

LA-UR-10-06341

Approved for public release;  
distribution is unlimited.

*Title:* Modeling Solid Rayleigh-Taylor Growth

*Author(s):* Ann M. Kaul, XCP-5

*Intended for:* 8th International Conference on New Models and Hydrocodes  
for Shock Wave Processes in Condensed Matter proceedings  
Paris, France  
May 24 - 28, 2010



Los Alamos National Laboratory, an affirmative action/equal opportunity employer, is operated by the Los Alamos National Security, LLC for the National Nuclear Security Administration of the U.S. Department of Energy under contract DE-AC52-06NA25396. By acceptance of this article, the publisher recognizes that the U.S. Government retains a nonexclusive, royalty-free license to publish or reproduce the published form of this contribution, or to allow others to do so, for U.S. Government purposes. Los Alamos National Laboratory requests that the publisher identify this article as work performed under the auspices of the U.S. Department of Energy. Los Alamos National Laboratory strongly supports academic freedom and a researcher's right to publish; as an institution, however, the Laboratory does not endorse the viewpoint of a publication or guarantee its technical correctness.

# Modeling solid Rayleigh-Taylor growth

A. Kaul<sup>1</sup>

<sup>1</sup>Los Alamos National Laboratory, XCP-5, P.O. Box 1663 – MS F663, Los Alamos, NM, USA

**Abstract.** Intense impulses applied to solid materials result in high strain rates, strong plastic strains and significant temperature increments. Data in such regimes would allow confidence in extending material strength models to strain rates of  $10^6 - 10^7 \text{ s}^{-1}$ . High explosives can be used to accelerate a plate with a perturbation on the side facing the HE, resulting in a Rayleigh-Taylor-like perturbation growth that depends on amplitude and wavelength of the initial surface perturbation, strength of the material, time dependence of the driving pressure force, and temperature of the material. Such experiments have been conducted on perturbed copper plates at LANL, using the LANSCE proton radiography beam to obtain multiple frames of data for each experiment. The results of numerical simulations of these experiments using a 2-D ALE code are presented.

## 1 The experiment

In its most basic form, the experiment consists of a planar high explosive (HE) lens and a copper (or other material) plate. Sinusoidal perturbations of a given wavelength and amplitude are machined into the “front” side of the plate (see figure 1), which faces the HE lens. A gap exists between the HE and the plate, allowing the expanding HE products to fill the gap and provide a shockless driving force on the plate. In addition, the edge of the plate is beveled to allow the plate to remain flat as the HE products expand around the outer edge of the plate. A typical wavelength for the perturbation is 2 mm; a typical peak-to-peak amplitude of the perturbation is 0.07 – 0.11 mm; a typical gap is 2 – 3 mm. The perturbations undergo a Rayleigh-Taylor-like growth that depends on amplitude and wavelength of the initial surface perturbation, thickness of the plate, strength of the material, time dependence of the driving pressure force, and temperature of the material.

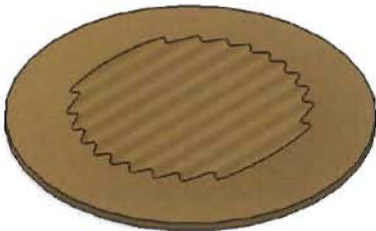


Fig. 1. The sinusoidally perturbed plate.

The LANSCE proton radiography beam is used to obtain multiple frames of data for each experiment. One such frame is shown in figure 2. The edge of the perturbation is then extracted from the radiograph and the data is typically presented as peak-to-peak amplitude as a function of either time or distance of plate movement. In addition, photon Doppler velocimetry (PDV) is used to provide a record of the velocity of the “back”, initially unperturbed side of the plate.

These experiments follow in the footsteps of Barnes at LANL[1] and Raevsky at VNIIEF[2].



Fig. 2. Proton radiography image of dynamic plate.

## 2 Full simulation

The largest issue for 2-D simulations of this experiment is the lack of a consistent 2-D symmetry. While the HE lens is obviously axisymmetric, the plate is a combination of an initially axisymmetric plate with a superimposed Cartesian perturbation. The best way to model the sinusoidal perturbations is to use a Cartesian description

of the plate, using a mesh as shown in figure 3. Only one side of the plate is modeled, with a reflective boundary at the plate center.



Fig. 3. Typical Lagrangian mesh for perturbed plate.

Use of a Cartesian geometry for the plate negates the use of an axisymmetric model for the HE lens. Thus, the HE lens is modeled by a planar equivalent of slabs of HE, ignited by a planar wave. The slabs match the center line of the lens in thickness.

Figure 4 shows a “full” simulation of the problem. The high explosives are shown in blue and yellow, the copper plate is shown in red, and the plastic enclosure is shown in green. The mesh size in this simulation is 0.25 mm. The initial setup is shown on the left and the final experimental time on the right. A closer look at the final time, as shown in figure 5, leads to the discovery that the waves reflected from the plastic do not propagate back to the plate, only part way through the gap between the plastic and the plate. Additionally the plate edge effects do not propagate to the center 3 – 4 wavelengths of the plate. Thus, several simplifications of the model can be attempted. One extremely useful simplification is to replace the plastic with a reflective outer boundary. The result can be seen in figure 6, with the reflective boundary on the left and the original model on the right. There is almost no impact on the final shape of the simulated plate from this change.

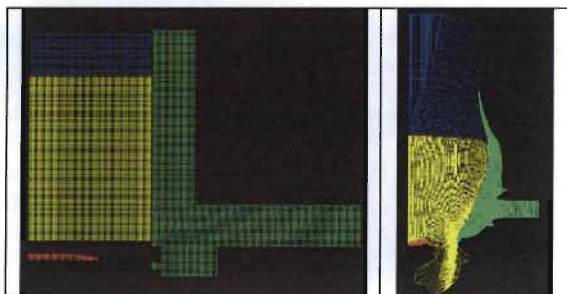


Fig. 4. “Full” simulation, initial time on left, final time on right.

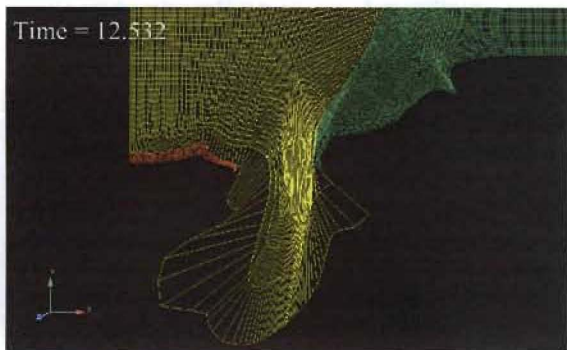


Fig. 5. Enlargement of simulated final time.

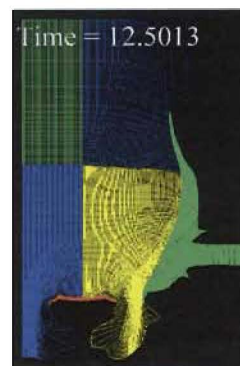


Fig. 6. Plastic enclosure on right replaced with reflective boundary on left.

### 3 Mesh Refinement

The mesh shown in the previous figures is extremely coarse, with only six cells across the plate thickness. As might be expected, the resulting simulations smear out the anticipated localizations of material properties and predict virtually no growth in perturbation amplitude. Mesh refinement is required to make more accurate predictions in this situation, so a simpler model with fewer cells needing fewer processors and shorter run times is needed.

Using the previously mentioned observation that the plate edge effects did not propagate into the center section of the plate, the chosen simpler model consists of only the center section of the plate, with reflective boundaries placed on both sides of four wavelengths of the plate. The final time for three simulations with mesh sizes of 0.1, 0.05 and 0.025 mm, respectively, are shown in figures 7 – 9. The plate is shown in either yellow or red, while the HE products are shown in either aqua or blue. It can be seen that with increasing mesh refinement, the expected bubbles on the spikes begin to appear.

The change in shape appears to be due to the increasing localization of plastic strain possible with a finer mesh. The final plastic strain calculated for the 0.025 mm mesh is seen in figure 10. The maximum plastic strain in this simulation is over 700 percent, while the maximum plastic strain in the 0.1 mm mesh is approximately 240 percent.

The simulated plate velocity as a function of time is plotted against the data in figure 11, showing that all three simulations agree reasonably well with the measured velocity of the plate. Level 1 designates the 0.1 mm mesh, level 2 designates the 0.05 mm mesh and level 3 designates the 0.025 mm mesh. The average peak-to-peak perturbation amplitudes as a function of time are plotted in figure 12, showing that standard Preston-Tonks-Wallace (PTW) [3] strength parameters for this copper adequately capture the rate of perturbation growth for all three cell sizes. It could be argued that one needs to use the 0.025 mm size to adequately capture the shape of the perturbation growth.

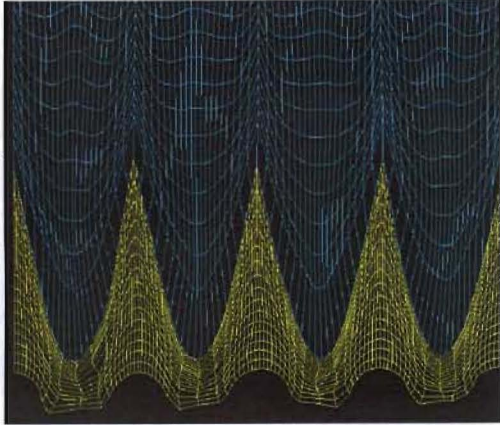


Fig. 7. Final simulation time for 0.1 mm mesh.

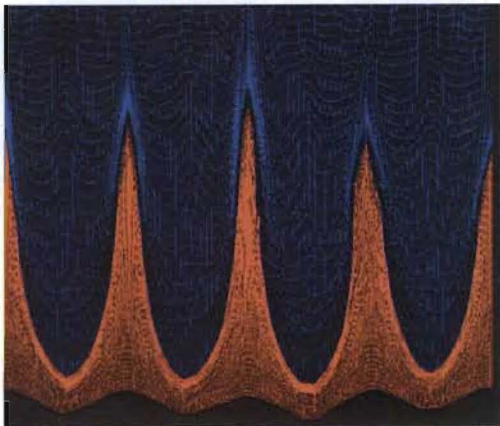


Fig. 8. Final simulation time for 0.05 mm mesh.

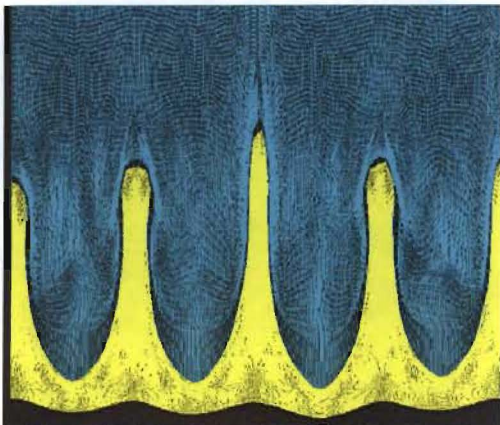


Fig. 9. Final simulation time for 0.025 mm mesh.

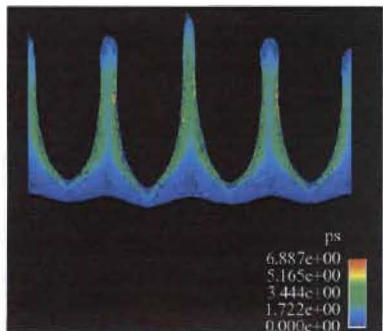


Fig. 10. Final plastic strain in 0.025 mm mesh.

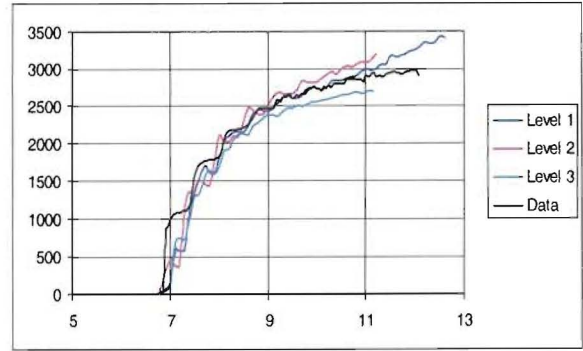


Fig. 11. Plate velocity as a function of time, simulated vs. data.

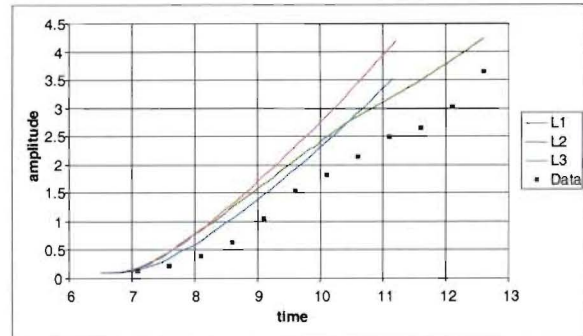


Fig. 12. Peak-to-peak perturbation amplitude as a function of time, simulated vs. data.

#### 4 Gaussian Plate

In order to address the lack of symmetries in the previous experiment, a different plate shape has been attempted. This plate has a single Gaussian point in the center of the side facing the HE lens, as shown in figure 13. There is no bevel on the edge of the plate. The same lens is used as in the previous experiment. Again, a gap exists between the HE and the plate so that the HE products provide a shockless loading to the plate.

This experiment was modeled using a reflective boundary to replace the plastic on the outside of the experimental setup, which still allows the HE products to expand into the gap between the plate and the plastic. The result can be seen in figure 14. Since the edge of the plate was not beveled, it moved into the radiographic line of sight, obscuring the growth of the center perturbation. The expansion of the HE products into the gap between the plate and the reflective boundary (the plastic enclosure in the experiment) produces a variation in pressure as a function of time across the perturbed surface, as can be seen in figure 15.

This simulation setup can now be used to predict the result of changes to the experimental configuration, such as plate material and gap dimension. As an example, the shape of the plate can be changed to accommodate the change in pressure across the perturbed surface. Beveling the surface slightly on the edge results in the simulation shown in figure 16. Here the perturbed surface has remained almost flat, thus allowing for radiographic capture of the temporal growth of the center perturbation.

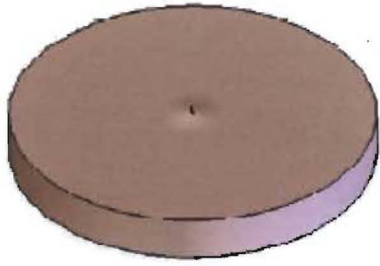


Fig. 13. The Gaussian point plate.

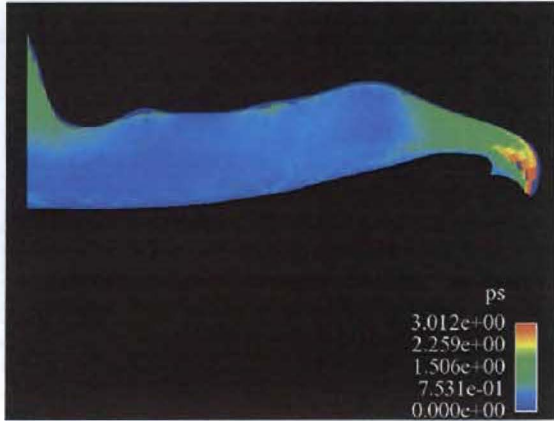


Fig. 14. Simulation of plastic strain in Gaussian point plate.

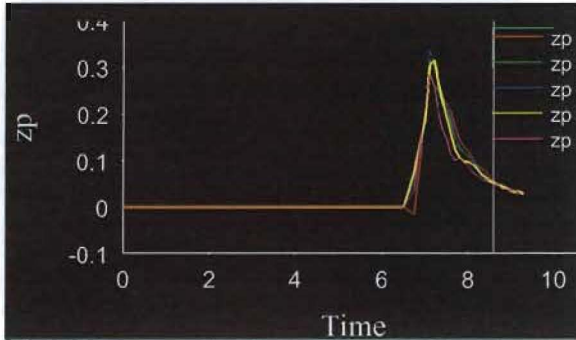


Fig. 15. Pressure vs. time for Gaussian plate perturbed surface.

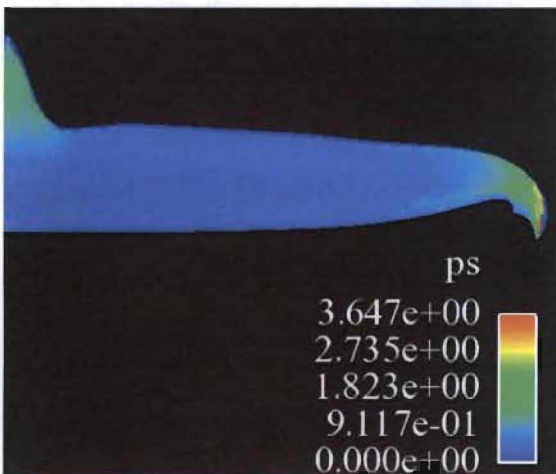


Fig. 16. Simulated plastic strain in revised Gaussian plate.

## 5 Conclusion

Data on solid material response to the application of high strain rates, strong plastic strains and significant temperature increments allows confidence in extending material strength models to these regimes. In order to develop such data, the LANSCE proton radiography beam was used to radiograph high explosives driven perturbed plates. The numerical simulations of these experiments using a 2-D ALE code presented in this paper show that the Preston-Tonks-Wallace strength model for annealed copper is adequate to capture the experimental behavior, given enough refinement in mesh size. Several simplifications to the model reduced the complexity of the simulation, while still allowing for accurate prediction of the experimental results.

To allow the simulations to more easily capture the HE lens behavior, an axisymmetric Gaussian plate is currently being developed for use in future experiments. The developed simulation capability is being used to help refine the new plate shape. Additionally, simulations of experimental variations such as the plate material and gap width are now possible.

## References

1. J.F. Barnes, P.J. Blewett, R.G. McQueen, K.A. Meyer, D. Venable, *J. Appl. Phys.* **45**, 727 (1974)
2. Y.V. Batkov, V.N. Knyazev, S.A. Novikov, V.A. Raevsky, N.D. Fishman, *J. Phys. IV* **10**, 793 (2000)
3. D.L. Preston, D.L. Tonks, D.C. Wallace, *J. Appl. Phys.* **39**, 211 (2003)