

## LA-UR-12-22322

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Title: Small deformation viscoplastic dynamic sphere problem

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Intended for: Society for Industrial and Applied Mathematics 2012 Annual Meeting,  
2012-07-09/2012-07-13 (Minneapolis, Minnesota, United States)



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# Small deformation viscoplastic dynamic sphere problem

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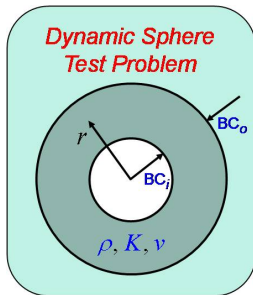
July 11, 2012

## Research objectives

- Obtain analytic solution to dynamic sphere test problem
- Develop software to evaluate solution
- Demonstrate 'convergence' of computed solution

## Schematic of dynamic sphere problem

- Analytic solution includes:
  - Dirichlet BC: Displacement
  - Neumann BC: Strain
  - Robin BC: Stress
- Time-varying BCs applied at  $r_i$ ,  $r_o$
- This talk focuses only on Dirichlet (displacement) BCs



## Outline

- Describe Bodner-Partom model of viscoplasticity.
- Describe Bodner-Partom dynamic sphere problem.
- Derive series solution for displacement.
- Describe numerical implementation of analytic solution.
- Demonstrate self-convergence of solution.

## Conservation law equations for isotropic viscoplastic material

- Formulated in material coordinates, so mass balance satisfied
- Constant temperature, so no energy equation
- Variables:
  - $u(x, t)$ : displacement
  - $\epsilon(x, t) = \frac{1}{2}(\nabla u + \nabla u^T)$ : total strain tensor
  - $\epsilon^p(x, t)$ : plastic strain tensor

$$\rho \ddot{u} = \nabla \cdot \sigma + b$$

$$\sigma = C(\epsilon - \epsilon^p)$$

$$u(x, 0) = u^{(0)}(x), \quad \dot{u}(x, 0) = u^{(1)}(x)$$

$$u|_{\partial\Omega} = u_b(x, t)$$

## Bodner-Partom viscoplastic constitutive model

The constitutive model variables are

- $\epsilon^P(x, t)$ : plastic strain tensor
- $Z(x, t)$ : isotropic hardening variable

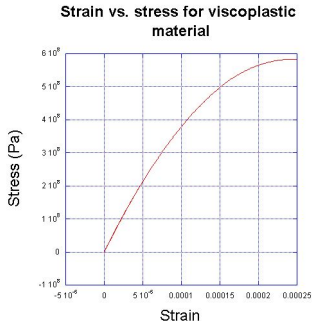
and the equations of the model are

$$\dot{\epsilon}^P = G\left(\frac{|S|}{Z}\right) \frac{S}{|S|}$$

$$\dot{Z} = \gamma(Z) G\left(\frac{|S|}{Z}\right) |S|$$

$$\epsilon^P(x, 0) = \epsilon^{P,(0)}(x), \quad Z(x, 0) = Z^{(0)}(x)$$

where  $S(x, t) = \sigma - \frac{1}{3}\text{tr}\sigma I$  is the stress deviator.



## Radially symmetric dynamic sphere IBVP

Let  $\lambda = -C\epsilon^P$  be plastic stress tensor. In spherical coordinates,

$$c_r^{-2}\ddot{u} = u'' + \frac{2}{r}u' - \frac{2}{r^2}u + c_r^{-2}f_r(\lambda)$$

$$\lambda_{rr} = -C_{rrrr}\epsilon_{rr}^P - 2C_{rr\theta\theta}\epsilon_{\theta\theta}^P$$

$$\lambda_{\theta\theta} = -C_{rr\theta\theta}\epsilon_{rr}^P - (C_{rrrr} + C_{rr\theta\theta})\epsilon_{\theta\theta}^P$$

$$u(r, 0) = d_r^0(r) \quad \dot{u}(r, 0) = v_r^0(r) \quad \epsilon_{rr}^P(r, 0) = 0 \quad \epsilon_{\theta\theta}^P(r, 0) = 0$$

$$u(r_i, t) = BC_i(t) \quad u(r_o, t) = BC_o(t)$$

where

$$f_r(\lambda) = b_r + \frac{1}{\rho}[\lambda'_{rr} + \frac{2}{r}(\lambda_{rr} - \lambda_{\theta\theta})].$$



## Analytic solution for $u$

- Assume  $\lambda_{rr}$ ,  $\lambda_{\theta\theta}$  are known.
- $u$  has the form  $u(r, t) = r^{-1/2}[\bar{w}(r, t) + \tilde{w}(r, t)]$ .
- $\bar{w}(r, t) = \gamma_0(t) + \gamma_1(t)r$  contains BCs.
- $\tilde{w}(r, t) = \sum_{n=1}^{\infty} a_n(t)\psi_n(r)$  contains plasticity.
- $a_n(t)$  is given by the equation

$$a_n(t) = c_{3,n} \cos c_r \sqrt{\lambda_n} t + c_{4,n} \sin c_r \sqrt{\lambda_n} t + \frac{1}{c_r \sqrt{\lambda_n}} \int_0^t F_n(s) \sin c_r \sqrt{\lambda_n} (t-s) ds,$$

$$F_n(t) = c_r^2 \frac{\int_{r_i}^{r_o} \tilde{f}(r, t) \psi_n(r) dr}{\int_{r_i}^{r_o} r \psi_n^2(r) dr}$$

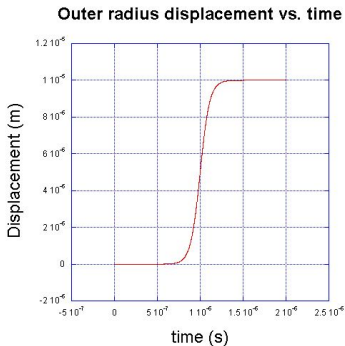
where  $\tilde{f} = L(\tilde{w}) + r^{3/2} c_r^{-2} f_r(\lambda)$ .

## Numerical implementation

- Choose number of grid points  $nr$  through shell, number of time steps  $nt$ , and number of eigenmodes  $nl$ .
- Numerical quadrature in time and space, including hereditary integral.
- Take  $\tilde{w}(r, t) = \sum_{n=1}^{nl} a_n(t)\psi_n(r)$  at each time step and grid point.
- Use material model to partition total strain (from  $u$ ) into elastic ( $\epsilon$ ) and plastic ( $\epsilon^P$ ) components.
- At each time step, iterate to find  $\epsilon^P$ ,  $\lambda$ , and  $u$ .
- Numerical error arises from quadrature, series truncation, and discretization in computing  $\epsilon^P$ .

## Self-convergence for test problem

- Consider convergence of analytic solution in  $nr$ ,  $nt$ ,  $nl$ .
- Compute to a final time of  $T = 2$  microseconds.
- At inner radius  $r_i$ , impose void displacement BCs:  $u(r_i, t) = 0$ .
- At outer radius  $r_o$ , impose time-varying smooth jump displacement BCs.



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## Self-convergence: Convergence in space

Take  $nt = 8000$ ,  $nl = 300$ .

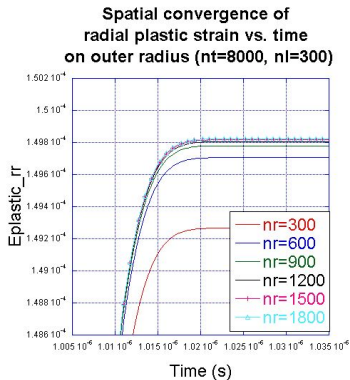
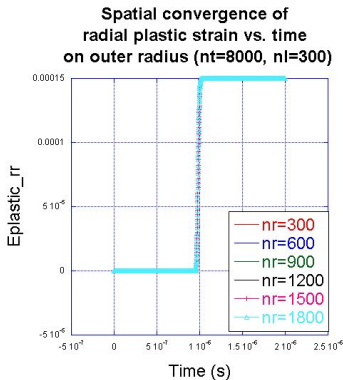


Figure: Left:  $nr$  convergence plot of  $\epsilon_{rr}^P$  vs. time at  $r_o$ . Right: Zoomed in plot of  $\epsilon_{rr}^P$ .

## Self-convergence: Convergence in time

Take  $nr = 1200$ ,  $nl = 300$ .

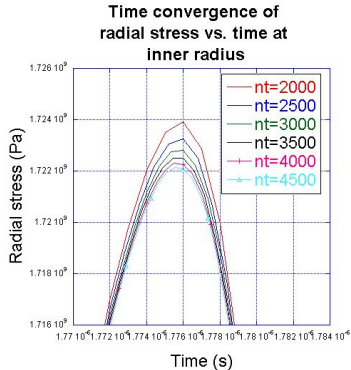
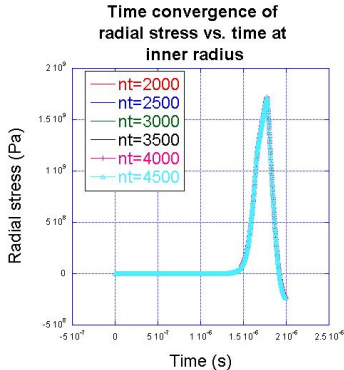


Figure: Left:  $nt$  convergence plot of  $\sigma_{rr}$  vs. time at  $r_i$ . Right: Zoomed in plot of  $\sigma_{rr}$ .

## Self-convergence: Convergence in eigenmode

Compute through shell at final time  $T = 2$  microseconds. Take  $nr = 1200$ ,  $nt = 3500$ .

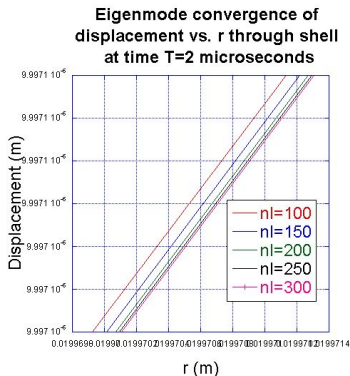
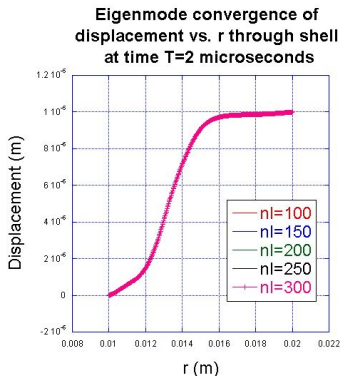


Figure: Left:  $nl$  convergence plot of  $u$  vs.  $r$  at time  $T = 2$  microseconds. Right: Zoomed in plot of  $u$ .

## Self-convergence: Quantitative analysis I

- We compute  $L^1(0, T)$  norm of percent errors of plastic strain relative to reference solution computed on extremely fine mesh to test spatial convergence.
- The order of convergence is 2.25.

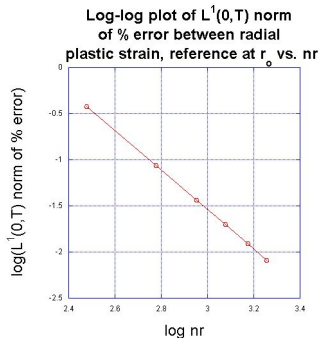


Figure: Log-log plot of  $L^1(0, T)$  norm of percent error of  $\epsilon_{rr}^p$  at  $r_o$  vs.  $nr$ .

## Self-convergence: Quantitative analysis II

- We compute  $L^1(0, T)$  norm of percent errors of stress relative to reference solution computed on extremely fine mesh to test time convergence.
- The order of convergence is 2.

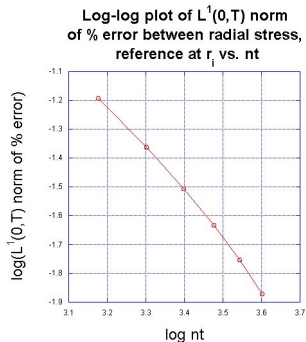
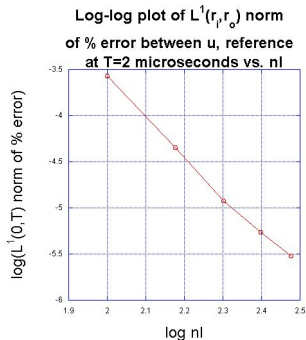


Figure: Log-log plot of  $L^1(0, T)$  norm of percent error of  $\sigma_{rr}$  at  $r_i$  vs.  $nt$ .



## Self-convergence: Quantitative analysis III

- We compute  $L^1(r_i, r_o)$  norm of percent errors of displacement relative to reference solution computed on extremely fine mesh to test eigenmode convergence.
- The order of convergence is 3.2.



**Figure:** Log-log plot of  $L^1(r_i, r_o)$  norm of percent error of  $u$  through shell at  $T = 2$  microseconds vs.  $nl$ .

## Summary

- We describe the Bodner-Partom constitutive model of plastic flow for a solid under small deformation.
- We derive an analytic solution for displacement in the form of an infinite series.
- We demonstrate convergence of a truncated solution under spatial, time, and eigenmode refinement.

## Future work

- Compare analytic solution to LANL physics code.
- Derive and study solution for other boundary conditions (Neumann, Robin).
- Derive and study solution for finite deformations.