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*Title:* Modal Analysis and SHM Investigation of CX-100 Wind Turbine Blade

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## **Vibration Testing and Structural Damage Identification of Wind Turbine Blades**

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2. Dept. of Mechanical Eng., University of Massachusetts Lowell, Lowell, MA 01854
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4. The Engineering Institute, Los Alamos National Laboratory, Los Alamos, NM 87545

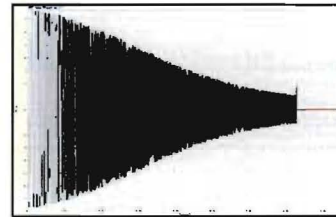
### **Abstract**

This paper presents the dynamic characterization of a CX100 blade using modal testing. Obtaining a thorough dynamic characterization of these turbine blades is important because they are complex structures, making them difficult to monitor for damage initiation and subsequent growth. This dynamic characterization was compared to a numerical model developed for validation. Structural Health Monitoring (SHM) techniques involving Lamb wave propagation, frequency response functions, and impedance based methods were also used to provide insight into blade dynamic response. SHM design parameters such as traveling distance of the wave, sensing region of the sensor and the power requirements were examined. Results obtained during modal and SHM testing will provide a baseline for future damage detection and mitigation techniques for wind turbine blades.

# Modal Analysis and SHM Investigation of CX-100 Wind Turbine Blade



Krystal Deines  
Timothy Marinone  
Ryan Schultz



Kevin Farinholt & Gyuhae Park



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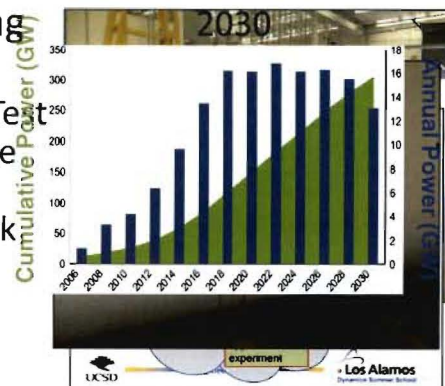


Introduction Free-Free Free-Free w/Mass Fixed-Free SHM Conclusions

## Agenda

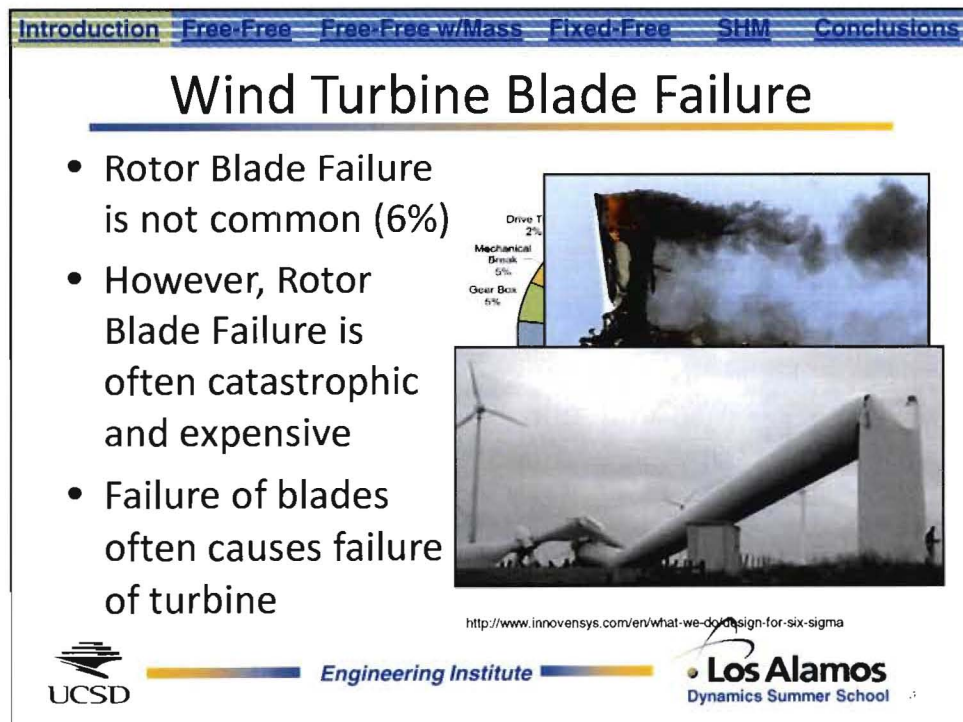
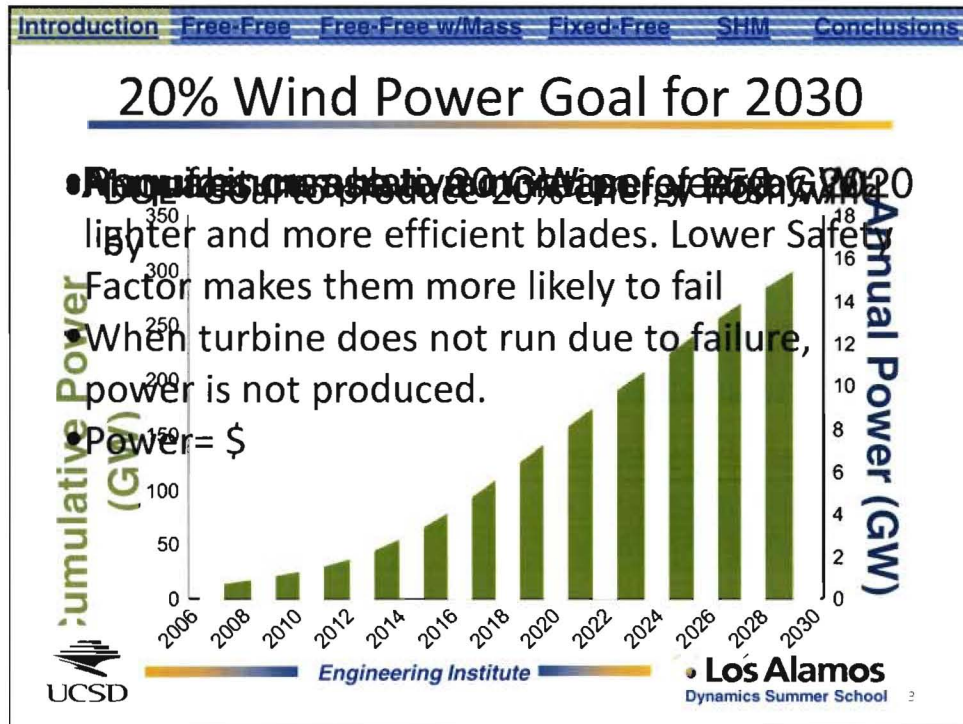
- Introduction
- CX-100 Modal Testing
  - Background
  - Free-Free Test
  - SHM
  - Previous work
  - Frequency Range
  - Conclusions
  - Environmental variability
  - Future Work

20% Wind Power Goal for 2030



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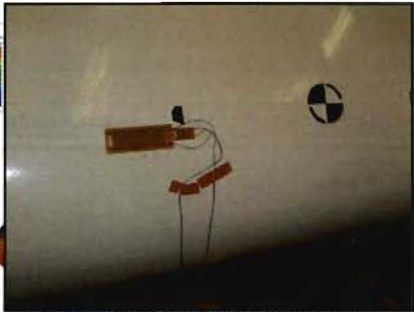




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## Predicting Blade Failure

- **Structural Health Monitoring**
  - Real-time monitoring of blade health for prediction
  - Requires baseline data as reference with



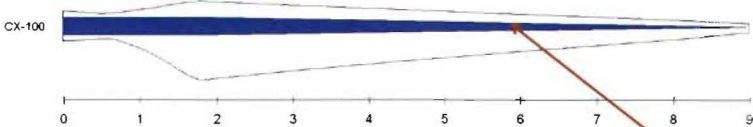

<http://www.nsecomposites.com/projects/wind-energy.html>

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## CX-100 Description

- 9 Meter Experimental Blade designed by Sandia National Laboratories
  - TX-100, CX-100, BSDS
- Key Feature: Carbon Fiber Spar Cap

Carbon Fiber Spar Cap



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## Previous Work - Modal Testing of Wind Turbine Blades

- Griffith and Carne (2010)
- Adams and White (2010)
  - Modal Testing of BSDS Blade
  - Modal Testing of CX-100 Blade in w/Seismic Mass
  - Demonstrated support has effect
  - Approach to simulate fixed frequencies boundary condition without fixed apparatus


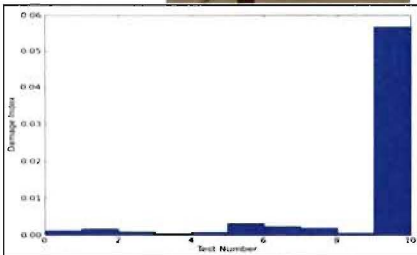



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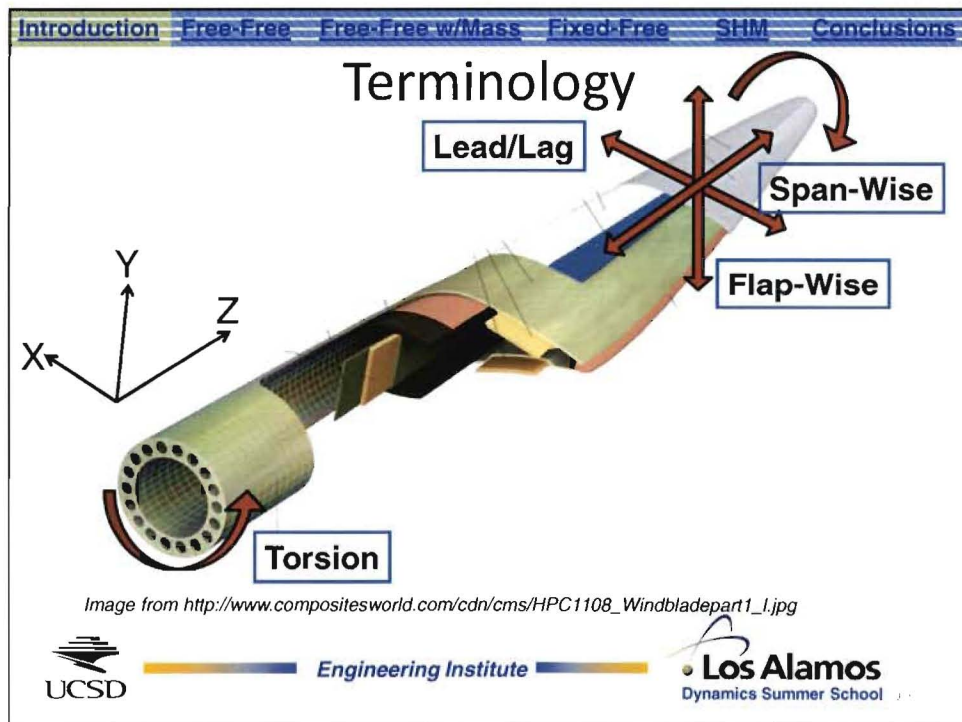
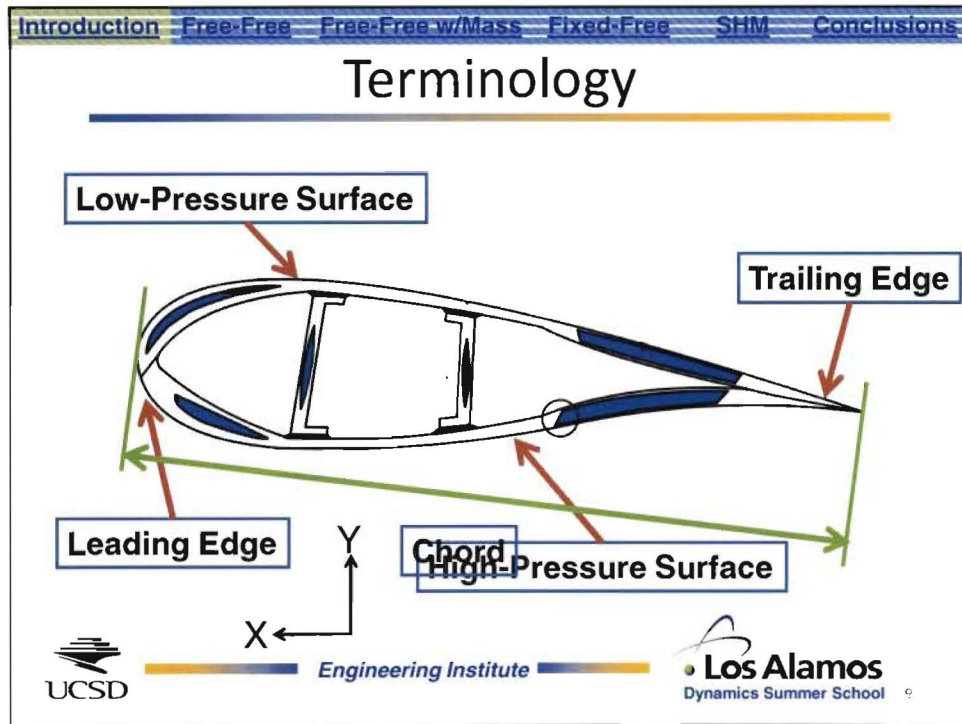
## Previous Work - Structural Health Monitoring of CX-100

- Light-Marquez et al
  - Lamb Wave, Frequency and Time SHM techniques examined
  - Simulated Damage on 1 Meter Section
  - Good local damage detection

Light-Marquez, A., Sobin, A., Park, G., Farinholt, K., "Structural Damage Identification in Wind Turbine Blades using Piezoelectric Active-sensing," Proceedings of the IMAC XXVIII, Feb. 1-4, 2010, Jacksonville, FL.

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## Free-Free

Q: Why Free-Free?

1. Simple setup

Q: What are some difficulties with Free-Free?

2. Easy to correlate model to

1. There's no such thing as free-free testing.

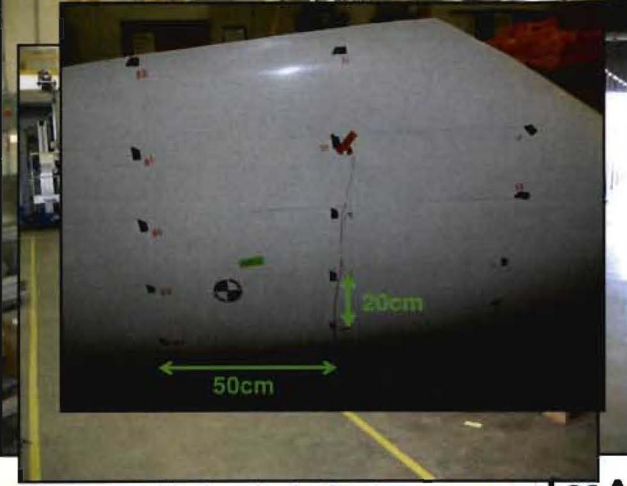
2. Care must be taken in the supporting of the blade to not distort modes of interest

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## Free-Free Modal Test #1

Use Immature System Motion Measurement of blade to capture



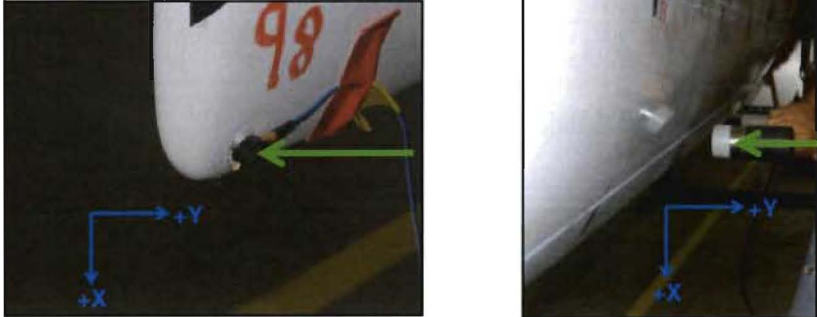
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## Impact & Measurement Directionality

➤ Impact & measure parallel with Y-axis

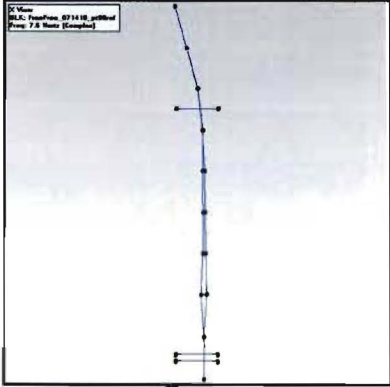


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## Free-Free #1 Mode Shapes & Frequencies

Mode	Frequency (Hz)	Description
1	7.61	1 <sup>st</sup> Flap Bending
2	18.1	1 <sup>st</sup> Lag Bending
3	20.2	2 <sup>nd</sup> Flap Bending
4	32.2	3 <sup>rd</sup> Flap Bending
5	45.1	2 <sup>nd</sup> Lag Bending
6	50.5	4 <sup>th</sup> Flap Bending
7	63.9	1 <sup>st</sup> Torsion
8	70.1	3 <sup>rd</sup> Lag Bending

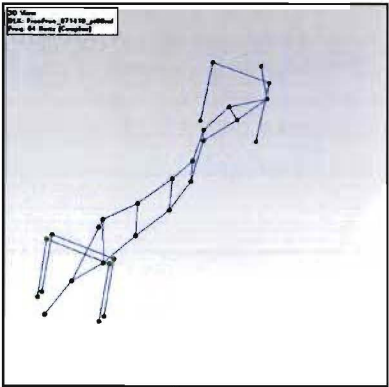


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## Free-Free #1 Mode Shapes & Frequencies

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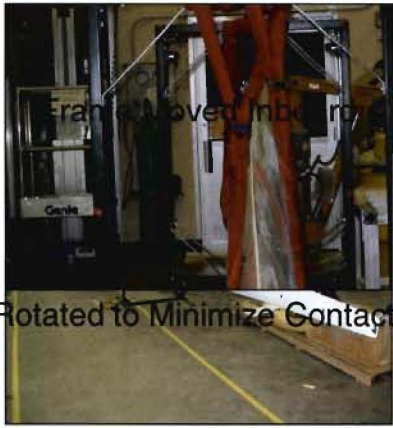


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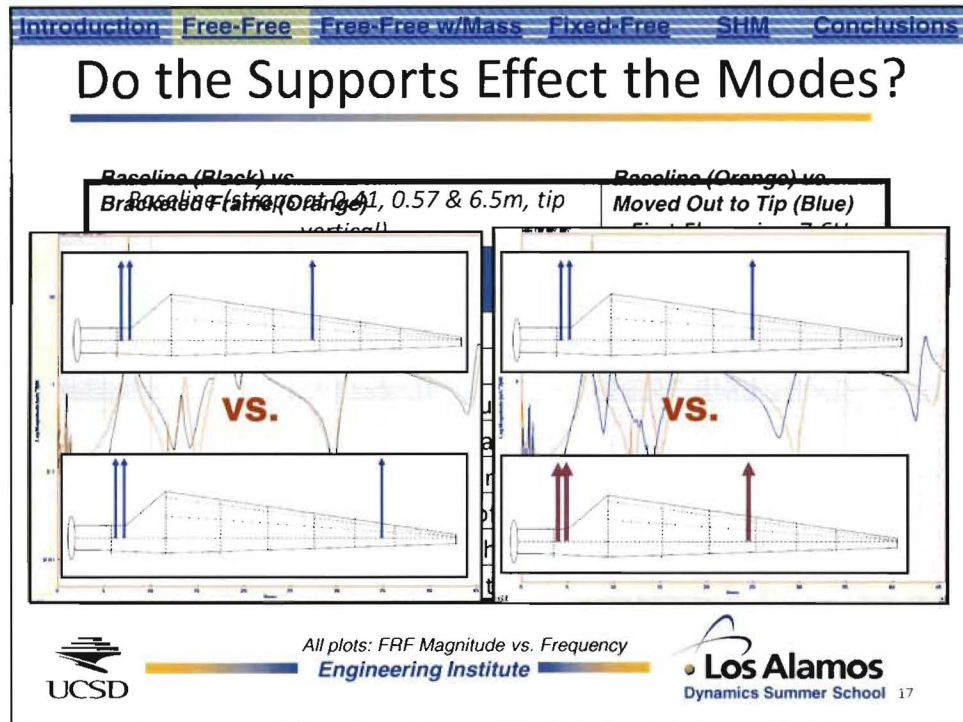
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## Do the Supports Effect the Modes?


VS.


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## Free-Free Test #2

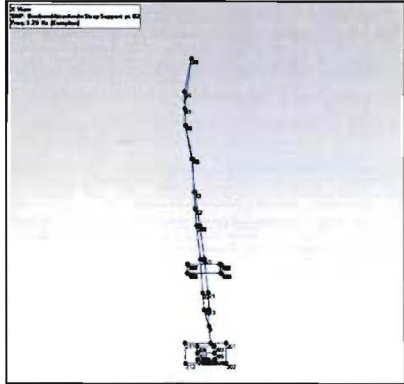
- Want to induce strain at root absent in Test #1
- Bolt Blade to Fixture (mass added to root)
- Fixture NOT bolted down

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## Free-Free #2 Mode Shapes & Frequencies

Mode	Frequency (Hz)	Description
1	3.29	1 <sup>st</sup> Flap Bending
2	8.72	2 <sup>nd</sup> Flap Bending
3	17.6	3 <sup>rd</sup> Flap Bending
4	30.7	4 <sup>th</sup> Flap Bending
5	45.0	5 <sup>th</sup> Flap Bending
6	50.9	1 <sup>st</sup> Torsion



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## Fixed-Free

Q: Why Fixed-Free?

Q: What are some difficulties with Fixed-Free?

1. There's no such thing as fixed-free testing
2. Care must be taken to determine coupling of blade with fixture
3. Fixture must also be accurately modeled


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## Fixed-Free Test

- Cantilevered as in service
- Blade bolted to Fixture
- Fixture bolted to Frame




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## Fixed-Free Mode Shapes & Frequencies

Mode	Frequency (Hz)	Description
1	3.22	1 <sup>st</sup> Flap Bending
2	4.15	1 <sup>st</sup> Lag Bending
3	8.81	2 <sup>nd</sup> Flap Bending
4	16.8	2 <sup>nd</sup> Lag Bending
5	19.2	3 <sup>rd</sup> Flap Bending
6	30.8	4 <sup>th</sup> Flap Bending
7	37.2	3 <sup>rd</sup> Lag Bending
8	43.9	1 <sup>st</sup> Torsion



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## Fixed-Free: Nonlinear?

- Linearity assumption needed for simplicity, modal testing
- Change Impact Force and note change in FRF
- Negligible Change in system response due to range of impact forces

250N (black) vs. 510N (red)

Plot: FRF Magnitude vs. Frequency

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## Fixed-Free: Nonlinear?

- Impact and Measure at Pt. 78 and 91 (Reciprocity)

Impacting at 91 (red)


Plot: FRF Magnitude vs. Frequency

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## Modal Tests Results


Test:	Mode Frequency (Hz)			
	1st Flap	2nd Flap	3rd Flap	4th Flap
Free-Free # 1 (Straps Only)	7.6	17.9	32.1	50.4
Free-Free #2 (Fixture + Strap)	3.3	8.7	17.6	30.7
Fixed-Free (bolted to fixture, frame)	3.2	8.8	19.2	30.8



Free #1



Free #2




Fixed


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
## SHM Investigation

- 9 MFC patches glued to high-pressure surface
  - 1 Large Actuation Patch
  - 8 Small Sensor Patches







#1:  
0.75m



#2:  
1.25m



#7:  
7.0m



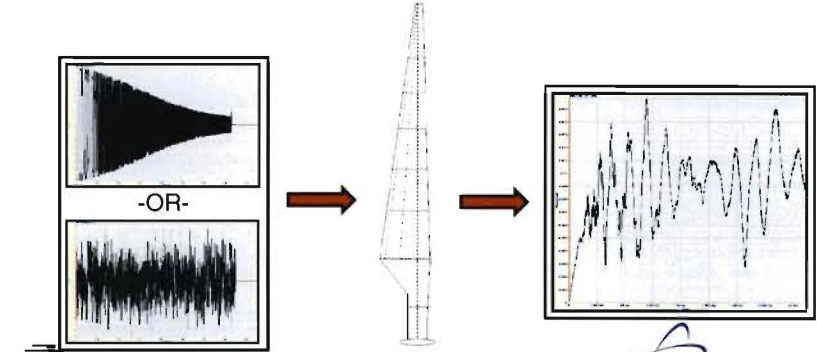
#8:  
8.5m

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## SHM Investigation

- Actuation MFC supplied with amplified sine chirp (154.8V peak) or burst random signal (179.8V peak) from 10Hz to 20kHz

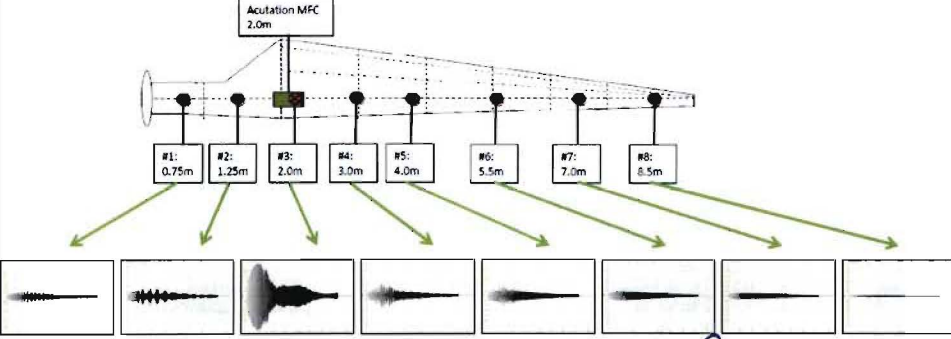


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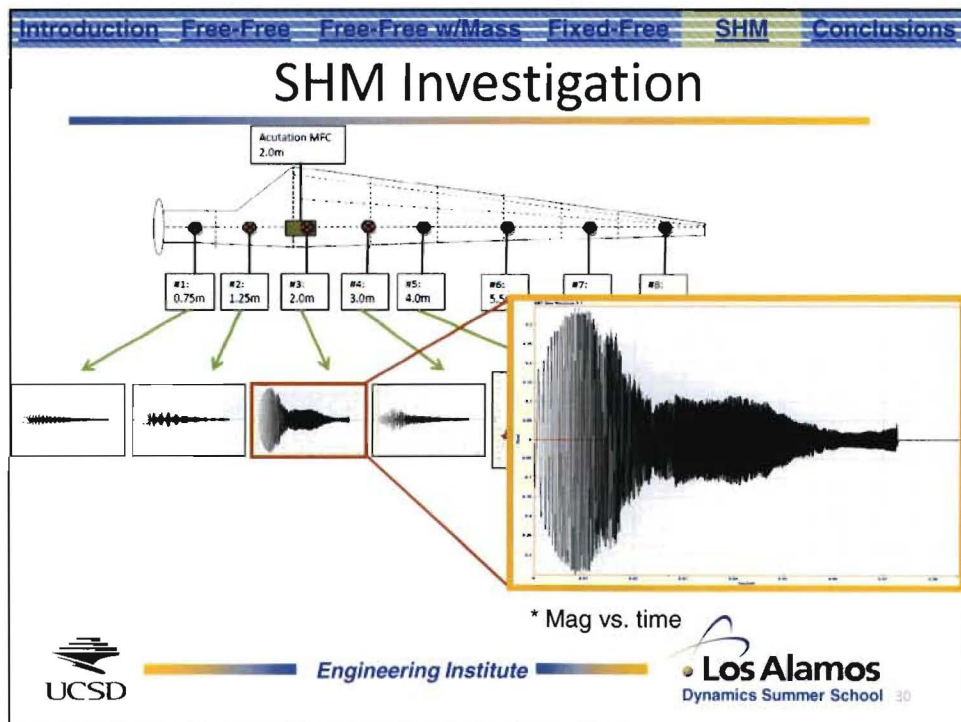
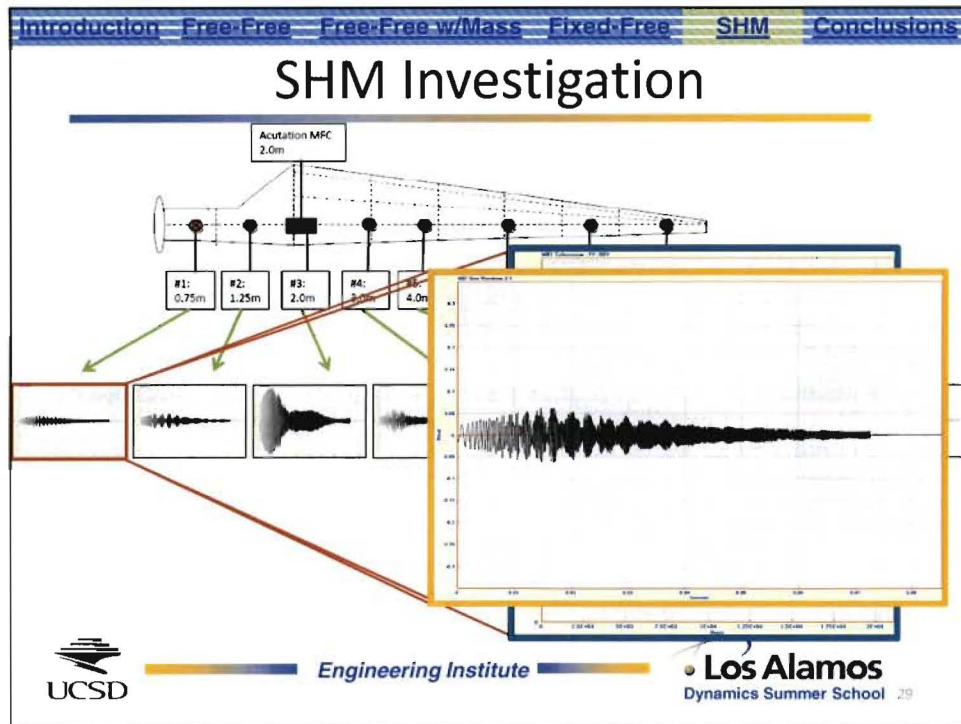
## SHM Investigation

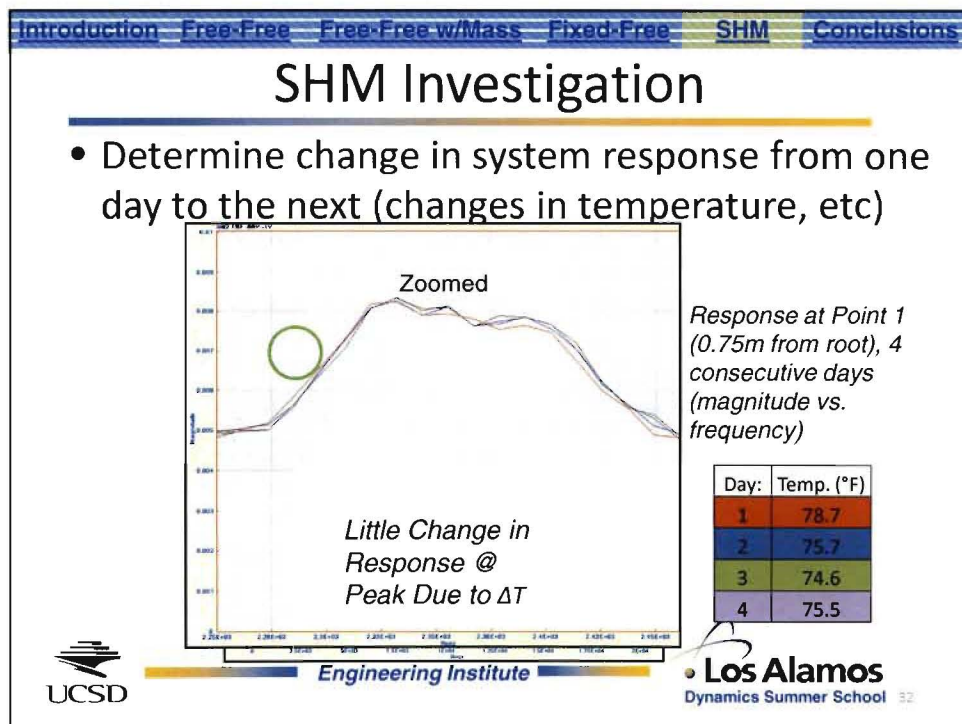
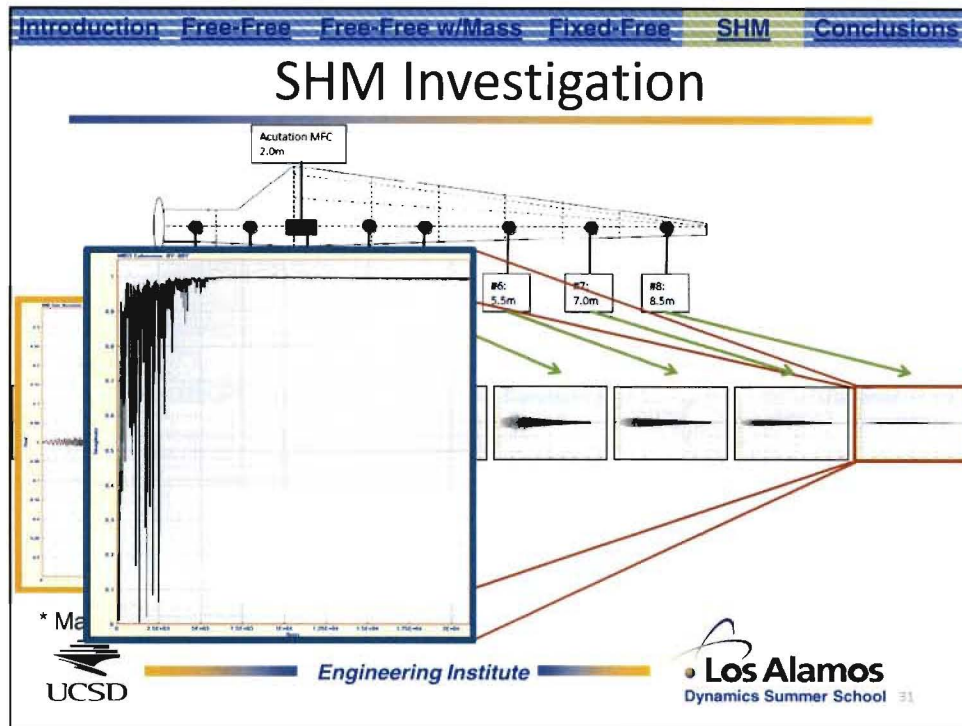
- Compare time response at various points
  - Amplitude of response maximum closest to actuation sensor



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## Conclusions

**Problem:**

*Wind Turbine Blade Predictive Reliability*



<http://wind-power-revolution.blogspot.com/2008/11/wind-turbine-failure-photos.html>

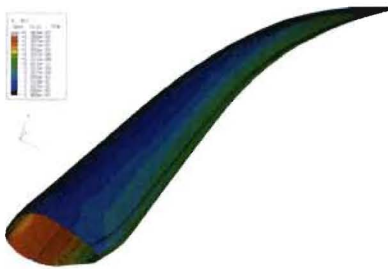

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## Conclusions

**Solution:**

*Validate Numerical Models and Design Effective SHM*

<http://www.nsecomposites.com/projects/wind-energy.html>


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## Conclusions

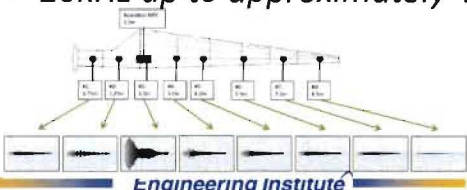
### Our Contribution:

- Determined mode shapes and frequencies of CX-100 blade in 3 different BC configurations to drive V&V



Free #1      Free #2      Fixed

- Determined that MFC patches may be used to excite 5kHz -> 20kHz up to approximately 4m from actuator

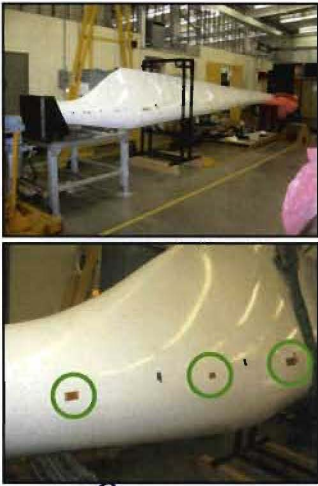


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## Future

- Modal Testing**
  - Integrate results of modal tests into numerical model of blade for V & V
  - Perform uncertainty quantification study
  - Better represent fixed-free condition with improved fixture
- Structural Health Monitoring**
  - Simulate damage on blade and detect with MFC sensor patches
  - Relocate actuator/sensors and monitor for optimal signal transfer



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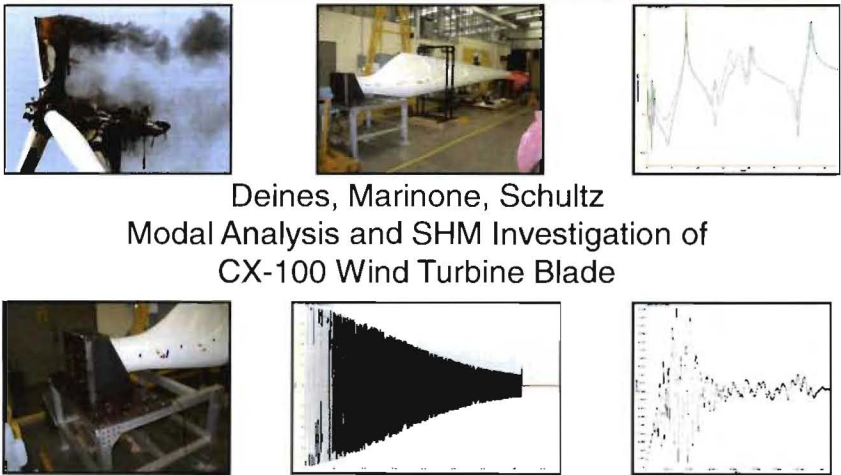
## Acknowledgments

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  - Dr. Charles Farrar
- Vibrant Technology Inc. (ME'scope Software)
- Abaqus, Inc. (ABAQUS Finite Element Software)
- Dr. Peter Avitabile (University of Massachusetts Lowell)

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## Questions?



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