

LA-UR-12-22852

Approved for public release; distribution is unlimited.

Title: Modeling Compressed Turbulence

Author(s): Israel, Daniel M.

Intended for: 12th International Workshop on the Physics of Compressible Turbulent Mixing, 2012-07-16 (Woburn, ---, United Kingdom)



Disclaimer:

Los Alamos National Laboratory, an affirmative action/equal opportunity employer, is operated by the Los Alamos National Security, LLC for the National Nuclear Security Administration of the U.S. Department of Energy under contract DE-AC52-06NA25396. By approving this article, the publisher recognizes that the U.S. Government retains nonexclusive, royalty-free license to publish or reproduce the published form of this contribution, or to allow others to do so, for U.S. Government purposes.

Los Alamos National Laboratory requests that the publisher identify this article as work performed under the auspices of the U.S. Department of Energy. Los Alamos National Laboratory strongly supports academic freedom and a researcher's right to publish; as an institution, however, the Laboratory does not endorse the viewpoint of a publication or guarantee its technical correctness.

# Modeling Compressed Turbulence

**Daniel M. Israel**  
**Los Alamos National Laboratory**  
**LA-UR 12-22852**

**13<sup>th</sup> International Workshop on the Physics of  
Compressible Turbulent Mixing**

**July 17, 2012**  
**Woburn, UK**

UNCLASSIFIED



Operated by Los Alamos National Security, LLC for the U.S. Department of Energy's NNSA

Slide 1



# Motivation

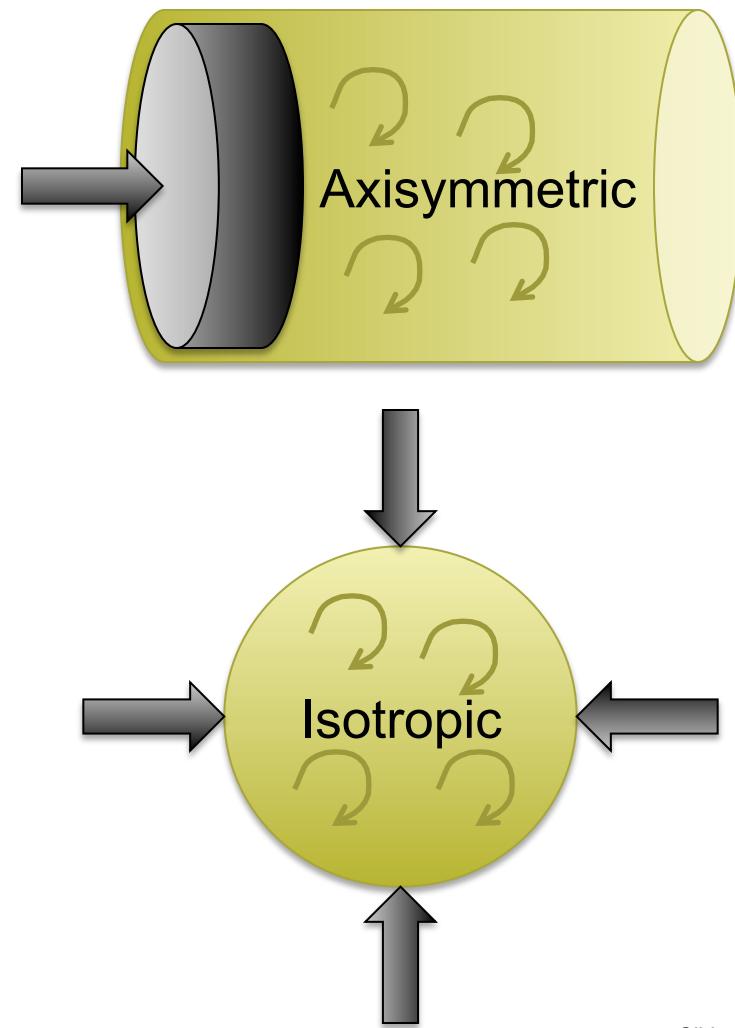
---

- From ICE to ICF, the effect of mean compression or expansion is important for predicting the state of the turbulence.
- When developing combustion models, we would like to know the mix state of the reacting species.
- This involves density and concentration fluctuations.
- To date, research has focused on the effect of compression on the turbulent kinetic energy.
- The current work provides constraints to help development and calibration for models of species mixing effects in compressed turbulence.

# Overview

---

- Consider a homogeneous anisotropic turbulent field subject to uniform mean compression.
- The flow can be decomposed into a mean flow and turbulent fluctuations.
  - The mean flow must be treated compressibly.
  - The turbulent fluctuations may be amenable to simpler models.
- For example, the DNS of Wu, et al. (1985), assumes the turbulent density fluctuations could be neglected.



# Approach

---

- Cambon, et al. (1992) demonstrate (based on an observation of Frisch) that a simple rescaling relates homogeneous isotropic compressed turbulence and decaying turbulence.
- Their analysis assumes
  - density fluctuations are not important
  - the fluctuations are homogeneous and isotropic
- The current work extends this analysis to cases which
  - include multiple species,
  - include density, concentration, and temperature fluctuations, and
  - are anisotropic.

# Outline

---

- **Give an high-level overview of the rescaling procedure.**
  - Mathematical details are being prepared for publication.
- **Present the scaling results.**
- **Briefly describe the physical case described by the rescaling.**
- **Apply the rescaling to some example turbulence model equations to illustrate the method for model calibration and development.**
- **Show two applications of the theory for model development and calibrations.**
  - Constraints for BHR model constants
  - Modeling the “rapid” pressure-strain

## Governing equations

---

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_i}{\partial x_i} = 0$$

$$\frac{\partial \rho u_i}{\partial t} + \frac{\partial \rho u_j u_i}{\partial x_j} = -\frac{\partial p}{\partial x_i} + \frac{\partial \sigma_{ij}}{\partial x_j} + \rho g_i$$

$$\frac{\partial \rho c}{\partial t} + \frac{\partial \rho u_j c}{\partial x_j} = \frac{\partial}{\partial x_j} \left[ \rho D \frac{\partial c}{\partial x_j} \right]$$

$$\frac{\partial \rho c_v T}{\partial t} + \frac{\partial \rho c_v u_j T}{\partial x_j} = -p \frac{\partial u_i}{\partial x_i} + \sigma_{ij} \frac{\partial u_i}{\partial x_j} + \frac{\partial}{\partial x_j} \left[ k \frac{\partial T}{\partial x_j} \right]$$

# Decomposition

---

- Introduce an ensemble average,

$$f = \langle f \rangle + f'$$

- and a Favre (density-weighted) average

$$\langle \rho f \rangle = \langle \rho \rangle \tilde{f}$$

$$f = \tilde{f} + f''$$

- and decompose the Navier-Stokes equations using

$$\rho = \langle \rho \rangle + \rho' \quad u_i = \tilde{u}_i + u_i'' \quad p = \langle p \rangle + p'$$

$$c = \tilde{c} + c'' \quad T = \tilde{T} + T''$$

## Averaged equations

- Assuming spatially homogeneous turbulence, the mean equation are:

$$\frac{1}{\langle \rho \rangle} \frac{\partial \langle \rho \rangle}{\partial t} + S_{ii} = 0$$

$$(\dot{S}_{ij} + S_{ik}S_{kj})x_j = -\frac{1}{\langle \rho \rangle} \frac{\partial \langle p \rangle}{\partial x_i} + g_i$$

$$\dot{C}_i + C_j S_{ji} = 0$$

$$(\dot{A}_i + A_j S_{ji})x_i = \frac{\langle \sigma_{ij} S_{ij} \rangle - \langle p S_{ii} \rangle}{\langle \rho \rangle c_v} - \dot{B}$$

$$\langle \rho \rangle \equiv \text{constant}$$

$$S_{ij}(t) = \frac{\partial \tilde{u}_i}{\partial x_j}$$

$$C_i(t) = \frac{\partial \tilde{c}}{\partial x_i}$$

$$\tilde{T} = A_i(t)x_i + B(t)$$

- Blaisdell, et al. (1991) give examples of meanflows that satisfy these constraints.
- The state equation will impose an additional constraint.
- Note that  $B$  is an unclosed quantity that would need to be solved for.

## Re-scaling

---

- Introduce a coordinate transform to remove the mean compression:

$$x_i^* = J^{-1/3} x_i \quad \frac{dt^*}{dt} = J^{-2/3}$$

where

$$J^{-1} = \exp\left(-\int_0^t S_{ii}(t') dt'\right) = \frac{\langle \rho \rangle}{\langle \rho(t=0) \rangle}$$

and the following re-scaling:

$$\rho(\mathbf{x}, t) = J^{-1}(t) \rho^*(\mathbf{x}^*, t^*) \quad p(\mathbf{x}, t) = J^{-5/3}(t) p^*(\mathbf{x}^*, t^*) \quad T(\mathbf{x}, t) = J^{-2/3}(t) T^*(\mathbf{x}^*, t^*)$$

$$u_i(\mathbf{x}, t) = S_{ij}(t) x_j + J^{-1/3}(t) u_i^*(\mathbf{x}^*, t^*) \quad c(\mathbf{x}, t) = c^*(\mathbf{x}^*, t^*)$$

## Invariance

---

- Applying the coordinate transform and re-scaling, the resulting equations are identical to those for homogeneous turbulence with no mean compression, with the following scalings

$$S_{ij}^* = J^{2/3} \left( S_{ij} - \frac{1}{3} S_{kk} \delta_{ij} \right)$$

$$g_i^* = J g_i$$

$$\nu^* = \nu \quad \alpha^* = \alpha \quad D^* = D$$

- Note the time-dependent body force.
- Note that kinematic viscosity is not rescaled, but the viscosity will change in time due to mean temperature change caused by the compression.

# Realizability

---

- **Of course, pressure, temperature, and concentration gradients cannot extend infinitely,**
  - but this is no more non-physical than the assumption of an “infinite box.”
- **The pressure gradient must be balanced by the concentration and/or temperature gradient,**
  - or the scale-height must be large.
- **Either the Atwood number must be small, or, temperature fluctuations must be negligible.**
- **In what follows, the internal energy equation will not be used.**

# Constraints for RANS

---

- Homogeneous buoyancy driven turbulence subject to an isotropic compression corresponds to freely evolving buoyancy driven turbulence with a time depended body force.
- Since this re-scaling is an exact analytic result, any RANS model should preserve it.
- Following Cambon, et al., we can neglect the viscosity variation, since in general, RANS models do not account for time variations in viscosity.
  - However, this indicates that the term  $(1/\nu) dv/dt$ , which is typically neglected in the derivation of the dissipation equation, must be included for compressed turbulence, as noted by many researchers (e.g. Coleman & Mansour)

## Setting the BHR coefficients

---

- The two-equation version of the BHR model (Besnard, et al., 1992) for homogeneous buoyancy driven turbulence undergoing mean compression reduces to the following set of ODEs:

$$\frac{\partial k}{\partial t} = a_3 g - R_{ij} S_{ij} - \varepsilon$$

$$\frac{\partial \varepsilon}{\partial t} = -C_{\varepsilon 1} R_{ij} S_{ij} - C_{\varepsilon 2} \frac{\varepsilon^2}{k} + C_{\varepsilon 3} \varepsilon S_{kk} - C_{\varepsilon 4} \frac{\varepsilon}{k} a_3 g$$

$$\frac{\partial a_3}{\partial t} = b g - C_{a1} \frac{\varepsilon}{k} a_3 + (C_{a2} - 1) a_3 S_{33}$$

$$\frac{\partial b}{\partial t} = -C_{b2} \frac{\varepsilon}{k} b$$

## Re-scaling the turbulence quantities

---

- Based on the exact re-scaling for the turbulent fluctuations, we can write the following re-scalings for the turbulence model quantities:

$$k(t) = \frac{1}{2} \langle u_i''(t) u_i''(t) \rangle = J^{-2/3} k^*(t^*)$$

$$\varepsilon(t) = \nu \left\langle \frac{\partial u_i''(t)}{\partial x_j} \frac{\partial u_j''(t)}{\partial x_i} \right\rangle = J^{-4/3} \varepsilon^*(t^*)$$

$$a_3(t) = -\langle u_3''(t) \rangle = J^{-1/3} a_3^*(t^*)$$

$$b(t) \approx \frac{\langle \rho'(t)^2 \rangle}{\langle \rho \rangle^2} = b^*(t^*)$$

- Inserting these into the BHR equations, and making use of  $S_{ij} = (d/3) \delta_{ij}$  and  $R_{ii} = 2k$  we find the following:

## Re-scaled BHR equations ( $k$ and $\varepsilon$ )

---

- Turbulent kinetic energy

$$\frac{\partial k^*}{\partial t^*} = a_3^* g - \varepsilon^*$$

- Dissipation Rate

$$\frac{\partial \varepsilon^*}{\partial t^*} = -C_{\varepsilon 2} \frac{\varepsilon^{*2}}{k^*} - C_{\varepsilon 4} \frac{\varepsilon^*}{k^*} a_3^* g^* + J^{2/3} \left( \frac{4}{3} - \frac{2}{3} C_{\varepsilon 1} - C_{\varepsilon 3} \right)$$

- So, to preserve the scaling we must require

$$C_{\varepsilon 3} = \frac{2}{3} (2 - C_{\varepsilon 1})$$

- This is consistent with the result found by Cambon, et al., for the simpler case, and assuming  $C_{\varepsilon 1}=1$ , following Reynolds.

## Re-scaled BHR equations ( $a$ and $b$ )

---

- Density-velocity correlation:

$$\frac{\partial a_3^*}{\partial t^*} = b^* g^* - C_{a1} \frac{\varepsilon^*}{k^*} a_3^* + J^{2/3} \frac{1}{3} (C_{a2} + 3) a_3^* d$$

- To preserve the scaling:

$$C_{a2} = -3$$

- Density self-correlation:

$$\frac{\partial b^*}{\partial t^*} = -C_{b2} \frac{\varepsilon^*}{k^*} b^*$$

- Does not impose further constraints

## Modeling the “rapid” pressure-strain

- Applying the transform to the exact Reynolds-stress equation gives:

$$\langle \rho \rangle \frac{\partial R_{ij}}{\partial t} = \langle \rho \rangle (R_{ik}S_{jk} + R_{jk}S_{ik}) + \langle \rho \rangle (a_i g_j + a_j g_i) + p' \frac{\partial u'_i}{\partial x_j} - \sigma'_{kj} \frac{\partial u'_i}{\partial x_k}$$

$$J^{-7/3} \rho_0 \frac{\partial R_{ij}^*}{\partial t} - \frac{2}{3} J^{-5/3} \rho_0 R_{ij}^* S_{ll} = J^{-5/3} \rho_0 (R_{ik}^* S_{jk} + R_{jk}^* S_{ik}) + J^{-7/3} \rho_0 (a_i^* g_j^* + a_j^* g_i^*)$$

$$+ J^{-7/3} p^* \frac{\partial u_i^*}{\partial x_j} - J^{-7/3} \sigma_{kj}^* \frac{\partial u_i^*}{\partial x_k}$$

$$J^{-7/3} \rho_0 \frac{\partial R_{ij}^*}{\partial t} = J^{-7/3} \rho_0 (R_{ik}^* S_{jk}^* + R_{jk}^* S_{ik}^*) + J^{-7/3} \rho_0 (a_i^* g_j^* + a_j^* g_i^*)$$

$$+ J^{-7/3} p^* \frac{\partial u_i^*}{\partial x_j} - J^{-7/3} \sigma_{kj}^* \frac{\partial u_i^*}{\partial x_k}$$

- As expected, the exact equation is invariant.
- All terms scale with  $J^{-7/3}$ .

## Tensor form of the “rapid” pressure-strain

---

- The pressure-strain is decomposed into a “slow” and “rapid” part.
- The standard incompressible model for the pressure strain assumes a linear tensor form:  $(\Pi_R^r)_{ij} = A_{lj}^{ki} (R_{ij}) S_{kl}$ 
  - Assume  $A$  scale as  $J^{-2/3}$  ( $\sim R_{ij}$ ).
  - Applying the invariance property, this form is not invariant, because it will have a new term containing the mean compression rate.
- Instead, we should use the form:

$$\begin{aligned} (\Pi_R^r)_{ij} &= A_{lj}^{ki} \left( S_{kl} - \frac{1}{3} S_{nn} \delta_{kl} \right) \\ &= J^{-2/3} A_{lj}^{*ki} \left( S_{kl} - \frac{1}{3} S_{nn} \delta_{kl} \right) \\ &= J^{-4/3} A_{lj}^{*ki} S_{kl}^* \\ &= J^{-4/3} A_{lj}^{*ki} \left( S_{kl}^* - \frac{1}{3} S_{nn}^* \delta_{kl} \right) \end{aligned}$$

# Conclusions

---

- The Cambon, et al., re-scaling has been extended to buoyancy driven turbulence, including the fluctuating density, concentration, and temperature equations.
- The new scalings give us helpful constraints for developing and validating RANS turbulence models.
  - For BHR,
$$C_{\varepsilon 3} = \frac{2}{3}(2 - C_{\varepsilon 1})$$
$$C_{a2} = -3$$
  - For “rapid” pressure-strain
$$(\Pi_R^r)_{ij} = A_{lj}^{ki} \left( S_{kl} - \frac{1}{3} S_{nn} \delta_{kl} \right)$$
- Future work
  - Further investigation into constraints on tensor forms
  - Examining time dependent viscosity effects
  - Application to other models (e.g. Grégoire, et al., 2005)

## Acknowledgements

---

- Rob Gore for his support and discussions.
- Ray Ristorcelli for his encouragement and helpful feedback.