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Abstract

We compare a staggered Lagrangian formulation with a cell-centered Lagrangian formulation for a two-material compressible flow. In both formulation, we assume a single velocity field and rely on pressure relaxation techniques to close the system of equations. We employ Tipton's mixture model for both formulation. However, for the cell-centered formulation, employing Tipton's model for the mixture cell results in loss of conservation of total energy. We propose a numerical algorithm to correct this energy discrepancy. We test both algorithms on the two-materials Sod shock tube test problem and compare the results with the analytical solution.

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Lagrangian Hydrodynamics Equations

$$\begin{aligned} \rho \frac{D}{Dt} \left(\frac{1}{\rho} \right) - \frac{\partial u}{\partial x} &= 0 & \text{+ Perfect gas equation of state} \\ \rho \frac{Du}{Dt} + \frac{\partial p}{\partial x} &= 0 & p = \rho e(\gamma - 1) \\ \rho \frac{DE}{Dt} + \frac{\partial}{\partial x} (\rho u) &= 0 \end{aligned}$$

$$\begin{aligned} \text{Density } \rho & \\ \text{Velocity } u & \\ \text{Pressure } p & \\ \text{Total energy } E &= e + \frac{1}{2} u^2 \\ \text{Specific internal energy } e & \end{aligned}$$

Staggered Lagrangian Formulation with Tipton's Closure Model

- Velocity at nodes and pressure at cell-centers
- Standard predictor-corrector time integration scheme (Shashkov, 2008)
 - Half-time step: Node position, cell volume, densities, pressure (adiabatic approximation)
 - Final update: velocity, node position, cell volume, densities, specific internal energies, pressure
 - Pressure augmented by artificial viscosity (von Neumann and Richtmyer)
- Each material has its own mass, material interface may not coincide with mesh faces (mixed cells)
- Tipton's model for pressure relaxation after half-time step

$$\delta V^{n+1/2} = \sum_k \delta V_k^{n+1/2} \quad p_k^{n+1/2} = p_k^n \left(1 + \frac{L}{c_k \delta t} \right) \left(\frac{\delta V_k^{n+1/2}}{V_k^n} \right) = p_k^{n+1/2}$$
- Consistent internal energies with total energy conservation

$$\begin{aligned} \text{Speed of sound } & c \\ \text{Length (cell-length) } & L \\ \text{Volume } & V \\ \text{Material indice } & k \end{aligned}$$

Cell-centered Lagrangian Formulation with Tipton's Closure Model

- Velocity and pressure at cell-centers
- 2nd order Godunov method with acoustic Riemann solver
- Predictor-corrector time integration scheme (Maire and Shashkov, 2008)
 - Half-time step: mass, momentum, energy update with Riemann states u^* and p^* from time n data
 - Final update: mass, momentum, energy update with Riemann states u^* and p^* from time $n+1/2$ data
- Each material has its own mass, material interface may not coincide with mesh faces (mixed cells)
- Tipton's model for pressure relaxation after predictor and corrector steps

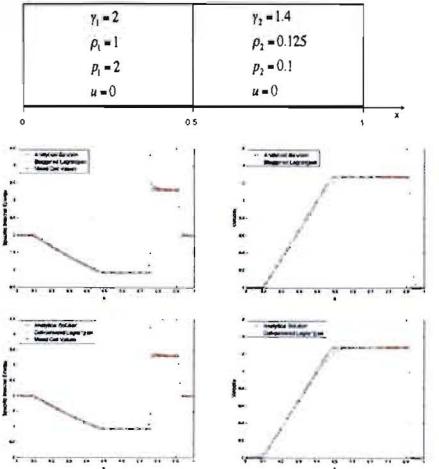
$$p = \sum_k f_k p_k$$
- Conservation of total energy by redistributing discrepancy in total internal energies to either material internal energies based on the sign of the discrepancy

References

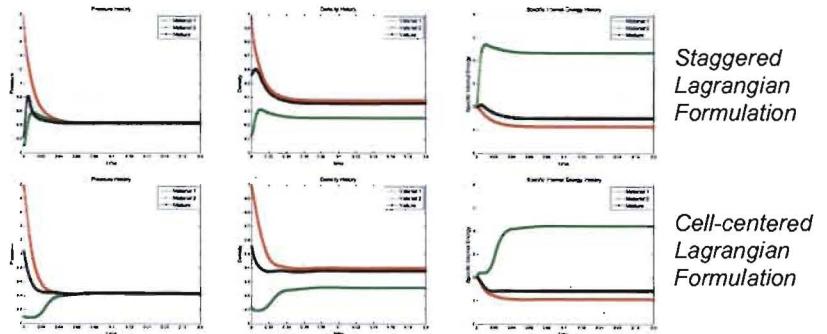
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Two-material Sod Shock Tube

- perfect gas with different gammas
- one-dimensional, 100 cells
- mixed cell volume fractions $f_1=0.5, f_2=0.5$
- results at final time $t=0.2$



Time-history plots in the mixed cell with Tipton's mixture model



Observations and Future Work

- Differences are noticeable in the specific internal energy plots and in the time history plots.
- The transient mixed pressure is always within the two material pressures for the cell-centered Lagrangian formulation, which is not the case for the staggered Lagrangian formulation.
- Other correction algorithms to ensure conservation of total energy could be designed and give other time-history behavior.

Acknowledgments

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