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Modeling Compressed Turbulence

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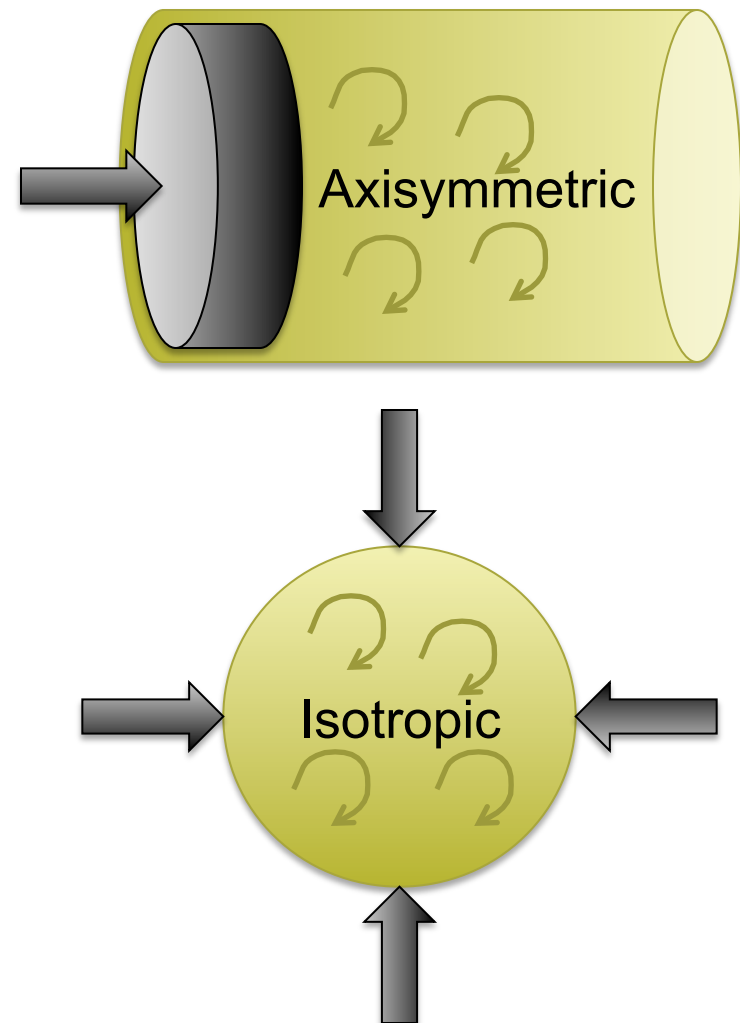
Slide 1

Motivation

- From ICE to ICF, the effect of mean compression or expansion is important for predicting the state of the turbulence.
- When developing combustion models, we would like to know the mix state of the reacting species.
- This involves density and concentration fluctuations.
- To date, research has focused on the effect of compression on the turbulent kinetic energy.
- The current work provides constraints to help development and calibration for models of species mixing effects in compressed turbulence.

Overview

- Consider a homogeneous anisotropic turbulent field subject to uniform mean compression.
- The flow can be decomposed into a mean flow and turbulent fluctuations.
 - The mean flow must be treated compressibly.
 - The turbulent fluctuations may be amenable to simpler models.
- For example, the DNS of Wu, et al. (1985), assumes the turbulent density fluctuations could be neglected.



Approach

- **Cambon, et al. (1992) demonstrate (based on an observation of Frisch) that a simple rescaling relates homogeneous isotropic compressed turbulence and decaying turbulence.**
- **Their analysis assumes**
 - density fluctuations are not important
 - the fluctuations are homogeneous and isotropic
- **The current work extends this analysis to cases which**
 - include multiple species,
 - include density, concentration, and temperature fluctuations, and
 - are anisotropic.

Outline

- **Give an high-level overview of the rescaling procedure.**
 - Mathematical details are being prepared for publication.
- **Present the scaling results.**
- **Briefly describe the physical case described by the rescaling.**
- **Apply the rescaling to some example turbulence model equations to illustrate the method for model calibration and development.**
- **Show two applications of the theory for model development and calibrations.**
 - Constraints for BHR model constants
 - Modeling the “rapid” pressure-strain

Governing equations

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_i}{\partial x_i} = 0$$

$$\frac{\partial \rho u_i}{\partial t} + \frac{\partial \rho u_j u_i}{\partial x_j} = -\frac{\partial p}{\partial x_i} + \frac{\partial \sigma_{ij}}{\partial x_j} + \rho g_i$$

$$\frac{\partial \rho c}{\partial t} + \frac{\partial \rho u_j c}{\partial x_j} = \frac{\partial}{\partial x_j} \left[\rho D \frac{\partial c}{\partial x_j} \right]$$

$$\frac{\partial \rho c_v T}{\partial t} + \frac{\partial \rho c_v u_j T}{\partial x_j} = -p \frac{\partial u_i}{\partial x_i} + \sigma_{ij} \frac{\partial u_i}{\partial x_j} + \frac{\partial}{\partial x_j} \left[k \frac{\partial T}{\partial x_j} \right]$$

Decomposition

- Introduce an ensemble average,

$$f = \langle f \rangle + f'$$

- and a Favre (density-weighted) average

$$\langle \rho f \rangle = \langle \rho \rangle \tilde{f}$$

$$f = \tilde{f} + f''$$

- and decompose the Navier-Stokes equations using

$$\rho = \langle \rho \rangle + \rho' \quad u_i = \tilde{u}_i + u_i'' \quad p = \langle p \rangle + p'$$

$$c = \tilde{c} + c'' \quad T = \tilde{T} + T''$$

Averaged equations

- Assuming spatially homogeneous turbulence, the mean equation are:

$$\frac{1}{\langle \rho \rangle} \frac{\partial \langle \rho \rangle}{\partial t} + S_{ii} = 0$$

$$(\dot{S}_{ij} + S_{ik} S_{kj}) x_j = - \frac{1}{\langle \rho \rangle} \frac{\partial \langle p \rangle}{\partial x_i} + g_i$$

$$\dot{C}_i + C_j S_{ji} = 0$$

$$(\dot{A}_i + A_j S_{ji}) x_i = \frac{\langle \sigma_{ij} S_{ij} \rangle - \langle p S_{ii} \rangle}{\langle \rho \rangle c_v} - \dot{B}$$

$$\langle \rho \rangle \equiv \text{constant}$$

$$S_{ij}(t) = \frac{\partial \tilde{u}_i}{\partial x_j}$$

$$C_i(t) = \frac{\partial \tilde{c}}{\partial x_i}$$

$$\tilde{T} = A_i(t) x_i + B(t)$$

- Blaisdell, et al. (1991) give examples of meanflows that satisfy these constraints.
- The state equation will impose an additional constraint.
- Note that B is an unclosed quantity that would need to be solved for.

Re-scaling

- Introduce a coordinate transform to remove the mean compression:

$$x_i^* = J^{-1/3} x_i \quad \frac{dt^*}{dt} = J^{-2/3}$$

where

$$J^{-1} = \exp\left(-\int_0^t S_{ii}(t') dt'\right) = \frac{\langle \rho \rangle}{\langle \rho(t=0) \rangle}$$

and the following re-scaling:

$$\rho(\mathbf{x}, t) = J^{-1}(t) \rho^*(\mathbf{x}^*, t^*) \quad p(\mathbf{x}, t) = J^{-5/3}(t) p^*(\mathbf{x}^*, t^*) \quad T(\mathbf{x}, t) = J^{-2/3}(t) T^*(\mathbf{x}^*, t^*)$$

$$u_i(\mathbf{x}, t) = S_{ij}(t) x_j + J^{-1/3}(t) u_i^*(\mathbf{x}^*, t^*) \quad c(\mathbf{x}, t) = c^*(\mathbf{x}^*, t^*)$$

Invariance

- Applying the coordinate transform and re-scaling, the resulting equations are identical to those for homogeneous turbulence with no mean compression, with the following scalings

$$S_{ij}^* = J^{2/3} \left(S_{ij} - \frac{1}{3} S_{kk} \delta_{ij} \right)$$

$$g_i^* = J g_i$$

$$\nu^* = \nu \quad \alpha^* = \alpha \quad D^* = D$$

- Note the time-dependent body force.
- Note that kinematic viscosity is not rescaled, but the viscosity will change in time due to mean temperature change caused by the compression.

Realizability

- **Of course, pressure, temperature, and concentration gradients cannot extend infinitely,**
 - but this is no more non-physical than the assumption of an “infinite box.”
- **The pressure gradient must be balanced by the concentration and/or temperature gradient,**
 - or the scale-height must be large.
- **Either the Atwood number must be small, or, temperature fluctuations must be negligible.**
- **In what follows, the internal energy equation will not be used.**

Constraints for RANS

- **Homogeneous buoyancy driven turbulence subject to an isotropic compression corresponds to freely evolving buoyancy driven turbulence with a time depended body force.**
- **Since this re-scaling is an exact analytic result, any RANS model should preserve it.**
- **Following Cambon, et al., we can neglect the viscosity variation, since in general, RANS models do not account for time variations in viscosity.**
 - However, this indicates that the term $(1/\nu) dv/dt$, which is typically neglected in the derivation of the dissipation equation, must be included for compressed turbulence, as noted by many researchers (e.g. Coleman & Mansour)

Setting the BHR coefficients

- The two-equation version of the BHR model (Besnard, et al., 1992) for homogeneous buoyancy driven turbulence undergoing mean compression reduces to the following set of ODEs:

$$\frac{\partial k}{\partial t} = a_3 g - R_{ij} S_{ij} - \varepsilon$$

$$\frac{\partial \varepsilon}{\partial t} = -C_{\varepsilon 1} R_{ij} S_{ij} - C_{\varepsilon 2} \frac{\varepsilon^2}{k} + C_{\varepsilon 3} \varepsilon S_{kk} - C_{\varepsilon 4} \frac{\varepsilon}{k} a_3 g$$

$$\frac{\partial a_3}{\partial t} = b g - C_{a1} \frac{\varepsilon}{k} a_3 + (C_{a2} - 1) a_3 S_{33}$$

$$\frac{\partial b}{\partial t} = -C_{b2} \frac{\varepsilon}{k} b$$

Re-scaling the turbulence quantities

- Based on the exact re-scaling for the turbulent fluctuations, we can write the following re-scalings for the turbulence model quantities:

$$k(t) = \frac{1}{2} \langle u_i''(t) u_i''(t) \rangle = J^{-2/3} k^*(t^*)$$

$$\varepsilon(t) = \nu \left\langle \frac{\partial u_i''(t)}{\partial x_j} \frac{\partial u_j''(t)}{\partial x_i} \right\rangle = J^{-4/3} \varepsilon^*(t^*)$$

$$a_3(t) = -\langle u_3''(t) \rangle = J^{-1/3} a_3^*(t^*)$$

$$b(t) \approx \frac{\langle \rho'(t)^2 \rangle}{\langle \rho \rangle^2} = b^*(t^*)$$

- Inserting these into the BHR equations, and making use of $S_{ij} = (d/3)\delta_{ij}$ and $R_{ii} = 2k$ we find the following:

Re-scaled BHR equations (k and ε)

- Turbulent kinetic energy

$$\frac{\partial k^*}{\partial t^*} = a_3^* g - \varepsilon^*$$

- Dissipation Rate

$$\frac{\partial \varepsilon^*}{\partial t^*} = -C_{\varepsilon 2} \frac{\varepsilon^{*2}}{k^*} - C_{\varepsilon 4} \frac{\varepsilon^*}{k^*} a_3^* g + J^{2/3} \left(\frac{4}{3} - \frac{2}{3} C_{\varepsilon 1} - C_{\varepsilon 3} \right)$$

- So, to preserve the scaling we must require

$$C_{\varepsilon 3} = \frac{2}{3}(2 - C_{\varepsilon 1})$$

- This is consistent with the result found by Cambon, et al., for the simpler case, and assuming $C_{\varepsilon 1}=1$, following Reynolds.

Re-scaled BHR equations (a and b)

- Density-velocity correlation:

$$\frac{\partial a_3^*}{\partial t^*} = b^* g^* - C_{a1} \frac{\varepsilon^*}{k^*} a_3^* + J^{2/3} \frac{1}{3} (C_{a2} + 3) a_3^* d$$

- To preserve the scaling:

$$C_{a2} = -3$$

- Density self-correlation:

$$\frac{\partial b^*}{\partial t^*} = -C_{b2} \frac{\varepsilon^*}{k^*} b^*$$

- Does not impose further constraints

Modeling the “rapid” pressure-strain

- Applying the transform to the exact Reynolds-stress equation gives:

$$\langle \rho \rangle \frac{\partial R_{ij}}{\partial t} = \langle \rho \rangle (R_{ik} S_{jk} + R_{jk} S_{ik}) + \langle \rho \rangle (a_i g_j + a_j g_i) + p' \frac{\partial u'_i}{\partial x_j} - \sigma'_{kj} \frac{\partial u'_i}{\partial x_k}$$

$$J^{-7/3} \rho_0 \frac{\partial R_{ij}^*}{\partial t} - \frac{2}{3} J^{-5/3} \rho_0 R_{ij}^* S_{ll} = J^{-5/3} \rho_0 (R_{ik}^* S_{jk}^* + R_{jk}^* S_{ik}^*) + J^{-7/3} \rho_0 (a_i^* g_j^* + a_j^* g_i^*)$$

$$+ J^{-7/3} \overline{p^* \frac{\partial u_i^*}{\partial x_j^*}} - J^{-7/3} \overline{\sigma_{kj}^* \frac{\partial u_i^*}{\partial x_k^*}}$$

$$J^{-7/3} \rho_0 \frac{\partial R_{ij}^*}{\partial t} = J^{-7/3} \rho_0 (R_{ik}^* S_{jk}^* + R_{jk}^* S_{ik}^*) + J^{-7/3} \rho_0 (a_i^* g_j^* + a_j^* g_i^*)$$

$$+ J^{-7/3} \overline{p^* \frac{\partial u_i^*}{\partial x_j^*}} - J^{-7/3} \overline{\sigma_{kj}^* \frac{\partial u_i^*}{\partial x_k^*}}$$

- As expected, the exact equation is invariant.
- All terms scale with $J^{-7/3}$.

Tensor form of the “rapid” pressure-strain

- The pressure-strain is decomposed into a “slow” and “rapid” part.
- The standard incompressible model for the pressure strain assumes a linear tensor form: $(\Pi_R^r)_{ij} = A_{lj}^{ki} (R_{ij}) S_{kl}$
 - Assume A scale as $J^{-2/3}$ ($\sim R_{ij}$).
 - Applying the invariance property, this form is not invariant, because it will have a new term containing the mean compression rate.
- Instead, we should use the form:

$$\begin{aligned}(\Pi_R^r)_{ij} &= A_{lj}^{ki} \left(S_{kl} - \frac{1}{3} S_{nn} \delta_{kl} \right) \\&= J^{-2/3} A_{lj}^{*ki} \left(S_{kl} - \frac{1}{3} S_{nn} \delta_{kl} \right) \\&= J^{-4/3} A_{lj}^{*ki} S_{kl}^* \\&= J^{-4/3} A_{lj}^{*ki} \left(S_{kl}^* - \frac{1}{3} S_{nn}^* \delta_{kl} \right)\end{aligned}$$

Conclusions

- The Cambon, et al., re-scaling has been extended to buoyancy driven turbulence, including the fluctuating density, concentration, and temperature equations.
- The new scalings give us helpful constraints for developing and validating RANS turbulence models.

- For BHR,
$$C_{\varepsilon 3} = \frac{2}{3}(2 - C_{\varepsilon 1})$$

$$C_{a2} = -3$$

- For “rapid” pressure-strain
$$\left(\Pi_R^r\right)_{ij} = A_{lj}^{ki} \left(S_{kl} - \frac{1}{3} S_{nn} \delta_{kl} \right)$$

- **Future work**

- Further investigation into constraints on tensor forms
- Examining time dependent viscosity effects
- Application to other models (e.g. Grégoire, et al., 2005)

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