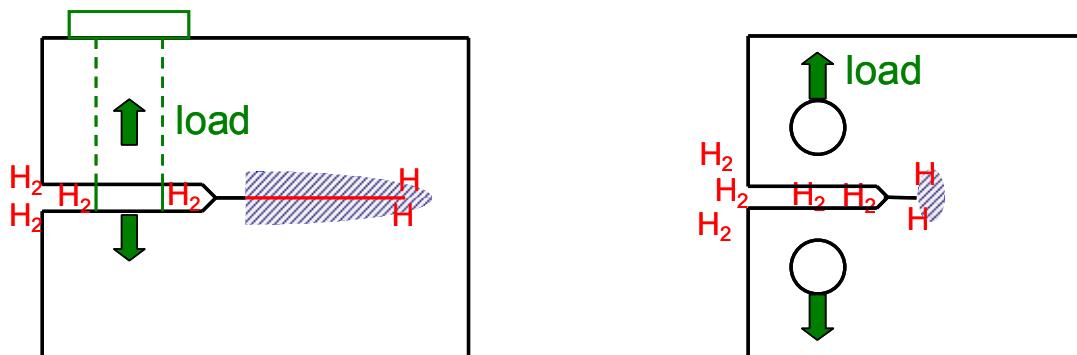
- Higher strength alloys with lower K_{TH}
- Slow environment assisted cracking kinetics
 - Favors static tests which do not impede EAC kinetics
- Ex: [Bolt load compact specimen \(WOL\)](#)
 - Developed and accepted into ASTM E1681 based on successful results from high-strength alloys with low fracture threshold values
 - **Consequences of applying this type of test method to lower strength steels not thoroughly explored**
- Literature reports suggest thresholds from constant displacement tests may be non-conservative for lower strength steels ($\sigma_y <\sim 1000$ MPa)



Gangloff, *Comprehensive Structural Integrity*, Vol. 6, (2003), pp. 31-101.

Objectives

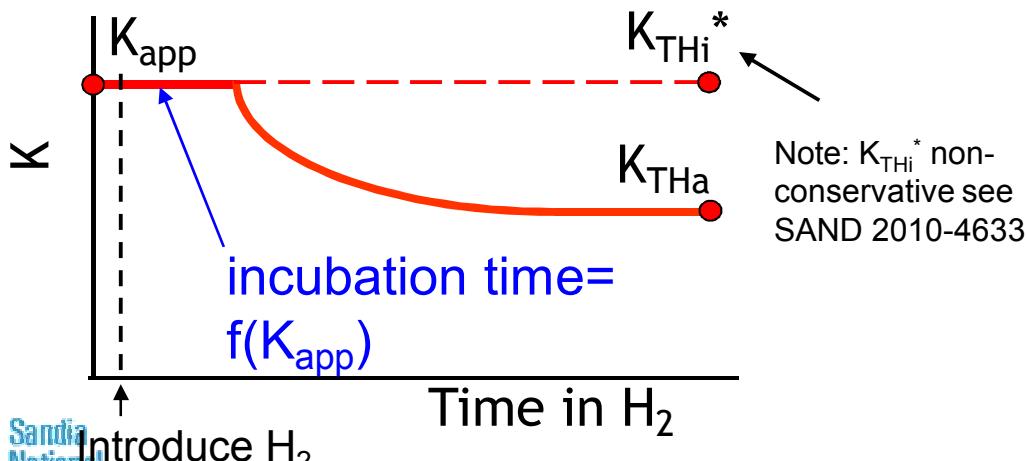
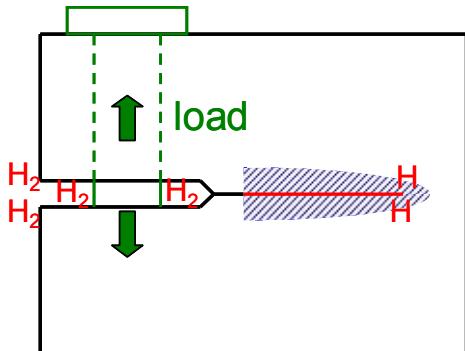
- Evaluate and compare constant displacement and rising displacement test methods
 - Tests conducted in 100 MPa hydrogen gas
- Explain differences between these test methods in a crack tip mechanics framework
- Goal: Demonstrate that constant displacement tests do not measure the same physical property as rising displacement tests when the fracture mechanism is strain controlled
 - this difference can be explained by considering the crack tip strain fields



Two methods for measuring K_{TH} evaluated

Constant Displacement

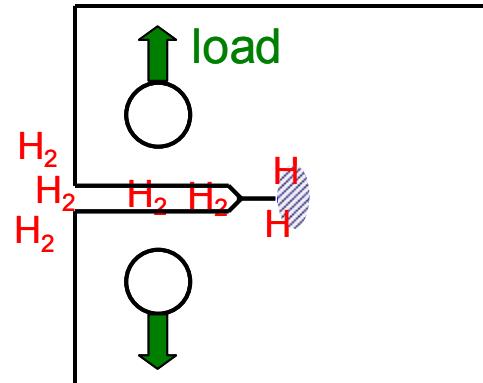
- K_{THa} - measured at *crack arrest*
- ASTM E1681



Rising Displacement

- K_{THi} - measured at *crack initiation*
- Use elastic-plastic J-Integral (ASTM E1820)

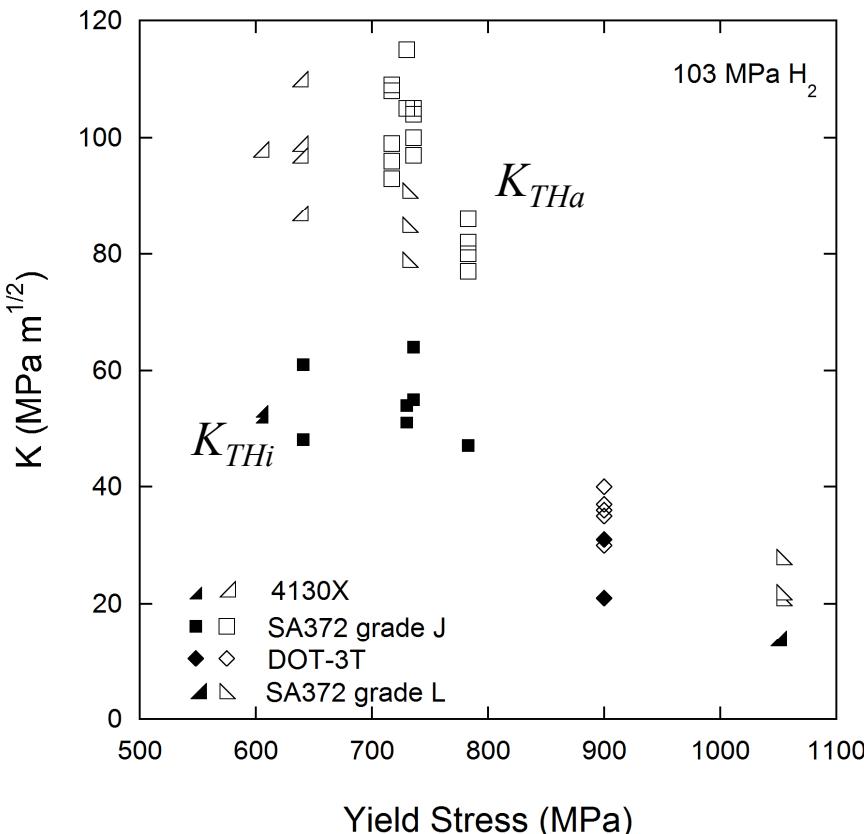
$$K_{THi} = \sqrt{J_{Ic} E'}$$



Comparison of arrest and initiation thresholds

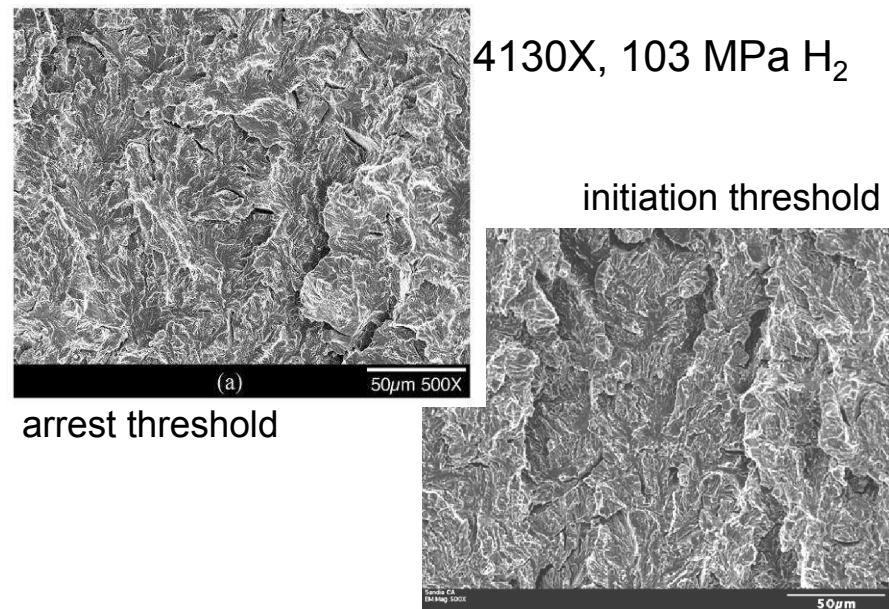
Differences: $K_{THa} > K_{THi}$

- Note: FEA demonstrates K-dominance at K_{THa} (SAND2010-4633)



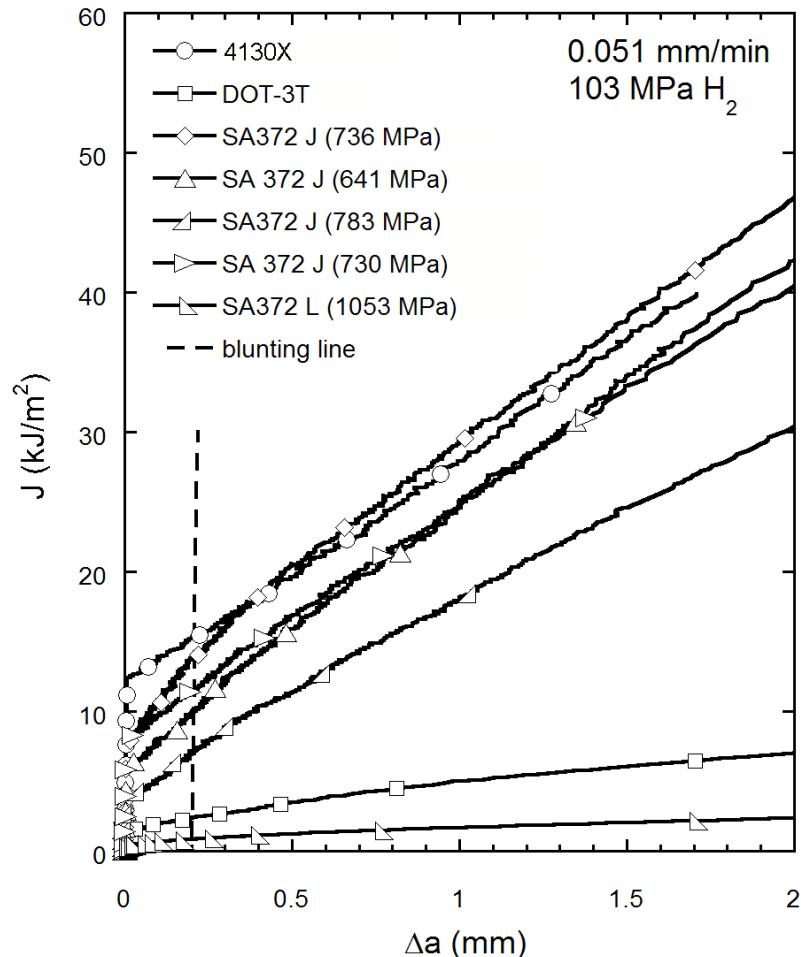
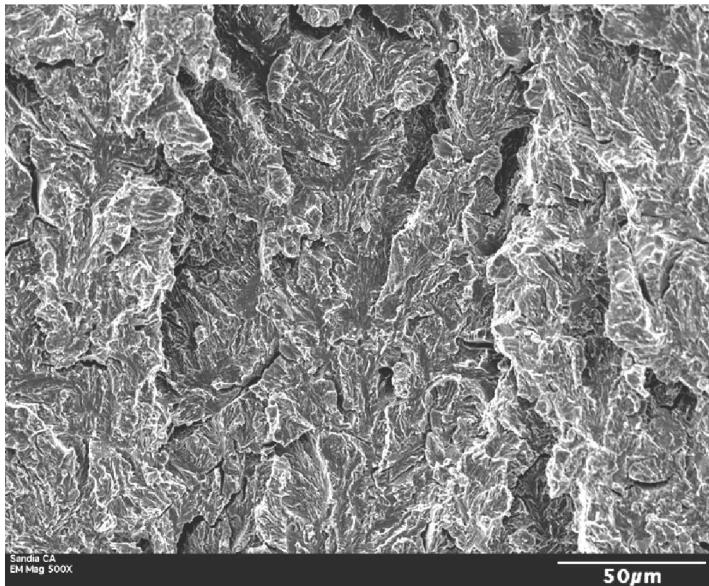
Similarities:

- Both thresholds increase with decreasing strength
- Fracture surface appearance suggest fracture mechanism is the same



Fracture mechanism is strain controlled

- Fracture surface plasticity
- R-curve
- Consensus in the literature
 - e.g. Takeda and McMahon, *Met Trans A*, 1981



Stationary crack tip strain field provides relationship between K_{THi} and fracture strain

- Strain decays ahead of **stationary** crack tip $\propto 1/r$ (HRR singularity)

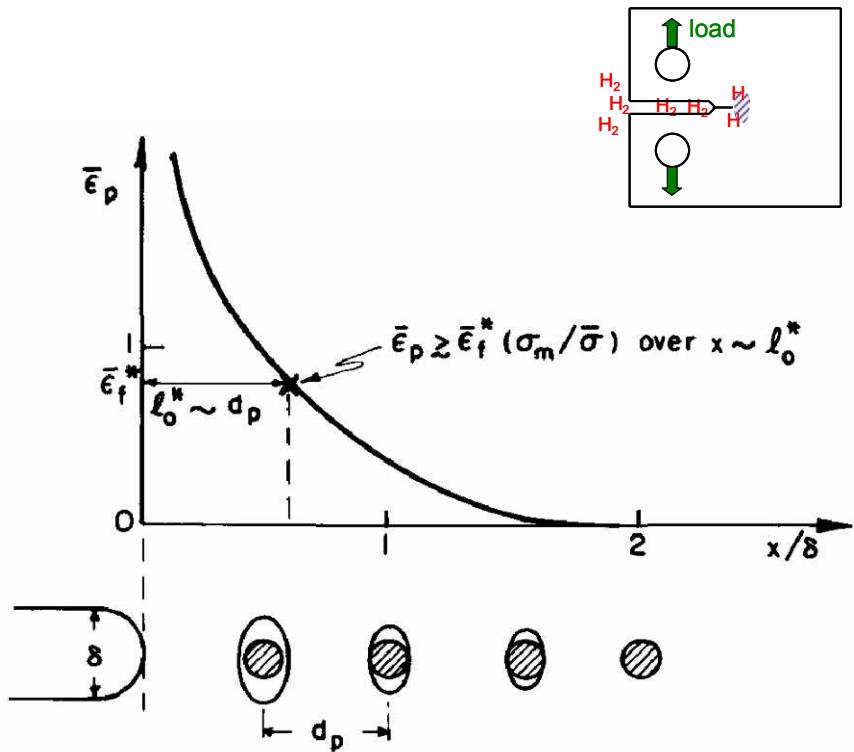
$$\varepsilon_{ij} \approx k \left(\frac{J}{\sigma_0 r} \right)$$

- Stress intensity factor is related to strain, ε , at distance, r , from crack tip:

$$K_{THi} \approx C \sqrt{E \sigma_0 l^* \varepsilon_f^H}$$

$$K_{THi} \approx \sigma_0 \sqrt{l^*} \sqrt{\frac{\varepsilon_f^H}{\varepsilon_0}}$$

l^* is a critical distance from crack tip



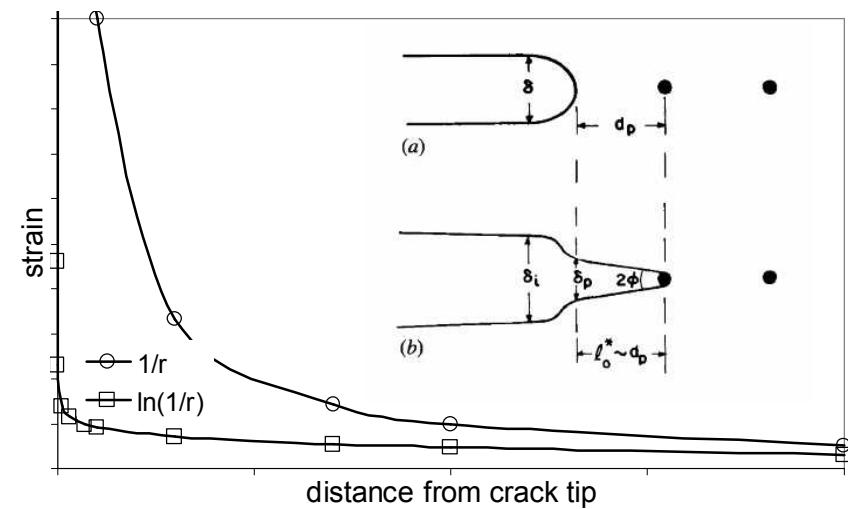
Ritchie and Thompson, *Met Trans*, 1985

•Analogous relationship for K_{THa} needs to be developed

Strain field associated with propagating crack is relevant to arrest threshold

- Region of elastic unloading occurs in wake of **propagating** crack
- Leads to weakening of strain singularity
 - Strains decay ahead of propagating crack $\propto \ln(1/r)$

$$\gamma^p \approx \frac{M}{\sigma_0} \frac{dJ}{da} + \frac{1.88(5-4\upsilon)\sigma_0}{2E} \ln\left(\frac{J}{r}\right)$$



Rice *et al*, ASTM STP700, 1980

Analytical expression for propagating crack strain field developed for R-curve behavior

- Strain field for propagating crack

$$\gamma^p \approx \frac{M}{\sigma_0} \frac{dJ}{da} + \frac{1.88(5-4v)\sigma_0}{2E} \ln\left(\frac{J}{r}\right)$$

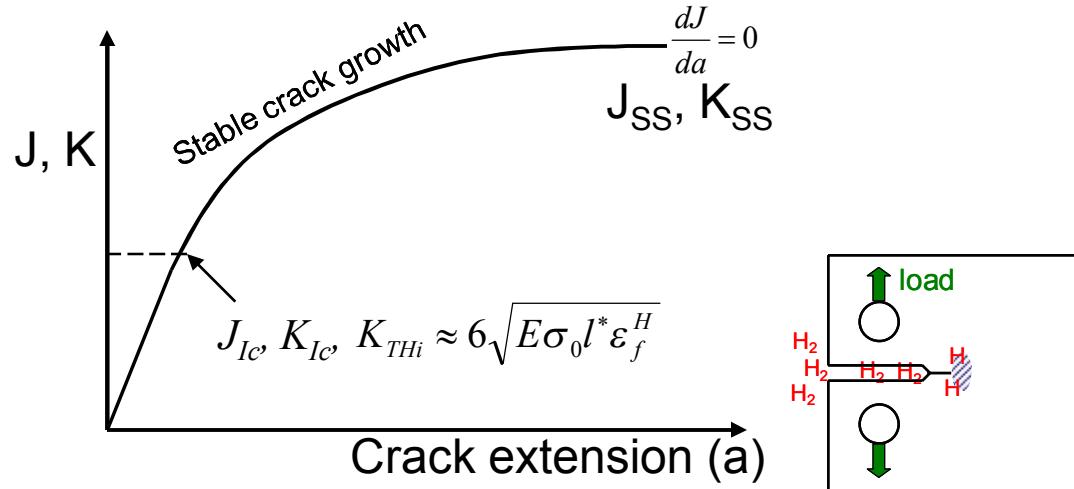
- Criterion for continued crack extension

$$\gamma_f^p \approx \frac{M}{\sigma_0} \frac{dJ}{da} + \frac{1.88(5-4v)\sigma_0}{2E} \ln\left(\frac{J}{l^*}\right)$$

Fracture strain

$$J = K^2 / E'$$

$$\gamma_f^p \approx \frac{M}{\sigma_0} \frac{dJ}{da} + \frac{1.88(5-4v)\sigma_0}{2E} \ln\left(\frac{K^2}{El^*}\right)$$



Two-term field with $\ln(1/r)$ singularity presumed to represent strains for propagating crack under decreasing K

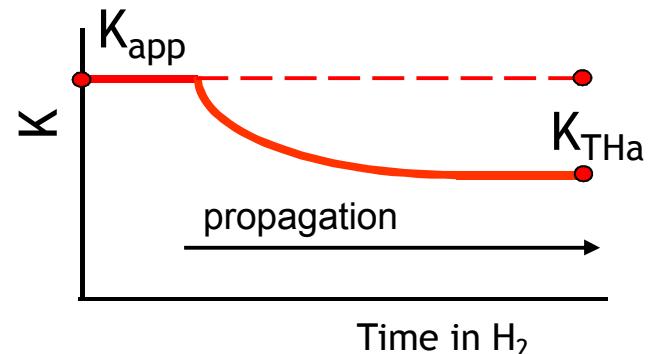
Strain field for propagating crack provides relationship between K_{THa} and fracture strain

- Assume limiting case: strain represented by $\ln(1/r)$ term
- When $K_{app} > K_{THa}$

$$\gamma_f^p < \frac{1.88(5-4v)\sigma_0}{2E} \ln\left(\frac{K^2}{El^*}\right)$$

- When $K_{app} = K_{THa}$

$$\gamma_f^p = \frac{1.88(5-4v)\sigma_0}{2E} \ln\left(\frac{K_{THa}^2}{El^*}\right)$$



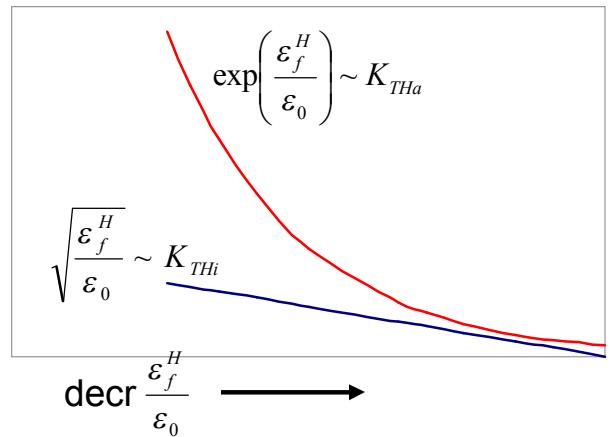
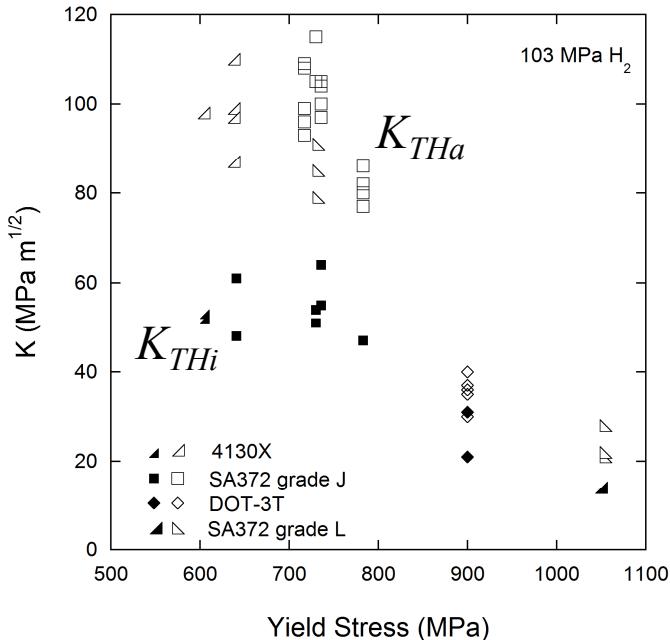
$$K_{THa} \approx \sigma_0 \sqrt{l^*} \exp\left(\frac{\varepsilon_f^H}{\varepsilon_0}\right)$$

Crack tip mechanics-based models support $K_{THa} > K_{THi}$ for strain controlled fracture

- If fracture involves plasticity, e.g. $\varepsilon_f^H > \varepsilon_0$
 - K_{THa} must be greater than K_{THi}

$$K_{THa} \approx \sigma_0 \sqrt{l^*} \exp\left(\frac{\varepsilon_f^H}{\varepsilon_0}\right)$$
$$K_{THi} \approx \sigma_0 \sqrt{l^*} \sqrt{\frac{\varepsilon_f^H}{\varepsilon_0}}$$

K_{THa} , K_{THi} equivalent only when fracture ductility is small



Conclusions

- Subcritical cracking thresholds measured using constant displacement test methods (K_{THa}) are greater than those measured using rising displacement methods (K_{THi})
- Hydrogen-assisted subcritical cracking of low- to moderate-strength pressure vessel steels occurs via strain controlled mechanisms
- Weaker strain singularity of propagating crack ($\sim \ln(1/r)$) compared to stationary crack ($\sim 1/r$) can account for arrest thresholds (K_{THa}) exceeding initiation thresholds (K_{THi})