

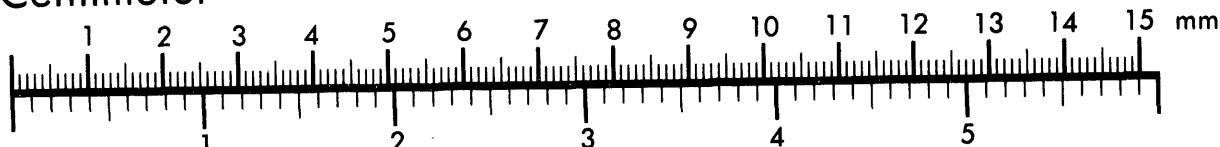


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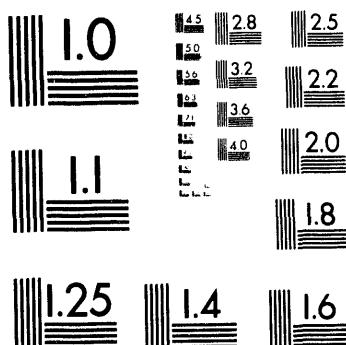
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**ANALYSIS OF COBBLY SOILS FOR COBBLES-TO-FINES CORRECTIONS TO
RADIONUCLIDE CONCENTRATIONS AT THE NEW RIFLE, COLORADO,
PROCESSING SITE**

May 1994

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EXECUTIVE SUMMARY

A contamination depth and cobbly soil characterization study was performed in November and December 1993 at the Uranium Mill Tailings Remedial Action (UMTRA) Project's New Rifle, Colorado, processing site. This study was initiated due to a concurrence by the U.S. Nuclear Regulatory Commission (NRC) clarifying that the allowable residual contamination in soil should be averaged over the total mass of the soil volume, including cobbles and gravels (i.e., bulk concentration). The New Rifle processing site has a high percentage of cobbles and gravels underlying the pile and other contaminated areas, which preliminary excavation designs have identified for removal and disposal. The main purpose of this study was to evaluate the relative mass percentage and radionuclide concentrations of cobbles and gravels in order to determine the bulk contamination concentrations, revise the underlying excavation design depths, and improve verification methods. Another important goal of the study was to acquire more accurate contamination depth data (profile) for the subpile material. The observations from these components of the study resulted in the following conclusions:

- On average, 75 percent of the cobbly soil beneath the pile and contaminated areas is cobble and gravel having radionuclide levels below the cleanup standards. The cobbles and gravels will not require excavation, although excavation was indicated in previous designs.
- Radium-226 (Ra-226) contamination depths from past characterization studies were significantly overestimated in many areas; therefore, less excavation will be required in these areas.
- Thorium-230 (Th-230) has not migrated preferentially in suspect areas at the site in significant levels that would require excavation below the excavation depths required for Ra-226.
- The amount of excavation to be carried out below the water table has decreased significantly because 1) more accurate data on contamination depth have been compiled, and 2) cobble/gravel parameters have been used to meet the bulk concentration limits for contamination. These two factors have resulted in lower contamination levels at depth.

In summary, this recharacterization study will probably reduce the volume of material for excavation/disposal by several hundred thousand cubic yards and significantly reduce the amount of ground water expected to be pumped out of the excavation during cleanup.

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LIST OF ACRONYMS AND ABBREVIATIONS

<u>Acronym</u>	<u>Definition</u>
ALARA	as low as reasonably achievable
cm	centimeter
DOE	U.S. Department of Energy
EPA	U.S. Environmental Protection Agency
ft	foot
m	meter
m ²	square meter
NRC	U.S. Nuclear Regulatory Commission
pCi/g	picocuries per gram
pCi/L	picocuries per liter
pCi/m ² s	picocuries per square meter per second
pH	acidity
Ra-226	radium-226
Rn-222	radon-222
Th-230	thorium-230
UMTRA	Uranium Mill Tailings Remedial Action
UMTRCA	Uranium Mill Tailings Radiation Control Act
μR/hr	microroentgens per hour

1.0 INTRODUCTION

1.1 STANDARDS AND CRITERIA

Remedial action at the New Rifle, Colorado, processing site is being performed under the *Uranium Mill Tailings Radiation Control Act* (UMTRCA) of 1978 (42 USC §7901 *et seq.*). Under the UMTRCA, the U.S. Environmental Protection Agency (EPA) is responsible for developing appropriate and applicable standards for the cleanup of radiologically contaminated land and buildings at 24 designated sites, including the New Rifle, Colorado, inactive processing site. The UMTRCA states that the U.S. Department of Energy (DOE) shall "select and perform remedial actions at the designated processing sites and disposal sites in accordance with the general standards" prescribed by the EPA. Regulations governing the required remedial action at inactive uranium processing sites were promulgated by the EPA in 1983 and are contained in 40 CFR Part 192 (1993), *Health and Environmental Protection Standards for Uranium and Thorium Mill Tailings*.

Subpart B of 40 CFR Part 192 consists of standards for the cleanup of land and buildings. The standards applicable to land cleanup activities are as follows:

Remedial actions shall be conducted so as to provide reasonable assurance that, as a result of residual radioactive materials from any designated processing site, the concentration of radium-226 in land averaged over an area of 100 square meters (m^2) shall not exceed the background level by more than --

- 1) Five picocuries per gram (pCi/g), averaged over the first 15 centimeters (cm) of soil below the surface, and
- 2) Fifteen pCi/g, averaged over 15-cm-thick layers of soils more than 15 cm below the surface.

In addition, 40 CFR Part 192 provides criteria for applying supplemental standards for the cleanup and stabilization of other radionuclides that present a hazard commensurate with radium-226 (Ra-226) (40 CFR §192.21 (1993)), such as thorium-230 (Th-230). The *Generic Protocol for Thorium-230 Cleanup/Verification at UMTRA Project Sites* (Appendix A) under development by the DOE UMTRA Project Office has received oral NRC approval for implementation. Fundamental provisions of the protocol are as follows:

- Th-230 concentrations exceeding Ra-226 concentrations will be remediated such that Ra-226 concentrations 1000 years in the future, including both *in situ* Ra-226 and Ra-226 produced by natural decay of Th-230 over a 1000-year period, averaged over 100 m^2 , will not exceed background levels

by more than 5 pCi/g in the first 15-cm surface soil layer or 15 pCi/g in successive 15-cm subsurface layers.

- For deeply buried material, excavations will be stopped when the RAEOM computer code, using site-specific parameters, calculates a radon-222 (Rn-222) flux of 3.9 picocuries per square meter per second (pCi/m²s) and expected long-term conditions are appropriate, or when construction safety or feasibility becomes a concern.
- Excavation of elevated Th-230 encountered below the water table in the saturated zone will be assessed relative to the practicality with which dewatering can be performed. An as-low-as-reasonably-achievable (ALARA) analysis using pathway techniques will be performed in cases where a major portion of the site contains Th-230 that extends into the saturated zone, and excavation into the zone is impractical.

The EPA standards were originally based on an understanding of radiologically contaminated, fine-grained, tailings-like soil. However, the NRC has concurred that the soil cleanup standards for cobble soil should have a universal interpretation of *bulk* soil concentrations, where bulk is defined as the total activity in picocuries divided by the total sample mass in grams, independent of the radionuclide distribution as a function of soil size fraction (Appendix A). Recognizing that UMTRA Project site cleanup activities will entail the cleanup of radiologically contaminated cobble soil, the NRC also has concurred on a procedure developed by the DOE for excavation control and verification of cobble subsoil (Appendix A). The accepted protocol is based on establishing a representative mass partition function that is the ratio of the mass of the soil fraction retained on a #4 sieve to the mass of the soil fraction passing a #4 sieve, and the characteristic radionuclide concentration on the larger soil size fraction retained on a #4 mesh sieve. The mass partition function can be developed and applied for the entire site or for each 100-m² grid (see Appendix A). Bulk radionuclide concentration can be determined using the mass partition function, the radionuclide concentration on the larger size soil fraction, and radiometric/radiochemical measurements of only the finer soil fraction passing a #4 sieve.

The standards given above are based on *bulk* Ra-226 concentrations elevated above background level. Measurements of background radioactivity near the New Rifle, Colorado, processing site, have resulted in the following determinations (DOE, 1992):

- Background gamma exposure rates at 1 meter (m) above the earth average 15 microroentgens per hour (μ R/hr).
- Background Ra-226 concentrations in the soil near the processing site average 1.2 pCi/g.

- Background Rn-222 concentrations in air at various locations near the processing site average approximately 0.4 picocuries per liter (pCi/L).

1.2 REMEDIAL ACTION

The remedial action at the processing site will be conducted to remove the tailings and contaminated materials to meet the EPA *bulk* soil cleanup standards for surface and subsurface soils. The site areas disturbed by remedial action excavation will be either contoured or backfilled with uncontaminated soil and contoured to restore the site. The final contours will produce a final surface grade that will create positive drainage from the site.

2.0 PHYSICAL AND RADIOLOGICAL EVALUATION

A site characterization study was conducted in November and December 1993 to determine the nature of the cobbly subsoil profile and contamination levels underlying the New Rifle, Colorado, processing site and to ascertain 1) the mass partitioning of the subpile soil relative to a #4 mesh sieve, and 2) the radiological contamination associated with the cobbly soil size fractions passing and retained on a #4 mesh sieve. The purpose of this investigation was to obtain the necessary parameters to characterize the bulk radionuclide concentrations for the site foundation soil, particularly the subpile area. With these more recent site characterization data, appropriate depths for excavating radiologically contaminated cobbly subsoil may be determined. These data also provide necessary information regarding the way in which excavation control and verification should be performed in cobbly soils.

2.1 TEST PIT OPERATION AND CHARACTERIZATION RESULTS

Operations consisted of excavating 22 test pits with a backhoe. Lithological logging, sampling, and photographing of the pits were also carried out. Test pit locations are shown in Figures 2.1 and 2.2, and selected photographs of pits and operations are found in Appendix B. Pits were distributed over accessible areas of the subpile (11 total), around the north, south and east sides of the pile perimeter (8 total), and in areas representing background conditions for the site (3 total). Lithological logging data for each test pit are found in Appendix C.

Test pits were excavated into the cobbly soil layer underlying the site and sampled in accordance with the NRC-approved protocol (Appendix A). Sampling was terminated in general at or slightly below the level that free water was encountered in the test pits. This was done because of difficulty in obtaining representative samples from below the water surface. Test pit location 4 (M-CF-04 and M-CF-04A, Appendix C) was excavated a second time to obtain additional 1-foot (ft) (0.3-m) increment samples at depths from which the initial samples may have been accidentally cross-contaminated during the first sampling. The granular material in test pit location 29 (M-CF-29) was determined to be contaminated fill material from earlier site backfill operations; therefore, its cobbles-to-fines ratio (mass partition function) and radionuclide data were not representative of the site's natural cobbly soil. These data were not used in the study.

For each pit, a representative composite sample of the cobbly soil layer was divided using appropriate gradation techniques into fractions greater and less than a #4 mesh sieve to determine mass partition functions (Appendix D). Composite samples of both soil fractions in the cobbly soil were analyzed for Ra-226 and Th-230 (Appendix E). Table 2.1 lists the individual, average, and statistical mass partition functions and cobble (> #4 mesh) radionuclide concentrations for the test pits.

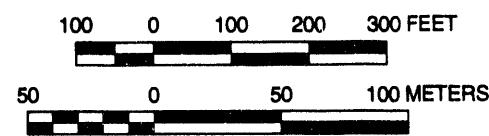
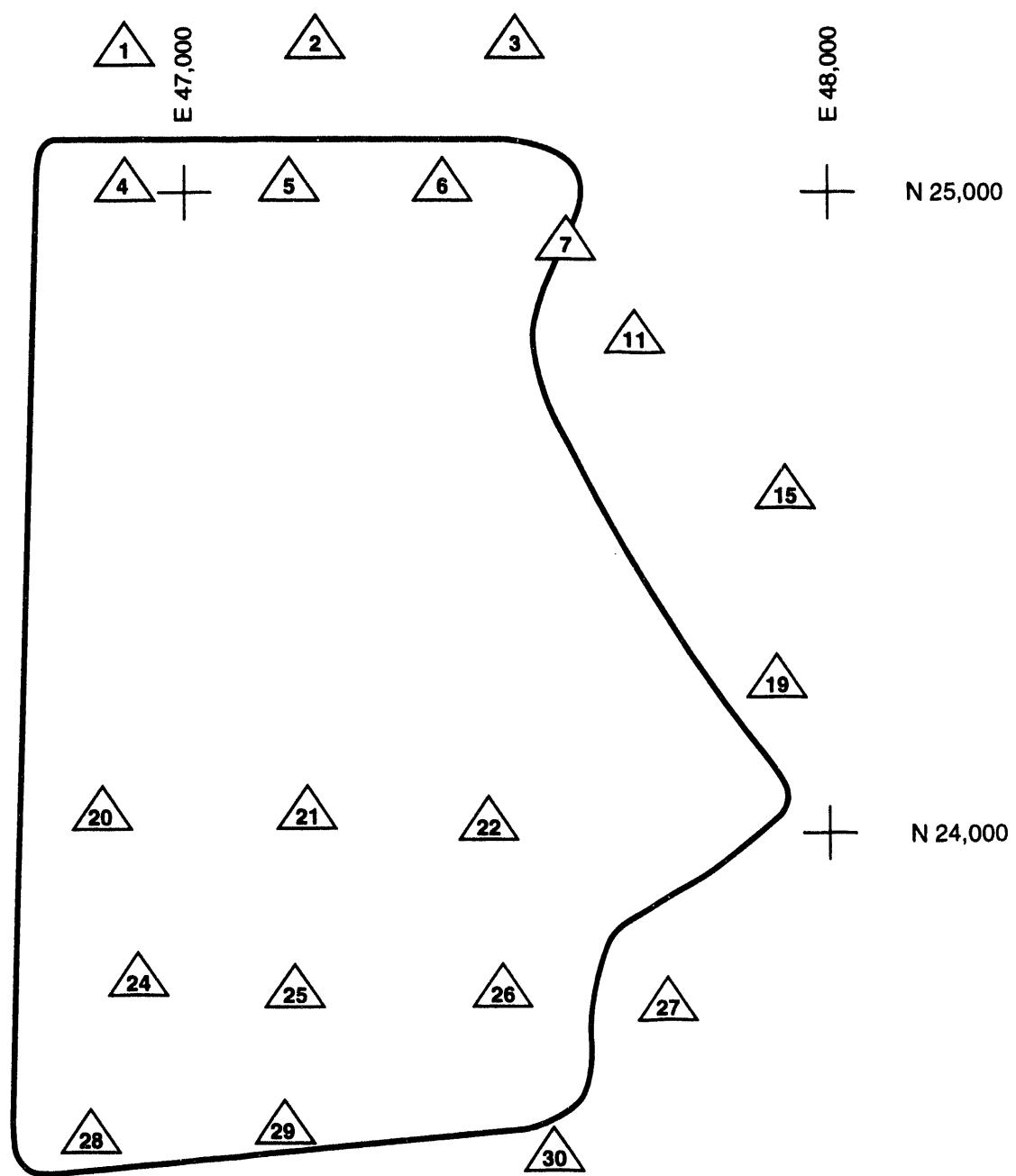


FIGURE 2.1
TEST PIT LOCATIONS, SUBPILE AND OFFPILE

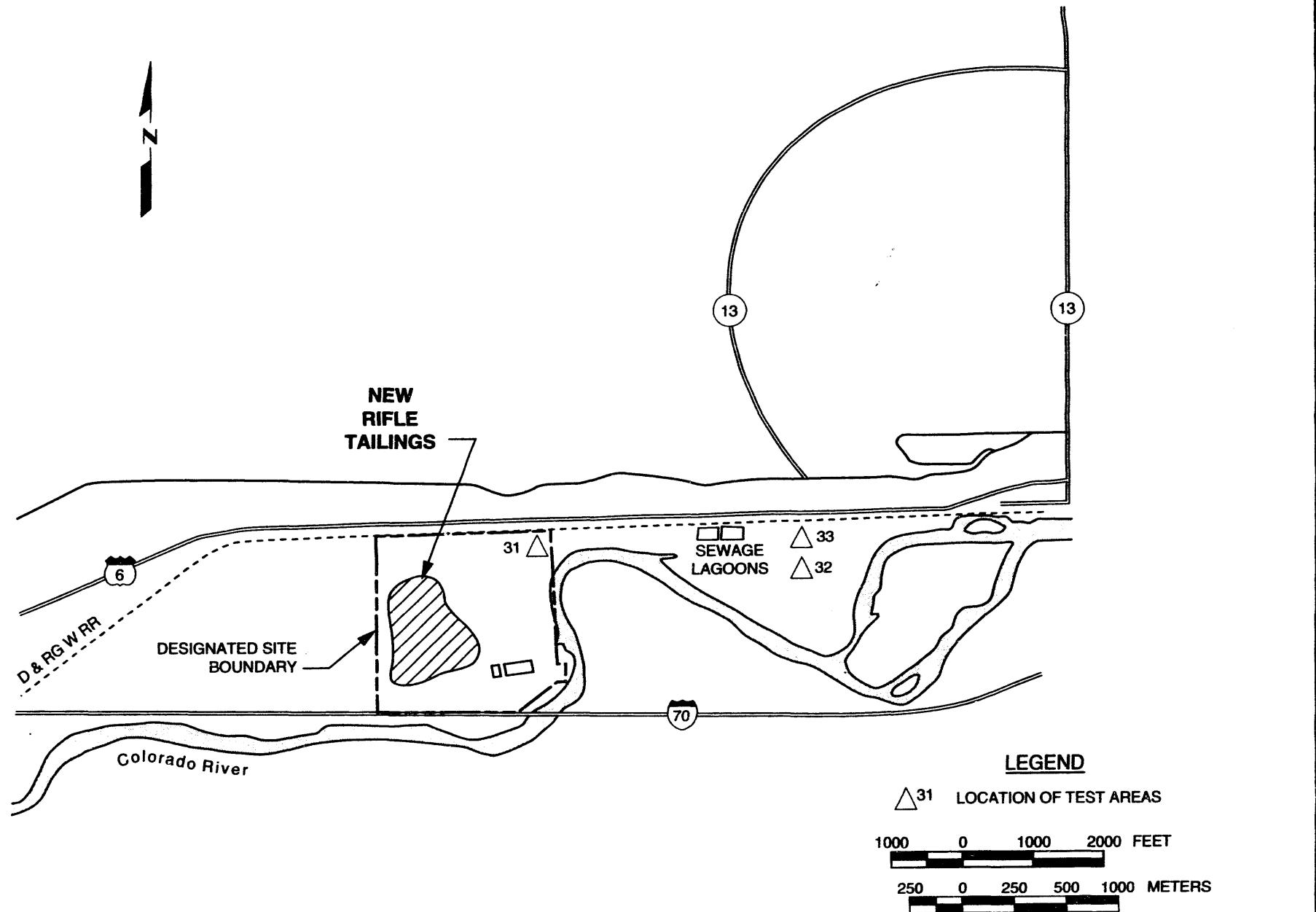


FIGURE 2.2
TEST PIT LOCATIONS, BACKGROUND

Table 2.1 Summary of mass partition functions and radionuclide concentrations for composite soil samples retained on a #4 mesh sieve

Test pit ID and statistical summary	Location	Mass partition function ^a	Radionuclide concentration mass fraction > #4 sieve	
			Ra-226 (pCi/g)	Th-230 (pCi/g)
M-CF-01	Offpile	4.92	1.1	1.1
M-CF-02	Offpile	2.15	0.7	0.9
M-CF-03	Offpile	2.38	1.7	0.5
M-CF-04	Subpile	3.18	0.6	0.7
M-CF-05	Subpile	3.46	1.4	0.3
M-CF-06	Subpile	No data	3.3	1.6
M-CF-07	Subpile	2.72	2.0	1.7
M-CF-11	Offpile	3.24	0.8	0.4
M-CF-15	Offpile	2.88	0.9	0.8
M-CF-19	Offpile	3.22	0.8	0.7
M-CF-20	Subpile	5.41	0.5	0.8
M-CF-21	Subpile	4.49	1.6	1.2
M-CF-22	Subpile	3.83	0.9	0.9
M-CF-24	Subpile	1.84	0.9	0.7
M-CF-25	Subpile	3.65	0.8	1.3
M-CF-26	Subpile	1.90	0.7	0.5
M-CF-27	Offpile	5.67	0.8	0.8
M-CF-28	Subpile	9.42	0.8	0.5
M-CF-30	Offpile	3.85	1.2	0.6
M-CF-31	Background	3.59	0.9	0.7
M-CF-32	Background	4.21	1.8	1.1
M-CF-33	Background	4.52	1.6	0.5
Average	All	3.83	1.2	0.8
Standard deviation		1.67	0.6	0.4
95% confidence level ^b		3.20	1.4	0.9
Average	Background	4.11	1.4	0.8
Standard deviation		0.47	0.5	0.3
95% confidence level ^b		3.32	2.2	1.3
Average	Subpile	3.99	1.2	0.9
Standard deviation		2.20	0.8	0.5
95% confidence level ^b		2.71	1.6	1.2
Average	Offpile	3.54	1.0	0.7
Standard deviation		1.22	0.3	0.2
95% confidence level ^b		2.72	1.2	0.8
Average	Subpile and offpile	3.79	1.1	0.8
Standard deviation		1.80	0.7	0.4
95% confidence level ^b		3.05	1.4	1.0

^aMass partition function equates to cobbles-to-fines ratio, $f = (M > \#4)/(M < \#4)$.^bThe upper 95 percent confidence level value is shown for the radionuclide concentrations, and the lower 95 percent confidence level value for the mass partition functions.

In addition to the requirements in the cobbles-to-fines protocol, an aliquot of the fine soil size fraction (<#4 mesh sieve) was obtained from each 1-ft (0.3-m) test pit depth increment (except in tailings) and separately analyzed for Ra-226 and Th-232. One to four of these increment samples for each test pit were also analyzed for Th-230 to determine the potential for significant Th-230 contamination at depth below Ra-226 contamination. Measurements of acidity (pH) in selected soil layers in subpile and offpile test pits were also taken in the field to determine whether there were acidic conditions that would enhance Th-230 mobility (see data in lithological logs of Appendix C).

2.2 STATISTICAL PARAMETERS FOR COBBLES-TO-FINES CORRECTIONS

The original plans developed for test pit locations had a total of approximately 30 subpile and offpile test pits. Ten of these locations were inaccessible during the study because they were underneath about 50 ft (15.3 m) of tailings. However, the data gathered from this study are considered to be sufficient for obtaining the necessary parameters to implement the statistical approach of cobbles-to-fines corrections at the site due to the following:

- Observed consistency in the mass partition functions and low radionuclide concentrations in the cobbles (Table 2.1).
- Spatial representativeness of pit locations (Figure 2.1).
- Uniformity of the geological conditions in the underlying natural cobbly soil (Appendix C).

Additionally, the protocol's method for determining conservative values for the statistical mass partition functions and cobble radionuclide concentrations was reviewed. This review revealed that using data from less than 30 test pits should actually result in more conservatism in developing the statistical values when using representative sampling plans.

The average, standard deviation and statistical values for the mass partition function and cobble radionuclide concentrations for each grouping (subpile, offpile, background, and all combined) of test pits are shown at the bottom of Table 2.1. The data from test pit M-CF-29 were not used because of its apparent unnatural contents (backfill). No mass partition function was available for test pit M-CF-06, because technical problems (cave-in) rendered the measurement nonrepresentative.

This information demonstrates the relative consistency in the physical and radiological characteristics of the cobbly soil layer in all of the test pits. In determining the correct values for calculating bulk concentrations from cobbles-to-fines corrections, the subpile and offpile combined data appear to be the most applicable because of the proximity to areas that may apply the corrections. These critical values that will be used in the correction calculations are 3.05 for the statistical mass partition function, and 1.4 and 1.0 for the

statistical Ra-226 and Th-230 cobble radionuclide concentrations, respectively. Using the statistical mass partition function and statistical Ra-226 cobble concentration for all of the pits (1.4 pCi/g, which is more appropriate than using 2.2 pCi/g from the small number of background test pits), a bulk Ra-226 background concentration of 1.4 pCi/g is established in this study.

3.0 CHANGES TO EXCAVATION DESIGN

From the lithological logging data (Appendix C), the thickness of the layers of relatively clean fine-grained soil (sand, silt, clay, etc.) above the cobbly soil interface in these pits ranged from 0 ft to 16 ft (0 m to 4.9 m), and averaged 5 ft (1.5 m). Cobbly soil was encountered immediately at the surface in five of the subpile test pits where the sand/silt/clay layer was previously removed with the tailings (all on the south side of the pile). At other UMTRA Project sites, Ra-226 adsorbs or precipitates within the first 1 or 2 ft (0.3 or 0.6 m) of soil below the pile or other contaminated material (DOE, 1994). This process was also apparent in many of the test pits at New Rifle. From the results for Th-230 characterization of the fines (1-ft [0.3-m] increment samples, Appendix E), it can be concluded that mobilization of Th-230 below the Ra-226 contamination was not apparent in most of the test pits (see Ra-226 and Th-230 profile data in test pit logs of Appendix C). This was somewhat expected when considering the typically neutral-to-basic pH observed in the soils. The few pits that showed Th-230 mobilization (disequilibrium with Ra-226) did not reveal levels that would require excavation beyond the Ra-226 excavation depth.

From these observations and the profiling (1-ft [0.3-m] increment samples) data on the radionuclide contamination, it is apparent that the cobbles-to-fines corrections may not be needed in most remediated areas because the contamination does not extend into the cobbly subsoil. This has resulted in a significant change in contamination depths. Original site characterization data (DOE, 1985) used in the remedial action excavation design showed the contamination in many of the test pit areas to be deeper, from 1 to 6 ft (0.3 to 1.8 m). This change in known contamination depths affects estimated excavation depths in the design, as shown in Table 3.1. The data changes are most likely due to the original study using bore hole drilling techniques, which involved drilling and sampling the subpile soil through various depths of tailings and contaminated materials. It appears that using a backhoe and not having a large (approximately 50-ft [15-m]) layer of tailings to penetrate for sampling subpile soil improved the accuracy of data for the actual contamination depth. The availability of these improved contamination depth data enables engineering and scheduling efforts to more accurately handle disposal of the actual volume of contaminated material. These data indicate that the total volume of contaminated material is less than that originally identified by an estimated several hundred thousand cubic yards, if test pit conditions are representative of the remaining site contaminated areas.

Table 3.1 New Rifle, Colorado, estimated excavation depth based on cobbles-to-fines ratio and contamination profiles

Area	Plan excavation depth		Excavation based on cobbles/fines profiles		Delta ^a	
	ft	m	ft	m	ft	m
1	6	1.8	1	0.3	(5)	(1.5)
2	5	1.5	0	0	(5)	(1.5)
3	5-6	1.5-1.8	2	0.6	(3-4)	(0.9-1.2)
4, 4A	13	4.0	9	2.7	(4)	(1.2)
5	13	4.0	11	3.4	(2)	(0.6)
6	16	4.9	13+	4.0+	--	--
			Insufficient data available			
7	14	4.3	14	4.3	0	0
11	5	1.5	2	0.6	(3)	(0.9)
15	5	1.5	4	1.2	(1)	(0.3)
19	6	1.8	1	0.3	(5)	(1.5)
20	5	1.5	0	0	(5)	(1.5)
21	5	1.5	0	0	(5)	(1.5)
22	6	1.8	6	1.8	0	0
24	4	1.2	0	0	(4)	(1.2)
25	6	1.8	1	0.3	(5)	(1.5)
26	6	1.8	1	0.3	(5)	(1.5)
27	6	1.8	8	2.4	2	0.6
28	2	0.6	1	0.3	(1)	(0.3)
29	3	0.9	Insufficient data available		--	--
30	6	1.8	4	1.2	(2)	(0.6)

^aNumbers within parentheses indicate amount of reduced excavation; numbers without parentheses indicate amount of increased excavation.

4.0 CONCLUSIONS

Site cleanup, including the excavation control and verification, will involve the cobbles-to-fines corrections in remediated areas when applicable. Th-230 was not observed to be a significant concern in excavation design, and its residual concentrations will be further verified according to the requirements in the *Generic Protocol for Thorium-230 Cleanup/Verification at UMTRA Project Sites* (Appendix A). Whenever the application of the cobble-to-fines correction is in doubt (for example, when it appears that there is only a small percentage of cobbles), grid verification based on a representative sample will be used or grid-specific mass partition functions will be measured to demonstrate compliance with EPA soil cleanup standards.

For site verification, the *statistical cobbles radionuclide concentrations at the upper 95 percent confidence limit and the statistical mass partition function at the lower 95 percent confidence limit* are used to determine allowable fines concentrations in subpile and offpile areas (calculation JEG-RFL-03-94-09-06-00). On this basis, for cobbly subsoil to comply with the bulk cleanup standards (total 1000-year Ra-226 concentrations from residual Ra-226 and Th-230 not to exceed 15 pCi/g above background = 1.4 pCi/g *bulk* Ra-226 concentration), the corresponding concentrations in the finer soil size fraction (passing a #4 mesh sieve) in the subpile and offpile areas could vary as follows:

1. $C_{<\#4 Ra} = 62.2 \text{ pCi/g Ra-226}$, when the Th-230 concentrations on the finer fraction, $C_{<\#4 Th}$, are less than or equal to 63.7 pCi/g;
2. $C_{<\#4 Th} = 176.5 \text{ pCi/g Th-230}$, if there is evidence that the Th-230 has differentially migrated relative to Ra-226, and the residual *bulk* Ra-226 concentration is 1.4 pCi/g ($C_{<\#4 Ra} = 1.2 \text{ pCi/g}$), corresponding to average background concentrations; or
3. Th-230 concentrations (pCi/g) determined by the following relation for residual Ra-226 concentrations measured on the finer soil size fraction, ($C_{<\#4 Ra}$), in the range of 1.2 to 62.2 pCi/g,

$$C_{<\#4 Th} = 178.8 - 1.85 \times C_{<\#4 Ra}$$

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6.0 REFERENCES

DOE (U.S. Department of Energy), 1994. *Site-Specific Analysis of Radiological and Physical Parameters for Cobbly Soils at the Gunnison, Colorado, Processing Site, Revision 1*, DOE/AL-62350-53F, DOE UMTRA Project Office, Albuquerque Operations Office, Albuquerque, New Mexico.

DOE (U.S. Department of Energy), 1992. *Remedial Action Plan and Site Design for Stabilization of the Inactive Uranium Mill Tailings Sites at Rifle, CO, Final, Volume II*, DOE/AL-050506.0000, DOE UMTRA Project Office, Albuquerque Operations Office, Albuquerque, New Mexico.

DOE (U.S. Department of Energy), 1985. *Radiologic Characterization of the Rifle, Colorado, Uranium Mill Tailings Remedial Action Sites*, GJ-29, by the Bendix Field Engineering Corporation for the DOE UMTRA Project Office, Albuquerque Operations Office, Albuquerque, New Mexico.

CODE OF FEDERAL REGULATIONS

40 CFR Part 192, *Health and Environmental Protection Standards for Uranium and Thorium Mill Tailings*, U.S. Environmental Protection Agency (1993).

UNITED STATES CODE

42 USC §7901 *et seq.*, *Uranium Mill Tailings Radiation Control Act*, November 8, 1978.

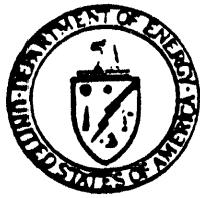
APPENDIX A

**U.S. DEPARTMENT OF ENERGY/U.S. NUCLEAR
REGULATORY COMMISSION CORRESPONDENCE**

**PROCEDURE FOR BULK RADIONUCLIDE
DETERMINATION, EXCAVATION CONTROL, AND SITE
VERIFICATION FOR SOILS CONTAINING COBBLES**

**GENERIC PROTOCOL FOR THORIUM-230
CLEANUP/VERIFICATION AT UMTRA PROJECT SITES**

**U.S. DEPARTMENT OF ENERGY/U.S. NUCLEAR
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Rockville, MD 20852

Dear Mr. Summeier:

Historically, the majority of Ra-226 contaminated materials being cleaned up at Uranium Mill Tailings Remedial Action (UMTRA) Project sites consisted of tailings, ore spoils, tailings intermixed with fine-grained soils (windblown and vicinity properties) and fine-grained soils under residual milling waste (tailings and raffinate ponds). However, in 1988, conditions encountered while remediating Th-230 contamination which persisted once Ra-226 had been removed at both the Riverton, Wyoming, and Durango, Colorado, sites were substantially different.

At both sites, which were located on alluvial floodplains, subsurface soils consisted of a large percentage of cobbles and gravels which were retained on a #4 sieve (4.76 mm). In addition, it was determined that approximately 95 percent of the total concentration of radioactivity was deposited on the fines (those soils passing a #4 sieve).

Based on these considerations and the fact that cleanup verification sampling routinely employed by the Remedial Action Contractors did not readily accommodate sampling and analysis of materials greater than #4 sieve, the following protocol for Th-230 cleanup/verification to a bulk subsurface concentration of 35 pCi/g was adopted and approved by the U.S. Department of Energy (DOE) and the U.S. Nuclear Regulatory Commission (NRC) in modifications to the Remedial Action Plans for those sites.

1. Determine the "fines mass fraction" by collecting several (10) representative bulk field samples, and separating fractions greater than and less than a #4 sieve:

fines mass fraction = mass fines/mass total = unitless fraction

2. Determine Ra-226 (or Th-230) concentration (passing the #4 sieve) in verification samples collected and analyzed according to standard methodology described in MK-Ferguson Company (MK-F) Procedure RAC-015, "Verification Procedures for Vicinity Properties and Tailings Sites."
3. Determine "bulk" Ra-226 (or Th-230) concentration during cleanup and verification by correcting the Ra-226 (or Th-230) concentration on fines as follows:

$$\text{bulk Ra-226 concentration} = (\text{fines Ra-226 concentration}) \times (\text{fines mass fraction}) \text{ or,}$$
$$\text{bulk Th-230 concentration} = (\text{fines Th-230 concentration}) \times (\text{fines mass fraction})$$

The DOE proposes to adopt this basic protocol, on a site specific basis, as a standard operating practice for cleanup and verification of both residual Ra-226 and Th-230 contamination at UMTRA sites yet to be remediated. The bulk concentrations of Ra-226 and Th-230 determined by the above procedure will comply with the remediation standard for Ra-226, and supplemental cleanup requirements for Th-230, as specified in 40 CFR 192. Bulk Ra-226 concentrations will not exceed 5 and 15 pCi/g for respective 15 cm deep surface and subsurface layers averaged over 100 m². Similarly, the bulk concentration of subsurface Th-230 in 15 cm depth increments will not exceed 35 pCi/g averaged over 100 m². The details of the protocol will be more completely described in an addendum to Procedure RAC-015 which will address when the protocol would be implemented; the number of samples needed to provide the initial value for the fines mass fraction; the frequency of updating/verifying the fines mass fraction as work progresses across a site; how the fines mass fraction used will be logged on field data sheets, etc. It will also be included in future updates of the Technical Approach Document and referenced as appropriate in Remedial Action Plans for sites where it will be applied.

The sites where this protocol could be applied would likely include Grand Junction, Gunnison, Rifle, Slick Rock, and Naturita, Colorado, since they are all located on alluvial floodplains possessing characteristics similar to those described above. Therefore, the DOE requests the NRC's concurrence that such a protocol is consistent with the requirements of 40 CFR 192 and that its contractors should be directed to formally incorporate the protocol into standard operating procedures and address its potential application in site Remedial Action Plans.

Mr. John Surmeier

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SEP 06 1991

If you should have any further questions regarding this request, please call Mr. Don Metzler of my staff at (FTS) 845-5657.

sincerely,

Glenton B. Gray III
On Mark L. Matthews, P.E.
Project Manager
Uranium Mill Tailings Remedial Action
Project Office

cc:

F. Bosiljevac, UMTRA
S. Hill, TAC
M. Miller, TAC
D. Gonzales, TAC
J. Oldham, MK-F
D. Carlson, MK-F
M. Madsen, CN-Geotech



UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D.C. 20585

SEP 17 1991

Mr. Mark L. Matthews P.E.
Project Manager
Uranium Mill Tailings Remedial Action
Project Office
Department of Energy
Albuquerque Operations Office
P.O. Box 5400
Albuquerque, New Mexico 87115

Dear Mr. Matthews:

Your letter of September 6, 1991, requested U.S. Nuclear Regulatory Commission (NRC) concurrence in the use of a procedure for determining and verifying radium-226 concentrations at locations with large quantities of cobbly material. Your letter states that at several Title I sites, DOE has encountered large quantities of radium-226 or thorium-230 contaminated material with a high content of cobbly material (greater than a No. 4 sieve size). Your tests show that the contained radioactivity is concentrated in the finer fraction with the coarse fraction containing negligible quantities (less than 5 percent). Procedures presently in use by your contractors for sampling and analyses are designed for relatively fine grained homogeneous soils with a minimum of larger material and are not adequate to characterize the radioactive concentrations in the heterogeneous size material being encountered. Your proposed approach would rely on measurement of the radium-226 or thorium-230 content in the finer fraction to obtain an average concentration for the entire sample.

We agree that determining an average radium-226 or thorium-230 content over an entire sample would be consistent with the Environmental Protection Agency (EPA) standards in 40 CFR 192 if the radium-226 content of the two size fractions and the percentage of each size fraction are properly factored. Part 192.12 states that the concentration of radium-226 in land can be averaged over an area of 100 square meters to meet the standards of not exceeding background level by more than 5 pCi/g averaged over the first 15 cm of soil below the surface and 15 pCi/g averaged over 15 cm thick layers of soil more than 15 cm below the surface.

You plan to address the details of the procedure in a section to be added to Procedure RAC-015 which will define when the procedure would be used, the number and distribution of samples to be taken, the determination of the radium-226 distribution and size fractions, and other appropriate details.

We agree that the proposed approach has the potential for maintaining compliance with EPA's standards while avoiding over excavation of contaminated

Mark Matthews

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material. However, for final concurrence, we will have to review the details of your revised Procedure RAC-015 and the effects of its implementation on a site-specific basis. Any questions can be addressed to Allan Mullins of my staff at FTS-492-0578.

Sincerely,



John J. Surmeier, Chief
Uranium Recovery Branch
Division of Low-Level Waste Management
and Decommissioning, NMSS

cc: D. Metzler, DOE, Alb.



UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D. C. 20555

APR 4 1992

Mr. Albert R. Chernoff, Project Manager
Uranium Mill Tailings Remedial Action
Project Office
U.S. Department of Energy.
Albuquerque Operations Office
P.O. Box 5400
Albuquerque, New Mexico 87115

Dear Mr. Chernoff:

We have reviewed the procedure on "Bulk Radionuclide Determination, Excavation Control, and Site Verification For Cobbly Soils" sent with your letter of March 26, 1992, and supplemented by a revised Page 12 sent by facsimile on March 30, 1992. We hereby concur with its use on U.S. Department of Energy Uranium Mill Tailings Remedial Action Project sites containing a high percentage of cobbly subsoil. This procedure, designated RAC-OP-003, should be referenced in the specific Remedial Action Plans for those sites where it will be used.

One item of note concerns the section of the procedure discussing authority (Section 1.3). This section should be revised to reference this letter of concurrence rather than the September 17, 1991, letter cited, which agreed with the concept but did not concur with the procedure.

Any questions should be addressed to Allan Mullins of my staff at FTS 964-2578.

Sincerely,

A handwritten signature in black ink, appearing to read "John J. Surmeier".

John J. Surmeier, Chief
Uranium Recovery Branch
Division of Low-Level Waste Management
and Decommissioning, NMSS

cc: D. Metzler, DOE Alb
P. Mann, DOE Alb
D. Gonzalez, TAC

**PROCEDURE FOR BULK RADIONUCLIDE
DETERMINATION, EXCAVATION CONTROL, AND SITE
VERIFICATION FOR SOILS CONTAINING COBBLES**



MK-FERGUSON COMPANY
A MORRISON KNUDSEN COMPANY

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 **CWM Federal Environmental Services, Inc.**

INTERIM CHANGE NOTICE

(ICN)

ICN NO. SOP-OP-003-4 ICN-01/REV#0

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Page 1 of 1

ROCEDURE NUMBER: OP-003-4

REVISION NUMBER: 0

EFFECTIVE DATE

OF ICN: 9/21/92

CHANGES REQUESTED
BY:

Steve Hamp (DOE)

CHANGES GENERATED
BY:

Dave Andrews

PROBLEM STATEMENT/CORRECTIVE ACTION

The DOE has requested a few changes to improve clarity and content. Improvements shall be as indicated.

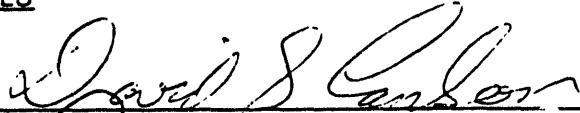
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remove pages 4 through 11, Rev. 0 and replace with new pages 4 through 11, Rev. 0 ICN-01.

PROVAL SIGNATURES

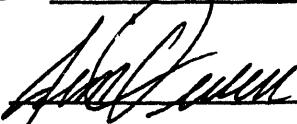
Please sign and date)

P & E MANAGER:



DATE: 10/1/92

PP MANAGER:



DATE: 10/1/92

PO MANAGER:



DATE: 9/29/92

COORDINATOR:



DATE: 9/29/92

Health Physics Standard Operating Procedures

Title: SOIL VERIFICATION USING COBBLES-TO-FINES CORRECTION

Procedure No.: OP-003-4

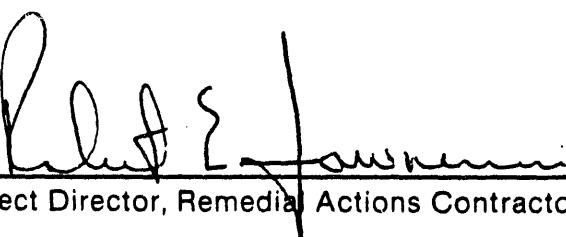
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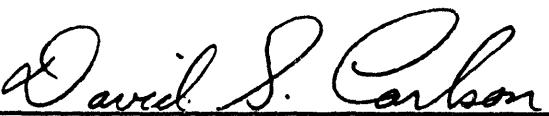
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APPROVAL HP CONTROLLED COPY 45

APPROVED:

 4-17-92
Project Director, Remedial Actions Contractor, UMTRA Project

APPROVED:

 4/17/92
Health Physics and Environment Manager, Remedial Actions Contractor, UMTRA Project

APPROVED:

 4/17/92
Health Physics Programs Manager, Remedial Actions Contractor, UMTRA Project

APPROVED:

 4-17-92
Health Physics Operations Manager, Remedial Actions Contractor, UMTRA Project



Soil Verification Using Cobbles-To-Fines Correction

1.0 SCOPE

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1.1 Purpose

This procedure will be used for determining and verifying average bulk radionuclide concentrations for radium-226 (Ra-226), thorium-230 (Th-230), and, if necessary, thorium-232 (Th-232) at locations where the subsoil consists of a percentage of cobbles in the bulk sample sufficient to affect measurement of the total radionuclide concentration. Excavation control and verification will be based on bulk concentrations determined by this procedure.

1.2 Applicability

This procedure may be applied in areas designated for routine soil excavation and verification (see RAC-OP-003) where the subsoil media contains a high percentage of cobbles.

1.3 Authority

Letter to A.R. Chernoff, DOE/UMTRA from J.J. Surmeier, NRC dated April 4, 1992.

2.0 REFERENCES

- 2.1 RAC Health Physics Procedure RAC-RP-005 - Radiological Instrumentation.
- 2.2 RAC Health Physics Procedure RAC-OP-002 - Excavation Control Procedure
- 2.3 RAC Health Physics Procedure RAC-OP-003

3.0 DEFINITIONS

- 3.1 Cobbles - The portion of a composite soil sample which will not pass through a #4 mesh sieve.
- 3.2 Fines - The portion of a composite soil sample which will pass through a #4 mesh sieve.
- 3.3 Mass partition function, f , of a cobbly soil sample - the ratio of the dry mass of the cobbles ($M_{>4}$), to the dry mass of the fines ($M_{<4}$):

$$f = M_{>4}/M_{<4} \text{ (cobble to fine ratio),}$$

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where the total dry mass of the sample, M_T , is

$$M_T = M_{<#4} + M_{>#4}.$$

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3.4 Radiological concentration (Ra-226, Th-230, or Th-232), in picocuries per gram (pCi/g), for the fines or cobbles, are designated by $C_{<#4}$ and $C_{>#4}$, respectively.

3.5 Bulk radionuclide concentration (Ra-226, Th-230, or Th-232), in pCi/g, is designated by C_B , and calculated using

$$C_B = \text{Total Sample Radioactivity (pCi)} / \text{Total Dry Mass of Sample (g)}$$

$$C_B = (C_{<#4} \times M_{<#4} + C_{>#4} \times M_{>#4}) / (M_{<#4} + M_{>#4})$$

$$C_B = C_{<#4} (1/(1+f)) + C_{>#4} (f/(1+f)).$$

3.6 Student t distribution (t) - the mathematical quantity used to define the distribution of test statistics for small sample populations; used herein to determine the lower and upper 95 percent confidence values for mass partition function and cobble radionuclide concentrations respectively.

3.7 Running Average - The determination of statistical quantities based on the available data and recalculated as more data becomes available.

3.8 Statistical Mass Partition Function (f_L) - The mass partition function (f), at the lower 95 percent confidence value calculated from test pit or running average data.

3.9 Statistical Cobble Radionuclide Concentration ($C_{>u}$) - The cobble radionuclide concentration ($C_{>#4}$) at the upper 95 percent confidence value calculated from test pit or running average data.

4.0 REQUIREMENTS
4.1 Prerequisites

4.1.1 All instruments used under this procedure shall have valid calibration.

4.1.2 Backup data (correlations, etc.) must be acquired, retained on-site, and made available for audit, on all methods and analyses used for excavation control and verification measurements.

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4.2 Tools, Material, Equipment

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4.2.1 Buckets, wheelbarrows, #4 mesh sieves or screens (4.8 millimeter), shovels or backhoe, weighing scale up to 200 lbs., drying oven, and other materials, as necessary, to obtain representative bulk soil samples. It should be noted that a 1/4 inch hardware cloth is approximately equivalent to a #4 mesh sieve, and may be used in lieu of a #4 mesh sieve.

4.3 Precautions/Limits

N/A

4.4 Acceptance Criteria

N/A

5.0 PROCEDURE
5.1 Site Evaluation

5.1.1 This guidance applies to processing sites and vicinity property areas. If the work area under consideration is less than 0.5 acre, the mass partition function (f) will be based on soil sampling from one centrally located test pit.

5.1.2 The statistical mass partition function (f_L) and statistical cobble radionuclide concentration ($C_{>u}$) may be determined by analysis of samples collected from test pits prior to construction. The purpose for developing a statistical mass partition function is only to obtain an estimate of the excavation depth required for compliance with radiological cleanup standards.

5.1.3 Approximately 30 (preferably uniformly distributed) sampling locations (test pits) should be used for the entire site. Fewer test pits may be used on small sites with prior approval from the HP & E Manager.

5.1.4 If test pit excavation activities are performed during remedial action, the statistical mass partition function (f_L) shall be obtained by calculating a running average of the corresponding parameters obtained as test pit work progresses across the site.

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5.2 Test Pit Soil Sampling and Analysis

- 5.2.1 Dig each test pit to the estimated depth of contamination at the location, and record the test pit surface elevation and maximum depth of each test pit. If groundwater is encountered, the elevation of the water level at the time of test pitting shall be recorded.
- 5.2.2 Collect one composite sample from each test pit. The composite soil sample shall be comprised of all the material contained in a standard shovel from each one foot increment (no material shall be discarded). Sampling shall begin at the cobbly soil surface or tailings/cobbly soil interface and continue through a minimum of 5 feet of cobbly material or all the cobbly material (whichever is less).
- 5.2.3 Sieve the composite sample through a #4 mesh sieve, collecting the fines and cobbles in separate buckets of known weight. Weigh both fractions separately. Thoroughly mix the fine fraction and extract two (2) representative 500 gram can samples.
- 5.2.4 Determine the percent moisture content by weight of one of the can samples and calculate the adjusted dry weight of the fines. Calculate the adjusted dry weight of the cobbles assuming a moisture content of 1.5 percent. Record all pertinent information on the Cobbles to Fines Calculation Sheet (Attachment 1). Calculate the mass partition function (f) for the test pit using the adjusted dry weight of the fines and cobbles in the relation defined in Definition 3.3.
- 5.2.5 The second can shall be analyzed by the site laboratory for Ra-226 (and Th-232 if necessary) and sent to the vendor laboratory for Ra-226 and Th-230 analysis (and Th-232 if necessary). Record on-site and vendor analysis results on Attachment 1.

Note: Analysis for Th-232 shall only be performed if the site characterization indicates Th-232 is present.

- 5.2.5.1 Using the initial on-site analysis results and the vendor analysis results for all test pit or running average samples, a Ra-226 correction factor shall be established using the following equation:

$$\text{Ra-226 C.F.} = \frac{R_1 + R_2 + \dots + R_n}{n}$$

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where, C.F. = correction factor,
 R_n = Vendor results (pCi/g) divided by
 initial OCS, results (pCi/g) for the
 nth sample ('e., 1, 2, ...n), and
 n = number of ratios.

5.2.5.2 The correction factor shall be updated using the pertinent analyses results from QA samples (section 5.10).

5.2.6 Ship the fraction retained on the #4 sieve from each test pit to the vendor laboratory, in the 5-gallon bucket. This material shall be cleaned, crushed, and analyzed for Ra-226, Th-230 and, if necessary, Th-232. Record vendor analysis results on Attachment 1.

5.2.7 Calculate the bulk radionuclide concentration (C_b) for the test pit using the mass partition function (f) for the test pit (section 5.2.4), the vendor radiological concentration of the fines (C_{<#4;}), and the radiological concentration of the cobbles (C_{>#4;}) in the equation defined in Definition 3.5. Bulk radionuclide concentrations should be calculated for Ra-226, Th-230, and Th-232 (if necessary).

5.3 Establish background bulk radionuclide concentrations for Ra-226, Th-230, and, if necessary, Th-232, by the sampling and analyses detailed in steps 5.2.1 through 5.2.6 at three uncontaminated background locations containing cobbly subsoil of similar geologic deposition.

5.4 Statistical Mass Partition Function - Alternative 1 (Test Pits)

5.4.1 Upon completion of test pit sampling, pertinent data shall be compiled on the Statistical Data Sheet (Attachment 2), and the statistical mass partition function shall be calculated using the following equation:

$$f_L = \bar{f} - t(s/\sqrt{n})$$

where, f_L = statistical average mass partition function at the lower 95 percent confidence value,
 \bar{f} = mean mass partition functions of n samples,
 s = sample standard deviation for the n samples,
 t = t from Attachment 3, and
 n = number of observations.

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5.4.2 The mean of the sample population is determined as follows:

$$\bar{f} = \frac{f_1 + f_2 + \dots + f_n}{n}$$

where, $f_{1,2 \text{ or } n}$ = the value of f for sample 1, 2, or n ; and
 n = the number of samples.

5.4.3 The standard deviation is calculated as follows:

$$s = \sqrt{\frac{\sum_{n=1}^n (f_n - \bar{f})^2}{n - 1}}$$

where, s = sample standard deviation,
 f_n = value of f for sample n ,
 \bar{f} = mean of f for n samples, and
 n = number of samples.

5.4.4 The statistical cobble radionuclide concentration for Ra-226, Th-230 and Th-232 (if necessary) shall be calculated using the following equation:

$$C_{95} = \bar{C} + t(s/\sqrt{n})$$

where, C_{95} = The statistical cobble radionuclide concentration at the upper 95 percent confidence value,
 \bar{C} = mean radionuclide concentration of the n samples,
 s = standard deviation of the 30 samples,
 t = t from Attachment 3, and
 n = number of samples.

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5.5 Statistical Mass Partition Function Alternative 2 (Running Average)

5.5.1 The statistical mass partition function (f_L) and the statistical cobble radionuclide concentration ($C_{>u}$) may be obtained by calculating a running average of the corresponding parameters using the equations in sections 5.4.1 and 5.4.4 respectively. Compile data on the Statistical Data Sheet and recalculate f_L and $C_{>u}$ as data is obtained from each new test pit.

5.6 The statistical mass partition function and statistical cobble radionuclide concentration for alternative 1 or 2, will only be used for excavation control to obtain an estimate of the final excavation depth to comply with EPA's radiological cleanup standards. Final excavation depths and verification will be determined as described in section 5.7 through 5.9.

5.6.1 By solving the equation in section 3.5 for $C_{<#4}$ and using the statistical mass partition function (f_L) and the statistical cobble radionuclide concentration ($C_{>u}$) an estimate of the allowable fines radionuclide concentration may be obtained as follows:

$$C_{<#4} = \frac{C_B - C_{>u} [f_L / (1 + f_L)]}{[1 / (1 + f_L)]}$$

where, $C_{<#4}$ = The estimated fines radionuclide concentration,
 C_B = the applicable limit (i.e., 5 or 15 pCi/g for Ra-226 or Th-232 or 35 pCi/g for Th-230),
 f_L = statistical mass partition function, and
 $C_{>u}$ = statistical cobble radionuclide concentration.

5.7 Verification Soil Sampling & Analysis

5.7.1 Grid the entire site into squares of 100 yd² (-100 m²). Grids shall be uniformly distributed over the site so as to obtain representative data. Record location and elevation for each 100 yd² grid.

5.7.2 Further subdivide each grid where excavation control is being performed into approximately 10 x 10 foot squares (see below). Subdividing grids may normally be done visually by the technician performing the survey. Soil sample extraction will be performed at each of the nine 10 x 10 foot squares within the grid. Each soil plug should consist of all the material contained in a standard shovel. This will include soil, rock, small/large gravel and cobble. No material is to be discarded. The soil plug will be taken to a depth of 15 centimeters (cm). Sample collection shall be random (non-biased).

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(30')

0	0	0
(30')	0	0
0	0	0

0 = sample location

- 5.7.3** The nine soil plugs (80-100 lbs combined weight) comprise a composite sample.
- 5.7.4** Sieve the composite sample through a #4 mesh sieve, collecting the fines and cobbles in separate buckets of known weight. Thoroughly mix the fine fraction.

5.8 Site Verification Alternative 1 (Grid Specific)

- 5.8.1** For verification alternative 1, weigh both fractions separately and record information on Attachment 1.
- 5.8.2** Extract two (2) 500g can samples of the fine fraction for moisture content and radiological analysis.
- 5.8.3** Determine the moisture content of the fines and calculate the adjusted dry weight. Calculate the adjusted dry weight of cobbles assuming a moisture content of 1.5 percent. Calculate and record the mass partition function for the grid (Attachment 1).
- 5.8.4** Analyze the second can sample of fines for Ra-226 and, if necessary, Th-232 with the on-site OCS. Calculate the corrected radionuclide concentration using the site Ra-226 correction factor determined in section 5.2.5.1.

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5.8.5 Calculate the bulk radionuclide concentration C_B for the grid using the grid specific mass partition function, radionuclide concentration of the fines (the initial corrected concentration shall be used for calculating the Ra-226 bulk radionuclide concentration) and the statistical cobbles radionuclide concentration ($C_{>u}$) in the formula in section 3.5. All data shall be recorded on Form F1-OP-003-4.

5.8.6 Dry, seal and store the sample for 20 day on-site analysis.

5.8.7 After a minimum of 20 days, reanalyze the sample and calculate the final bulk radionuclide concentration (C_B) for the grid.

5.9 Site Verification Alternative 2 (Statistical - Running Average)

5.9.1 For each 100 m² grid, a 9-plug composite soil sample of the fines soil will be obtained following the technique outlined in Section 5.7.

5.9.2 Extract a 500g can sample of the fine fraction for radiometric analysis. Discard the larger size soil fraction.

5.9.3 Analyze the can sample for Ra-226 and, if necessary, Th-232 with the on-site OCS. Calculate the corrected radionuclide concentration using the site correction factor determined in section 5.2.5.1.

5.9.4 Calculate the bulk radionuclide concentration for the grid using the radionuclide concentration of the fines (the initial corrected concentration shall be used for calculating the Ra-226 bulk radionuclide concentration), the statistical mass partition function (f_L) and the statistical cobble radionuclide concentration ($C_{>u}$) in the formula from section 3.5 as modified below.

$$C_B = C_{<4}[1/(1 + f_L)] + C_{>u}[f_L/(1 + f_L)]$$

Record the pertinent data on the Alternative 2 Bulk Concentration Data Sheet (Attachment 4).

5.9.5 Dry, seal and store the sample for 20 day on-site analysis.

5.9.6 After a minimum of 20 days, reanalyze the sample and calculate the final bulk radionuclide concentration (C_B) for the grid.

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5.10 The verification sample from the 25th 100 m² grid of each block will be sent to an outside Vendor laboratory for independent Ra-226, Th-230, and, if necessary, Th-232 analyses in accordance with Quality Assurance requirements.

6.0 RECORDS/REPORTS/NOTIFICATIONS

6.1 All data shall be recorded on the appropriate data sheet.

7.0 ATTACHMENTS

7.1 Attachment 1 - Cobble to Fines Calculation Sheet (F1-OP-003-4)

7.2 Attachment 2 - Statistical Data Sheet (F2-OP-003-4)

7.3 Attachment 3 - Critical Values of t.

7.4 Attachment 4 - Alternative 2 Bulk Concentration Data Sheet (F4-OP-003-4)

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Attachment 1

COBBLES TO FINES CALCULATION SHEET

Site: _____

Sheet _____ of _____

Sample/Grid I.D. _____

Date: _____

Fines	Cobbles	Moisture Content Fines
Wt. Sample & Bucket _____	Wt. Sample & Bucket _____	Wet Wt. Sample/Pan _____
Wt. Bucket _____	Wt. Bucket _____	Dry Wt. Sample/Pan _____
Wt. Sample _____	Wt. Sample _____	Tare Wt. Pan _____
Adjusted _____	Adjusted _____	Wt. Water* _____
Dry Wt.(M _{<64})* _____	Dry Wt.(M _{>64})* _____	Wt. Soil** _____
		Percent Water(*/**) _____

* Adjusted Dry Wt. of the Fines = Wt. Sample x (1 - % water)

** Adjusted Dry Wt. of the Cobbles = Wt. Sample x (1 - .015)

Mass Partition function (f) = M_{>64}/M_{<64} = _____

Radiological Analysis	²²⁶ Ra (pCi/g)	²³⁰ Th (pCi/g)	²³² Th (pCi/g)	COMMENTS
Cobbles (C _{>64})				
On-Site Analysis	*			
Fines (C _{<64})	**	N/A		

Vendor Analysis				
Fines (C _{<64})				
Bulk Radionuclide Concentration (C _B)	#			
	##			
	###			

* Initial; ** Initial Corrected; *** 20 day (N/A for Test Pit or Running AVE.)

Using Vendor; ## Using Initial Corrected; ### Using 20 day (N/A for Test Pits or Running AVE.)

²²⁶Ra Correction Factor: _____

Reviewed By: _____ Date: _____

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Attachment 2

STATISTICAL DATA SHEET

Date: _____ Sheet _____ of _____
Size: _____

Statistical Mass Partition Function (f_i) =

Statistical Cobalt Radionuclide Concentration (C_{stat}) =

720Ba Correction Factor (C_E) =

Date: _____

E2-003-4

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Attachment 3

CRITICAL VALUES OF t

$n-1$	$t_{.050}$
1	6.314
2	2.920
3	2.353
4	2.132
5	2.015
6	1.943
7	1.895
8	1.860
9	1.833
10	1.812
11	1.796
12	1.782
13	1.771
14	1.761
15	1.753
16	1.746
17	1.740
18	1.734
19	1.729
20	1.725
21	1.721
22	1.717
23	1.714
24	1.711
25	1.708
26	1.706
27	1.703
28	1.701
29	1.699
inf.	1.645

FOR INFORMATION ONLY

Attachment 4

ALTERNATIVE 2 BULK CONCENTRATION DATA SHEET

Biological Analysis [Lines]

11

Rev. No.:

$$\text{Statistical Cobles Radionuclide Concentration } C_{\text{stat}} = C_{\text{stat}} [1 / (1 + f_{\text{I}}) + C_{\text{stat}} f_{\text{I}} / (1 + f_{\text{I}})] \quad \text{Statistical}$$

111

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F4-OP-003-4

**GENERIC PROTOCOL FOR THORIUM-230
CLEANUP/VERIFICATION AT UMTRA PROJECT SITES**

Generic Protocol for Thorium-230 Cleanup/Verification at UMTRA Project Sites

The excavation of materials contaminated with thorium-230 (Th^{230}) at one or more UMTRA Project sites may require extensive, deep removal of soil materials to ensure that the radium-226 (Ra^{226}) concentrations will comply with EPA's surface and subsurface soil cleanup standards (i.e., 40 CFR 192). The following discussion presents a unified approach for the future application of standards for Th^{230} at the UMTRA Sites.

1. Introduction

The cleanup of radiologically contaminated soils on UMTRA Project sites provides explicit requirements for the remediation of soils contaminated with Radium-226 (Ra^{226}), which include limits of 5 and 15 picocuries/gram (pCi/g) for the initial and successive 15 centimeter (cm) deep layers, respectively, averaged over an area of 100 m². If other radionuclides are encountered in sufficient quantities and concentrations to constitute a significant radiological hazard, the supplemental standards provisions of 40 CFR 192.21 and 40 CFR 192.22 provide guidance for performing remedial action for these radionuclides to reduce residual radioactivity to levels that are as low as reasonable achievable.

Thorium-230 (Th^{230}), which naturally decays, with a half-life of 77,000 years, to form Ra^{226} is also present in uranium mill tailings and contaminated soils. Therefore, it may be readily shown that for soils containing initial Ra^{226} and Th^{230} concentrations, at time $t=0$, of $\text{Ra}^{226}(t=0)$ and $\text{Th}^{230}(t=0)$, respectively, the Ra^{226} concentration at any later time, t , is:

$$\text{Ra}^{226}(t) = \text{Ra}^{226}(t=0) e^{-\lambda t} + \text{Th}^{230}(t=0) (1 - e^{-\lambda t}),$$

where λ is the decay constant for Ra^{226} , or 4.32×10^{-4} yrs⁻¹.

Furthermore, the geochemical behavior of Ra^{226} and Th^{230} in typical UMTRA site environments have been observed to be significantly different. Under neutral or basic soil conditions, neither Ra^{226} nor Th^{230} are preferentially mobile geochemically (i.e., both radionuclides will form chemical compounds that have similar potential for migrating into soils). However, under acidic conditions, the chemical forms taken by these radionuclides are significantly different in their potential for depth migration in soil, with Th^{230} being more mobile than Ra^{226} .

In windblown tailings areas, mill yards, and ore storage areas of UMTRA sites, it has been observed that: 1) the surface and subsurface soils are normally at neutral pH; 2) the radiological material does not contain abundant quantities of free acid; and 3) the Ra^{226} and Th^{230} concentrations are in near secular equilibrium (their activities are approximately equal). The near secular equilibrium for the radiological contamination in these areas results from the fact that most of the uranium ores processed were in near equilibrium. Therefore, the application of soil cleanup procedures for Ra^{226} according to EPA standards would also reduce the Th^{230} concentrations to acceptable levels by default, and the total Ra^{226} as a function of time will not exceed 5 or 15 pCi/g, for surface and subsurface soil respectively.

However, under acidic soil conditions that may prevail in the foundation soil under uranium mill tailings, the subpile region, or in surface and subsurface soils of raffinate or evaporation

pond, the different geochemical interactions of Ra²²⁶ and Th²³⁰ will cause these radionuclides to differentially migrate. Generally, under these conditions, Ra²²⁶ is adsorbed or co-precipitated on soil within a depth of one to two feet, and Th²³⁰ migrates deeper into the subsoil until neutralization of the transporting pore water occurs, where it is removed from solution by the formation of insoluble precipitates or co-precipitates (thorium or thoro-ferro hydroxides, for example). For example, at the Spook, Wyoming site, Th²³⁰ differentially migrated as deep as 20 feet below the raffinate pond before being stabilized by neutralization. In order to be in harmony with the supplemental standards provisions to reduce Th²³⁰ concentrations to as low as reasonably achievable (ALARA), and to come as close to meeting otherwise applicable standards as is reasonable under the circumstances, an excavation depth less than 20 feet was selected as a viable solution for this site.

It may be concluded that the cleanup of the initial Ra²²⁶ contamination according to standards does not necessarily mitigate against the ultimate ingrowth of residual Ra²²⁶ with time due to the radioactive decay of residual Th²³⁰ in all areas within a site. As a consequence, residual Ra²²⁶ concentrations at a later date, due to ingrowth from Th²³⁰ contamination, may pose an undesirable health hazard. Therefore, the supplemental standards provision of 40 CFR 192 requires the development of a cleanup criterion for Th²³⁰, which is health protective by reducing exposures to levels that are ALARA, keeping in consideration the measures necessary to implement the remedial actions under the circumstances that exist at the site. The following procedure establishes appropriate remedial action concentration limits for Th²³⁰, and is proposed to be implemented at UMTRA Project sites after concurrence from all governing agencies involved with activities at each site agree to its implementation.

2. Generic Protocol

As can be seen from the equation presented in the introduction, the overall 1000-year maximum concentration of Ra²²⁶ in the soils will either be equal to the present Ra²²⁶ inventory (if Th²³⁰ concentrations are equal to or less than Ra²²⁶ concentrations), or the total Ra²²⁶ inventory one thousand years in the future (if Th²³⁰ concentrations exceed Ra²²⁶ concentrations). If Ra²²⁶ concentrations are equal to or exceed Th²³⁰ concentrations, the site will already meet the Th²³⁰ supplemental standard by default when the site is remediated to the 40 CFR 192 standards for Ra²²⁶.

- (1) Therefore, the supplemental standard chosen for Th²³⁰ needs only to ensure that the overall Ra²²⁶ concentration one thousand years in the future, when averaged over 100 square-meter areas, will not exceed either 5 pCi/g in the first 15 cm layer or 15 pCi/g in successive 15 cm layers.

It should be noted that the Ra²²⁶ concentrations are considered to be bulk concentrations, as determined by the recently developed, NRC-approved protocol for excavation control and soil verification of cobbly subsoils.

2.1 Protocol for Contamination at Depth

As the depths of excavations become deeper to remove elevated Th²³⁰, the thickness of overlying fill material that is eventually used to remediate the site will increase. As a result, attenuation of radon-222 (Rn²²²) diffusing through the overlying fill material will also increase.

Therefore, as the overlying clean fill material thickness increases, the resultant attenuation of the radon generated from the associated ingrowth of Ra²²⁶ will allow higher residual concentrations of Th²³⁰ to be left in place, while still attaining a level of protection equivalent to the intent of the Ra²²⁶ soil cleanup standards. To determine this concentration, the NRC model (presented in the Draft Generic Environmental Impact Statement on Uranium Milling; NUREG-0511; April 1979) can be used to determine the radon-222 (Rn²²²) flux that would produce 0.02 Working Levels (WL) in a hypothetical structure built on a 100 square-meter (m²) grid. The following equation was used:

$$C = FAB/(VR \cdot 1000), \text{ where:}$$

C = Rn²²² concentration (pCi/l)
F = Rn²²² flux (pCi/m²·s)
A = Area over which the flux enters (m²)
B = Flux reduction factor for entering structure (unitless)
V = Volume of the structure (m³)
R = Effective Rn²²² removal rate (s⁻¹)
1000 = conversion factor (l/m³)

In areas where basements are feasible (based on local construction practices and deep groundwater table), it should be assumed that the thickness of fill material is eight feet less than the depth of the excavation. Using A = 103m², B = 0.5, V = 250m³, and R = 1.98x10⁻⁴ s⁻¹, a flux of 3.9 pCi/m²·s would produce indoor air concentrations of approximately 4.0 pCi/l Rn²²². Assuming radon daughters are present at 50% equilibrium, this would correspond to 0.02 WL.

(2) Thus, the RAECom computer code can be used to calculate the resultant flux from higher concentrations at depth as one factor to consider in determining if further excavation is warranted. As long as the calculated flux is less than 3.9 pCi/m²·s, it can be assumed that equivalent protection is provided as long as the backfill thickness is maintained. Therefore, the analysis will consider the potential future (at least 200 years) erosion and land use in the determination of excavation depth. The calculations shall use site-specific parameters when available. Reasonably conservative parameters that consider the expected site conditions shall be used when site-specific data are unavailable. Selection on backfill materials with superior (low) diffusion coefficients may be included in the ALARA considerations of the design. When evaluating this option for the Th-230 supplemental standard, considerations of the construction hazards to remedial action workers and the feasibility of the anticipated construction requirements should be taken into account.

2.2 Protocol for Contamination in the Saturated Zone

Another scenario potentially impacting excavations to remove elevated Th²³⁰ concentrations is when groundwater is encountered at shallow depths. Since the Th²³⁰ contamination has been present within the saturated zone long enough for soluble constituents to have been mobilized, it is reasonable to assume that any remaining Th²³⁰ that may be encountered within a saturated zone will not be appreciably mobilized by pH neutral groundwater. Furthermore, it is known that the diffusion coefficient decreases dramatically as soils approach full

saturation until it reaches values typical of water (Radon Attenuation Handbook for Uranium Mill Tailings Cover Design; NUREG/CR-3533; April 1984). It is therefore reasonable to assume that Rn²²² generated within a saturated zone generally will not diffuse to the surface. Finally, it is very difficult to perform deep, cost effective excavations within a saturated zone.

(3) Therefore, whenever shallow groundwater is encountered, the following options will be considered:

- (a) Excavation into the saturated zone will be considered when water pumping or other controls are reasonable and when high concentrations of Th²³⁰ extend only a short distance into the saturated zone.
- (b) An ALARA analysis will be performed in cases where a major portion of the site contains Th-230 which extends into the saturated zone, and excavation into the zone is impractical. The ALARA analysis will use reasonably conservative assumptions to project future doses. If water pumping or other controls are not reasonable, excavation will halt at the level of the water table (a nominal extra foot of excavation may be considered so long as it does not require pumping/dewatering).

3. Verification Sampling

Under typical site conditions, verification of the Th²³⁰ supplemental standard is to be achieved by a three-tiered sampling approach.

- (4) In areas within an UMTRA processing site that are suspected of preferentially mobilizing thorium contamination over radium contamination (e.g., under raffinate pits), based upon process knowledge or other sources such as previous sampling data, 100% of the grids are to be sampled and analyzed for Th²³⁰.
- (5) In subpile areas, 10% of the grids will be sampled.
- (6) In areas where process knowledge and characterization data indicates no potential for preferential mobilization (e.g., windblown tailings), grids will not be sampled for Th²³⁰.

An analysis of verification data from the Tuba City, Arizona, UMTRA site, which has completed remediation and used this strategy, found no instances in the area sampled at the rate of 1 out of 25 grids where Th²³⁰ concentrations would cause future (i.e., at t = 1000 years) expected Ra²²⁶ concentrations to exceed 40 CFR 192 standards for Ra²²⁶. Furthermore, preliminary results confirm the expectation that Th²³⁰ concentrations are generally equal to or less than Ra²²⁶ concentrations in areas other than beneath the raffinate pits, and Ra²²⁶ concentrations are well correlated to Th²³⁰ concentrations in these areas.

If any verification samples exceed the Th²³⁰ criteria of this protocol, the surrounding eight grids will be examined to determine whether or not these grids also exceed the criteria. If sample results have not been generated for the surrounding grids already, archived samples of such grids will be analyzed. If any of the surrounding grids also exceed the Th²³⁰ criteria,

the surrounding eight grids around such grids will also be examined. This process will continue until no more of the surrounding grids exceed the Th²³⁰ criteria. All grids that exceed the criteria will undergo further remediation unless there is sufficient justification and concurring parties agreement to do otherwise.

4. Conclusion

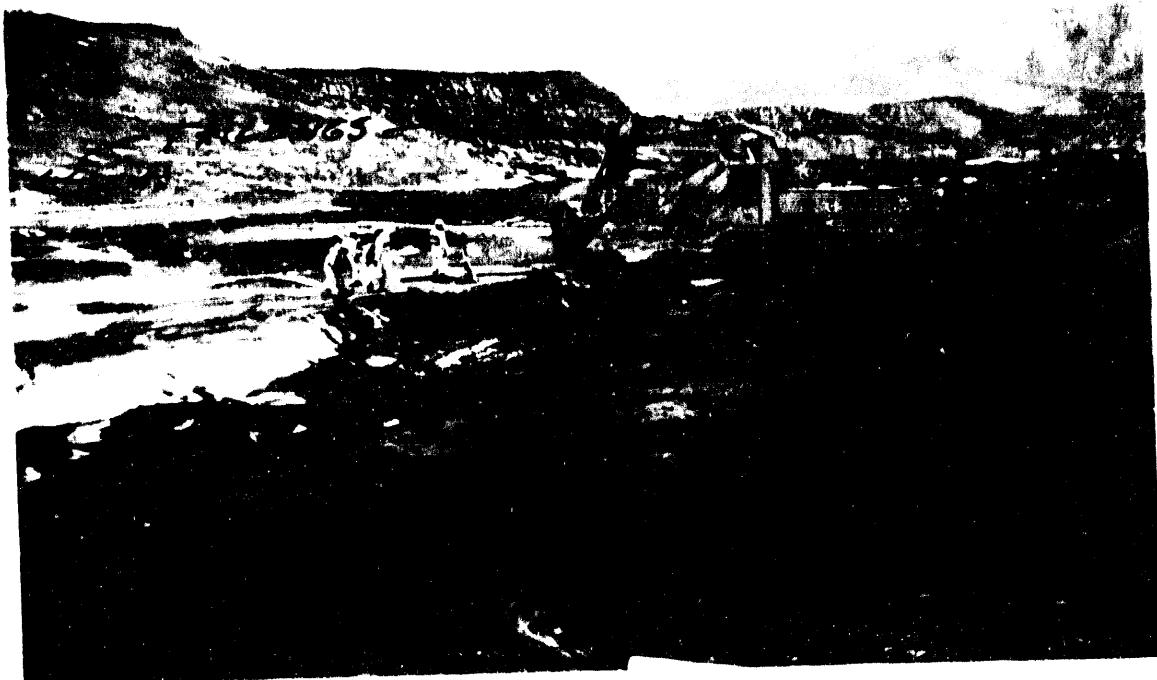
Based upon the above discussions, the following generic protocol shall be used for the excavation of Th²³⁰ at all future UMTRA Project sites:

- (1) Excavate bulk Th²³⁰ to a 1000-year corrected bulk Ra²²⁶ concentration of 5 or 15 pCi/g (as appropriate) in 15-cm layers;
- (2) For deeply buried material, stop excavations when the RAECOM computer code, using site-specific parameters, calculates a Rn²²² flux of 3.9 pCi/m²-s and expected long-term conditions are appropriate or when construction safety or feasibility become a concern;
- (3) Consider the following options whenever shallow groundwater is encountered:
 - (a) Excavate into the saturated zone when water pumping or other controls are reasonable, especially when high concentrations of Th²³⁰ extend only a short distance into the saturated zone.
 - (b) An ALARA analysis will be performed in cases where a major portion of the site contains Th-230 which extends into the saturated zone, and excavation into the zone is impractical. The ALARA analysis will use reasonably conservative assumptions to project future doses. Halt excavations at the level of the water table when water pumping or other controls are not reasonable (a nominal extra foot of excavation may be considered so long as it does not require pumping/dewatering).
- (4) Perform verification sampling for bulk Th²³⁰ in all grids underneath raffinate pits or other areas suspected of having a mechanism to preferentially mobilize Th²³⁰ over Ra²²⁶;
- (5) Perform verification sampling for bulk Th²³⁰ in 10% of the grids underneath sub-pile areas; and
- (6) Do not perform verification sampling for bulk Th²³⁰ in grids for which process knowledge and characterization data indicates no potential for preferential migration.
- (7) When practical, delay backfilling until verification results are obtained.

APPENDIX B
PHOTOGRAPHS OF TEST PITS AND OPERATIONS

**PHOTOS OF FIELD SAMPLING
AND GRADATION DETERMINATION**

3/5



Test Pits were located around the perimeter of the tailings pile and in areas where the tailings have been removed.

2/2)



Test Pit Locations



Excavation depths were measured using a survey rod.



Depth of test pit is measured upon completion of the pit.



Samples for radiological analysis were collected from test pit walls.



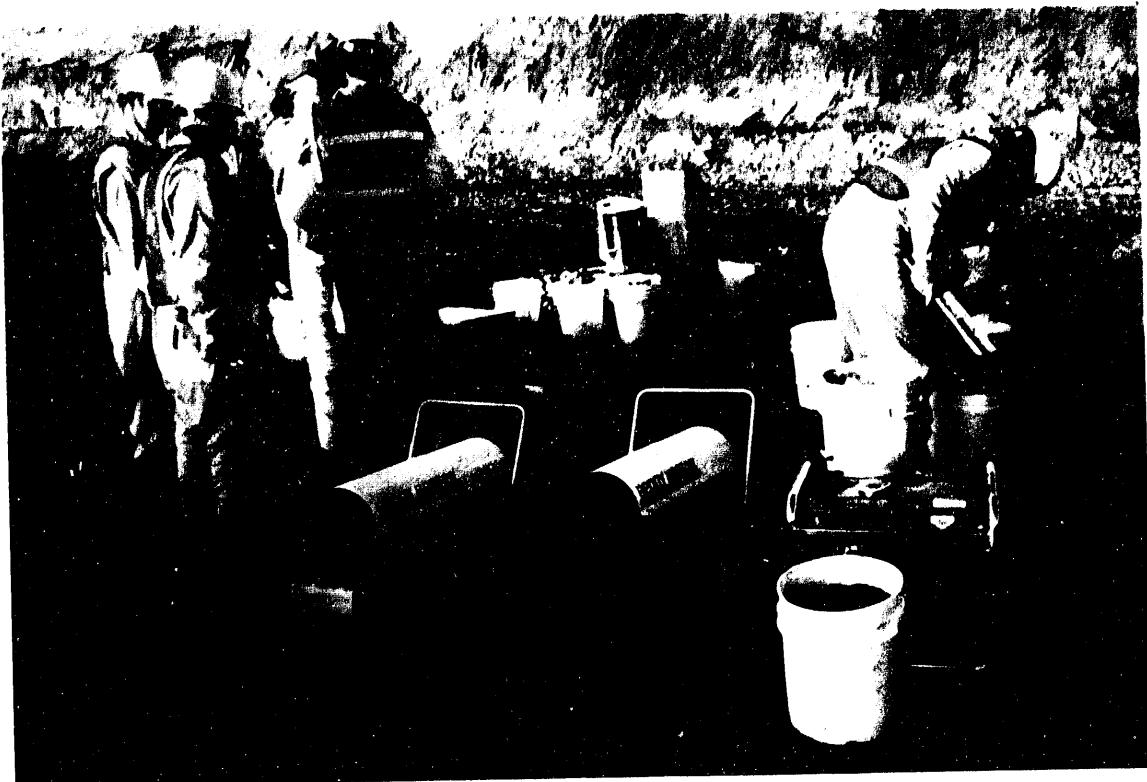
Samples of the gravel were taken for determination of radioactivity.



Gravel samples were collected in one-foot intervals and placed on plastic sheets in order to carry out the gradation analysis.



Sample of sand gravel and cobbles taken from the test pits.



Drying and screening gravel (Cobbles and Fines) samples.



Sample too wet to screen (See photo above).



Screening semi-dry samples.



Screening and weighting gravel samples in order to determine the cobbles to fines ratio.

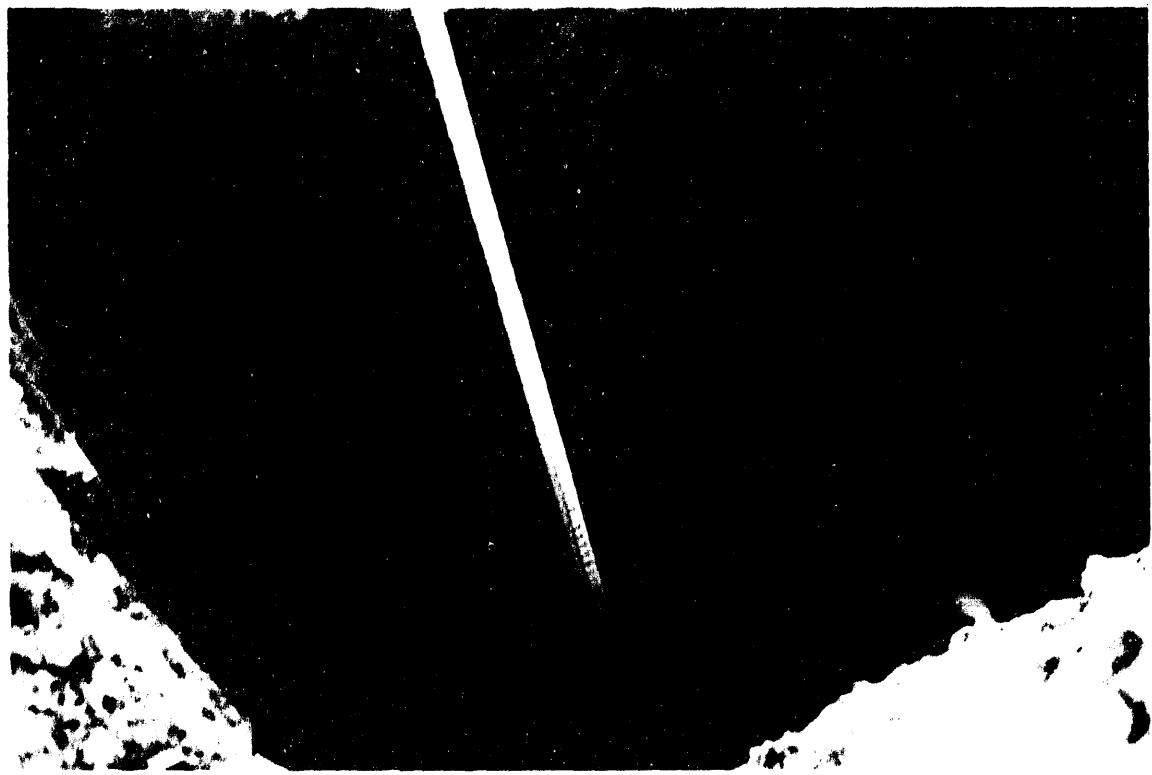
PHOTOS OF TEST PITS



TP M-CF-01. Clay-silt soil overlying gravel deposits.



TP M-CF-01. Note organic rich clay layer above gravel deposit.



TP M-CF-01. Note sands, gravels, cobbles and boulders in the bottom of the test pit. Note the carbonaceous coating on the gravels and the film on the water surface.



TP M-CF-02. Note highly carbonaceous (peat) layer.





TP M-CF-03. Bottom of
test pit. Note film on
surface of the ground
water.



TP M-CF-03. Very dry
soil overlaying gravels.
Note black carbonaceous
coating on gravels.



3/13



TP M-CF-04. The top five feet of the test pit is in tailings. Personnel are collecting tailings samples for radiological analysis.



TP M-CF-04. Soil profile beneath tailings with gravels in the bottom.

TP M-CF-05. Test pit profile showing lavender colored tailings on top of the original vegetated ground surface. Bottom of test pit shows gravels with a black carbonaceous coating.





TP M-CF-06. Lavender and yellow tailings overlying clayey soil.
Bottom of test pit shows slightly carbonaceous gravels.



TP M-CF-07. Tailings overlying clay soil and gravels. Perched water in the tailings and equipment vibration caused severe caving of the tailings resulting in contamination of samples from the underlying material.



TP M-CF-11. Excavation at old collection pond. Note oxidized and acidified upper sediments (yellow pockets) of tailings. Gravels are highly organic (carbonaceous).



TP M-CF-11. Sample of highly carbonaceous gravels and cobbles.

3/4



TP M-CF-15. Excavation at North end of old acid pond.

3/3



TP M-CF-15. Pond sediments overlying tailings which overlie clay soil in the bottom of the test pit.



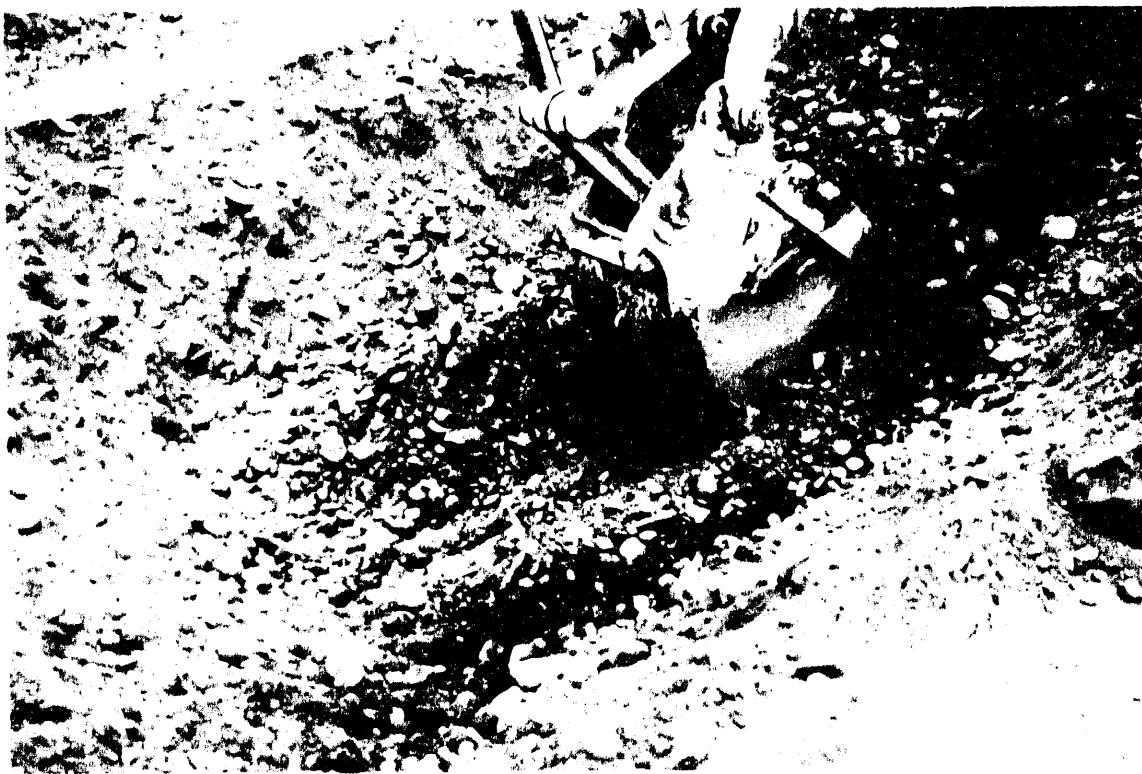
TP M-CF-19. Below 5 feet, the backhoe bucket encountered refusal on a cemented layer of gravels and cobbles.



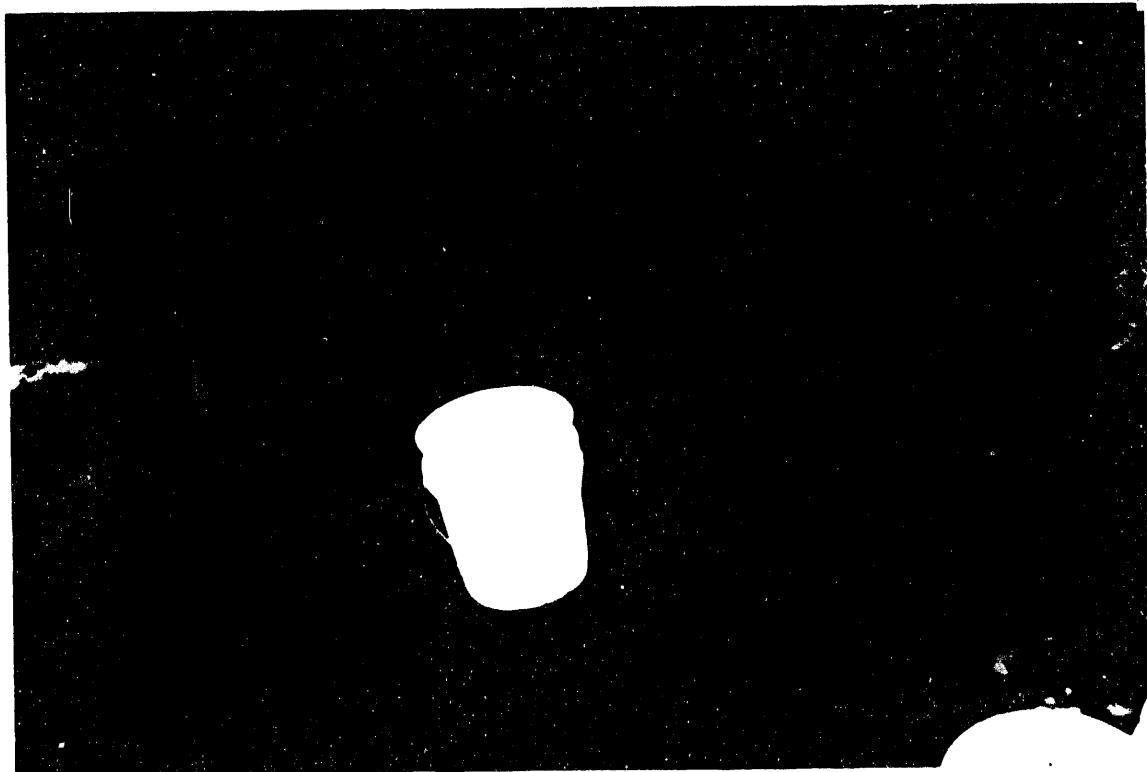
TP M-CF-20. Beginning excavation. Note one inch of tailings on the surface.



TP M-CF-20. Bottom of test pit in sand, gravel and cobbles. Ground water encountered at a shallow depth.



TP M-CF-22. About 4-feet of road fill overlying the in-situ cobbles and gravels.



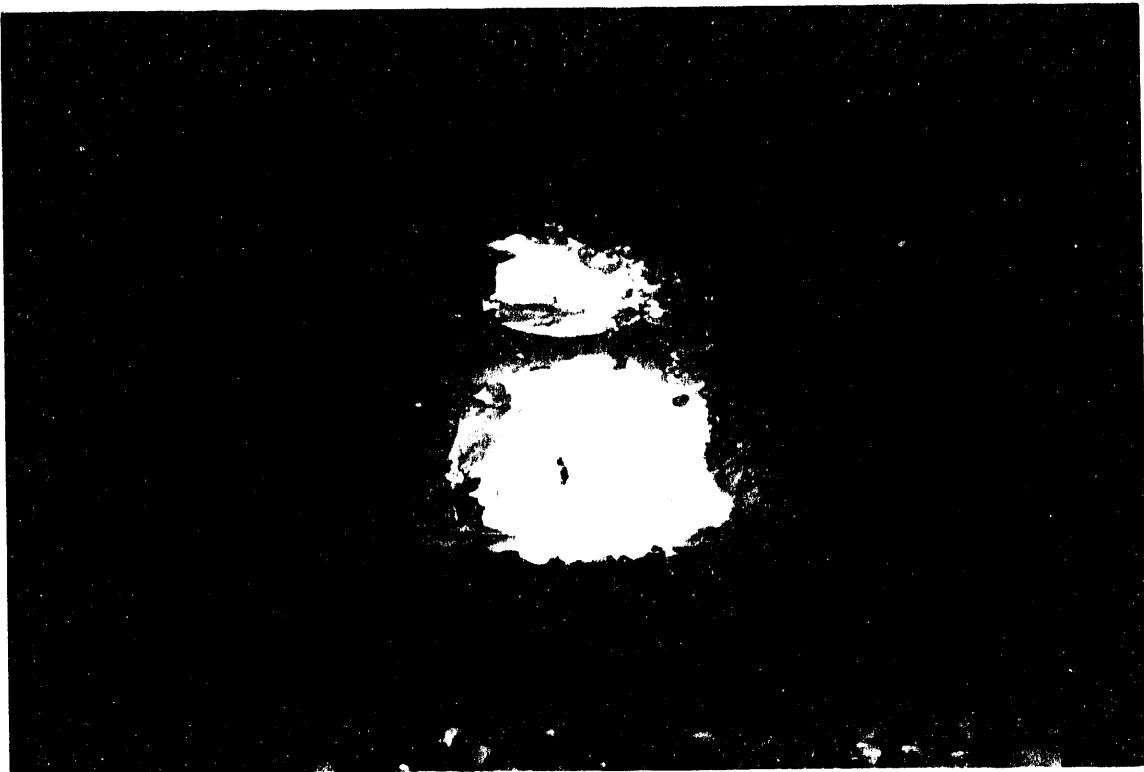
TP M-CF-22. Sample of cobbles and boulders with a carbonaceous coating.



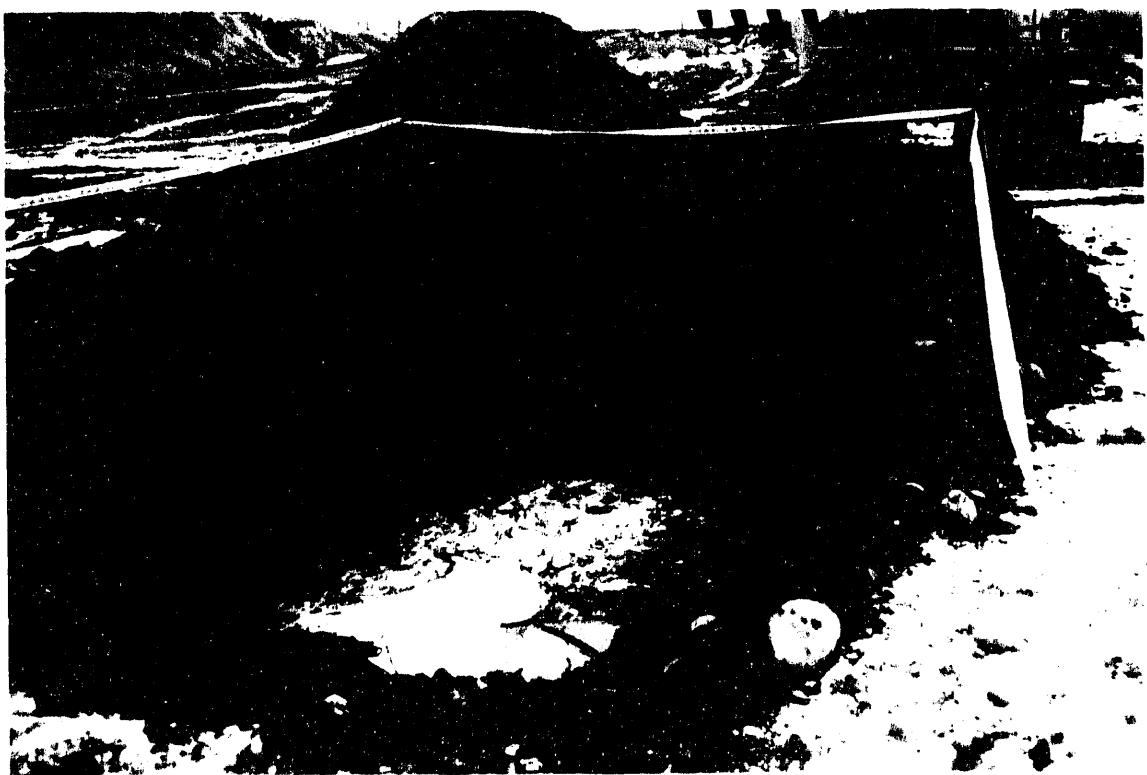
TP M-CF-25. Unsuccessful attempt to dewater the pit to allow collection of samples below the water table.



TP M-CF-25. Sample obtained from below the water table (Note how fines have been removed by the flushing action of the water when the water drains out of the sample).



TP M-CF-26. Water encountered at the interface of the soil overburden and the underlying cobbles and gravels.



TP M-CF-26. Water level two hours after excavation.



TP M-CF-27. About 4 feet of fill and wood trash overlying tailings.
Bottom of the test pit is in gravels and cobbles.



TP M-CF-28. Entire test pit in gravel, cobbles, and boulders. Black organic coating at 3 feet.



TP M-CF-29. Gravels, cobbles, and boulders overlying a clay layer.
Water encountered near the interface.



TP M-CF-31. Sand gravel and cobbles in a background pit.

APPENDIX C
TEST PIT LOGS

TEST PIT LOG

PROJECT UMTRA			SITE RIFLE	LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-01	
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N25130E46890	BEGUN 11/30/93	COMPLETED 11/30/93	GROUND ELEV. 5275.0	GROUND WATER DEPTH (FT) 16.5	LOGGED BY: J.CERCONE/G.LINDSEY	
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	RA-226 pCi/gr	TH-232 pCi/gr	TH-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
1	SS-2242		SILTY CLAY, (CL), low to medium plasticity, brown, dry to moist, vertical roots.	24.0	2.2				
2	SS-2243			5.5	1.6				
3	SS-2244			4.3	1.8	10±1			FINES: Ra-226 (1,000 year) = 6.3 pCi/gr.
4	SS-2245		Some calcite casts and stringers at 2 to 4 feet.	2.5	1.1				
5	SS-2246			5.9	1.4				PVC pipe at 4 feet connecting two adjacent sumps.
6	SS-2247			1.9	1.8	3.8±0.8			FINES: Ra-226 (1,000 year) = 2.6 pCi/gr.
7	SS-2248			1.4	1.8				-Plan Exc. Depth at 6.0'.
8	SS-2249			1.7	1.7				
9	SS-2250		CLAY-SILT, (CL-ML), low plasticity, dark gray brown, moist, becoming more clayey with depth.	1.5	2.0				Heavy odor.
10	SS-2251			1.3	1.3				
11	SS-2252			2.0	1.5				
12	SS-2253			1.6	1.5				
13	SS-2254			0.9	1.6		9.5		
14	SS-2255		ORGANIC CLAY, (OL), dark gray to black, moist to saturated.	1.8	1.9	4.5±0.9			FINES: Ra-226 (1,000 year) = 2.7 pCi/gr. Strong odor.
	SS-2256		GRAVELS, (GW), with cobbles to 12", well graded, approx. 30-35% fines, cobbles are	2.0	1.6		9.6		
	SS-2257			0.9	1.7				
								SHEET 1 OF 2	TEST PIT NO. M-CF-01
 MORRISON KNUDSEN CORPORATION ENVIRONMENTAL SERVICES DIVISION									

TEST PIT LOG

PROJECT UMTRA			SITE RIFLE	LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-01			
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N25130E46890	BEGUN 11/30/93	COMPLETED 11/30/93	GROUND ELEV. 5275.0	GROUND WATER DEPTH (FT) 16.5	LOGGED BY: J.CERCON/G.LINDSEY			
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		RA-226 pCi/gr	TH-232 pCi/gr	TH-230 pCi/gr	pH	WATER DEPTH FT	REMARKS PHOTOGRAPH	
16	SS-2258		coated with a black organic stain.		1.0	1.4	0.9±0.4		▼	FINES: Ra-226 (1,000 year) = 0.1 pCi/gr. Strong organic odor. Film of organic matter on top of ground water.	
	SS-2259				0.9	1.6					
	SS-2260				1.3	1.4		9.0			
	SS-2261				0.9	1.2					
			BOTTOM OF TEST PIT AT 17.5'							COBBLES (Composite): Sample Depth 15' to 17'. Ra-226 Th-232 Th-230 Ra-226(1,000 yr) 1.1±0.6 1.1±0.4 FINES (Composite): Sample Depth 15' to 17'. Ra-226 Th-232 Th-230 Ra-226(1,000 yr) 4.6±1.1 3.1±0.7 +#4 sieve = 83.1% -#4 sieve = 16.9%	
										SHEET 2 OF 2	TEST PIT NO. M-CF-01



MORRISON KNUDSEN CORPORATION
ENVIRONMENTAL SERVICES DIVISION

TEST PIT LOG

PROJECT UMTRA			SITE RIFLE	LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-02	
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N25130 E47190	BEGUN 12/2/93	COMPLETED 12/2/93	GROUND ELEV. 5274.6	GROUND WATER DEPTH (FT) 15.0	LOGGED BY: J.CERCOME/G.LINDSEY	
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATE	REMARKS PHOTOGRAPH
1	SS-2492		SILTY CLAY, (CL), low plasticity, med. brown, slightly moist to dry, some roots.	2.2	1.3				Upper 6" frozen ground. Soil profile appears to represent several periods of deposition (Paleo Soils).
2	SS-2493			1.1	1.6				
3	SS-2494			1.9	2.8	1.0±0.4			FINES: Ra-226 (1,000 year) = 1.6 pCi/gr.
4	SS-2495			3.0	2.2				
5	SS-2496			1.0	1.8				
6	SS-2497			1.1	1.8				-Plan Exc. Depth at 5'.
7	SS-2498		SILT, (ML), low plasticity, reddish brown, moist, loose.	1.3	1.5				
8	SS-2499			2.3	1.6	9.2			
9	SS-2500		SILTY CLAY, (CL), low plasticity, gray to black, moist, abundant organic material (carbonaceous).	1.5	1.6				Strong aromatic odor.
10	SS-2501			1.4	1.2				
11	SS-2502			0.6	1.3				
12	SS-2503			1.3	1.7				
13	SS-2504			1.7	1.3				
	SS-2505		PEAT, organic material layer.	1.4	1.3	9.3			
	SS-2506		GRAVELS, (GM), 2.5" max., poorly graded in a silty matrix.	2.0	1.5				
	SS-2507			1.2	1.4				
	SS-2508			1.8	1.5				



MORRISON KNUDSEN CORPORATION
ENVIRONMENTAL SERVICES DIVISION

SHEET
1
OF
2

TEST PIT NO.
M-CF-02

TEST PIT LOG

PROJECT UNTRA				SITE RIFLE	LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-02		
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N25130 E47190	BEGUN 12/2/93	COMPLETED 12/2/93	GROUND ELEV. 5274.6	GROUND WATER DEPTH (FT) 15.0	LOGGED BY: J.CERCONE/G.LINDSEY			
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH	
15	SS-2509		GRAVELS, (GP), with cobbles to 12", poorly graded in a sandy matrix (20-50%) cobbles average 3"-6" (30-35%).		1.1	1.3	9.2			Film of organic matter on water surface (gas bubbling up to surface).	
	SS-2510				1.8	1.6					
	SS-2511				1.1	1.5					
	SS-2512				1.4	1.3					
	SS-2513				1.0	1.8					
	SS-2514				1.4	1.9					
	SS-2515				1.1	1.4					
	SS-2516				1.6	1.5					
	SS-2517				1.8	1.3					
16	SS-2518		BOTTOM OF TEST PIT AT 18.0'		1.7	1.3				COBBLES (Composite): Sample Depth 13' to 16'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 0.7 ± 0.5 0.9 ± 0.4 FINES (Composite): Sample Depth 13' to 16'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 1.7 ± 0.7 2.3 ± 0.6 +#4 sieve = 68.3% -#4 sieve = 31.7%	
									SHEET 2 OF 2	TEST PIT NO. M-CF-02	



TEST PIT LOG

PROJECT			SITE		LOCATION			JOB NO.	TEST PIT NO.		
UMTRA			RIFLE		NEW RIFLE, COLORADO			3885-70	M-CF-03		
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:			
GREEN		BACKHOE	N25170 E47450	12/2/93	12/2/93	5278.4	21.0	J.CERCONE/G.LINDSEY			
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION			RA-226 pCi/gr	TH-232 pCi/gr	TH-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
1			<u>POND SEDIMENT</u> , silt in a CaCO ₃ matrix, buff colored with a surface covering of 2"-3" of yellowish slimy sand.								
2	SS-2519		<u>SILTY CLAY</u> , (CL), low plasticity, light brown, dry, roots (trace).			1.4	1.5		5.7		
3	SS-2520					2.0	1.5	4.1±0.8			FINES: Ra-226 (1,000 year) = 2.7 pCi/gr.
4	SS-2521					2.0	1.7		8.8		
5	SS-2522		Sandy silt, light brown, dry.			9.8	1.6				-Plan Exc. Depth at 5' to 6'.
6	SS-2523					1.5	1.3				
7	SS-2524		Silty-clay, low plasticity, med. brown, slightly moist.			1.1	1.5				
8	SS-2525					1.4	1.4		8.8		
9	SS-2526					1.3	1.3		8.8		
10	SS-2527					1.3	1.5				
11	SS-2528		<u>CLAY</u> , (CL), med. to low plasticity, brown, moist, 4" to 6" thick layers.			1.2	1.4				
12	SS-2529					1.4	1.4				
13	SS-2530		Interlayered seams of sand and silt.			0.9	1.4				
14	SS-2531					1.2	1.3				
								SHEET 1 OF 2	TEST PIT NO. M-CF-03		



MORRISON KNUDSEN CORPORATION
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TEST PIT LOG



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SHEET
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OF
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TEST PIT NO.

TEST PIT LOG

PROJECT UMTRA			SITE RIFLE			LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-04	
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N24890 E46900	BEGUN 11/30/93	COMPLETED 11/30/93	GROUND ELEV. 5274.5	GROUND WATER DEPTH (FT) 16.5	LOGGED BY: J.CERCONE/G.LINDSEY			
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION			Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
1			TAILINGS, (ML-SP), silty sand, gray to reddish brown, moist, yellowish-brown seam (1.0 ft thick).						5.45		pH Depth: 1'-4'.
2			Color changed to gray with brown spots.								
3											
4											
5	SS-2267		CLAY, (CL), low plasticity, (TOPSOIL), brown, moist to wet.			85.0	3.7				Vegetation visible at interface.
6	SS-2268					92.0	4.0	32±2.0			FINES: Ra-226 (1,000 year) = 71.0 pCi/gr.
7	SS-2269					1.2	1.4				
8	SS-2270		Saturated (Perched water?).			44.0	2.2				
9	SS-2271		Gypsum stringers.			1.6	1.4				
10	SS-2272					13.0	1.9	7.6±1.1			FINES: Ra-226 (1,000 year) = 11.1 pCi/gr.
11	SS-2273					12.0	1.8				
12			SILTY GRAVEL, (GM), aromatic organic odor, some organic coating.						8.1		
13	SS-2274		GRAVELS, (GW-GP), with cobbles and boulders to 16".			2.7	1.6				-Plan Excav. Depth 13'.
14	SS-2275					2.1	1.5				
	SS-2276					* 10.0	1.8				
	SS-2277					* 14.0	1.8				



MORRISON KNUDSEN CORPORATION
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TEST PIT NO.
M-CF-04

TEST PIT LOG

PROJECT UMTRA				SITE RIFLE		LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-04
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N24890 E46900	BEGUN 11/30/93	COMPLETED 11/30/93	GROUND ELEV. 5274.5	GROUND WATER DEPTH (FT) 16.5	LOGGED BY: J.CERCONE/G.LINDSEY		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
16	SS-2278	[REDACTED]			2.7	1.6			▼	* Possible cross contamination.
	SS-2279	[REDACTED]			3.2	1.2				
	SS-2280	[REDACTED]			* 11.0	1.3				
	SS-2281	[REDACTED]			* 10.0	1.4				
	SS-2282	[REDACTED]			* 28.0	2.4				
	SS-2283	[REDACTED]			* 51.0	2.5				
	SS-2284	[REDACTED]			* 15.0	1.7		7.8		
19			BOTTOM OF TEST PIT AT 19.0'							



MORRISON KNUDSEN CORPORATION

ENTERTAINMENT SERVICES DIVISION

SHEET

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TEST PIT NO.

M-CF-04

TEST PIT LOG

PROJECT UMTRA			SITE RIFLE		LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-04A		
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N24890 E46900	BEGUN 11/30/93	COMPLETED 11/30/93	GROUND ELEV. 5274.5	GROUND WATER DEPTH (FT) 16.5	LOGGED BY: J.CERCONE/G.LINDSEY			
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH	
1											
2											
3											
4											
5			Not Logged See Test Pit M-CF-04. This test pit was dug to collect uncontaminated samples between 11' and 17'.								
6											
7											
8											
9											
10											
11	SS-2463		<u>SILTY GRAVEL</u> , (GM), aromatic organic odor, some organic coating.		8.5	1.6					
12	SS-2464				11.0	2.0	9.3±1.2			FINES: Ra-226 (1,000 year) = 10.4 pCi/gr.	
13	SS-2465				17.0	2.0		8.1			
14	SS-2466		<u>GRAVELS</u> , (GW-GP), with cobbles and boulders to 16".		17.0	1.5				-Plan Excav. Depth 13'.	
	SS-2467				9.2	1.9					
	SS-2468				11.0	1.4					
	SS-2469				3.2	1.5					
	SS-2470				4.2	1.5					
										SHEET 1 OF 2	TEST PIT NO. M-CF-04A



MORRISON KNUDSEN CORPORATION
ENVIRONMENTAL SERVICES DIVISION

TEST PIT LOG

PROJECT UMTRA				SITE RIFLE		LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-04A
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N24890 E46900	BEGUN 11/30/93	COMPLETED 11/30/93	GROUND ELEV. 5274.5	GROUND WATER DEPTH (FT) 16.5	LOGGED BY: J.CERCONE/G.LINDSEY		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
	SS-2471				1.9	1.5				
16	SS-2472				2.4	1.6			▼	
	SS-2473				2.4	1.1				
	SS-2474				2.1	1.2				
17										
18										
19			BOTTOM OF TEST PIT AT 19.0'							COBBLES (Composite): Sample depth 11' to 16'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 0.6±0.5 0.7±0.3 FINES (Composite): Sample depth 11' to 16'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 7.4±1.4 6.6±1.0 +#4 sieve = 76.1% -#4 sieve = 23.9%



TEST PIT LOG

PROJECT UMTRA			SITE RIFLE	LOCATION NEW RIFLE, COLORADO				JOB NO. 3885-70	TEST PIT NO. M-CF-05	
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N24890 E47140	BEGUN 11/30/93	COMPLETED 11/30/93	GROUND ELEV. 5273.7	GROUND WATER DEPTH (FT) 18.0	LOGGED BY: J.CERCON/G. LINDSEY		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		RA-226 pCi/gr	TH-232 pCi/gr	TH-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
1			TAILINGS, (SM), silty sand, gray, moist to saturated, with interbedded 6" to 8" thick layers of slimes.					5.0		pH Depth: 1'-6'.
2										
3										
4										
5										
6			5.5'-6.0' Slime layer lavender color, saturated.							
7										
8										
9			CLAY, (CL), low plasticity, brown, moist, dry vegetation and roots.							Vegetation visible at interface.
10										
11	SS-2295				3.0	1.8		4.9		
12	SS-2296		SANDY SILT, (ML), dark brown, with some roots.		1.3	1.8	1.2±0.5	7.4		FINES: Ra-226 (1,000 year) = 1.3 pCi/gr.
13	SS-2297		CLAY, (CL), black, moist to saturated, carbonaceous.		1.8	1.6				-Plan Exc. Depth at 13'.
14	SS-2298				1.1	1.9				
15	SS-2300		Silty clay, light brown, thinly bedded.		1.1	1.6				
16	SS-2301		GRAVELS, (GP), with cobbles to 6'.		1.6	1.2		7.2		COBBLES (Composite): Sample Depth 16' to 21'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 1.4±0.6 0.3±0.2
17	SS-2302				5.5	1.3				FINES (Composite): Sample Depth 16' to 21'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 2.5±0.8 2.3±0.6
18	SS-2304				5.7	1.3				+#4 sieve = 77.6%
19	SS-2305				1.1	1.1				-#4 sieve = 22.4%
20	SS-2306				1.3	1.1				
	SS-2307				4.1	1.2				
	SS-2308				3.6	1.4				
	SS-2309				3.1	1.1				
			BOTTOM OF TEST PIT AT 20.0'							
								SHEET 1 OF 1	TEST PIT NO. M-CF-05	



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ENVIRONMENTAL SERVICES DIVISION

TEST PIT LOG

PROJECT UMTRA				SITE RIFLE		LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-06
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N24890 E47380	BEGUN 11/30/93	COMPLETED 11/30/93	GROUND ELEV. 5276.8	GROUND WATER DEPTH (FT) 18.8	LOGGED BY: J.CERCON/G.LINDSEY		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
1			TAILINGS, (SM), silty sand, gray, moist, loose, several seams and pockets of green slimes.							
2										
3										
4								5.0	pH Depth: 1'-8'.	
5										
6										
7			Becoming pale yellow.							
8										
9										
10										
11										
12								5.0	pH Depth: 8'-15'.	
13			Original ground surface. <u>SANDY CLAY</u> , (CL), brown, moist.							
14	SS-2310				2.3	1.4	1.6±0.5		FINES: Ra-226 (1,000 year) = 2.1 pCi/gr.	
									SHEET 1 OF 2	TEST PIT NO. M-CF-06



MORRISON KNUDSEN CORPORATION
ENVIRONMENTAL SERVICES DIVISION

TEST PIT LOG

PROJECT UMTRA			SITE RIFLE		LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-06		
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N24890 E47380	BEGUN 11/30/93	COMPLETED 11/30/93	GROUND ELEV. 5276.8	GROUND WATER DEPTH (FT) 18.8	LOGGED BY: J.CERCONE/G.LINDSEY			
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH	
16			GRAVELS, (GP), with cobbles to 6', sand matrix of 30%-40% fines, average size cobble is 3"-4", max. cobble size is 8".							-Plan Exc. Depth 16'.	
17											
18											
19											
20											
21										Water rose to this level after pit was excavated. (Free water was not encountered during excavation to 25').	
22											
23											
24	SS-2313				* 85.0	3.0	6.5			pH Depth: 20'-25'.	
25	SS-2314		BOTTOM OF TEST PIT AT 25.0'		* 41.0	2.5	6.5			* Possible Cross Contamination.	
COBBLES (Composite): Sample Depth 18' to 22'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 3.3_{0.9} 1.6_{0.5}										SHEET 2 OF 2	TEST PIT NO. M-CF-06



MORRISON KNUDSEN CORPORATION
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TEST PIT LOG

PROJECT UMTRA			SITE RIFLE	LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-07	
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N24850 E47500	BEGUN 12/2/93	COMPLETED 12/2/93	GROUND ELEV. 5277.9	GROUND WATER DEPTH (FT) Not Encountered	LOGGED BY: G. LINDSEY	
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	RA-226 pCi/gr	TH-232 pCi/gr	TH-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
1			TAILINGS, (SM), silty sand, fine, gray. Reddish brown color from 1'-5'.						
2									
3									
4									
5			Turning to purple color.						
6			Clayey slimes.						
7									
8									
9									
10			Very wet, possibly perched water.						Perched water in tailings and equipment vibration cause severe caving and possible cross contamination.
11									
12									
13									
14	SS-2541		CLAY, (CL), silty, dark gray, carbonaceous.	1.5	1.6	4.9			-Plan Exc. Depth at 14'.
15	SS-2542			3.0	1.4	1.8+0.5	4.9		FINES: RA-226 (1,000 year) = 2.6 pCi/gr.
16	SS-2543			2.0	1.2				FINES: RA-226 (1,000 year) = 5.3 pCi/gr.
17	SS-2544		GRAVELS, (GP), with cobbles to 12".	5.9	1.3	4.2+0.8			* Possible Cross Contamination.
18	SS-2545			8.2	1.3				COBBLES (Composite): Sample Depth 17'-21'.
19	SS-2546			* 17.0	1.5				RA-226 TH-232 TH-230 RA-226 (1,000 yr)
20	SS-2547			* 20.0	1.5				2.0+0.7 1.7+0.5
21			BOTTOM OF TEST PIT AT 21.0'						FINES (Composite): Sample Depth 17'-21'.
									RA-226 TH-232 TH-230 RA-226 (1,000 yr)
									220+10 120+4
									+#4 sieve = 73.1%.
									-#4 sieve = 26.9%



TEST PIT LOG

PROJECT UMTRA			SITE RIFLE	LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-11			
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N24700 E47670	BEGUN 12/2/93	COMPLETED 12/2/93	GROUND ELEV. 5268.0	GROUND WATER DEPTH (FT) 10.0	LOGGED BY: G.LINDSEY			
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		RA-226 pCi/gr	TH-232 pCi/gr	TH-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH	
1			<u>TAILINGS</u> , (ML), silt, light gray with red brown oxidized yellow slimes.								
2			<u>CLAY</u> , (CL), silty, dark brown, moist.								
3	SS-2437		Silty clay, carbonaceous.		0.9	1.3	1.2±0.5	6.6		FINES: Ra-226 (1,000 year) = 1.0 pCi/gr.	
4	SS-2438				16.0	2.2		8.5			
5	SS-2439				6.5	1.5		8.2		-Plan Exc. Depth at 5'.	
6	SS-2440		<u>GRAVELS</u> , (GP), with cobbles to 12", black, carbonaceous.		2.4	1.7	7.7±1.1			FINES: Ra-226 (1,000 year) = 4.3 pCi/gr.	
7	SS-2441				2.5	1.2				FINES: Ra-226 (1,000 year) = 9.8 pCi/gr.	
8	SS-2442				3.2	1.3	22±2				
9	SS-2443				3.6	1.0					
10	SS-2444				2.0	1.1					
11	SS-2445				2.2	1.1					
12	SS-2446				7.1	1.3	25±2	8.8	▼	FINES: Ra-226 (1,000 year) = 16.3 pCi/gr.	
	SS-2447		Partly Cemented Conglomerate (Refusal to backhoe).		7.1	1.2					
BOTTOM OF TEST PIT AT 12.0'									COBBLES (Composite): Sample Depth 6' to 10'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 0.8±0.5 0.4±0.3 FINES (Composite): Sample Depth 6' to 10'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 4.2±1.1 8.9±1.2 +#4 sieve = 76.4% -#4 sieve = 23.6%.		
										SHEET 1 OF 1	TEST PIT NO. M-CF-11



MORRISON KNUDSEN CORPORATION
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TEST PIT LOG

PROJECT UMTRA				SITE RIFLE			LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-15			
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N24410 E47825	BEGUN 12/1/93	COMPLETED 12/1/93	GROUND ELEV. 5267.2	GROUND WATER DEPTH (FT) 10.5	LOGGED BY: G. LINDSEY						
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION			RA-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH			
1	SS-2448		SILT, (ML), clayey, dark brown, pond sediments with oxidized seams.			167.0	3.3							
1	SS-2449		(FILL) per field staff.			555.0	10.0							
2	SS-2450		TAILINGS, (ML), silt, light gray.			471.0	9.2							
3	SS-2451		CLAY, (CL), silty, med. to low plasticity, dark brown, moist.			128.0	2.5							
4	SS-2452					8.6	1.6	12±1.0			FINES: Ra-226 (1,000 year) = 9.8 pCi/gr.			
5	SS-2453					3.5	1.3	5.0±4.0			FINES: Ra-226 (1,000 year) = 4.0 pCi/gr. -Plan Exc. Depth at 5'.			
6	SS-2454					1.9	1.2							
7	SS-2455		CLAY, (CL), silty, low plasticity, dark brown, moist to saturated.			1.1	1.2		8.8					
8	SS-2456					16.0	1.3	23±2.0			FINES: Ra-226 (1,000 year) = 18.5 pCi/gr. COBBLES (Composite): Sample Depth 10' to 13'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 0.9±0.5 0.8±0.4			
9	SS-2457					11.0	1.1				FINES (Composite): Sample Depth 10' to 13'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 6.3±1.4 13±1			
10	SS-2458		GRAVELS, (GW), with cobbles to 5", dark gray to black, carbonaceous.			2.0	1.3				+#4 sieve = 74.2%. -#4 sieve = 25.8%.			
11	SS-2460		Cemented below 11.0'.			7.9	1.2	8.8±1.2			FINES: Ra-226 (1,000 year) = 8.2 pCi/gr.			
12	SS-2461					2.8	1.2							
12	SS-2459					2.2	1.0							
13	SS-2462		Refusal to Backhoe bucket.			2.6	1.2							
			BOTTOM OF TEST PIT AT 13.0'											
			Note: Pit located in the bottom of a gypsum pond.											
								SHEET	1	TEST PIT NO.	M-CF-15			
								OF						



TEST PIT LOG

PROJECT UMTRA				SITE RIFLE		LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-19		
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE		COORDINATES N24160 E47900		BEGUN 12/1/93	COMPLETED 12/1/93	GROUND ELEV. 5267.1	GROUND WATER DEPTH (FT) not encountered	LOGGED BY: J.CERCONE/G.LINDSEY		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION			Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DEPTH FT	REMARKS PHOTOGRAPH	
1	SS-2428		SAND , (SM), silty, light brown, moist.			41.0	1.8		6.9			
2	SS-2430		ALLUVIUM			2.1	1.6	4.8±0.9	7.1		FINES Ra-226 (1,000 year) = 3.0 pCi/gr.	
3	SS-2429		ALLUVIUM			2.0	1.9					
4	SS-2431		GRAVELS , (GP), with cobbles in a sand matrix, iron oxide and calcite cementation.			7.3	1.5		9.2		FINES Ra-226 (1,000 year) = 20 pCi/gr.	
5	SS-2432		GRAVELS , (GP), with cobbles in a sand matrix, iron oxide and calcite cementation.			7.1	1.5	44±3.0				
6	SS-2433		GRAVELS , (GP), with cobbles in a sand matrix, iron oxide and calcite cementation.			9.5	1.5					
7	SS-2434		Hard digging with backhoe bucket below 5 feet.			10.0	1.9					
8	SS-2435		Cemented with CaCO ₃ .			5.9	1.6	19±2.0			FINES Ra-226 (1,000 year) = 10.5 pCi/gr.	
9	SS-2436		Refusal to Backhoe.			6.0	1.7		9.1		-Plan Exc. Depth 6'.	
BOTTOM OF TEST PIT AT 6.7'.												
Note: Pit located in the bottom of a gypsum pond.												
										COBBLES (Composite): Sample Depth 3.5' to 5.5'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 0.8±0.5 0.7±0.3 FINES (Composite): Sample Depth 3.5' to 5.5'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 6.5±1.3 16±2 +#4 sieve = 76.3%. -#4 sieve = 23.7%.	TEST PIT NO.	
										SHEET 1 OF 1	TEST PIT NO. M-CF-19	



MORRISON KNUDSEN CORPORATION
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TEST PIT LOG



MORRISON KNUDSEN CORPORATION
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SHEET
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OF
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TEST PIT NO.
M-CF-20

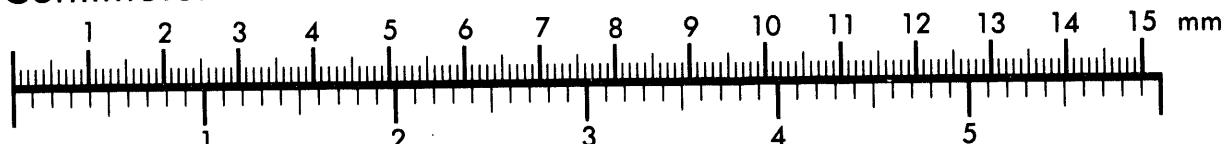


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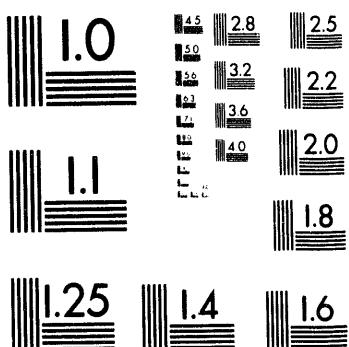
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2 of 3

TEST PIT LOG

PROJECT UMTRA				SITE RIFLE		LOCATION NEW RIFLE, COLORADO				JOB NO. 3885-70	TEST PIT NO. M-CF-21
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N23900 E47180	BEGUN 12/1/93	COMPLETED 12/1/93	GROUND ELEV. 5261.4	GROUND WATER DEPTH (FT) 4.5	LOGGED BY: G.LINDSEY			
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATE	REMARKS PHOTOGRAPH	
	SS-2361		COBBLES, (GP), to 12", some sand and gravel.		4.7	1.3	5.7±0.9			FINES: Ra-226 (1,000 year) = 5.1 pCi/gr. 1 inch of tailings on the surface.	
1	SS-2362				17.0	1.4					
	SS-2363				16.0	1.5					
2	SS-2364				12.0	1.7		8.4			
	SS-2365				13.0	1.9					
3	SS-2366				25.0	1.7					
	SS-2367				28.0	1.7					
4	SS-2368				11.0	1.2					
	SS-2369				9.5	1.2	12±1.0			FINES: Ra-226 (1,000 year) = 10.4 pCi/gr. +#4 sieve = 81.8%. -#4 sieve = 18.2%. -Plan Exc. Depth 5'.	
5											
6			BOTTOM OF TEST PIT AT 6.0'							COBBLES (Composite): Sample Depth 2' to 6'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 1.6±0.7 1.2±0.4 FINES (Composite): Sample Depth 2' to 6'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 32±3 55±3	
										SHEET 1 OF 1	TEST PIT NO. M-CF-21
 MORRISON KNUDSEN CORPORATION ENVIRONMENTAL SERVICES DIVISION											

TEST PIT LOG

PROJECT UMTRA				SITE RIFLE			LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-22
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N23900 E47430	BEGUN 12/1/93	COMPLETED 12/1/93	GROUND ELEV. 5262.9	GROUND WATER DEPTH (FT) 6.0	LOGGED BY: J.CERCONE/G.LINDSEY			
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION			Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATE	REMARKS PHOTOGRAPH
1			<u>FILL</u> , gravels and cobbles in a silty sand matrix.								
2											
3											
4			<u>COBBLES</u> , (GP), with boulders, black, carbonaceous, little sand and gravel.								
5											
6	SS-2388					2.6	1.0	1.9±0.6	7.3	▼	COBBLES (Composite): Sample Depth 4' to 8'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 0.9±0.5 0.9±0.4
7	SS-2389					3.3	1.2				FINES (Composite): Sample Depth 4' to 8'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 2.4±0.8 2.5±0.6
8			BOTTOM OF TEST PIT AT 8.0'								+#4 sieve = 79.3%. -#4 sieve = 20.7%. FINES: Ra-226 (1,000 year) = 2.4 pCi/gr. -Plan Exc. Depth at 6'.



MORRISON KNUDSEN CORPORATION
ENVIRONMENTAL SERVICES DIVISION

SHEET
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TEST PIT NO.
M-CF-22

TEST PIT LOG

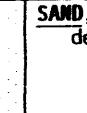
PROJECT UMTRA				SITE RIFLE		LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-24
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N23700 E46915	BEGUN 12/1/93	COMPLETED 12/1/93	GROUND ELEV. 5259.2	GROUND WATER DEPTH (FT) 2.8	LOGGED BY: G. LINDSEY		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
1	SS-2390		<u>COBBLES</u> , to 4" with sand.		1.6	0.8				
2	SS-2391				1.1	1.6				
2	SS-2392		<u>GRAVELS (GP)</u> , with cobbles.		1.8	1.0	1.9±0.6			FINES: Ra-226 (1,000 year) = 1.8 pCi/gr.
3	SS-2393				1.7	1.0		7.9	▼	
3	SS-2394				2.7	1.2				
4	SS-2395				3.0	1.3				
4	SS-2396				1.8	0.8				-Plan Exc. Depth at 4'.
5	SS-2397				2.0	1.3				
			BOTTOM OF TEST PIT AT 5.0'							
										COBBLES (Composite): Sample Depth 2' to 5'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 0.9±0.5 0.7±0.4 FINES (Composite): Sample Depth 2' to 5'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 2.6±0.8 3.6±0.8 +#4 sieve = 64.8%. -#4 sieve = 35.2%.
									SHEET 1 OF 1	TEST PIT NO. M-CF-24
 MORRISON KNUDSEN CORPORATION ENVIRONMENTAL SERVICES DIVISION										

TEST PIT LOG

PROJECT UMTRA				SITE RIFLE	LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-25	
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N23640 E47180	BEGUN 12/1/93	COMPLETED 12/1/93	GROUND ELEV. 5263.2	GROUND WATER DEPTH (FT) 8.0	LOGGED BY: J.CERCONE/G.LINDSEY		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
-	SS-2311		SILTY CLAY, (CL) , med. plasticity, dark brown, moist to saturated.		10.0	1.6				
1	SS-2312				1.5	1.6	1.2 ± 0.5			FINES: Ra-226 (1,000 year) = 1.4 pCi/gr.
2	SS-2315				1.1	1.0		7.5		
3	SS-2316		Very moist.		1.0	1.1				
4	SS-2317		Organic seam.		1.4	1.0				
5	SS-2319		CLAYEY SILT, (ML) , reddish brown-probably from oxidation.		1.0	1.0				
6	SS-2318				6.7	1.4	5.2 ± 0.9	7.0		FINES: Ra-226 (1,000 year) = 6.2 pCi/gr. -Plan Exc. Depth at 6'.
7	SS-2320		COBBLES, (GW-GP) , to 12", with sand and gravel, clean material.		0.9	1.4				
8	SS-2321				1.5	1.2				
9	SS-2322				0.6	1.0				
SS-2323					1.1	1.0				
SS-2398					12.0	1.4				
SS-2399					8.5	1.5				
10			BOTTOM OF TEST PIT AT 10.0'							COBBLES (Composite): Sample Depth 6.5' to 8.5'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 0.8 ± 0.5 1.3 ± 0.5 FINES (Composite): Sample Depth 6.5' to 8.5'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 5.4 ± 1.2 4.1 ± 0.8 #4 sieve = 78.5%. #4 sieve = 21.5%.
								SHEET 1	TEST PIT NO. M-CF-25	



TEST PIT LOG

PROJECT UMTRA				SITE RIFLE		LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-26
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N23640 E47480	BEGUN 12/1/93	COMPLETED 12/1/93	GROUND ELEV. 5263.5	GROUND WATER DEPTH (FT) 7.5	LOGGED BY: J.CERCONE/G.LINDSEY		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
1	SS-2324		<u>FILL</u> , dark brown, fine grained, with a lot of debris.		11.0	1.8				FINES: Ra-226 (1,000 year) = 7.5 pCi/gr. Debris and fill to 3 feet on north side of the pit.
2	SS-2325		<u>SAND</u> , (SP), little silt, gray to brown, med. dense.		7.1	1.5	8.1±1.1			
3	SS-2326				6.8	1.6		7.5		
4	SS-2327				0.9	1.5				
5	SS-2328				1.0	1.2	0.6±0.4			FINES: Ra-226 (1,000 year) = 0.9 pCi/gr.
6	SS-2329				1.2	0.8				
7	SS-2330				1.0	0.9	7.6 7.1	7.0		-Plan Exc. Depth at 6'.
8	SS-2331				7.6	1.0	15±2.0	7.1		FINES: Ra-226 (1,000 year) = 10.2 pCi/gr.
9	SS-2400		<u>GRAVELS</u> , (GP), with cobbles to 6".		2.0	0.8	2.6±0.7			FINES: Ra-226 (1,000 year) = 2.2 pCi/gr.
			BOTTOM OF TEST PIT AT 9.5'							COBBLES (Composite): Sample Depth 8' to 9.5'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 0.7±0.5 0.5±0.3 FINES (Composite): Sample Depth 8' to 9.5'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 1.9±0.7 1.4±0.5 +#4 sieve = 65.5%. -#4 sieve = 34.5%.
									SHEET 1 OF 1	TEST PIT NO. M-CF-26



MORRISON KNUDSEN CORPORATION
ENVIRONMENTAL SERVICES DIVISION

TEST PIT LOG

PROJECT UMTRA			SITE RIFLE	LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-27		
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N23640 E47725	BEGUN 12/1/93	COMPLETED 12/1/93	GROUND ELEV. 5267.0	GROUND WATER DEPTH (FT) 11.0	LOGGED BY: J.CERCONE/G.LINDSEY		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
	SS-2332		FILL , mixed soil with tailings, wood.		281.0	8.3				
1	SS-2333				336.0	5.2				
2	SS-2334				370.0	7.8				
3	SS-2335		Oxidized zone at 3 to 4 feet.		349.0	7.1				
4	SS-2336		TAILINGS , (CL-ML), reddish brown with orange seams (3").		364.0	8.7	6.8			
5	SS-2337				150.0	4.5				
6	SS-2338		Slimes, gray, saturated.		1103.0	44.0	6.9			-Plan Exc. Depth at 6'.
7	SS-2339				2792.0	64.0				
8	SS-2340		SILTY CLAY , (CL), dark brown, some roots.		9.0	1.5	8.2			
9	SS-2345		GRAVELS , (GP), with cobbles to 12".		9.4	1.8	7.3+1.1			FINES: Ra-226 (1,000 year) = 8.7 pCi/gr.
10	SS-2346				10.0	1.7				
	SS-2341				2.3	1.0				
	SS-2342				2.3	1.0				
11	SS-2343		BOTTOM OF TEST PIT AT 11.0'		7.8	1.3				COBBLES (Composite): Sample Depth 9.5' to 11.0'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 0.8+0.5 0.8+0.4 FINES (Composite): Sample Depth 9.5' to 11.0'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 3.2+0.9 1.4+0.5 +#4 sieve = 85.0%. -#4 sieve = 15.0%.
	SS-2344				7.6	1.3				



MORRISON KNUDSEN CORPORATION
ENVIRONMENTAL SERVICES DIVISION

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OF

TEST PIT NO.

M-CF-27

TEST PIT LOG

PROJECT UMTRA				SITE RIFLE			LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-28
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N23400 E46900	BEGUN 12/1/93	COMPLETED 12/1/93	GROUND ELEV. 5258.0	GROUND WATER DEPTH (FT) 2.0	LOGGED BY: G.LINDSEY			
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH	
1	SS-2401		COBBLES, (GP), to 12", with black organic silt.		10.4	1.8	38+2.0			FINES: Ra-226 (1,000 year) = 20.1 pCi/gr.	
2	SS-2402				13.0	1.2	40+2.0			FINES: Ra-226 (1,000 year) = 22.5 pCi/gr.	
3	SS-2403				12.0	1.0				-Plan Exc. Depth at 2'.	
4	SS-2404				6.9	1.1		6.5		FINES: Ra-226 (1,000 year) = 15.2 pCi/gr.	
5	SS-2405				7.2	1.3	30+2.0				
			BOTTOM OF TEST PIT AT 4.5'							COBBLES (Composite): Sample Depth 0' to 4.5'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 0.8+0.5 0.5+0.3 FINES (Composite): Sample Depth 0' to 4.5'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 4.2+1.0 11+1 +#4 sieve = 90.4%. -#4 sieve = 9.6%.	
										SHEET 1 OF 1	TEST PIT NO. M-CF-28
 MORRISON KNUDSEN CORPORATION ENVIRONMENTAL SERVICES DIVISION											

TEST PIT LOG

PROJECT UNTRA				SITE RIFLE			LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-29	
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N23450 E47130	BEGUN 12/1/93	COMPLETED 12/1/93	GROUND ELEV. 5262.2	GROUND WATER DEPTH (FT) 3.8	LOGGED BY: G.LINDSEY				
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION			RA-226 pCi/gr	TH-232 pCi/gr	TH-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH	
1	SS-2406		<u>FILL</u> , mixed sand, gravel and cobbles to 12", dark brown.			186.0	5.4					Ra-226 (1,000 yr) = 176.0 pCi/gr. -Plan Exc. Depth at 3'. Perched water table?
	SS-2407					178.0	4.5					
	SS-2408					99.0	3.0					
	SS-2409					96.0	3.1					
	SS-2410					115.0	3.7	290±10				
	SS-2411					131.0	3.4					
2	<u>SILTY CLAY</u> , (CL), med. plasticity, black, with carbonized roots. Med. gray seam at 4.5' - 5.0'.			6.9								
3	<u>BOTTOM OF TEST PIT AT 6.5'</u>											
4	<u>BOTTOM OF TEST PIT AT 6.5'</u>											
5	<u>BOTTOM OF TEST PIT AT 6.5'</u>											
6	<u>BOTTOM OF TEST PIT AT 6.5'</u>											
COBBLES (Composite): Sample Depth 0' to 4'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 2.1±0.8 2.3±0.6 FINES (Composite): Sample Depth 0' to 4'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 110±10 230±10 +#4 sieve = 78.2%. -#4 sieve = 21.8%.										SHEET 1 OF	TEST PIT NO. M-CF-29	
 MORRISON KNUDSEN CORPORATION												



MORRISON KNUDSEN CORPORATION
ENVIRONMENTAL SERVICES DIVISION

SHEET

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TEST PIT NO.

M-CF-29

TEST PIT LOG

PROJECT UMTRA			SITE RIFLE	LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-30		
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N23400 E47265	BEGUN 12/1/93	COMPLETED 12/1/93	GROUND ELEV. 5262.2	GROUND WATER DEPTH (FT) 8.3	LOGGED BY: J.CERcone		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		RA-226 pCi/gr	TH-232 pCi/gr	TH-230 pCi/gr	PH	WATER DATA	REMARKS PHOTOGRAPH
1	SS-2412		<u>FILL</u> , silty gravel, poorly graded, brown, moist, low plasticity.		34.0	2.5				
2	SS-2413				11.0	1.5				
3	SS-2414				236.0	4.3		7.3		
4	SS-2417		<u>SILTY SAND</u> , (SM), gray, moist.		142.0	3.5				Tailings?
5	SS-2418		<u>CLAY</u> , (CL), low to med. plasticity, black, moist to saturated, organic.		9.8	1.4				
6	SS-2419				13.0	1.5	32+2.0			FINES: Ra-226 (1,000 year) = 19.7 pCi/gr.
7	SS-2420		<u>GRAVELS</u> , (GW), with cobbles, well graded, cobbles to 8" max., fines are med. to coarse sand.		16.0	1.4				
8	SS-2421				12.0	1.1				Plan Excavation Depth at 6'.
9	SS-2422				30.0	1.5				
	SS-2423				30.0	1.5				
	SS-2424				4.4	1.2	22+2.0			FINES: Ra-226 (1,000 year) = 10.6 pCi/gr.
	SS-2425				6.0	1.1				
	SS-2426				* 52.0	2.7				
	SS-2427				* 47.0	1.3				
			BOTTOM OF TEST PIT AT 9.0'							
			* Possible Cross Contamination.							
										COBBLES (Composite): Sample Depth 4.5' to 7.5'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 1.2+0.6 0.6+0.4
										FINES (Composite): Sample Depth 4.5' to 7.5'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 3.0+0.9 6.9+1.0
										+#4 sieve = 79.4%.
										-#4 sieve = 20.6%.



MORRISON KNUDSEN CORPORATION
ENVIRONMENTAL SERVICES DIVISION

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TEST PIT NO.
M-CF-30

TEST PIT LOG

PROJECT			UMTRA		SITE		LOCATION		JOB NO.	TEST PIT NO.				
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:	3885-70	M-CF-31				
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION			Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH			
1	SS-2475		CLAY, (CL), light brown, slightly moist, some roots.			1.6	1.9							
2	SS-2476					1.1	2.3							
3	SS-2477					1.5	2.8							
3	SS-2478		SANDY SILT, (ML), to SILTY SAND, (SM), dark brown, moist, loose.			1.5	2.3							
4	SS-2479					1.8	2.0							
5	SS-2480					0.6	1.5							
6	SS-2481		GRAVELS, (GP-GW), with cobbles to 4", matrix of fine sand.			0.8	1.5							
7	SS-2482					0.9	1.6							
8	SS-2483					1.3	1.5							
8	SS-2484					0.8	1.4							
9	SS-2485		GRAVELS, (GP-GW), with cobbles to 6", matrix of coarse sand.			1.3	1.3							
9	SS-2486					0.7	1.0							
10	SS-2487					0.7	1.1							
10	SS-2488					0.8	1.2							
11	SS-2489					1.0	1.2							
11	SS-2490					0.6	1.2							
12	SS-2491					1.0	1.1							
12 BOTTOM OF TEST PIT AT 12.0' (BACKGROUND PIT LOCATED AT NORTHEAST CORNER OF NEW RIFLE SITE).														
								SHEET	TEST PIT NO.					
								1 OF 1	M-CF-31					



MORRISON KNUDSEN CORPORATION
ENVIRONMENTAL SERVICES DIVISION

TEST PIT LOG

PROJECT UMTRA				SITE RIFLE		LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-32
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N24648 E51357	BEGUN 12/2/93	COMPLETED 12/2/93	GROUND ELEV. 5271.5	GROUND WATER DEPTH (FT) 3.0	LOGGED BY: J.CERCONE		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		RA-226 pCi/gr	TH-232 pCi/gr	TH-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
1	SS-2370	[REDACTED]	GRAVELS , (GP), with cobbles to 12", poorly graded, with coarse sand, slightly moist, all gravels and cobbles appear clean and fresh.		1.3	1.0			▼	COBBLES (Composite): Sample Depth 0' to 4.0'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 1.8 ± 0.7 1.1 ± 0.4 FINES (Composite): Sample Depth 0' to 4.0'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 1.7 ± 0.7 0.9 ± 0.4 +#4 sieve = 80.8%. -#4 sieve = 19.2%.
	SS-2371				1.2	1.3				
	SS-2372				0.9	1.0				
	SS-2374				1.5	1.1				
	SS-2373				1.4	1.4				
	SS-2375				1.3	1.3				
	SS-2376				1.1	1.0				
	SS-2377				1.0	1.0				
	SS-2378				1.2	1.2				
5	SS-2479		BOTTOM OF TEST PIT AT 5.0'.							
			(BACKGROUND PIT LOCATED IN CON SY INC. GRAVEL PIT).							
									SHEET 1 OF 1	TEST PIT NO. M-CF-32
 MORRISON KNUDSEN CORPORATION ENVIRONMENTAL SERVICES DIVISION										

TEST PIT LOG

PROJECT UMTRA			SITE RIFLE	LOCATION NEW RIFLE, COLORADO			JOB NO. 3885-70	TEST PIT NO. M-CF-33			
CONTRACTOR GREEN		EXCAVATION METHOD BACKHOE	COORDINATES N24877 E51355	BEGUN 12/2/93	COMPLETED 12/2/93	GROUND ELEV. 5275.2	GROUND WATER DEPTH (FT) 7.2	LOGGED BY: J.CERCONC			
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION		Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH	
1			CLAY, (CL), (TOP SOIL), some roots. SILT, (ML), light brown, moist.								
2											
3			CLAY, (CH), med. to high plasticity, black, saturated, organic .								
4											
5											
6	SS-2380		GRAVELS, (GW), with cobbles to 4", well graded, black to gray, organic coating.		1.3	1.1				COBBLES (Composite): Sample Depth 7.0' to 9.0'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 1.6+0.7 0.5+0.3	
7	SS-2381				1.1	1.3				FINES (Composite): Sample Depth 7.0' to 9.0'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 1.6+0.7 1.3+0.5	
8	SS-2382				1.0	1.2				+#4 sieve = 81.9%.	
9	SS-2383				0.9	0.9				-#4 sieve = 18.1%.	
SS-2384					0.7	0.8					
SS-2385					1.0	1.3					
9			BOTTOM OF TEST PIT AT 9.0'. (BACKGROUND PIT LOCATED IN CON SY INC. GRAVEL PIT).								
										SHEET 1 OF 1	TEST PIT NO. M-CF-33



APPENDIX D

MASS PARTITION FUNCTIONS
(COBBLES-TO-FINES RATIOS)

INTER-OFFICE CORRESPONDENCE

TO: **Grant Cherrington** DATE: **December 13, 1993**
FROM: **David Farr**
LOCATION: **San Francisco** LOCATION: **Rifle, CO 3050**
SUBJECT: **Cobbles to Fines Test Result**

As requested, we have performed particle size analyses on New Rifle site subpile material test pit samples obtained by TAC, MKES and DOE representatives during recent test pit investigations. Enclosed are the results.

As discussed during initial test pit examination, the cobble to fine analyses were performed on composite bulk samples ranging in weight from 1000 to 1500 pounds each. The larger sized samples were required due to concerns about the smaller samples originally specified being representative. To expedite this process, the bulk samples were reduced to manageable proportions in accordance with the ASTM C-136 practice of sample reduction. An explanation of this practice has been provided in the attached calculation sheet (Attachment 1).

The dry weight of the +1" and +#4 fractions was calculated using an assumed 1.5% moisture as recommended by ASTM C-136. A representative sample of the +1", including a proportionate amount of the -1" to +#4 material, was collected for radium and thorium analysis. These samples were then given to site H.P. personnel to be sent out for analysis.

It should be noted that a few of the calculation sheets do not indicate the depth of the sample as this data was not provided to us.

Should you require further information, please advise.

File: 4.15 w/ enclosure

cc: Randy Withee w/o enclosure
QC File w/ enclosure

Tan

ATTACHMENT 1
CALCULATIONS

1. A representative sample of between 1000 to 1500 pounds of material was split on the 1" sieve and weights of each fraction were obtained. The +1" fraction was corrected assuming a 1.5% moisture and the -1" fraction corrected by actual moisture content. Dry weights were calculated and added together to determine the total sample weight.
2. The -1" fraction was reduced to a manageable sized representative sample of approximately 50 pounds, split on the #4 sieve and weights were obtained for each fraction. A moisture sample was obtained from the -#4 material for correction and the +#4 fraction was corrected using an assumed moisture content of 1.5%. Dry weights were calculated. Percentages of the +#4 and -#4 were then calculated.
3. The percentages of +#4 and -#4 obtained from the reduced -1" fraction were then adjusted back to a whole sample basis by multiplying by the original dry weight of the whole -1" fraction. This weight was then added to the +1" fraction to determine the +#4 weight on a whole sample basis.
4. The weight of the +#4 and -#4 (cobbles and fines) is then expressed as a percentage of the total sample weight.

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #1

DATE TESTED: 12-6-93

DEPTH: 15.0' - 17.0'

TECHNICIAN: David M. Jones

CHECKED BY: Steve Miller

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>836.28</u> lbs.	- 1" WET WEIGHT	<u>381.92</u> lbs.
% MOIST	<u>1.5 %</u>	% MOIST	<u>11.6 %</u>
DRY WEIGHT	<u>823.92</u> lbs.	DRY WEIGHT	<u>342.82</u> lbs.

TOTAL SAMPLE WEIGHT 1166.14 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>24.01</u> lbs.	- #4 WET WEIGHT	<u>35.12</u> lbs.
% MOIST	<u>1.5 %</u>	% MOIST	<u>9.6 %</u>
DRY WEIGHT	<u>23.66</u> lbs.	DRY WEIGHT	<u>32.04</u> lbs.

REDUCED SAMPLE WEIGHT 55.70 lbs.

% + #4 IN REDUCED SAMPLE 42.5 %
 % - #4 IN REDUCED SAMPLE 57.5 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>145.44</u> lbs.
+ DRY WT. OF +1" IN BULK SAMPLE	<u>823.92</u> lbs.
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>969.36</u> lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>652.6 g</u>
DRY WEIGHT	<u>585.0 g</u>
WT. OF WATER	<u>67.6 g</u>
% MOISTURE	<u>11.6 %</u>

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>969.36</u> lbs.
TOTAL SAMPLE WEIGHT	<u>1166.14</u> lbs.

% + #4 (COBBLES) 83.1 %

% - #4 (FINES) 16.9 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #2

DATE TESTED: 12-6-93

DEPTH: 13.0' - 16.0'

TECHNICIAN: David M. Tamm

CHECKED BY: Steve Miller

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>667.73</u> lbs	- 1" WET WEIGHT	<u>553.67</u> lbs
% MOIST	<u>1.5 %</u>	% MOIST	<u>10.5 %</u>
DRY WEIGHT	<u>657.86</u> lbs.	DRY WEIGHT	<u>501.06</u> lbs.

TOTAL SAMPLE WEIGHT 1158.92 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>12.60</u> lbs.	- #4 WET WEIGHT	<u>37.18</u> lbs.
% MOIST	<u>1.5 %</u>	% MOIST	<u>9.2 %</u>
DRY WEIGHT	<u>12.41</u> lbs.	DRY WEIGHT	<u>34.05</u> lbs.

REDUCED SAMPLE WEIGHT 46.46 lbs.

% + #4 IN REDUCED SAMPLE 26.7 %
 % - #4 IN REDUCED SAMPLE 73.3 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>133.78</u> lbs.
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>657.86</u> lbs.
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>791.64</u> lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION		REDUCED SAMPLE -#4	
WET WEIGHT	<u>572.9</u>	WET WEIGHT	<u>472.6</u>
DRY WEIGHT	<u>518.6</u>	DRY WEIGHT	<u>432.7</u>
WT. OF WATER	<u>54.3</u>	WT. OF WATER	<u>39.9</u>
% MOISTURE	<u>10.5 %</u>	% MOISTURE	<u>9.2 %</u>

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>791.64</u> lbs
TOTAL SAMPLE WEIGHT	<u>1158.92</u> lbs.

% + #4 (COBBLES) 68.3 %

% - #4 (FINES) 31.7 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #3

DATE TESTED: 12-7-93

DEPTH: 18.0' - 21.0'

TECHNICIAN: Daniel M. Farn

CHECKED BY: Spencer with

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>706.30</u> lbs	- 1" WET WEIGHT	<u>561.82</u> lbs
% MOIST	<u>1.5 %</u>	% MOIST	<u>14.3 %</u>
DRY WEIGHT	<u>695.86</u> lbs	DRY WEIGHT	<u>491.53</u> lbs

TOTAL SAMPLE WEIGHT 1187.39 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>15.83</u> lbs	-#4 WET WEIGHT	<u>44.75</u> lbs
% MOIST	<u>1.5 %</u>	% MOIST	<u>13.7 %</u>
DRY WEIGHT	<u>15.60</u> lbs	DRY WEIGHT	<u>39.36</u> lbs

REDUCED SAMPLE WEIGHT 54.96 lbs.

% + #4 IN REDUCED SAMPLE 28.4 %
 % -#4 IN REDUCED SAMPLE 71.6 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>139.59</u> lbs
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>695.86</u> lbs.
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>835.45</u> lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>523.1</u> g
DRY WEIGHT	<u>460.0</u> g
WT. OF WATER	<u>63.1</u> g
% MOISTURE	<u>13.7 %</u>

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>835.45</u> lbs.
TOTAL SAMPLE WEIGHT	<u>1187.39</u> lbs.

% + #4 (COBBLES) 70.4 %

% -#4 (FINES) 29.6 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #4

DATE TESTED: 12/7/93

DEPTH: 11.0' - 16.0'

TECHNICIAN: Dan M. J. M.

CHECKED BY: Spur Witz

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>781.77 lbs.</u>
% MOIST	<u>1.5 %</u>
DRY WEIGHT	<u>770.22 lbs</u>

- 1" WET WEIGHT	<u>458.61 lbs</u>
% MOIST	<u>5.4 %</u>
DRY WEIGHT	<u>435.11 lbs</u>

TOTAL SAMPLE WEIGHT 1205.33 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>21.04 lbs</u>
% MOIST	<u>1.5 %</u>
DRY WEIGHT	<u>20.73 lbs</u>

- #4 WET WEIGHT	<u>15.4257 lbs</u>
% MOIST	<u>5.1 %</u>
DRY WEIGHT	<u>40.50 lbs</u>

REDUCED SAMPLE WEIGHT 61.23 lbs

% + #4 IN REDUCED SAMPLE	<u>33.9 %</u>
% - #4 IN REDUCED SAMPLE	<u>66.1 %</u>

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>147.50 lbs</u>
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>770.22 lbs</u>
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>917.72 lbs.</u>

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION

WET WEIGHT	<u>558.8 g</u>
DRY WEIGHT	<u>530.2 g</u>
WT. OF WATER	<u>28.6 g</u>
% MOISTURE	<u>5.4 %</u>

REDUCED SAMPLE -#4

WET WEIGHT	<u>464.3 g</u>
DRY WEIGHT	<u>441.7 g</u>
WT. OF WATER	<u>22.6 g</u>
% MOISTURE	<u>5.1 %</u>

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>917.72 lbs</u>
TOTAL SAMPLE WEIGHT	<u>1205.33 lbs</u>

% + #4 (COBBLES) 76.1 %

% - #4 (FINES) 23.9 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #5

DATE TESTED: 12-7-93

DEPTH: 16.0' - 21.0'

TECHNICIAN: David M. Jones

CHECKED BY: Spac. Wilt

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>692.10 lbs</u>	- 1" WET WEIGHT	<u>525.88 lbs</u>
% MOIST	<u>1.5 %</u>	% MOIST	<u>7.2 %</u>
DRY WEIGHT	<u>681.87 lbs</u>	DRY WEIGHT	<u>490.56 lbs</u>

TOTAL SAMPLE WEIGHT 1172.43 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>24.34 lbs</u>	- #4 WET WEIGHT	<u>30.99 lbs.</u>
% MOIST	<u>1.5 %</u>	% MOIST	<u>12.0 %</u>
DRY WEIGHT	<u>23.98 lbs</u>	DRY WEIGHT	<u>27.67 lbs</u>

REDUCED SAMPLE WEIGHT 51.65 lbs.

% + #4 IN REDUCED SAMPLE 46.4 %
 % - #4 IN REDUCED SAMPLE 53.6 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>227.62 lbs</u>
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>681.87 lbs</u>
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>909.49 lbs.</u>

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>547.7 g</u>
DRY WEIGHT	<u>488.9 g</u>
WT. OF WATER	<u>58.8 g</u>
% MOISTURE	<u>12.0 %</u>

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>909.49 lbs</u>
TOTAL SAMPLE WEIGHT	<u>1172.43 lbs</u>

% + #4 (COBBLES) 77.6 %

% - #4 (FINES) 22.4 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #7

DATE TESTED: 12-7-93

DEPTH: 17.0' - 21.0'

TECHNICIAN: David M. Far

CHECKED BY: Span Witz

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>700.77</u>	lbs	- 1" WET WEIGHT	<u>50.88</u>	lbs
% MOIST	<u>1.5</u>	%	% MOIST	<u>11.5</u>	%
DRY WEIGHT	<u>690.41</u>	lbs	DRY WEIGHT	<u>450.12</u>	lbs

TOTAL SAMPLE WEIGHT 1140.53 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>18.12</u>	lbs	- #4 WET WEIGHT	<u>42.51</u>	lbs
% MOIST	<u>1.5</u>	%	% MOIST	<u>11.2</u>	%
DRY WEIGHT	<u>17.85</u>	lbs	DRY WEIGHT	<u>38.23</u>	lbs

REDUCED SAMPLE WEIGHT 56.08 lbs

% + #4 IN REDUCED SAMPLE 31.8 %
 % - #4 IN REDUCED SAMPLE 68.2 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>143.14</u>	lbs
+ DRY WT. OF +1" IN BULK SAMPLE	<u>690.41</u>	lbs
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>833.55</u>	lbs

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>530.19</u>
DRY WEIGHT	<u>475.5</u> g
WT. OF WATER	<u>54.6</u> g
% MOISTURE	<u>11.5</u> %
	<u>531.8</u> g
	<u>478.3</u> g
	<u>53.5</u> g
	<u>11.2</u> %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>833.55</u>	lbs
TOTAL SAMPLE WEIGHT	<u>1140.53</u>	lbs

% + #4 (COBBLES) 73.1 %

% - #4 (FINES) 26.9 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #11

DATE TESTED: 12-7-93

DEPTH: 6.0' - 10.0'

TECHNICIAN: Dave D. M. Farn

CHECKED BY: Spm with

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>1031.55</u>	lbs	- 1" WET WEIGHT	<u>574.17</u>	lbs
% MOIST	<u>1.5</u>	%	% MOIST	<u>13.9</u>	%
DRY WEIGHT	<u>1016.11</u>	lbs	DRY WEIGHT	<u>504.10</u>	lbs

TOTAL SAMPLE WEIGHT 1520.21 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>15.62</u>	lbs	- #4 WET WEIGHT	<u>41.74</u>	lbs
% MOIST	<u>1.5</u>	%	% MOIST	<u>10.2</u>	%
DRY WEIGHT	<u>15.39</u>	lbs	DRY WEIGHT	<u>37.88</u>	lbs

REDUCED SAMPLE WEIGHT 53.27 lbs.

% + #4 IN REDUCED SAMPLE	<u>145.68</u>	28.9	%
% - #4 IN REDUCED SAMPLE	<u>71.1</u>	%	

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF - 1" IN BULK SAMPLE	<u>145.68</u>	lbs
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>1016.11</u>	lbs
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>1161.79</u>	lbs

MOISTURE CORRECTIONS

BULK SAMPLE - 1" FRACTION	REDUCED SAMPLE - #4
WET WEIGHT	<u>526.0</u> g
DRY WEIGHT	<u>461.8</u> g
WT. OF WATER	<u>64.2</u> g
% MOISTURE	<u>13.9</u> %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>1161.79</u> lbs
TOTAL SAMPLE WEIGHT	<u>1520.21</u> lbs

% + #4 (COBBLES) 76.4 %

% - #4 (FINES) 23.6 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #15

DATE TESTED: 12/6/93

DEPTH: 10.0' - 13.0'

TECHNICIAN: Howard M. Fenn

CHECKED BY: Spam with

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>650.45</u> lbs	- 1" WET WEIGHT	<u>586.97</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>11.2</u> %
DRY WEIGHT	<u>640.84</u> lbs	DRY WEIGHT	<u>527.05</u> lbs

TOTAL SAMPLE WEIGHT 1168.69 lbs

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>22.30</u> lbs	- #4 WET WEIGHT	<u>31.60</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>8.2</u> %
DRY WEIGHT	<u>21.97</u> lbs	DRY WEIGHT	<u>29.21</u> lbs

REDUCED SAMPLE WEIGHT 51.18 lbs.

% + #4 IN REDUCED SAMPLE 42.9 %
 % - #4 IN REDUCED SAMPLE 57.1 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>226.45</u>
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>640.84</u>
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>876.29</u> lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>603.4</u> g
DRY WEIGHT	<u>542.6</u> g
WT. OF WATER	<u>60.8</u> g
% MOISTURE	<u>11.2</u> %
	<u>568.6</u> g
	<u>525.3</u> g
	<u>43.3</u> g
	<u>8.2</u> %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>867.29</u> lbs
TOTAL SAMPLE WEIGHT	<u>1168.69</u> lbs

% + #4 (COBBLES) 74.2 %

% - #4 (FINES) 25.8 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #19

DATE TESTED: 12-3-93

DEPTH: 3.5' - 5.5'

TECHNICIAN: David M. Farn

CHECKED BY: John W. H.

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>717.17</u>	lbs	-1" WET WEIGHT	<u>480.03</u>	lbs
% MOIST	<u>1.5</u>	%	% MOIST	<u>7.3</u>	%
DRY WEIGHT	<u>706.57</u>	lbs	DRY WEIGHT	<u>447.37</u>	lbs

TOTAL SAMPLE WEIGHT 1153.94 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>19.02</u>	lbs	-#4 WET WEIGHT	<u>31.94</u>	lbs
% MOIST	<u>1.5</u>	%	% MOIST	<u>7.9</u>	%
DRY WEIGHT	<u>18.74</u>	lbs	DRY WEIGHT	<u>29.60</u>	lbs

REDUCED SAMPLE WEIGHT 48.34 lbs.

% + #4 IN REDUCED SAMPLE 38.8 %
 % -#4 IN REDUCED SAMPLE 61.2 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 173.58 lbs
 + DRY WT. OF + 1" IN BULK SAMPLE 706.57 lbs
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 880.15 lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>600.0</u> g
DRY WEIGHT	<u>559.1</u> g
WT. OF WATER	<u>40.9</u> g
% MOISTURE	<u>7.3</u> %
	<u>492.1</u> g
	<u>455.9</u> g
	<u>36.2</u> g
	<u>7.9</u> %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 880.15 lbs
 TOTAL SAMPLE WEIGHT 1153.94 lbs

% + #4 (COBBLES) 76.3 %

% -#4 (FINES) 23.7 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #20

DATE TESTED: 12-3-93

DEPTH: 45 to 7

TECHNICIAN: Daniel M. Jarr

CHECKED BY: Tom Wilt

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>845.63</u> lbs	- 1" WET WEIGHT	<u>348.28</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>7.2</u> %
DRY WEIGHT	<u>833.13</u> lbs	DRY WEIGHT	<u>324.89</u> lbs

TOTAL SAMPLE WEIGHT 1158.02 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>28.43</u> lbs	- #4 WET WEIGHT	<u>37.41</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>7.2</u> %
DRY WEIGHT	<u>28.01</u> lbs	DRY WEIGHT	<u>34.90</u> lbs

REDUCED SAMPLE WEIGHT 62.91 lbs.

% + #4 IN REDUCED SAMPLE	<u>44.5</u> %
% - #4 IN REDUCED SAMPLE	<u>55.5</u> %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>144.58</u> lbs
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>833.13</u> lbs
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>977.71</u> lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>693.8</u> g
DRY WEIGHT	<u>647.4</u> g
WT. OF WATER	<u>46.4</u> g
% MOISTURE	<u>7.2</u> %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>977.71</u> lbs
TOTAL SAMPLE WEIGHT	<u>1158.02</u> lbs

% + #4 (COBBLES) 84.4 %

% - #4 (FINES) 15.6 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #21

DATE TESTED: 12-3-93

DEPTH: 2'-6'

TECHNICIAN: David M. J. M.

CHECKED BY: John W. B.

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>833.19</u> lbs	- 1" WET WEIGHT	<u>402.59</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>9.9</u> %
DRY WEIGHT	<u>820.88</u> lbs	DRY WEIGHT	<u>366.32</u> lbs

TOTAL SAMPLE WEIGHT 1187.20 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>19.88</u> lbs	- #4 WET WEIGHT	<u>30.68</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>8.7</u> %
DRY WEIGHT	<u>19.59</u> lbs	DRY WEIGHT	<u>28.22</u> lbs

REDUCED SAMPLE WEIGHT 47.81 lbs.

% + #4 IN REDUCED SAMPLE 41.0 %
 % - #4 IN REDUCED SAMPLE 59.0 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>150.19</u> lbs
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>820.88</u> lbs
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>971.07</u> lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>716.0</u> g
DRY WEIGHT	<u>647.0</u> g
WT. OF WATER	<u>69.0</u> g
% MOISTURE	<u>9.9</u> %
	<u>495.1</u> g
	<u>455.3</u> g
	<u>39.8</u> g
	<u>8.7</u> %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>971.07</u> lbs
TOTAL SAMPLE WEIGHT	<u>1187.20</u> lbs

% + #4 (COBBLES) 81.8 %

% -#4 (FINES) 18.2 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #22

DATE TESTED: 12-1-93

DEPTH: +3 - 6.5'

TECHNICIAN: Daniel M. Farn

CHECKED BY: Stan Weller

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>847.35</u> lbs	- 1" WET WEIGHT	<u>471.52</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>13.4</u> %
DRY WEIGHT	<u>834.83</u> lbs	DRY WEIGHT	<u>415.80</u> lbs

TOTAL SAMPLE WEIGHT 1250.63 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>20.68</u> lbs	-#4 WET WEIGHT	<u>38.41</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>13.8</u> %
DRY WEIGHT	<u>20.37</u> lbs	DRY WEIGHT	<u>33.75</u> lbs

REDUCED SAMPLE WEIGHT 54.12 lbs.

% + #4 IN REDUCED SAMPLE	<u>37.6</u> %
% -#4 IN REDUCED SAMPLE	<u>62.4</u> %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>156.34</u> lbs
+ DRY WT. OF +1" IN BULK SAMPLE	<u>834.83</u> lbs
= TOTAL DRY WEIGHT OF +#4 IN BULK SAMPLE	<u>991.17</u> lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>734.2</u> g
DRY WEIGHT	<u>647.3</u> g
WT. OF WATER	<u>86.9</u> g
% MOISTURE	<u>13.4</u> %
	<u>581.5</u> g
	<u>80.1</u> g
	<u>13.8</u> %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF +#4	<u>991.17</u> lbs
TOTAL SAMPLE WEIGHT	<u>1250.63</u> lbs

% + #4 (COBBLES) 79.3 %

% -#4 (FINES) 20.7 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #24

DATE TESTED: 12-2-93

DEPTH: 2 - 5'

TECHNICIAN: Daniel M. Farn

CHECKED BY: Spa. units

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>617.88</u> lbs	- 1" WET WEIGHT	<u>600.51</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>15.0</u> %
DRY WEIGHT	<u>608.75</u> lbs	DRY WEIGHT	<u>522.18</u> lbs

TOTAL SAMPLE WEIGHT 1130.93 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>12.92</u> lbs	- #4 WET WEIGHT	<u>44.87</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>9.2</u> %
DRY WEIGHT	<u>12.73</u> lbs	DRY WEIGHT	<u>41.09</u> lbs

REDUCED SAMPLE WEIGHT 53.82 lbs.

% + #4 IN REDUCED SAMPLE 23.7 %
 % - #4 IN REDUCED SAMPLE 76.3 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>123.76</u> lbs
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>608.75</u> lbs
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>732.51</u> lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>539.9</u>
DRY WEIGHT	<u>494.6</u>
WT. OF WATER	<u>45.3</u>
% MOISTURE	<u>9.2</u> %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>732.51</u> lbs
TOTAL SAMPLE WEIGHT	<u>1130.93</u> lbs

% + #4 (COBBLES) 64.8 %

% - #4 (FINES) 35.2 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #25

DATE TESTED: 12/1/93

DEPTH: 6.5' - 8.5'

TECHNICIAN: David M. Foss

CHECKED BY: Steve Smith

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>739.64</u> lbs	- 1" WET WEIGHT	<u>576.66</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>10.8</u> %
DRY WEIGHT	<u>728.71</u> lbs	DRY WEIGHT	<u>466.30</u> lbs

TOTAL SAMPLE WEIGHT 1195.01 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>34.01</u> lbs	- #4 WET WEIGHT	<u>45.98</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>11.4</u> %
DRY WEIGHT	<u>33.51</u> lbs	DRY WEIGHT	<u>41.27</u> lbs

REDUCED SAMPLE WEIGHT 74.78 lbs.

% + #4 IN REDUCED SAMPLE 44.8 %
 % - #4 IN REDUCED SAMPLE 55.2 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>208.90</u> lbs
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>728.71</u> lbs
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>937.61</u> lbs

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION		REDUCED SAMPLE -#4	
WET WEIGHT	<u>855.5</u> g	648.9	g
DRY WEIGHT	<u>771.0</u> g	<u>582.4</u> g	
WT. OF WATER	<u>83.7</u> g	<u>66.5</u> g	
% MOISTURE	<u>10.8</u> %	<u>11.4</u> %	

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>937.61</u> lbs
TOTAL SAMPLE WEIGHT	<u>1195.01</u> lbs

% + #4 (COBBLES) 78.5 %

% - #4 (FINES) 21.5 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #26

DATE TESTED: 12-6-95

DEPTH: 8.0' - 9.5'

TECHNICIAN: Donald M. Morris

CHECKED BY: Stan Wilt

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>675.65</u> lbs	- 1" WET WEIGHT	<u>624.43</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>6.4</u> %
DRY WEIGHT	<u>665.67</u> lbs	DRY WEIGHT	<u>586.87</u> lbs

TOTAL SAMPLE WEIGHT 1252.54 lbs

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>14.66</u> lbs	- #4 WET WEIGHT	<u>42.90</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>6.0</u> %
DRY WEIGHT	<u>14.44</u> lbs	DRY WEIGHT	<u>40.47</u> lbs

REDUCED SAMPLE WEIGHT 54.91 lbs.

% + #4 IN REDUCED SAMPLE 26.3 %
 % - #4 IN REDUCED SAMPLE 73.7 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 154.35 lbs
 + DRY WT. OF +1" IN BULK SAMPLE 665.67 lbs
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 820.02 lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>551.0</u> g
DRY WEIGHT	<u>518.1</u> g
WT. OF WATER	<u>32.9</u> g
% MOISTURE	<u>6.4</u> %
	<u>557.1</u> g
	<u>525.5</u> g
	<u>31.6</u> g
	<u>6.0</u> %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 820.02 lbs
 TOTAL SAMPLE WEIGHT 1252.54 lbs

% + #4 (COBBLES) 65.5 %

% - #4 (FINES) 34.5 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #27

DATE TESTED: 12-3-93

DEPTH: 9.5'-11.0'

TECHNICIAN: David M. Tamm

CHECKED BY: Steve Miller

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>900.36 lbs</u>	- 1" WET WEIGHT	<u>319.62 lbs</u>
% MOIST	<u>1.5 %</u>	% MOIST	<u>11.0 %</u>
DRY WEIGHT	<u>887.05 lbs</u>	DRY WEIGHT	<u>287.95 lbs</u>

TOTAL SAMPLE WEIGHT 1175.00 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>21.64 lbs</u>	- #4 WET WEIGHT	<u>37.10 lbs</u>
% MOIST	<u>1.5 %</u>	% MOIST	<u>11.0 %</u>
DRY WEIGHT	<u>21.32 lbs</u>	DRY WEIGHT	<u>33.42 lbs</u>

REDUCED SAMPLE WEIGHT 54.74 lbs.

% + #4 IN REDUCED SAMPLE	<u>38.9 %</u>
% - #4 IN REDUCED SAMPLE	<u>61.1 %</u>

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>112.01 lbs</u>
+ DRY WT. OF +1" IN BULK SAMPLE	<u>887.05 lbs</u>
= TOTAL DRY WEIGHT OF +#4 IN BULK SAMPLE	<u>999.06 lbs.</u>

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>705.3 g</u>
DRY WEIGHT	<u>635.5 g</u>
WT. OF WATER	<u>69.8 g</u>
% MOISTURE	<u>11.0 %</u>
	<u>646.8 g</u>
	<u>582.5 g</u>
	<u>64.3 g</u>
	<u>11.0 %</u>

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF +#4	<u>999.06 lbs</u>
TOTAL SAMPLE WEIGHT	<u>1175.00 lbs</u>

% + #4 (COBBLES) 85.0 %

% -#4 (FINES) 15.0 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #28

DATE TESTED: 12-3-93

DEPTH: 0.0' - 4.5'

TECHNICIAN: Howard M. Foss

CHECKED BY: Steve Weller

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>938.47 lbs</u>	- 1" WET WEIGHT	<u>161.34 lbs</u>
% MOIST	<u>1.5 %</u>	% MOIST	<u>21.5 %</u>
DRY WEIGHT	<u>924.60 lbs</u>	DRY WEIGHT	<u>132.79 lbs</u>

TOTAL SAMPLE WEIGHT 1057.39 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>13.87 lbs</u>	- #4 WET WEIGHT	<u>40.77 lbs</u>
% MOIST	<u>1.5 %</u>	% MOIST	<u>9.5 %</u>
DRY WEIGHT	<u>13.67 lbs</u>	DRY WEIGHT	<u>44.54 lbs</u>

REDUCED SAMPLE WEIGHT 58.21 lbs.

% + #4 IN REDUCED SAMPLE	<u>23.5 %</u>
% - #4 IN REDUCED SAMPLE	<u>76.5 %</u>

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>31.21 lbs</u>
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>924.60 lbs</u>
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>955.81 lbs.</u>

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>876.5 g</u>
DRY WEIGHT	<u>721.2 g</u>
WT. OF WATER	<u>155.3 g</u>
% MOISTURE	<u>21.5 %</u>
	<u>515.5 g</u>
	<u>470.7 g</u>
	<u>44.8 g</u>
	<u>9.5 %</u>

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>955.81 lbs</u>
TOTAL SAMPLE WEIGHT	<u>1057.39 lbs</u>

% + #4 (COBBLES) 90.4 %

% - #4 (FINES) 9.6 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #30

DATE TESTED: 12-6-93

DEPTH: 4.5'-7.5'

TECHNICIAN: Darrell M. Jones

CHECKED BY: John Miller

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>874.78</u> lbs	- 1" WET WEIGHT	<u>502.99</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>6.6</u> %
DRY WEIGHT	<u>861.85</u> lbs	DRY WEIGHT	<u>471.85</u> lbs

TOTAL SAMPLE WEIGHT 1333.70 lbs

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>21.41</u> lbs	- #4 WET WEIGHT	<u>30.74</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>4.3</u> %
DRY WEIGHT	<u>21.09</u> lbs	DRY WEIGHT	<u>29.47</u> lbs

REDUCED SAMPLE WEIGHT 50.56 lbs.

% + #4 IN REDUCED SAMPLE	<u>41.7</u> %
% - #4 IN REDUCED SAMPLE	<u>58.3</u> %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>196.76</u> lbs
+ DRY WT. OF +1" IN BULK SAMPLE	<u>861.85</u> lbs
= TOTAL DRY WEIGHT OF +#4 IN BULK SAMPLE	<u>1058.61</u> lbs

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION

WET WEIGHT	<u>649.0</u> g
DRY WEIGHT	<u>609.0</u> g
WT. OF WATER	<u>40.0</u> g
% MOISTURE	<u>6.6</u> %

REDUCED SAMPLE -#4

WET WEIGHT	<u>528.9</u> g
DRY WEIGHT	<u>507.0</u> g
WT. OF WATER	<u>21.9</u> g
% MOISTURE	<u>4.3</u> %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>1058.61</u> lbs
TOTAL SAMPLE WEIGHT	<u>1333.70</u> lbs

% + #4 (COBBLES) 79.4 %

% - #4 (FINES) 20.6 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: BACKGROUND PIT (ON-SITE) #31

DATE TESTED: 12-7-93

DEPTH: 3.5 - 11.5

TECHNICIAN: James D. Miller

CHECKED BY: Spencer Miller

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>786.00</u>	<u>lbs.</u>	- 1" WET WEIGHT	<u>454.95</u>	<u>lbs</u>
% MOIST	<u>1.5</u>	<u>%</u>	% MOIST	<u>10.7</u>	<u>%</u>
DRY WEIGHT	<u>774.38</u>	<u>lbs</u>	DRY WEIGHT	<u>410.98</u>	<u>lbs</u>

TOTAL SAMPLE WEIGHT 1185.36 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>20.31</u>	<u>lbs</u>	- #4 WET WEIGHT	<u>37.92</u>	<u>lbs</u>
% MOIST	<u>1.5</u>	<u>%</u>	% MOIST	<u>11.2</u>	<u>%</u>
DRY WEIGHT	<u>20.01</u>	<u>lbs</u>	DRY WEIGHT	<u>34.10</u>	<u>lbs</u>

REDUCED SAMPLE WEIGHT 54.11 lbs.

% + #4 IN REDUCED SAMPLE 37.0 %
 % - #4 IN REDUCED SAMPLE 63.0 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>152.06</u>	<u>lbs</u>
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>774.38</u>	<u>lbs</u>
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>926.44</u>	<u>lbs</u>

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>639.4</u> <u>g</u>
DRY WEIGHT	<u>577.8</u> <u>g</u>
WT. OF WATER	<u>61.6</u> <u>g</u>
% MOISTURE	<u>10.7</u> <u>%</u>
	<u>515.6</u> <u>g</u>
	<u>463.8</u> <u>g</u>
	<u>57.8</u> <u>g</u>
	<u>11.2</u> <u>%</u>

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>926.44</u>	<u>lbs</u>
TOTAL SAMPLE WEIGHT	<u>1185.36</u>	<u>lbs</u>

% + #4 (COBBLES) 78.2 %

% - #4 (FINES) 21.8 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #32

DATE TESTED: 12-8-93

DEPTH: 0.0' - 4.0'

TECHNICIAN: Howard Miller

CHECKED BY: Spencer Smith

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>909.88</u> lbs	- 1" WET WEIGHT	<u>492.38</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>3.7</u> %
DRY WEIGHT	<u>896.43</u> lbs	DRY WEIGHT	<u>474.81</u> lbs

TOTAL SAMPLE WEIGHT 1371.24 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>33.73</u> lbs	- #4 WET WEIGHT	<u>42.64</u> lbs
% MOIST	<u>1.5</u> %	% MOIST	<u>3.1</u> %
DRY WEIGHT	<u>33.23</u> lbs	DRY WEIGHT	<u>41.36</u> lbs

REDUCED SAMPLE WEIGHT 74.59 lbs.

% + #4 IN REDUCED SAMPLE 44.6 %
 % - #4 IN REDUCED SAMPLE 55.4 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>211.77</u> lbs
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>896.43</u> lbs
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>1108.20</u> lbs

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT	<u>655.9</u> g
DRY WEIGHT	<u>632.5</u> g
WT. OF WATER	<u>23.4</u> g
% MOISTURE	<u>3.7</u> %
	<u>413.5</u> g
	<u>401.2</u> g
	<u>12.3</u> g
	<u>3.1</u> %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>1108.20</u> lbs
TOTAL SAMPLE WEIGHT	<u>1371.24</u> lbs

% + #4 (COBBLES) 80.8 %

% -#4 (FINES) 19.2 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #33

DATE TESTED: 12-8-93

DEPTH: 7.0' - 9.0'

TECHNICIAN: Dave Miller

CHECKED BY: Steve Wilt

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>923.26 lbs</u>	- 1" WET WEIGHT	<u>413.68 lbs</u>
% MOIST	<u>1.5 %</u>	% MOIST	<u>9.0 %</u>
DRY WEIGHT	<u>909.62 lbs</u>	DRY WEIGHT	<u>379.52 lbs</u>

TOTAL SAMPLE WEIGHT 1289.14 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>26.16 lbs</u>	- #4 WET WEIGHT	<u>44.09 lbs</u>
% MOIST	<u>1.5 %</u>	% MOIST	<u>6.9 %</u>
DRY WEIGHT	<u>25.77 lbs</u>	DRY WEIGHT	<u>41.24 lbs</u>

REDUCED SAMPLE WEIGHT 67.02 lbs.

% + #4 IN REDUCED SAMPLE	<u>38.5 %</u>
% - #4 IN REDUCED SAMPLE	<u>61.5 %</u>

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>146.12 lbs</u>
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>909.62 lbs</u>
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>1055.74 lbs.</u>

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION		REDUCED SAMPLE -#4	
WET WEIGHT	<u>535.1 g</u>	WET WEIGHT	<u>525.2 g</u>
DRY WEIGHT	<u>491.1 g</u>	DRY WEIGHT	<u>491.4 g</u>
WT. OF WATER	<u>44.0 g</u>	WT. OF WATER	<u>33.8 g</u>
% MOISTURE	<u>9.0 %</u>	% MOISTURE	<u>6.9 %</u>

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>1055.74 lbs</u>
TOTAL SAMPLE WEIGHT	<u>1289.14 lbs</u>

% + #4 (COBBLES) 81.9 %

% - #4 (FINES) 18.1 %

APPENDIX E
LABORATORY RADIOLOGICAL TEST RESULTS

**VENDOR LABORATORY RADIOLOGICAL
MEASUREMENTS: COMPOSITE SOIL SAMPLES >#4
MESH SIEVE**



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

31-Jan-94

Attn:
Project: Rifle

Received: 21-Dec-93 11:38
PO #: 3050451110740 #338

Job: 939351E

Status: Final



ANALYTICAL REPORT PACKAGE

CASE NARRATIVE	i
ANALYTICAL RESULTS	R-1
QUALITY CONTROL REPORT	Q-1

accept and
forwarded to Board
Chairman for

FOR INFORMATION ONLY



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

31-Jan-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

Page: i
Copy: 1 of 3

Attn: Received: 21-Dec-93 11:38
Project: Rifle PO #: 3050-511-10740 #338

Job: 939351E Status: Final

CASE NARRATIVE

A total of 23 Soil samples were received on 21-Dec-93. All were properly preserved and in good condition. As stated in the chain of custody, the samples were run for the following analyses: Ra-226 and Th-230. Our procedures are summarized on the Quality Control Data Sheet. All samples were extracted and analyzed within the proper holding times.

Quality control standards for organic and inorganic analyses followed the appropriate SW-846 or EPA methodology. For radiochemistry, the acceptance criteria for spikes and laboratory control standards is fifteen percent, plus the counting error. Duplicates will pass if the Replicate Error Ratio (RER) is 1.00 or less. The RER is defined as follows:

$$\text{RER} = \frac{\text{ABS}(R_2 - R_1)}{\text{SQRT}(\text{ERROR}_1^2 + \text{ERROR}_2^2)}$$

where: R_1/R_2 = original/duplicate sample result
 $\text{ERROR}_1/\text{ERROR}_2$ = total 2 sigma uncertainty of R_1/R_2

All QC checks, including duplicates, spikes, and blanks, passed.

Signed:

Steve L. Sincoff
Steven L. Sincoff, Ph.D.
Director of Operations



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

31-Jan-94

Page: R-1

Copy: 1 of 3

Status: Final

MK-FERGUSON (Rifle)

Analyte: Ra-226

Project: Rifle

Fraction: Total

Date Analyzed: 01/25-01/31

Method: SM-705

LLD: 0.3

Units: pCi/g

Date

Lab Id	Sampled	Matrix	Sample Id	Concentration+ 2 σ
939351-1	30-Nov-93	Soil	RFL-SS-2649-01-CTF	1.1±0.6 -
939351-2	6-Dec-93	Soil	RFL-SS-2650-02-CTF	0.7±0.5 -
939351-3	7-Dec-93	Soil	RFL-SS-2651-03-CTF	1.7±0.7 -
939351-4	7-Dec-93	Soil	RFL-SS-2652-04-CTF	0.6±0.5 -
939351-5	7-Dec-93	Soil	RFL-SS-2653-05-CTF	1.4±0.6 -
939351-6	30-Nov-93	Soil	RFL-SS-2654-06-CTF	3.3±0.9 -
939351-7	7-Dec-93	Soil	RFL-SS-2655-07-CTF	2.0±0.7 -
939351-8	7-Dec-93	Soil	RFL-SS-2656-11-CTF	0.8±0.5 -
939351-9	6-Dec-93	Soil	RFL-SS-2657-15-CTF	0.9±0.5 -
939351-10	3-Dec-93	Soil	RFL-SS-2658-19-CTF	0.8±0.5 -
939351-11	2-Dec-93	Soil	RFL-SS-2659-20-CTF	0.5±0.4 -
939351-12	2-Dec-93	Soil	RFL-SS-2660-21-CTF	1.6±0.7 -
939351-13	10-Dec-93	Soil	RFL-SS-2661-22-CTF	0.9±0.5 -
939351-14	2-Dec-93	Soil	RFL-SS-2662-24-CTF	0.9±0.5 -
939351-15	1-Dec-93	Soil	RFL-SS-2663-25-CTF	0.8±0.5 -
939351-16	6-Dec-93	Soil	RFL-SS-2664-26-CTF	0.7±0.5 -
939351-17	6-Dec-93	Soil	RFL-SS-2665-27-CTF	0.8±0.5 -
939351-18	3-Dec-93	Soil	RFL-SS-2666-28-CTF	0.8±0.5 -
939351-19	3-Dec-93	Soil	RFL-SS-2667-29-CTF	2.1±0.8 -
939351-20	6-Dec-93	Soil	RFL-SS-2668-30-CTF	1.2±0.6 -
939351-21	7-Dec-93	Soil	RFL-SS-2669-31-CTF	0.9±0.5 -
939351-22	9-Dec-93	Soil	RFL-SS-2670-32-CTF	1.8±0.7 -
939351-23	9-Dec-93	Soil	RFL-SS-2671-33-CTF	1.6±0.7 -

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BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

31-Jan-94

Page: R-2

Copy: 1 of 3

Status: Final

MK-FERGUSON (Rifle)

Analyte: Th-230

Fraction: Total

Method: USAEC

Units: pCi/g

Project: Rifle

Date Analyzed: 01/20-01/26

LLD: 0.4

<u>Lab Id</u>	<u>Date Sampled</u>	<u>Matrix</u>	<u>Sample Id</u>	<u>Concentration+ 2σ</u>
939351-1	30-Nov-93	Soil	RFL-SS-2649-01-CTF	1.1±0.4-
939351-2	6-Dec-93	Soil	RFL-SS-2650-02-CTF	0.9±0.4-
939351-3	7-Dec-93	Soil	RFL-SS-2651-03-CTF	0.5±0.3-
939351-4	7-Dec-93	Soil	RFL-SS-2652-04-CTF	0.7±0.3-
939351-5	7-Dec-93	Soil	RFL-SS-2653-05-CTF	0.3±0.2-
939351-6	30-Nov-93	Soil	RFL-SS-2654-06-CTF	1.6±0.5-
939351-7	7-Dec-93	Soil	RFL-SS-2655-07-CTF	1.7±0.5-
939351-8	7-Dec-93	Soil	RFL-SS-2656-11-CTF	0.4±0.3-
939351-9	6-Dec-93	Soil	RFL-SS-2657-15-CTF	0.8±0.4-
939351-10	3-Dec-93	Soil	RFL-SS-2658-19-CTF	0.7±0.3-
939351-11	2-Dec-93	Soil	RFL-SS-2659-20-CTF	0.8±0.4-
939351-12	2-Dec-93	Soil	RFL-SS-2660-21-CTF	1.2±0.4-
939351-13	10-Dec-93	Soil	RFL-SS-2661-22-CTF	0.9±0.4-
939351-14	2-Dec-93	Soil	RFL-SS-2662-24-CTF	0.7±0.4-
939351-15	1-Dec-93	Soil	RFL-SS-2663-25-CTF	1.3±0.5-
939351-16	6-Dec-93	Soil	RFL-SS-2664-26-CTF	0.5±0.3-
939351-17	6-Dec-93	Soil	RFL-SS-2665-27-CTF	0.8±0.4-
939351-18	3-Dec-93	Soil	RFL-SS-2666-28-CTF	0.5±0.3-
939351-19	3-Dec-93	Soil	RFL-SS-2667-29-CTF	2.3±0.6-
939351-20	6-Dec-93	Soil	RFL-SS-2668-30-CTF	0.6±0.4-
939351-21	7-Dec-93	Soil	RFL-SS-2669-31-CTF	0.7±0.4-
939351-22	9-Dec-93	Soil	RFL-SS-2670-32-CTF	1.1±0.4-
939351-23	9-Dec-93	Soil	RFL-SS-2671-33-CTF	0.5±0.3-



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

31-Jan-94

Page: Q-1

Copy: 1 of 3

Status: Final

MK-FERGUSON (Rifle)

QUALITY CONTROL REPORT

Sample Id	Ra-226		Th-230	
	Total pCi/g	+ 2 σ	Total pCi/g	+ 2 σ
Duplicate	3.8	± 1.0	0.7	± 0.4
Duplicate	4.2	± 1.0	0.4	± 0.3
RER	0.18		0.46	
Std (found value)	80	± 6	101	± 7
Std (true value)	99		97	
Std % rec.	81		104	
Blank	0.0	± 0.1	0.0	± 0.1
Spike % rec.	96		77	

FOR INFORMATION ONLY



BARRINGER LABORATORIES INC.
15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

31-Jan-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

Page: Q-2
Copy: 1 of 3

Attn: Received: 21-Dec-93 11:38
Project: Rifle PO #: 3050-511-10740 #338

Job: 939351E Status: Final

Abbreviations:

Parameters:

Ra-226 : Radium-226
Th-230 : Thorium-230

Units:

pCi/g : picoCuries per gram



FOR INFORMATION ONLY

BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

31-Jan-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

Page: Q-3
Copy: 1 of 3

Attn: Received: 21-Dec-93 11:38
Project: Rifle PO #: 3050-511-10740 #338

Job: 939351E Status: Final

QUALITY CONTROL DATA SHEET

Received by: rc Via: Client

Sample Container Type: 5gal bucket
Additional Lab Preparation: None

Parameter	Method	Preservative	Analyst	Analysis Dates
Ra-226	SM-705	None	Lowrey	01/25-01/31
Th-230	USAEC	None	Kyle	01/20-01/26



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

31-Jan-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

Page: Q-4
Copy: 1 of 3

Attn:
Project: Rifle

Received: 21-Dec-93 11:38
PO #: 3050-511-10740 #338

Job: 939351E

Status: Final

Signed:

Helene Langlois
.....
Radiochemistry Manager

Barringer Laboratories, Inc. will return or dispose of your samples 30 days from the date your final report is mailed, unless otherwise specified by contract. Barringer Laboratories, Inc. reserves the right to return samples prior to the 30 days if radioactive levels exceed our license.

cc: Helene Langlois, MK-FERGUSON (Rifle)



LABORATORY SERVICES AUTHORIZATION FORM

Robert Fencil
Requisitioner

12/20/93
Date

24 hours	Need Date	Priority	<input checked="" type="checkbox"/> Urgent
1/21/94			<input checked="" type="checkbox"/> Standard

Rifle, CO
Location

3050-511-10740
P.O. Number

338
Request No.

ATTENTION LABORATORY:
All reports and invoices must
Reference PO and Request Nos

Type of Sample: Water Soil Environmental Air Sample
 Occupational Air Sample Vegetation

Type of Analysis: Ra-226 Th-230 Nat U. Gross Alpha
 Gross Beta Solubility
 Other (Specify under special instructions)

Special Instructions/Comments: _____

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
EL-SS-2649-01-CTF	11/30/93	~68 lbs	Test Pit #1 Cobbles
EL-SS-2650-02-CTF	12/1/93		Test Pit #2 Cobbles
EL-SS-2651-03-CTF	12/7/93		Test Pit #3 Cobbles
EL-SS-2652-04-CTF	12/7/93		Test Pit #4 Cobbles
EL-SS-2653-05-CTF	12/7/93		Test Pit #5 Cobbles
EL-SS-2654-06-CTF	11/30/93		Test Pit #6 Cobbles
EL-SS-2655-07-CTF	12/7/93		Test Pit #7 Cobbles
EL-SS-2656-11-CTF	12/7/93		Test Pit #11 Cobbles
EL-SS-2657-15-CTF	12/10/93		Test Pit #15 Cobbles
EL-SS-2658-19-CTF	12/3/93		Test Pit #19 Cobbles

CHAIN-OF-CUSTODY

Relinquished by (Site Representative Signature): <i>James Stadelman</i>	Date/Time 12-21-93 0700
Carrier: <i>Donald Frank</i>	Date/Time 12-21-93 0700
Received at Lab by (Lab Representative Signature):* <i>Donald Frank</i>	Date/Time 12-21-93 1138

Barringer Chain-of-Custody as per contract will be attached

MK-F/CWMFES USE ONLY:

Elly Walker

MK-F Site Manager

Technical Review:

Robert Fencil

Health Physics Site Manager

Date:

Approved Vendor
For Radioanalytical Services

Copy to: HPP Manager



FOR INFORMATION ONLY

935

LABORATORY SERVICES AUTHORIZATION FORM
(CONTINUATION PAGE)

Page 2 of 2

3050-511-10740/33
P.O. Number/Request Nu

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
RFL-SS-2659-20-CTF	12/2/93	-68 lbs	Test Pit #20 Cobb
RFL-SS-2660-21-CTF	12/2/93		Test Pit #21 Cobb
RFL-SS-2661-22-CTF	12/10/93		Test Pit #22 Cobb
RFL-SS-2662-24-CTF	12/2/93		Test Pit #24 Cobb
RFL-SS-2663-25-CTF	12/1/93		Test Pit #25 Cobb
RFL-SS-2664-26-CTF	12/6/93		Test Pit #26 Cobb
RFL-SS-2665-27-CTF	12/6/93		Test Pit #27 Cobb
RFL-SS-2666-28-CTF	12/3/93		Test Pit #28 Cobb
RFL-SS-2667-29-CTF	12/3/93		Test Pit #29 Cobb
RFL-SS-2668-30-CTF	12/6/93		Test Pit #30 Cobb
RFL-SS-2669-31-CTF	12/7/93		Test Pit #31 Cobb
RFL-SS-2670-32-CTF	12/9/93		Test Pit #32 Cobb
RFL-SS-2671-33-CTF	12/9/93	↓	Test Pit #33 Cobb

N

A

ENGINEERS
AND
CONSTRUCTORS



HEADQUARTERS OFFICE
ONE ERIEVIEW PLAZA
CLEVELAND, OHIO U.S.A. 44114
PHONE: (216) 523-3800 TELEX 685542

FOR INFORMATION ONLY

*Rich C -
please file in folder
Thanks,
June

REPLY TO: MK-FERGUSON COMPANY
REMEDIAL ACTIONS
CONTRACTOR-LMTRIA PROJECT
P.O. BOX 8130
ALBUQUERQUE, NEW MEXICO U.S.A. 87110

January 5, 1994

Barringer Laboratories
15000 West 6th Avenue, Suite 300
Golden, Colorado 80401
Attn: June Brennan

Subject: Job No. 9351 - Rifle Site

Dear Ms. Brennan:

As per discussions today with Jim Turner, Barringer Laboratories is authorized to subcontract sample preparation work for samples containing large stone and cobbles for the subject Job Number.

Please contact Jim Turner at (505) 845-5868, if you have any questions.

Sincerely,

MK-Ferguson Company

D.L. Blasdel

Don L. Blasdel
Procurement Manager

DLB/JBT/jmg

Fax: 94-35
Date 1-5-94 4:19 P.M.
Delivered to June

Received by Veronica
BARRINGER LABORATORIES, INC.

BLI Job #93 9351

Rec'd Date 12-21-93

DECS3-PM-LabData11-CUSTODIAL

BARRINGER LABORATORIES, INC.
Internal Chain-of-Custody Record

6035i

**VENDOR LABORATORY RADIOLOGICAL
MEASUREMENTS: COMPOSITE SOIL SAMPLES <#4
MESH SIEVE**

FOR INFORMATION ONLY

Recd. 3/14/94



BARRINGER LABORATORIES INC.

15000 W 8TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

9-Mar-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

Attn:
Project: Rifle

Received: 28-Feb-94 09:20
PO #: 3050-511-10740 #356

Job: 941417E

Status: Final

ANALYTICAL REPORT PACKAGE

CASE NARRATIVE i

ANALYTICAL RESULTS R-1

QUALITY CONTROL REPORT.....Q-1

FOR INFORMATION ONLY



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

9-Mar-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

Page: i
Copy: 1 of 3

Attn: Received: 28-Feb-94 09:20
Project: Rifle PO #: 3050-511-10740 #356

Job: 941417E Status: Final

CASE NARRATIVE

A total of 22 Soil samples were received on 28-Feb-94. All were properly preserved and in good condition. As stated in the chain of custody, the samples were run for the following analyses: Ra-226 and Th-230. Our procedures are summarized on the Quality Control Data Sheet. All samples were extracted and analyzed within the proper holding times.

Quality control standards for organic and inorganic analyses followed the appropriate SW-846 or EPA methodology. For radiochemistry, the acceptance criteria for spikes and laboratory control standards is fifteen percent, plus the counting error. Duplicates will pass if the Replicate Error Ratio (RER) is 1.00 or less. The RER is defined as follows:

$$\text{RER} = \frac{\text{ABS}(\text{R}_2 - \text{R}_1)}{\text{SQRT}(\text{ERROR}_1^2 + \text{ERROR}_2^2)}$$

where: R_1/R_2 = original/duplicate sample result
 $\text{ERROR}_1/\text{ERROR}_2$ = total 2 sigma uncertainty of R_1/R_2

All QC checks, including duplicates, spikes, and blanks, passed.

Signed:

..... *Steven L. Sincoff*

Steven L. Sincoff, Ph.D.
Director of Operations



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

9-Mar-94

Page: R-1

Copy: 1 of 3

Status: Final

MK-FERGUSON (Rifle)

Analyte: Ra-226

Project: Rifle

Fraction: Total

Date Analyzed: 03/04/03/08

Method: SM-705

LLD: 0.3

Units: pCi/g

Lab Id	Sampled	Matrix	Sample Id	Date	Concentration+ 2 σ
941417-1	6-Dec-93	Soil	RFL-SS-2596-TP-1-CTF		4.6±1.1
941417-2	6-Dec-93	Soil	RFL-SS-2598-TP-2-CTF		1.7±0.7
941417-3	7-Dec-93	Soil	RFL-SS-2600-TP-3-CTF		1.9±0.7
941417-4	7-Dec-93	Soil	RFL-SS-2602-TP-4-CTF		7.4±1.4
941417-5	7-Dec-93	Soil	RFL-SS-2604-TP-5-CTF		2.5±0.8
941417-6	7-Dec-93	Soil	RFL-SS-2606-TP-7-CTF		220±10
941417-7	7-Dec-93	Soil	RFL-SS-2608-TP-11-CTF		4.2±1.1
941417-8	6-Dec-93	Soil	RFL-SS-2610-TP-15-CTF		6.3±1.4
941417-9	2-Dec-93	Soil	RFL-SS-2612-TP-19-CTF		6.5±1.3
941417-10	2-Dec-93	Soil	RFL-SS-2614-TP-20-CTF		8.6±1.5
941417-11	6-Dec-93	Soil	RFL-SS-2616-TP-21-CTF		32±3
941417-12	6-Dec-93	Soil	RFL-SS-2618-TP-22-CTF		2.4±0.8
941417-13	1-Dec-93	Soil	RFL-SS-2620-TP-24-CTF		2.6±0.8
941417-14	1-Dec-93	Soil	RFL-SS-2622-TP-25-CTF		5.4±1.2
941417-15	6-Dec-93	Soil	RFL-SS-2624-TP-26-CTF		1.9±0.7
941417-16	3-Dec-93	Soil	RFL-SS-2626-TP-27-CTF		3.2±0.9
941417-17	9-Dec-93	Soil	RFL-SS-2628-TP-28-CTF		4.2±1.0
941417-18	6-Dec-93	Soil	RFL-SS-2630-TP-29-CTF		110±10
941417-19	6-Dec-93	Soil	RFL-SS-2632-TP-30-CTF		3.0±0.9
941417-20	9-Dec-93	Soil	RFL-SS-2634-TP-32-CTF		1.7±0.7
941417-21	9-Dec-93	Soil	RFL-SS-2636-TP-33-CTF		1.6±0.7
941417-22	7-Dec-93	Soil	RFL-SS-2638-TP-BKG-CTF		1.8±0.8



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

9-Mar-94

Page: R-2

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Status: Final

MK-FERGUSON (Rifle)

Analyte: Th-230

Project: Rifle

Fraction: Total

Date Analyzed: 03/03-03/08

Method: USAEC

LLD: 0.4

Units: pCi/g

Date

Lab Id	Sampled	Matrix	Sample Id	Concentration+ 2 σ
941417-1	6-Dec-93	Soil	RFL-SS-2596-TP-1-CTF	3.1±0.7
941417-2	6-Dec-93	Soil	RFL-SS-2598-TP-2-CTF	2.3±0.6
941417-3	7-Dec-93	Soil	RFL-SS-2600-TP-3-CTF	5.7±1.0
941417-4	7-Dec-93	Soil	RFL-SS-2602-TP-4-CTF	6.6±1.0
941417-5	7-Dec-93	Soil	RFL-SS-2604-TP-5-CTF	2.3±0.6
941417-6	7-Dec-93	Soil	RFL-SS-2606-TP-7-CTF	120±4
941417-7	7-Dec-93	Soil	RFL-SS-2608-TP-11-CTF	8.9±1.2
941417-8	6-Dec-93	Soil	RFL-SS-2610-TP-15-CTF	13±1
941417-9	2-Dec-93	Soil	RFL-SS-2612-TP-19-CTF	16±2
941417-10	2-Dec-93	Soil	RFL-SS-2614-TP-20-CTF	17±2
941417-11	6-Dec-93	Soil	RFL-SS-2616-TP-21-CTF	55±3
941417-12	6-Dec-93	Soil	RFL-SS-2618-TP-22-CTF	2.5±0.6
941417-13	1-Dec-93	Soil	RFL-SS-2620-TP-24-CTF	3.6±0.8
941417-14	1-Dec-93	Soil	RFL-SS-2622-TP-25-CTF	4.1±0.8
941417-15	6-Dec-93	Soil	RFL-SS-2624-TP-26-CTF	1.4±0.5
941417-16	3-Dec-93	Soil	RFL-SS-2626-TP-27-CTF	1.4±0.5
941417-17	9-Dec-93	Soil	RFL-SS-2628-TP-28-CTF	11±1
941417-18	6-Dec-93	Soil	RFL-SS-2630-TP-29-CTF	230±10
941417-19	6-Dec-93	Soil	RFL-SS-2632-TP-30-CTF	6.9±1.0
941417-20	9-Dec-93	Soil	RFL-SS-2634-TP-32-CTF	0.9±0.4
941417-21	9-Dec-93	Soil	RFL-SS-2636-TP-33-CTF	1.3±0.5
941417-22	7-Dec-93	Soil	RFL-SS-2638-TP-BKG-CTF	2.2±0.6

BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

9-Mar-94

Page: Q-1

Copy: 1 of 3

Status: Final

MK-FERGUSON (Rifle)**QUALITY CONTROL REPORT**

<u>Sample Id</u>	Ra-226	Th-230
	Total	Total
	pCi/g	+ 2 σ
Duplicate	0.0	± 0.2
Duplicate	0.3	± 0.4
RER	0.58	0.00
Std (found value)	91	± 6
Std (true value)	99	
Std % rec.	91	102
Blank	0.0	± 0.1
Spike % rec.	92	94



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

9-Mar-94

Page: Q-2
Copy: 1 of 3

Attn: Received: 28-Feb-94 09:20
Project: Rifle PO #: 3050-511-10740 #356

Job: 941417E Status: Final

Abbreviations:

Parameters:

Ra-226 : Radium-226
Th-230 : Thorium-230

Units:

pCi/g : picoCuries per gram



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

9-Mar-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

Page: Q-3
Copy: 1 of 3

Attn: Received: 28-Feb-94 09:20
Project: Rifle PO #: 3050-511-10740 #356

Job: 941417E Status: Final

QUALITY CONTROL DATA SHEET

Received by: rc Via: UPS

Sample Container Type: 500g can
Additional Lab Preparation: 100 mesh

Parameter	Method	Preservative	Analyst	Analysis Dates
Ra-226	SM-705	None	Lowrey	03/04-03/08
Th-230	USAEC	None	Melcher	03/03-03/08



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

9-Mar-94

Page: Q-4
Copy: 1 of 3

Attn:
Project: Rifle

Received: 28-Feb-94 09:20
PO #: 3050-511-10740 #356

Job: 941417E

Status: Final

Signed:

Gill V. Israel
.....
Radiochemistry Manager

Barringer Laboratories, Inc. will return or dispose of your samples 30 days from the date your final report is mailed, unless otherwise specified by contract. Barringer Laboratories, Inc. reserves the right to return samples prior to the 30 days if radioactive levels exceed our license.

cc: Helene Langlois, MK-FERGUSON (Rifle)



941417

LABORATORY SERVICES AUTHORIZATION FORM

Page 1 of 2

Dept Fencil
Requisitioner

2/25/94
Date

<u>3/14/94</u>		FOR INFORMATION ONLY
Need Data	<input checked="" type="checkbox"/>	Urgent
<input checked="" type="checkbox"/>		Priority
		Standard

file, CO
Location

3050-511-10740
P.O. Number

356
Request No.

ATTENTION LABORATORY:
All reports and invoices must
Reference PO and Request Nos.

Type of Sample: Water Soil Environmental Air Sample
 Occupational Air Sample Vegetation

Type of Analysis: Ra-226 Th-230 Nat U. Gross Alpha
 Gross Beta Solubility
 Other (Specify under special instructions)

Special Instructions/Comments: Fence, composite

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
L-SS-2596-TP-1-CTF	12/6/93	4539	TP-1 15-17'
L-SS-2598-TP-2-CTF	12/6/93	4739	TP-2 13-16'
L-SS-2600-TP-3-CTF	12/7/93	4509	TP-3 18-21'
L-SS-2602-TP-4-CTF	12/7/93	4539	TP-4 11-16'
L-SS-2604-TP-5-CTF	12/7/93	4529	TP-5 16-21'
L-SS-2606-TP-7-CTF	12/7/93	4329	TP-7 11-21' 390/904
L-SS-2608-TP-11-CTF	12/7/93	4239	TP-11 6-10'
L-SS-2610-TP-15-CTF	12/6/93	4609	TP-15 10-13'
L-SS-2612-TP-19-CTF	12/2/93	4509	TP-19 3.5-5.5'
L-SS-2614-TP-20-CTF	12/2/93	5209	TP-20 1-5'

CHAIN-OF-CUSTODY

<u>linquished by (Site Representative Signature):</u> <u>Bobbie R. Hickey</u>	Date/Time <u>2/25/94 @ 1047</u>
<u>Carrier:</u> <u>UPS Pickup Record # 272 076 087</u>	Date/Time
<u>Received at Lab by (Lab Representative Signature):*</u> <u>R. Cunzani</u>	Date/Time <u>02/28/94 0920</u>

Arranger Chain-of-Custody as per contract will be attached

K-F/CWMFES USE ONLY:

Scott B
K-F Site Manager

Health Physics Site Manager

Technical Review:

Date:

to: Approved Vendor
For Radioanalytical Services

Copy to: HPP Manager



94141

LABORATORY SERVICES AUTHORIZATION FORM
(CONTINUATION PAGE)

FOR INFORMATION ONLY

Page 2 of 1

3050-511-10740

P.O. Number/Request Nu

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
REL-SS-2616-TP-21-CTF	12/6/93	502 g	TP-21 1-5'
REL-SS-2618-TP-22-CTF	12/6/93	634 g	TP-22 4-7'
REL-SS-2620-TP-24-CTF	12/1/93	509 g	TP-24 2.5-5'
REL-SS-2622-TP-25-CTF	12/1/93	487 g	TP-25 6.5-8.5'
REL-SS-2624-TP-26-CTF	12/6/93	508 g	TP-26 8-9.5'
REL-SS-2626-TP-27-CTF	12/3/93	520 g	TP-27 9.5-11'
REL-SS-2628-TP-28-CTF	12/9/93	510 g	TP-28 0-15'
REL-SS-2630-TP-29-CTF	12/6/93	458 g	TP-29 0-3' 350/4
REL-SS-2632-TP-30-CTF	12/6/93	518 g	TP-30 4.5-7.5'
REL-SS-2634-TP-32-CTF	12/9/93	469 g	TP-32 0-4'
REL-SS-2636-TP-33-CTF	12/9/93	454 g	TP-33 0-4'
REL-SS-2638-TP-BKG-CTF	12/7/93	471 g	TP-BKG 7-12'

N

A

BARRINGER LABORATORIES, INC.

Internal Chain-of-Custody Record 0417

BLI Job #94	1417	Rec'd by <i>MM</i>
		Rec'd date <i>2-28-94</i>

How Disposed (circle one) Return / Waste / Sewer

Sign-off Date

BULK DRY

Sample Type

Soil

Comments

Sample #'s

22

Location

Soil

BULK COLD

Sample Type

Comments

Sample #'s

Location

PREPPED DRY

PREPPED COLD

Type *Soil*Analyst *JW*

Type

Analyst

Start *3/1/94*Complete *3/3/94*

Start

Complete

Comments

Sample #'s *1-22*Location *Soil Prep Shelf Y6*

Sample #'s

Location

Date	Samp #'	Time Out	Initials	Date	Samp #'	Time Out	Initials	Date	Samp #'	Time Out	Initials	Date	Samp #'	Time Out	Initials
3/1/94	6	0750	BS	3/1/94	0920	BS		3/3/94	2010	1-22	DM	3/3/94	2350	DM	
3/1/94	1-22	3:30	WW	3/1/94	12:30	WW		3/4/94	0215	0312	MM	3/4/94	0345	MM	

**VENDOR LABORATORY TH-230 MEASUREMENTS OF
1-FT DEPTH INCREMENT SOIL SAMPLES <#4 MESH**

BARRINGER LABORATORIES INC.

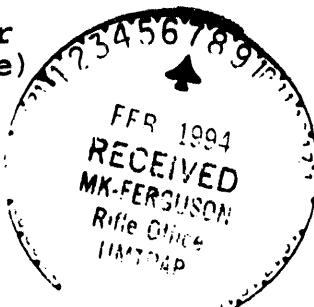
15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

1-Feb-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

Attn:
Project: Rifle

Job: 939420E



FOR INFORMATION ONLY

Received: 30-Dec-93 09:30
PO #: 3050-511-10740 #341

Status: Final

ANALYTICAL REPORT PACKAGE

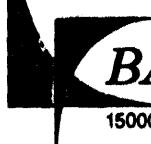
CASE NARRATIVE.....i

ANALYTICAL RESULTS.....R-1

QUALITY CONTROL REPORT.....Q-1

OK
RS

Inv.	Spec.	Info	Anal.	Qty
1	AVT-EE			
2	C5W0501			
3	EEF-CL			
4	SG-01			
5	SW-10			
6	SW-11			
7	SW-12			
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BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

1-Feb-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

FOR INFORMATION ONLY

Page: i
Copy: 1 of 3

Attn:
Project: Rifle

Received: 30-Dec-93 09:30
PO #: 3050-511-10740 #341

Job: 939420E

Status: Final

CASE NARRATIVE

A total of 30 Soil samples were received on 30-Dec-93. All were properly preserved and in good condition. As stated in the chain of custody, the samples were run for the following analysis: Th-230. Our procedures are summarized on the Quality Control Data Sheet. All samples were extracted and analyzed within the proper holding times.

Quality control standards for organic and inorganic analyses followed the appropriate SW-846 or EPA methodology. For radiochemistry, the acceptance criteria for spikes and laboratory control standards is fifteen percent, plus the counting error. Duplicates will pass if the Replicate Error Ratio (RER) is 1.00 or less. The RER is defined as follows:

$$\text{RER} = \frac{\text{ABS}(R_2 - R_1)}{\text{SQRT}(\text{ERROR}_1^2 + \text{ERROR}_2^2)}$$

where: R_1/R_2 = original/duplicate sample result
 $\text{ERROR}_1/\text{ERROR}_2$ = total 2 sigma uncertainty of R_1/R_2

All QC checks, including duplicates, spikes, and blanks, passed.

Signed:

.....
Steven L. Sincoff, Ph.D.
Director of Operations



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

1-Feb-94
 Page: R-1
 Copy: 1 of 3
 Status: Final

MK-FERGUSON (Rifle)
FOR INFORMATION ONLY

Analyte: Th-230

Fraction: Total

Method: USAEC

Units: pCi/g

Project: Rifle

Date Analyzed: 01/28-01/02

LLD: 0.4

Lab Id	Date	Sampled	Matrix	Sample Id	Concentration+ 2σ
939420-1	1-Dec-93	Soil	RFL-SS-2360	✓	16±2
939420-2	1-Dec-93	Soil	RFL-SS-2354	✓	2.7±0.7
939420-3	1-Dec-93	Soil	RFL-SS-2312	✓	1.2±0.5
939420-4	1-Dec-93	Soil	RFL-SS-2392	✓	1.9±0.6
939420-5	1-Dec-93	Soil	RFL-SS-2419	✓	32±2
939420-6	1-Dec-93	Soil	RFL-SS-2402	✓	40±2
939420-7	1-Dec-93	Soil	RFL-SS-2331	✓	15±2
939420-8	1-Dec-93	Soil	RFL-SS-2345	✓	7.3±1.1
939420-9	1-Dec-93	Soil	RFL-SS-2388	✓	1.9±0.6
939420-10	3-Dec-93	Soil	RFL-SS-2464	✓	9.3±1.2
939420-11	2-Dec-93	Soil	RFL-SS-2452	✓	12±1
939420-12	2-Dec-93	Soil	RFL-SS-2460	✓	8.8±1.2
939420-13	2-Dec-93	Soil	RFL-SS-2437	✓	1.2±0.5
939420-14	2-Dec-93	Soil	RFL-SS-2494	✓	1.0±0.4
939420-15	30-Nov-93	Soil	RFL-SS-2268	✓	32±2
939420-16	30-Nov-93	Soil	RFL-SS-2247	✓	3.8±0.8
939420-17	30-Nov-93	Soil	RFL-SS-2258	✓	0.9±0.4
939420-18	30-Nov-93	Soil	RFL-SS-2244	✓	10±1
939420-19	30-Nov-93	Soil	RFL-SS-2255	✓	4.5±0.9
939420-20	2-Dec-93	Soil	RFL-SS-2520	✓	4.1±0.8
939420-21	1-Dec-93	Soil	RFL-SS-2435	✓	19±2
939420-22	1-Dec-93	Soil	RFL-SS-2361	✓	5.7±0.9
939420-23	2-Dec-93	Soil	RFL-SS-2542	✓	1.8±0.5
939420-24	2-Dec-93	Soil	RFL-SS-2440	✓	7.7±1.1
939420-25	2-Dec-93	Soil	RFL-SS-2544	✓	4.2±0.8
939420-26	30-Nov-93	Soil	RFL-SS-2310	✓	1.6±0.5
939420-27	30-Nov-93	Soil	RFL-SS-2296	✓	1.2±0.5
939420-28	1-Dec-93	Soil	RFL-SS-2325	✓	8.1±1.1
939420-29	1-Dec-93	Soil	RFL-SS-2369	✓	12±1
939420-30	1-Dec-93	Soil	RFL-SS-2318	✓	5.2±0.9



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

1-Feb-94

Page: Q-1

Copy: 1 of 3

Status: Final

MK-FERGUSON (Rifle)

QUALITY CONTROL REPORT

Sample Id	Th-230 Total pCi/g	+ 2 σ
Duplicate	5.2	± 0.9
Duplicate	4.6	± 0.9
RER	0.24	
Std (found value)	292	± 12
Std (true value)	305	
Std % rec.	96	
Blank	0.1	± 0.2
Spike % rec.	101	

FOR INFORMATION ONLY



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

1-Feb-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

FOR INFORMATION ONLY

Page: Q-2
Copy: 1 of 3

Attn:
Project: Rifle

Received: 30-Dec-93 09:30
PO #: 3050-511-10740 #341

Job: 939420E

Status: Final

Abbreviations:

Parameters:

Th-230 : Thorium-230

Units:

pCi/g : picoCuries per gram



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

1-Feb-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

FOR INFORMATION ONLY

Page: Q-3
Copy: 1 of 3

Attn: Received: 30-Dec-93 09:30
Project: Rifle PO #: 3050-511-10740 #341

Job: 939420E Status: Final
QUALITY CONTROL REPORT

QUALITY CONTROL DATA SHEET

Received by: rc Via: UPS

Sample Container Type: 500g can
Additional Lab Preparation: 100 mesh

Parameter	Method	Preservative	Analyst	Analysis Dates
Th-230	USAEC	None	Ortiz	01/28-02/01



MK-FERGUSON COMPANY
A MORRISON KNUDSEN COMPANY



CWM Environmental Services, Inc.

9420

LABORATORY SERVICES AUTHORIZATION FORM

Robert Fencil
Requisitioner

12/29/93
Date

4 Jan 29/93
Need Date
Priority Urgent
 Standard

Rifle, CO
Location

3050-511-10740
P.O. Number

341
Request No.

ATTENTION LABORATORY:
All reports and invoices may
reference P.O. and Request Nos.

FOR INFORMATION ONLY

Type of Sample: Water Soil Environmental Air Sample
 Occupational Air Sample Vegetation

Type of Analysis: Ra-226 Th-230 Nat U. Gross Alpha
 Gross Beta Solubility
 Other (Specify under special instructions)

Special Instructions/Comments: _____

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
RFL-SS-2360	12-1-93	696 gm	TP # 20 OUP
RFL-SS-2354	12-1-93	567 gm	TP # 20 OUP
L-SS-2312	12-1-93	419 gm	TP # 25
RFL-SS-2392	12-1-93	664 gm	TP # 24
RFL-SS-2419	12-1-93	510 gm	TP # 30
RFL-SS-2402	12-1-93	607 gm	TP # 28
RFL-SS-2331	12-1-93	592 gm	TP # 26
RFL-SS-2345	12-1-93	669 gm	TP # 27
RFL-SS-2388	12-1-93	632 gm	TP # 22
RFL-SS-2464	12-3-93	636 gm	TP # 4A OUP

CHAIN-OF-CUSTODY

Relinquished by (Site Representative Signature):

Bonnie L. McCard

Date/Time

12/29/93 1000

Carrier:

UPS Pickup Record # 220576058

Date/Time

Received at Lab by (Lab Representative Signature):*

R.C. Integre

Date/Time

12/30/93 0930

* Barringer Chain-of-Custody as per contract will be attached

MK-F/CWMFES USE ONLY

MK-F Site Manager

Robert Fencil
Health Physics Site Manager

Technical Review:

Date:

Ship to: Approved Vendor
For Radioanalytical Services

Copy to: HPP Manager

942

**LABORATORY SERVICES AUTHORIZATION FORM
(CONTINUATION PAGE)**

FOR INFORMATION ONLY

Page 2 of 2

3050-511-10740/ 341
P.O. Number/Request Num.

Rec'd Date 12-30-42

DEC03:PM:LabData11:CUSTODY



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1688

FOR INFORMATION ONLY

MAR 1994

RECEIVED
MK-FERGUSON
Rifle Office
UMTRAP

9-Mar-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

Attn:
Project: Rifle

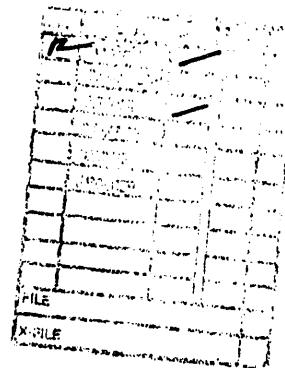
Received: 15-Feb-94 09:30
PO #: 3050-511-10740 #353

Job: 941337E

Status: Final

ANALYTICAL REPORT PACKAGE

CASE NARRATIVE.....	i
ANALYTICAL RESULTS.....	R-1
QUALITY CONTROL REPORT.....	Q-1





BARRINGER LABORATORIES INC.

FOR INFORMATION ONLY

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

9-Mar-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

Page: i
Copy: 1 of 3

Attn: Received: 15-Feb-94 09:30
Project: Rifle PO #: 3050-511-10740 #353

Job: 941337E

Status: Final

CASE NARRATIVE

A total of 5 Soil samples were received on 15-Feb-94. All were properly preserved and in good condition. As stated in the chain of custody, the samples were run for the following analysis: Th-230. Our procedures are summarized on the Quality Control Data Sheet. All samples were extracted and analyzed within the proper holding times.

Quality control standards for organic and inorganic analyses followed the appropriate SW-846 or EPA methodology. For radiochemistry, the acceptance criteria for spikes and laboratory control standards is fifteen percent, plus the counting error. Duplicates will pass if the Replicate Error Ratio (RER) is 1.00 or less. The RER is defined as follows:

$$\text{RER} = \frac{\text{ABS}(R2 - R1)}{\text{SQRT}(\text{ERROR1}^2 + \text{ERROR2}^2)}$$

where: R1/R2 = original/duplicate sample result
ERROR1/ERROR2 = total 2 sigma uncertainty of R1/R2

All QC checks, including duplicates, spikes, and blanks, passed.

Signed:

.....*Steven L. Sincoff*.....
Steven L. Sincoff, Ph.D.
Director of Operations



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

9-Mar-94

Page: R-1

Copy: 1 of 3

Status: Final

FOR INFORMATION ONLY

MK-FERGUSON (Rifle)

Analyte: Th-230

Project: Rifle

Fraction: Total

Date Analyzed: 03/07-03/09

Method: USAEC

LLD: 0.4

Units: pCi/g

Date

Lab Id	Sampled	Matrix	Sample Id	Concentration+ 2 σ
941337-1	1-Dec-93	Soil	RFL-SS-2405-TP28-CTF	30±2
941337-2	1-Dec-93	Soil	RFL-SS-2410-TP29-CTF	290±10
941337-3	1-Dec-93	Soil	RFL-SS-2424-TP30-CTF	22±2
941337-4	2-Dec-93	Soil	RFL-SS-2442-TP11-CTF	22±2
941337-5	2-Dec-93	Soil	RFL-SS-2446-TP11-CTF	25±2



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

9-Mar-94

Page: Q-1

Copy: 1 of 3

FOR INFORMATION Status: Final

MK-FERGUSON (Rifle)

QUALITY CONTROL REPORT

Th-230

Total

Sample Id	pCi/g	+ 2 σ
Duplicate	25	± 2
Duplicate	28	± 2
RER	0.35	
Std (found value)	103	± 8
Std (true value)	97	
Std % rec.	106	
Blank	0.1	± 0.3
Spike % rec.	121	



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

9-Mar-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

FOR INFORMATION ONLY Page: Q-2
Copy: 1 of 3

Attn:
Project: Rifle

Received: 15-Feb-94 09:30
PO #: 3050-511-10740 #353

Job: 941337E

Status: Final

Abbreviations:

Parameters:

Th-230 : Thorium-230

Units:

pCi/g : picoCuries per gram



BARRINGER LABORATORIES INC.

16000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION

9-Mar-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

Page: Q-3
Copy: 1 of 3

Attn: Received: 15-Feb-94 09:30
Project: Rifle PO #: 3050-511-10740 #353

Job: 941337E Status: Final

QUALITY CONTROL DATA SHEET

Received by: rc Via: UPS

Sample Container Type: 500g can
Additional Lab Preparation: 100 mesh

Parameter	Method	Preservative	Analyst	Analysis Dates
Th-230	USAEC	None	Ortiz	03/07-03/09



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

9-Mar-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

FOR INFORMATION ONLY

Page: Q-4
Copy: 1 of 3

Attn:
Project: Rifle

Received: 15-Feb-94 09:30
PO #: 3050-511-10740 #353

Job: 941337E

Status: Final

Signed:

.....
Radiochemistry Manager

Barringer Laboratories, Inc. will return or dispose of your samples 30 days from the date your final report is mailed, unless otherwise specified by contract. Barringer Laboratories, Inc. reserves the right to return samples prior to the 30 days if radioactive levels exceed our license.

cc: Helene Langlois, MK-FERGUSON (Rifle)

LABORATORY SERVICES AUTHORIZATION FORM

Page 1 of 1

Robert Fencil
Requisitioner

21/11/94
Date

<u>31/10/94</u>	<input checked="" type="checkbox"/> Urgent
<input type="checkbox"/> Need Data	<input type="checkbox"/> Standard
<input type="checkbox"/> Priority	

Rifle, CO

3050-511-10740
P.O. Number

353

FOR INFORMATION ONLY.

ATTENTION LABORATORY:
All reports and invoices must
reference P.O. and Request Nos

Type of Sample: Water Soil Environmental Air Sample
 Occupational Air Sample Vegetation

Type of Analysis: Ra-226 Th-230 Nat U. Gross Alpha
 Gross Beta Solubility
 Other (Specify under special instructions)

Special Instructions/Comments: _____

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
EL-SS-2405-TD28-CTF	12/1/93	100.8 g	TP#28 2-3'
EL-SS-2410-TD29-CTF	12/1/93	651 g	TP#29 2-3' 240 Pcs
EL-SS-2424-TD30-CTF	12/1/93	602 g	TP#30 7-8'
EL-SS-2442-TD11-CTF	12/2/93	624 g	TP#11 7-8'
EL-SS-2446-TD11-CTF	12/2/93	669 g	TP#11 9-10'
		N	
		A	

CHAIN-OF-CUSTODY

Released by (Site Representative Signature): <u>Bobbie V. Hickey</u>	Date/Time <u>2/11/94 @ 1600</u>
Carrier: <u>UPS Pick up Record # 212076082</u>	Date/Time <u>2/14/94</u>
Received at Lab by (Lab Representative Signature):* <u>R. C. Intzinger</u>	Date/Time <u>02/15/94 0530</u>

Arranger Chain-of-Custody as per contract will be attached

MK-F/CWMFES USE ONLY

MK-F Site Manager

Technical Review: _____

Robert Fencil
Health Physics Site Manager

Date: _____

to: Approved Vendor
For Radioanalytical Services

Copy to: HPP Manager



BARRINGER LABORATORIES, INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

FOR INFORMATION ON

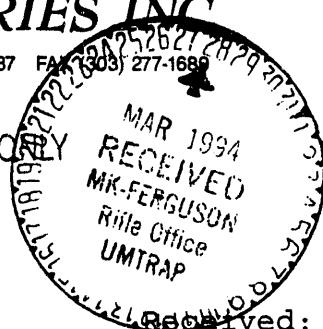
24-Mar-94

Attn:
Project: Rifle

RECEIVED: 16-Mar-94 09:25
PO #: 3050-511-10740 #360

Job: 941524E

Status: Final



ANALYTICAL REPORT PACKAGE

CASE NARRATIVE.....	i
ANALYTICAL RESULTS.....	R-1
QUALITY CONTROL REPORT.....	Q-1

special New Rifle CTF
OK R.F. 3-29-94



15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

24-Mar-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

FOR INFORMATION ONLY

Page: i
Copy: 1 of 3

Attn:
Project: Rifle

Received: 16-Mar-94 09:25
PO #: 3050-511-10740 #360

Job: 941524E

Status: Final

CASE NARRATIVE

A total of 9 Soil samples were received on 16-Mar-94. All were properly preserved and in good condition. As stated in the chain of custody, the samples were run for the following analysis: Th-230. Our procedures are summarized on the Quality Control Data Sheet. All samples were extracted and analyzed within the proper holding times.

Quality control standards for organic and inorganic analyses followed the appropriate SW-846 or EPA methodology. For radiochemistry, the acceptance criteria for spikes and laboratory control standards is fifteen percent, plus the counting error. Duplicates will pass if the Replicate Error Ratio (RER) is 1.00 or less. The RER is defined as follows:

$$\text{RER} = \frac{\text{ABS}(R_2 - R_1)}{\text{SQRT}(\text{ERROR}_1^2 + \text{ERROR}_2^2)}$$

where: R_1/R_2 = original/duplicate sample result
 $\text{ERROR}_1/\text{ERROR}_2$ = total 2 sigma uncertainty of R_1/R_2

All QC checks, including duplicates, spikes, and blanks, passed.

Signed:

..... *Steven L. Sincoff*

Steven L. Sincoff, Ph.D.
Director of Operations

BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

24-Mar-94

Page: R-1

Copy: 1 of 3

Status: Final

MK-FERGUSON (Rifle)**FOR INFORMATION ONLY****Analyte:** Th-230**Project:** Rifle**Fraction:** Total**Date Analyzed:** 03/21-03/22**Method:** USAEC**LLD:** 0.4**Units:** pCi/g

<u>Lab Id</u>	<u>Date Sampled</u>	<u>Matrix</u>	<u>Sample Id</u>	<u>Concentration</u> $\pm 2\sigma$
941524-1	30-Nov-93	Soil	RFL-SS-2272-CTF	7.6 \pm 1.1
941524-2	1-Dec-93	Soil	RFL-SS-2328-CTF	0.6 \pm 0.4
941524-3	1-Dec-93	Soil	RFL-SS-2357-CTF	0.6 \pm 0.4
941524-4	1-Dec-93	Soil	RFL-SS-2400-CTF	2.6 \pm 0.7
941524-5	1-Dec-93	Soil	RFL-SS-2401-CTF	38 \pm 2
941524-6	1-Dec-93	Soil	RFL-SS-2430-CTF	4.8 \pm 0.9
941524-7	1-Dec-93	Soil	RFL-SS-2432-CTF	44 \pm 3
941524-8	2-Dec-93	Soil	RFL-SS-2453-CTF	5.0 \pm 0.9
941524-9	2-Dec-93	Soil	RFL-SS-2456-CTF	23 \pm 2



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

24-Mar-94

Page: Q-1

Copy: 1 of 3

Status: Final

MK-FERGUSON (Rifle)

QUALITY CONTROL REPORT FOR INFORMATION ONLY

Th-230

Total

Sample Id	pCi/g	+ 2 σ
Duplicate	23	± 2
Duplicate	21	± 2
RER	0.28	
Std (found value)	327	± 13
Std (true value)	305	
Std % rec.	107	
Blank	0.0	± 0.2
Spike % rec.	90	



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

FOR INFORMATION ONLY

24-Mar-94

Page: Q-2
Copy: 1 of 3

Attn:
Project: Rifle

Received: 16-Mar-94 09:25
PO #: 3050-511-10740 #360

Job: 941524E

Status: Final

Abbreviations:

Parameters:

Th-230 : Thorium-230

Units:

pCi/g : picoCuries per gram



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

FOR INFORMATION ONLY

24-Mar-94

Page: Q-3
Copy: 1 of 3

Attn:
Project: Rifle

Received: 16-Mar-94 09:25
PO #: 3050-511-10740 #360

Job: 941524E

Status: Final

QUALITY CONTROL DATA SHEET

Received by: cs

Via: UPS

Sample Container Type: 500g can
Additional Lab Preparation: 100 mesh

Parameter	Method	Preservative	Analyst	Analysis Dates
Th-230	USAEC	None	Ortiz	03/21-03/22



BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

24-Mar-94

ATTN: Site Manager
MK-FERGUSON (Rifle)
P.O. Box 151
Rifle, CO 81650

FOR INFORMATION ONLY

Page: Q-4
Copy: 1 of 3

Attn:
Project: Rifle

Received: 16-Mar-94 09:25
PO #: 3050-511-10740 #360

Job: 941524E

Status: Final

Signed:

Helene Langlois
.....
Radiochemistry Manager

Barringer Laboratories, Inc. will return or dispose of your samples 30 days from the date your final report is mailed, unless otherwise specified by contract. Barringer Laboratories, Inc. reserves the right to return samples prior to the 30 days if radioactive levels exceed our license.

cc: Helene Langlois, MK-FERGUSON (Rifle)



LABORATORY SERVICES AUTHORIZATION FORM

Page 1 of 1

Albert Fencil
Requisitioner

3/14/94
Date

<u>4/1/94</u>	<input checked="" type="checkbox"/> Urgent
<input type="checkbox"/> Need Date	<input type="checkbox"/> Standard
<input checked="" type="checkbox"/> Priority	

Wife, CO
Location

3050-511-1074
P.O. Number

360
Request No.

ATTENTION LABORATORY:
All reports and invoices must
reference P.O. and Request Nos.

Type of Sample: Water Soil Environmental Air Sample
 Occupational Air Sample Vegetation

Type of Analysis: Ra-226 Th-230 Nat U. Gross Alpha
 Gross Beta Solubility
 Other (Specify under special instructions)

Special Instructions/Comments: _____

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
FL-SS-2272-CTF	11-30-93	627	TP #4
FL-SS-2328-CTF	12-01-93	517	TP #26
FL-SS-2357-CTF	12-01-93	582	TP #20
FL-SS-2400-CTF	12-01-93	648	TP #26
FL-SS-2401-CTF	12-01-93	610	TP #28
FL-SS-2430-CTF	12-01-93	531	TP #19
FL-SS-2432-CTF	12-01-93	534	TP #19
FL-SS-2453-CTF	12-02-93	537	TP #15
FL-SS-2456-CTF	12-02-93	531	TP #15

CHAIN-OF-CUSTODY

Relinquished by (Site Representative Signature):

Bobbie Dickey

Date/Time

3/14/94 1605

Carrier:

UPS DICKIE RECORD # 272 076 097

Date/Time

3/15/94

Received at Lab by (Lab Representative Signature):*

Stephenson

Date/Time

3-16-94 1925

Arranger Chain-of-Custody as per contract will be attached

NO FEE CHARGES USE ONLY

R. J. White

F Site Manager

Albert Fencil

Health Physics Site Manager

Date:

Technical Review:

**ON-SITE RADIOLOGICAL MEASUREMENTS OF 1-FT
DEPTH INCREMENT SOIL SAMPLES <#4 MESH SIEVE**

SITE NAME RIFLE, CO.

FOR INFORMATION ONLY

OCS SAMPLE LOG

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS *	Bi-214 PCl INITIAL 20 DAY	Tl-208 PCl INITIAL 20 DAY	MASS (grams) WET DRY	Ra-228 PCl/g INITIAL/CORR. 20 DAY	Th-232 PCl/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH	INITIAL 20 DAY	COMMENTS
11-20-93	RFL-SS-2237			400	512.1	853.3	404	1.3	2.1	✓	✓	✓	@ Surface
12-13-93	-001	11-19-93	11-22-93	566	502.1	537.0	363	1.4	1.5	✓	✓	✓	Main. Yard @ E.G. 601 cpm
11-20-93	RFL-SS-2238			500	274.7	795.9	401	0.69	2.0	✓	✓	✓	@ Surface
12-13-93	-002	11-19-93	11-22-93	468	459.2	722.7	350	1.3	2.1	✓	✓	✓	Main. Yard @ E.G. 573 cpm
11-20-93	RFL-SS-2239			402	636.3	522.4	336	1.9	1.6	✓	✓	✓	@ Surface
12-13-93	-003	11-19-93	11-22-93	568	550.1	709.6	291	1.8	2.4	✓	✓	✓	Main. Yard @ E.G. 546 cpm
11-22-93	RFL-SS-2240			510	345.9	113.2	522	0.66	2.2	✓	✓	✓	@ 18"
12-14-93	493	11-20-93	11-23-93	454	483.8	148.0	502	9.4	2.9	✓	✓	✓	10+65, 6+20 Lt.
11-22-93	RFL-SS-2241			412	1028.3	888.2	568	1.8	1.6	✓	✓	✓	@ 4'
12-14-93	493	11-20-93	11-23-93	548	1443.9	1419	515	2.8	2.8	✓	✓	✓	10+65, 4+80 Lt.
11-30-93	RFL-SS-2242			426	537.4	144	519	10.4	2.2	✓	✓	✓	TP#1
12-21-93	TP#1	11-30-93	12/1/93	130	1155.9	1115	452	24	2.3	✓	✓	✓	0-1
11-30-93	RFL-SS-2243			526	1737	882.2	550	5.2	1.6	✓	✓	✓	TP#1
12-21-93	TP#1	11-30-93	12/1/93	528	2841	1189	513	5.5	2.3	✓	✓	✓	1-2'
11-30-93	RFL-SS-2244			422	1187	896.9	503	2.4	1.8	✓	✓	✓	TP#1
12-21-93	TP#1	11-30-93	12/1/93	530	2011	1132	472	4.3	2.4	✓	✓	✓	2-3'
11-30-93	RFL-SS-2245			528	949.6	516.6	497	1.9	1.1	✓	✓	✓	TP#1
12-21-93	TP#1	11-30-93	12/1/93	434	1118	1001	456	2.5	2.2	✓	✓	✓	341
11-30-93	RFL-SS-2246			132	1894	819.5	608	3.1	1.4	✓	✓	✓	TP#1
12-23-93	TP#1	11-30-93	12/1/93	532	370	1247	523	5.9	2.4	✓	✓	✓	4-5'

Site Correction Factor = 1.8 2.0
 VP Correction Factor (if applicable) = 500
 Count Time = 500 sec., unless otherwise noted

REVIEWED BY: John Hartman
 Site Manager



MK-FE JSON COMPANY
A MORRIS KNUDSEN COMPANY



CWM Federal Environmental Services, Inc.

SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-228 pCi/g INITIAL/CORR. 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm 20 DAY	DEPTH >15cm 20 DAY	TECH INITIAL 20 DAY	COMMENTS
11/30/93	RFL-SS-2247			532	803	613.7	509	1.6	1.2	1.8	1.0	✓	TP#1
12/21/93	TP#1	11/30/93	12-1-93	532	885	1084	4600	1.9	2.4	✓	✓	✓	5-6'
11/30/93	RFL-SS-2248			434	521.7	896.9	495	1.1	1.8	✓	✓	✓	TP#1
12/21/93	TP#1	11/30/93	12-1-93	534	613	1132	450	1.4	2.5	✓	✓	✓	6-7'
11/30/93	RFL-SS-2249			534	845.8	871.7	501	1.7	1.7	✓	✓	✓	TP#1
12/21/93	TP#1	11/30/93	12-1-93	436	806	984	467	1.7	2.1	✓	✓	✓	7-8'
11/30/93	RFL-SS-2250			436	560.3	1106	566	0.99	2.0	✓	✓	✓	TP#1
12/22/93	TP#1	11/30/93	12/2/93	440	781.7	1001	516	1.5	1.9	✓	✓	✓	8-9'
11/30/93	RFL-SS-2251			536	588.6	738.4	553	1.1	1.3	✓	✓	✓	TP#1
12/21/93	TP#1	11/30/93	12-1-93	438	685	975	508	1.3	1.9	✓	✓	✓	9-10'
11/30/93	RFL-SS-2252			438	109.8	810.7	599	1.2	1.5	✓	✓	✓	TP#1
12/22/93	TP#1	11/30/93	12/2/93	540	1055	863.0	535	2.0	1.6	✓	✓	✓	10-11'
11/30/93	RFL-SS-2253			538	1130	805.5	548	2.1	1.5	✓	✓	✓	TP#1
12/21/93	TP#1	11/30/93	12-1-93	536	802	1141	506	1.6	2.3	✓	✓	✓	11-12'
11/30/93	RFL-SS-2254			440	763.4	914.3	585	1.3	1.6	✓	✓	✓	TP#1
12/21/93	TP#1	11-30-93	12-1-93	538	491	969	541	0.91	1.8	✓	✓	✓	12'-13'
11/30/93	RFL-SS-2255			540	607.7	1151	607	1.0	1.9	✓	✓	✓	TP#1
12/21/93	TP#1	11-30-93	12-1-93	440	986	1028	550	1.8	1.9	✓	✓	✓	13'-14'
11/30/93	RFL-SS-2256			442	740.2	1045	649	1.1	1.6	✓	✓	✓	TP#1
12/21/93	TP#1	11-30-93	12-1-93	552	1193	873	602	2.0	1.5	✓	✓	✓	14'-15' Screened*4

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY:

Robert H. Finsel
Site HP Manager

SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (gramme) WET DRY	Ra-228 pCi/g INITIAL/CORR. 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm 20 DAY	DEPTH >15cm 20 DAY	TECH INITIAL 20 DAY	COMMENTS
11-30-93	RFL-SS-2257			542	750.2	1122	679	1.1	1.7			✓	TP#1
12-28-93	TP#1 - DUP	11-30-93	12-2-93	454	541.5	914.3	587	0.92	1.6	✓	DEC		14'-15' Screened #4
11-30-93	RFL-SS-2258			444	481.5	916.5	696	0.69	1.4			✓	TP#1
12-21-93	TP#1	11-30-93	12-1-93	454	679	1170	653	1.0	1.8	✓		✓	15'-16' Screened #4
11-30-93	RFL-SS-2259			544	652.1	1074	668	0.98	1.6			✓	TP#1
12-28-93	TP#1 - DUP	11-30-93	12-2-93	452	543.1	1036	592	0.92	1.8	✓	DEC		15'-16' Screened #4
11-30-93	RFL-SS-2260			446	528.7	1010	732	0.73	1.4			✓	TP#1
12-22-93	TP#1	11-30-93	12/2/93	442	798.4	1062	601	1.3	1.8	✓		✓	16'-17' Screened #4
11-30-93	RFL-SS-2261			546	906.8	911.0	770	1.2	1.2			✓	TP#1
12-28-93	TP#1 - DUP	11-30-93	12/2/93	453	522	809.8	611	0.85	1.3	✓	DEC		16'-17' Screened #4
11-30-93	RFL-SS-2262			454	261040	8890	550	475	16.1			✓	TP#4
12-21-93	TP#4	11-30-93	12-1-93	554	382540	17635	505	758	35	✓		✓	0-1'
11-30-93	RFL-SS-2263			554	266640	11824	573	465	21			✓	TP#4
12-21-93	TP#4	11-30-93	12-1-93	456	349720	11990	527	664	23	✓		✓	1'-2'
11-30-93	RFL-SS-2264			456	282280	10736	581	486	18			✓	TP#4
12-21-93	TP#4	11-30-93	12-1-93	556	414310	20857	514	806	41	✓		✓	2'-3'
11-30-93	RFL-SS-2265			556	881530	46594	650	1356	72			✓	TP#4
12-22-93	TP#4	11-30-93	12/2/93	542	917900	61697	495	1980	125	✓		✓	3'-4'
11-30-93	RFL-SS-2266			458	856970	29892	604	1419	49			✓	TP#4
12-27-93	TP#4	11-30-93	12/2/93	400	959760	32192	453	2119	72	✓	DEC		4"-5"

Site Correction Factor = 1.8VP Correction Factor (if applicable) = 2.0Count Time = 500 sec., unless otherwise noted

REVIEWED BY:

John P. Finch
Site HP Manager

SITE NAME **RIFLE, CO.**

 OCS SAMPLE LOG **FOR INFORMATION ONLY**

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214 pCi INITIAL 20 DAY	Ti-208 pCi INITIAL 20 DAY	MASS (gram) WET DRY	Ra-228 pCi/g INITIAL/CONT. 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH ≤ 15cm > 15cm	TECH INITIAL 20 DAY	COMMENTS
												TP #4
11-30-93	RFL-SS-2267	11-30-93 10083	12/1/93	558	36629	2129	580	60	3.7	✓	TP	TP #4
12-21-93	TP#4			458	44658	2575	525	85	4.9	✓	TP	5'-6'
11-30-93	RFL-SS-2268			460	35265	2133	534	66	4.0	✓	TP	TP#4
12-21-93	TP#4	11-30-93	12/1/93	558	44725	2503	487	92	5.1	✓	TP	6'-7'
11-30-93	RFL-SS-2269			560	150.3	767.1	553	1.4	1.4	✓	TP	TP #4
12-21-93	TP#4	11-30-93	12/1/93	460	601	949	499	1.2	1.9	✓	TP	7'-8'
11-30-93	RFL-SS-2270			462	18151	1289	595	31	2.2	✓	TP	TP#4
12-21-93	TP#4	11-30-93	12/1/93	560	23625	1812	539	44	3.4	✓	TP	8'-9'
11-30-93	RFL-SS-2271			562	677.1	757.6	541	1.3	1.4	✓	TP	TP#4
12-31-93	TP#4	11-30-93	12/1/93	462	832	801	516	1.6	1.6	✓	TP	9'-10'
11-30-93	RFL-SS-2272			464	6445	1324	701	9.2	1.9	✓	TP	TP#4
12-21-93	TP#4	11-30-93	12/1/93	562	8385	1237	627	13	2.0	✓	TP	10'-11' Screened 4
11-30-93	RFL-SS-2273			564	5435	1208	690	7.9	1.8	✓	TP	TP#4
12-28-93	TP#4-DUP.	11-30-93	12-2-93	546	6570	1266	552	12	2.3	✓	TP	10'-11' Screened 4
11-30-93	RFL-SS-2274			466	1337	1062	645	2.1	1.6	✓	TP	TP#4
12-21-93	TP#4	11-30-93	12/1/93	464	1614	1132	601	2.7	1.9	✓	TP	13'-14' Screened 4
11-30-93	RFL-SS-2275			516	1121	958.9	639	1.8	1.5	✓	TP	TP #4
12-28-93	TP#4-DUP.	11-30-93	12/2/93	552	1195	1160	572	2.1	2.0	✓	TP	13'-14' Screened 4
11-30-93	RFL-SS-2276			472	5091	1080	586	8.7	1.8	✓	TP	TP #4
12-21-93	TP#4	11-30-93	12/1/93	466	5615	853	552	10	1.5	✓	TP	14'-15' Screened 4

 Site Correction Factor = 1.8

 VP Correction Factor (if applicable) = 2.0

 Count Time = 500 sec., unless otherwise noted

 REVIEWED BY: John H. Farber
 SITE HP Manager

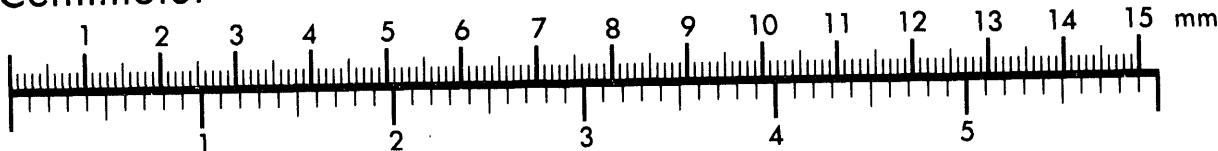


AIIM

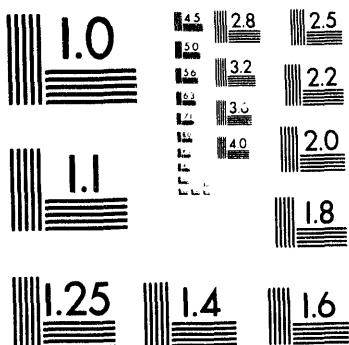
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3 of 3

SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214	Tl-208	MASS	Ra-226	Th-232	DEPTH	TECH	COMMENTS
					INITIAL 20 DAY	pCi INITIAL 20 DAY	pCi INITIAL 20 DAY	(grams) WET DRY	INITIAL/CORR. 20 DAY	pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	
11-30-93	RFL-SS-2277			573	6129	1103	620	9.9	1.8		PU	TP#4
12-28-93	TP#4-DUP	11-30-93	12-2-93	554	8020	1112	572	14	1.9	✓	DRC	14'-15' Screened 4
11-30-93	RFL-SS-2278			474	1255	1167	734	1.7	1.6		PU	TP#4
12-21-93	TP#4	11-30-93	12/1/93	564	1550	988	572	2.7	1.7	✓	SB	15'-16' Screened 4
11-30-93	RFL-SS-2279			575	1797	901.4	768	2.3	1.2		PU	TP#4
12-28-93	TP#4 - DUP	11-30-93	12/2/93	550	2166	1170	671	3.2	1.7	✓	DRC	15'-16' Screened 4
12/1/93	RFL-SS-2280			400	6602	1115	811	7.5	1.3		SB	TP#4
12/27/93	TP#4	11/30/93	12/2/93	402	8611	1202	776	11	1.5	✓	DRC	16-17' Screened 4
12/1/93	RFL-SS-2281			500	6324	1180	824	7.7	1.4		SB	TP#4
12/28/93	TP#4 - DUP	11/30/93	12/2/93	460	7105	1054	709	10	1.5	✓	DRC	16-17' Screened 4
12-1-93	RFL-SS-2282			502	15940	1889	798	20	2.4		PU	TP#4
12-27-93	TP#4	11-30-93	12-2-93	406	19325	1411	697	28	2.0	✓	DRC	17'-18' Screened 4
12-1-93	RFL-SS-2283			402	25979	1959	790	33	2.5		PU	TP#4
12-28-93	TP#4 - DUP	11-30-93	12-2-93	556	34033	1927	664	51	2.9	✓	DRC	17'-18' Screened 4
12-1-93	RFL-SS-2284			504	8549	129.5	775	11	1.7		PU	TP#4
12-27-93	TP#4	11-30-93	12-2-93	404	10678	1010	702	15	1.4	✓	DRC	18'-19'
12-1-93	RFL-SS-2285			404	28700	11067	559	514	20		PU	TP#5
12/22/93	TP#5	11-30-93	12/2/93	512	424670	22276	561	848	44	✓	SB	0'-1'
12-1-93	RFL-SS-2286			506	315560	15084	554	570	21		PU	TP#5
12/22/93	TP#5	11-30-93	12/2/93	444	435830	15430	494	882	31	✓	SB	1-2'

Site Correction Factor = 1.8VP Correction Factor (if applicable) = 2.0Count Time = 500 sec. unless otherwise notedREVIEWED BY: John T. Finch
Site HP Manager

SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-228 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH < 15cm > 15cm	TECH INITIAL 20 DAY	COMMENTS
12-1-93	RFL-SS- 2287			406	29780	10745	108	482	18		TP	TP #5
12/22/93	TP #5	11-30-93	12/2/93	514	42550	22450	540	788	42			2'-3'
12-1-93	RFL-SS- 2288			508	37615	18450	601	626	31		TP	TP #5
12/22/93	TP #5	11-30-93	12/2/93	416	46950	1577	528	889	29			3'-4'
12-1-93	RFL-SS- 2289			408	50440	18782	538	938	35		TP	TP #5
12/22/93	TP #5	11-30-93	12/2/93	516	10440	39016	466	1518	84			4'-5'
12-1-93	RFL-SS- 2290			510	620950	33745	639	972	53		TP	TP #5
12/22/93	TP #5	11-30-93	12/2/93	418	15380	23527	552	1329	43			5'-6'
12/1/93	RFL-SS- 2291			410	621290	23667	653	953	36			TP #5
12/22/93	TP #5	11/30/93	12/2/93	518	862430	51379	574	1502	90			7'-8' 6-7'
12/1/93	RFL-SS- 2292			512	546950	31299	533	1026	57			TP #5
12/22/93	TP #5	11/30/93	12/2/93	420	223750	24137	467	1550	52			7'-8'
12/1/93	RFL-SS- 2293			412	479130	17085	612	783	30			TP #5
12/22/93	TP #5	11/30/93	12/2/93	520	688400	39661	539	1277	74			9-10'
12/1/93	RFL-SS- 2294			514	647550	27740	540	1166	67			TP #5
12/22/93	TP #5	11/30/93	12/2/93	422	136020	2282	472	1559	53			10-11'
12/1/93	RFL-SS- 2295			414	1871	99216	540	3.5	1.8			TP #5
12/22/93	TP #5	11/30/93	12/2/93	522	1443	1180	482	3.0	2.4			11-12'
12/1/93	RFL-SS- 2296			516	2581	1285	716	3.6	1.8			TP #5
12/22/93	TP #5	11/30/93	12/2/93	424	1161	8212	62	1.3	1.4			12-13'

 Site Correction Factor = 1.8

 VP Correction Factor (if applicable) = 2.0

 Count Time = 500 sec., unless otherwise noted

 REVIEWED BY: John H. Jones

Site Manager

SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214 PCI INITIAL 20 DAY	Tl-208 PCI INITIAL 20 DAY	MASS (grams) WET DRY	Ra-226 PCI/g INITIAL 20 DAY	Th-232 PCI/g INITIAL 20 DAY	DEPTH ≤ 15cm > 15cm	TECH INITIAL 20 DAY	COMMENTS
12/1/93	RFL-SS- 2297	11/30/93	12/2/93	416	668.8	1019	618	1.1	1.1			TP #5
12/22/93	TP#5	11/30/93	12/2/93	524	985.7	901.4	550	1.8	1.6			13-14'
12/1/93	RFL-SS- 2298			518	613.7	1314	707	0.87	1.9			TP #5
12/22/93	TP#5	11/30/93	12/2/93	486	723.1	783.7	636	1.1	1.2			14-15'
12/1/93	RFL-SS- 2299	11/30/93	12/2/93	418	489090	18172	501	976.2	36.3			TP #5
12/22/93	TP#5	11/30/93	12/2/93	526	108260	44801	410	1727	109			8-9'
12/1/93	RFL-SS- 2300			520	772.6	1132	720	1.1	1.6			TP #5
12/22/93	TP#5	11/30/93	12/2/93	428	726.4	1028	639	1.1	1.6			15-16'
12/1/93	RFL-SS- 2301	11/30/93	12/2/93	420	1880	821.2	697	2.7	1.2			TP #5
12/22/93	TP#5	11/30/93	12/2/93	528	931.4	1036	599	1.6	1.7			16-17'
12/1/93	RFL-SS- 2302			523	3241	1026	771	4.2	1.3			TP #5
12/22/93	TP#5	11/30/93	12/2/93	430	3731	1028	675	5.5	1.5			16-17' screened
12/1/93	RFL-SS- 2303			422	4408	914.3	722	6.1	1.3			TP #25
12/22/93	TP#25	12/1/93	12/2/93	530	4667	930.2	595	7.8	1.6			C 10'
12/1/93	RFL-SS- 2304	11/30/93	12/2/93	524	3575	1045	809	4.4	1.3			TP #5
12/28/93	TP#5-Dup	12/1/93	12/2/93	402	3672	1239	649	5.7	2.0			TP #5
12/1/93	TP#5	11/30/93	12/3/93	424	10838	951.8	837	0.82	1.1			17-18' screened
12/28/93	TP#5	11/30/93	12/3/93	530	773.0	931.2	692	1.1	1.3			TP#5
12/1/93	RFL-SS- 2306			526	683.3	834.3	786	0.87	1.1			TP#5
12/28/93	TP#5-Dup	11/30/93	12/2/93	548	862.3	815.1	637	1.3	1.3			17-18' screened

Site Correction Factor = 1.8
 VP Correction Factor (if applicable) = 2.0
 Count Time = 500 sec. unless otherwise noted

REVIEWED BY: John J. Zeleny
 Site HP Manager

SITE NAME **RIFLE, CO.**
OCS SAMPLE LOG
FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-228 pCi/g INITIAL/CORR. 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12/1/93	RFL-SS- 2307			426	1794	870.7	757	2.4	1.2	P	B	TP#5
12/22/93	TP#5	11/30/93	12/2/93	432	2743	1036	661	4.1	1.6	✓	B	18-19' screened
12/1/93	RFL-SS- 2308			528	1552	1093	760	2.0	1.4		B	TP#5
12/28/93	TP#5-D10	11/30/93	12/2/93	456	2286	835.9	636	3.6	1.3	✓	DR	18-19' screened
12/1/93	RFL-SS- 2309			428	2231	870.7	789	2.8	1.1		B	TP#5
12-28-93	TP#5	11/30/93	12-3-93	526	2450	733.4	670	3.7	1.1	✓	DR	19-20'
12/1/93	RFL-SS- 2310			530	875.0	786.3	576	1.5	1.4		B	TP#6
12/22/93	TP#6	11/30/93	12/2/93	532	1190	652.1	517	2.3	1.3	✓	B	14-15'
12/1/93	RFL-SS- 2311			430	2804	801.1	501	5.6	1.6		B	TP#25
12/22/93	TP#25	11/30/93	12/2/93	434	4692	7924	465	10.0	1.7	✓	B	0-1'
12/1/93	RFL-SS- 2312			532	870.9	834.3	531	1.5	1.6		B	TP#25
12/27/93	TP#25	11/30/93	12/3/93	510	643.0	873.6	419	1.5	2.1	✓	DR	1-2'
12/1/93	RFL-SS- 2313			432	51311	2551	831	61.0	3.0		B	TP#6
12-28-93	TP #6	11/30/93	12-3-93	536	62733	2656	759	85	3.6	✓	DR	24-25'
12/1/93	RFL-SS- 2314			534	28096	2206	883	32	2.5		B	TP#6
12/22/93	TP #6	11/30/93	12/2/93	534	33553	5254	826	41	2.7	✓	B	24-25'
12/1/93	RFL-SS- 2315			434	752.6	653.1	648	1.2	1.0		B	TP#25
12/28/93	TP #25	11/30/93	12/3/93	438	534.8	801.1	517	1.1	1.5	✓	DR	2-3'
12/1/93	RFL-SS- 2316			536	757.8	680.8	631	1.2	1.1		B	TP#25
12-28-93	TP# 25	11/30/93	12/3/93	534	526.1	949.3	503	10	1.9	✓	DR	3-4'

 Site Correction Factor = 1.8

 VP Correction Factor (if applicable) = 2.0

 Count Time = 500 sec., unless otherwise noted

 REVIEWED BY: John H. Finsell
 Site HP Manager

SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214	Tl-208	MASS	Ra-226	Th-232	DEPTH	TECH	COMMENTS
					INITIAL 20 DAY	pCi INITIAL 20 DAY	pCi INITIAL 20 DAY	(grams) WET DRY	pCi/g INITIAL/CORR. 20 DAY	pCi/g INITIAL 20 DAY	<15cm >15cm	
12-1-93	RFL-SS- 2317			436	1054	705.3	725	1.5	0.97		PU	TP#25
12-28-93	TP#25	12-1-93	12-3-93	432	845.2	905.6	556	1.4	1.5	✓	DRC	4'-5'
12-1-93	RFL-SS-2318			538	1875	882.2	615	3.0	1.4		PU	TP#25
12-27-93	TP#25	12-1-93	12-3-93	454	3358	853.3	502	6.7	1.7	✓	DRC	6'-7'
12-1-93	RFL-SS- 2319			438	841.8	653.1	722	1.2	0.90		PU	TP#25
12/22/93	TP#25	12-1-93	12/2/93	436	588.9	766.3	618	0.95	1.2	✓	PU	5'-6'
12-1-93	RFL-SS- 2320			540	318.2	1064.4	759	.42	1.4		PU	TP#25
12-28-93	TP#25	12-1-93	12-3-93	540	542.3	1232	607	0.89	2.0	✓	DRC	7'-8' SCience
12-1-93	RFL-SS- 2321			440	730.5	846.9	772	.95	1.2		PU	TP#25
12-28-93	TP#25-Dup	12-1-93	12-3-93	506	914.9	920.6	622	1.5	1.5	✓	DRC	7'-8' SCience
12-1-93	RFL-SS- 2322			542	607.5	796.1	765	.79	1.0		PU	TP#25
12-28-93	TP#25	12-1-93	12-3-93	528	362.9	901.4	634	0.57	1.4	✓	DRC	8'-9' SCience
12-1-93	RFL-SS- 2323			442	660.9	801.1	792	.83	1.0		PU	TP#25
12-28-93	TP 25-Dup	12-1-93	12-3-93	518	703.0	719.2	657	1.1	1.1	✓	DRC	8'-9' SCience
12-1-93	RFL-SS- 2324			544	3305	930.2	524	6.3	1.8		PU	TP#26
12/22/93	TP 26	12-1-93	12/2/93	536	5072	1028.5	475	11	2.1	✓	PU	0'-1'
12-1-93	RFL-SS- 2325			444	2144	801.1	529	4.1	1.5		PU	TP#26
12/22/93	TP#26	12-1-93	12/2/93	438	3457	1010	487	7.1	2.1	✓	PU	1'-2'
12-1-93	RFL-SS- 2326			546	1805	911.0	582	3.1	1.6		PU	TP#26
12/22/93	TP#26	12-1-93	12/2/93	538	3517	1064	529	6.8	2.0	✓	PU	2'-3

 Site Correction Factor = 1.8

 VP Correction Factor (if applicable) = 2.0

 Count Time = 500 sec., unless otherwise noted

 REVIEWED BY: John H. Finner

Site HP Manager

COUNT DATE	SAMPLE ID	LOCATION	DATE	SAMPLED	TECH						COMMENTS		
					OC8	BI-214	20 DAY	INITIAL	PC1	PC2	TH-232	DEPTH	
12-1-93	RFL-SS-2327	TF#226	12-1-93	446	744.3	914.3	668	1.2	1.5	2.8	441	559	31-4-1
12-1-93	RFL-SS-2328	TF#226	12-1-93	548	359.0	632.9	547	1.2	1.5	2.8	507.7	442	TF#226
12-1-93	RFL-SS-2329	TF#226	12-1-93	448	545.8	593.1	759	1.2	1.5	2.8	448	548	41-5-1
12-1-93	RFL-SS-2330	TF#226	12-1-93	550	589.7	661.7	757	1.2	1.5	2.8	550	550	41-7-1
12-1-93	RFL-SS-2331	TF#226	12-1-93	449	600.3	705.3	633	1.2	1.5	2.8	449	449	41-7-1
12-1-93	RFL-SS-2332	TF#226	12-1-93	450	612.3	681.9	715	1.2	1.5	2.8	450	450	41-7-1
12-1-93	RFL-SS-2333	TF#227	12-1-93	451	624.0	696.0	593	1.2	1.5	2.8	451	451	41-2-1
12-1-93	RFL-SS-2334	TF#227	12-1-93	452	634.0	704.8	632	1.2	1.5	2.8	452	452	41-3-1
12-1-93	RFL-SS-2335	TF#227	12-1-93	453	644.0	711.9	589	1.2	1.5	2.8	453	453	41-4-1
12-1-93	RFL-SS-2336	TF#227	12-1-93	454	654.0	719.0	535	1.2	1.5	2.8	454	454	41-5-1
12-1-93	RFL-SS-2337	TF#227	12-1-93	455	664.0	731.9	539	1.2	1.5	2.8	455	455	41-6-1
12-1-93	RFL-SS-2338	TF#227	12-1-93	456	674.0	739.0	370	1.2	1.5	2.8	456	456	41-7-1
12-1-93	RFL-SS-2339	TF#227	12-1-93	457	684.0	748.8	356	1.2	1.5	2.8	457	457	41-8-1
12-1-93	RFL-SS-2340	TF#227	12-1-93	458	694.0	758.0	352	1.2	1.5	2.8	458	458	41-9-1
12-1-93	RFL-SS-2341	TF#227	12-1-93	459	704.0	766.0	534	1.2	1.5	2.8	459	459	41-10-1
12-1-93	RFL-SS-2342	TF#227	12-1-93	460	714.0	774.0	531	1.2	1.5	2.8	460	460	41-11-1
12-1-93	RFL-SS-2343	TF#227	12-1-93	461	724.0	784.0	529	1.2	1.5	2.8	461	461	41-12-1
12-1-93	RFL-SS-2344	TF#227	12-1-93	462	734.0	794.0	525	1.2	1.5	2.8	462	462	41-13-1
12-1-93	RFL-SS-2345	TF#227	12-1-93	463	744.0	804.0	521	1.2	1.5	2.8	463	463	41-14-1
12-1-93	RFL-SS-2346	TF#227	12-1-93	464	754.0	814.0	517	1.2	1.5	2.8	464	464	41-15-1
12-1-93	RFL-SS-2347	TF#227	12-1-93	465	764.0	824.0	513	1.2	1.5	2.8	465	465	41-16-1
12-1-93	RFL-SS-2348	TF#227	12-1-93	466	774.0	834.0	510	1.2	1.5	2.8	466	466	41-17-1
12-1-93	RFL-SS-2349	TF#227	12-1-93	467	784.0	844.0	506	1.2	1.5	2.8	467	467	41-18-1
12-1-93	RFL-SS-2350	TF#227	12-1-93	468	794.0	854.0	502	1.2	1.5	2.8	468	468	41-19-1
12-1-93	RFL-SS-2351	TF#227	12-1-93	469	804.0	864.0	500	1.2	1.5	2.8	469	469	41-20-1
12-1-93	RFL-SS-2352	TF#227	12-1-93	470	814.0	874.0	496	1.2	1.5	2.8	470	470	41-21-1
12-1-93	RFL-SS-2353	TF#227	12-1-93	471	824.0	884.0	492	1.2	1.5	2.8	471	471	41-22-1
12-1-93	RFL-SS-2354	TF#227	12-1-93	472	834.0	894.0	488	1.2	1.5	2.8	472	472	41-23-1
12-1-93	RFL-SS-2355	TF#227	12-1-93	473	844.0	904.0	484	1.2	1.5	2.8	473	473	41-24-1
12-1-93	RFL-SS-2356	TF#227	12-1-93	474	854.0	914.0	480	1.2	1.5	2.8	474	474	41-25-1
12-1-93	RFL-SS-2357	TF#227	12-1-93	475	864.0	924.0	476	1.2	1.5	2.8	475	475	41-26-1
12-1-93	RFL-SS-2358	TF#227	12-1-93	476	874.0	934.0	472	1.2	1.5	2.8	476	476	41-27-1
12-1-93	RFL-SS-2359	TF#227	12-1-93	477	884.0	944.0	468	1.2	1.5	2.8	477	477	41-28-1
12-1-93	RFL-SS-2360	TF#227	12-1-93	478	894.0	954.0	464	1.2	1.5	2.8	478	478	41-29-1
12-1-93	RFL-SS-2361	TF#227	12-1-93	479	904.0	964.0	460	1.2	1.5	2.8	479	479	41-30-1
12-1-93	RFL-SS-2362	TF#227	12-1-93	480	914.0	974.0	456	1.2	1.5	2.8	480	480	41-31-1
12-1-93	RFL-SS-2363	TF#227	12-1-93	481	924.0	984.0	452	1.2	1.5	2.8	481	481	41-32-1
12-1-93	RFL-SS-2364	TF#227	12-1-93	482	934.0	994.0	448	1.2	1.5	2.8	482	482	41-33-1
12-1-93	RFL-SS-2365	TF#227	12-1-93	483	944.0	1004.0	444	1.2	1.5	2.8	483	483	41-34-1
12-1-93	RFL-SS-2366	TF#227	12-1-93	484	954.0	1014.0	440	1.2	1.5	2.8	484	484	41-35-1
12-1-93	RFL-SS-2367	TF#227	12-1-93	485	964.0	1024.0	436	1.2	1.5	2.8	485	485	41-36-1
12-1-93	RFL-SS-2368	TF#227	12-1-93	486	974.0	1034.0	432	1.2	1.5	2.8	486	486	41-37-1
12-1-93	RFL-SS-2369	TF#227	12-1-93	487	984.0	1044.0	428	1.2	1.5	2.8	487	487	41-38-1
12-1-93	RFL-SS-2370	TF#227	12-1-93	488	994.0	1054.0	424	1.2	1.5	2.8	488	488	41-39-1
12-1-93	RFL-SS-2371	TF#227	12-1-93	489	1004.0	1064.0	420	1.2	1.5	2.8	489	489	41-40-1
12-1-93	RFL-SS-2372	TF#227	12-1-93	490	1014.0	1074.0	416	1.2	1.5	2.8	490	490	41-41-1
12-1-93	RFL-SS-2373	TF#227	12-1-93	491	1024.0	1084.0	412	1.2	1.5	2.8	491	491	41-42-1
12-1-93	RFL-SS-2374	TF#227	12-1-93	492	1034.0	1094.0	408	1.2	1.5	2.8	492	492	41-43-1
12-1-93	RFL-SS-2375	TF#227	12-1-93	493	1044.0	1104.0	404	1.2	1.5	2.8	493	493	41-44-1
12-1-93	RFL-SS-2376	TF#227	12-1-93	494	1054.0	1114.0	400	1.2	1.5	2.8	494	494	41-45-1
12-1-93	RFL-SS-2377	TF#227	12-1-93	495	1064.0	1124.0	396	1.2	1.5	2.8	495	495	41-46-1
12-1-93	RFL-SS-2378	TF#227	12-1-93	496	1074.0	1134.0	392	1.2	1.5	2.8	496	496	41-47-1
12-1-93	RFL-SS-2379	TF#227	12-1-93	497	1084.0	1144.0	388	1.2	1.5	2.8	497	497	41-48-1
12-1-93	RFL-SS-2380	TF#227	12-1-93	498	1094.0	1154.0	384	1.2	1.5	2.8	498	498	41-49-1
12-1-93	RFL-SS-2381	TF#227	12-1-93	499	1104.0	1164.0	380	1.2	1.5	2.8	499	499	41-50-1
12-1-93	RFL-SS-2382	TF#227	12-1-93	500	1114.0	1174.0	376	1.2	1.5	2.8	500	500	41-51-1
12-1-93	RFL-SS-2383	TF#227	12-1-93	501	1124.0	1184.0	372	1.2	1.5	2.8	501	501	41-52-1
12-1-93	RFL-SS-2384	TF#227	12-1-93	502	1134.0	1194.0	368	1.2	1.5	2.8	502	502	41-53-1
12-1-93	RFL-SS-2385	TF#227	12-1-93	503	1144.0	1204.0	364	1.2	1.5	2.8	503	503	41-54-1
12-1-93	RFL-SS-2386	TF#227	12-1-93	504	1154.0	1214.0	360	1.2	1.5	2.8	504	504	41-55-1
12-1-93	RFL-SS-2387	TF#227	12-1-93	505	1164.0	1224.0	356	1.2	1.5	2.8	505	505	41-56-1
12-1-93	RFL-SS-2388	TF#227	12-1-93	506	1174.0	1234.0	352	1.2	1.5	2.8	506	506	41-57-1
12-1-93	RFL-SS-2389	TF#227	12-1-93	507	1184.0	1244.0	348	1.2	1.5	2.8	507	507	41-58-1
12-1-93	RFL-SS-2390	TF#227	12-1-93	508	1194.0	1254.0	344	1.2	1.5	2.8	508	508	41-59-1
12-1-93	RFL-SS-2391	TF#227	12-1-93	509	1204.0	1264.0	340	1.2	1.5	2.8	509	509	41-60-1
12-1-93	RFL-SS-2392	TF#227	12-1-93	510	1214.0	1274.0	336	1.2	1.5	2.8	510	510	41-61-1
12-1-93	RFL-SS-2393	TF#227	12-1-93	511	1224.0	1284.0	332	1.2	1.5	2.8	511	511	41-62-1
12-1-93	RFL-SS-2394	TF#227	12-1-93	512	1234.0	1294.0	328	1.2	1.5	2.8	512	512	41-63-1
12-1-93	RFL-SS-2395	TF#227	12-1-93	513	1244.0	1304.0	324	1.2	1.5	2.8	513	513	41-64-1
12-1-93	RFL-SS-2396	TF#227	12-1-93	514	1254.0	1314.0	320	1.2	1.5	2.8	514	514	41-65-1
12-1-93	RFL-SS-2397	TF#227	12-1-93	515	1264.0	1324.0	316	1.2	1.5	2.8	515	515	41-66-1
12-1-93	RFL-SS-2398	TF#227	12-1-93	516	1274.0	1334.0	312	1.2	1.5	2.8	516	516	41-67-1
12-1-93	RFL-SS-2399	TF#227	12-1-93	517	1284.0	1344.0	308	1.2	1.5	2.8	517	517	41-68-1
12-1-93	RFL-SS-2400	TF#227	12-1-93	518	1294.0	1354.0	304	1.2	1.5	2.8	518	518	41-69-1
12-1-93	RFL-SS-2401	TF#227	12-1-93	519	1304.0	1364.0	300	1.2	1.5	2.8	519	519	41-70-1
12-1-93	RFL-SS-2402	TF#227	12-1-93	520	1314.0	1374.0	296	1.2	1.5	2.8	520	520	41-71-1
12-1-93	RFL-SS-2403	TF#227	12-1-93	521	1324.0	1384.0	292	1.2	1.5	2.8	521	521	41-72-1
12-1-93	RFL-SS-2404	TF#227	12-1-93	522	1334.0	1394.0	288	1.2	1.5	2.8	522	522	41-73-1
12-1-93	RFL-SS-2405	TF#227	12-1-93	523	1344.0	1404.0	284	1.2	1.5	2.8	523	523	41-74-1
12-1-93	RFL-SS-2406	TF#227	12-1-93	524	1354.0	1414.0	280	1.2	1.5	2.8	524	524	41-75-1
12-1-93	RFL-SS-2407	TF#227	12-1-93	525	1364.0	1424.0	276	1.2	1.5	2.8	525	525	41-76-1
12-1-93	RFL-SS-2408	TF#227	12-1-93	526	1374.0	1434.0	272	1.2	1.5	2.8	526	526	41-77-1
12-1-93	RFL-SS-2409	TF#227	12-1-93	527	1384.0	1444.0	268	1.2	1.5	2.8	527	527	41-78-1
12-1-93	RFL-SS-2410	TF#227	12-1-93	528	1394.0	1454.0	264	1.2	1.5	2.8	528	528	

SITE NAME

RIFLE, CO.

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OCS SAMPLE LOG

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COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-226 pCi/g INITIAL/CORR. 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-1-93	RFL-SS- 2337 TP#27	12-1-93	12-2-93	456	55,241	2665	584	99	4.5	✓	PU	TP#27 5'-6'
12-28-93				468	81496	3596	545	150	6.7	✓	DRC	
12-1-93	RFL-SS- 2338 TP#27	12-1-93	12-2-93	558	473560	24,922	564	840	44		PU	TP#27 6'-7'
12-28-93				567	564630	25,766	512	1103	50	✓	DRC	
12-1-93	RFL-SS- 2339 TP#27	12-1-93	12-3-93	458	1044100	37568	596	1753	64		PU	TP#27 7'-8'
12-27-93				451	1044300	34839	392	2792	87	✓	DRC	
12-1-93	RFL-SS- 2340 TP#27	12-1-93	12/3/93	560	4668	8534	556	84	1.5		PU	TP#27 8'-9'
12/29/93				42	3996	809.8	442	9.0	1.8	✓	PU	
12-1-93	RFL-SS- 2341 TP#27	12-1-93	12-3-93	460	1099	818.5	790	1.4	1.0		PU	TP#27 10'-11' Screen
12-28-93				436	1437	748.3	634	2.3	1.2	✓	DRC	
12-1-93	RFL-SS- 2342 TP#27-DUP	12-1-93	12-3-93	562	1414	843.9	821	1.8	1.0		PU	TP#27 10'-11' Screen
12-28-93				412	1533	862.0	674	2.3	1.3	✓	DRC	
12-1-93	RFL-SS- 2343 TP#27	12-1-93	12-2-93	3707	3707	1045	790	4.7	1.3		PU	TP#27 11'-12' Screen
12-28-93				470	5068	914.3	696	7.8	1.4	✓	DRC	
12-1-93	RFL-SS- 2344 TP#27-DUP	12-1-93	12-2-93	564	3892	1017	769	5.1	1.3		PU	TP#27 11'-12' Screen
12-28-93				563	4861	911.0	637	7.6	1.4	✓	DRC	
12-1-93	RFL-SS- 2344 PS 2345 1/2	12-1-93	12-3-93	464	4699	1480	819	5.7	1.8		PU	TP#27 9'-10' Screen
12-28-93				500	6267	1912	669	9.4	2.7	✓	DRC	
12-1-93	RFL-SS- 2346 TP#27-DUP	12-1-93	12/3/93	566	5932	2381	829	7.2	1.7		PU	TP#27 9'-10' Screen
12/29/93				506	6822	1256	684	10.	1.8	✓	PU	

 Site Correction Factor = 1.8

 VP Correction Factor (if applicable) = 2.0

 Count Time = 500 sec., unless otherwise noted

REVIEWED BY:


 Site HP Manager


 SITE NAME **RIFLE, CO.**
OCS SAMPLE LOG
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SITE NAME	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET/DRY	Re-228 pCi/0 INITIAL 20 DAY	Th-232 pCi/0 INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-2-93	RFL-SS- 2347			400	768.6	896.9	576	1.3	1.6	✓	TP#19	(20071227)
11/11/94	TP#19	12-1-93	12/3/93	426	781.7	1001	551	1.4	1.8	✓	TP#19	(20071227)
12-2-93	RFL-SS- 2348			500	387.5	1026	407.9	0.95	2.5	✓	TP#1	(20071227)
2-11-94	TP#1	11-30-93	12/2/93	508	402.2	934.6	407.9	0.99	2.3	✓	TP#1	(20071227)
12-2-93	RFL-SS- 2349			502	1226	911.0	489.4	2.5	1.9	✓	TP#4	(20071227)
2-11-94	TP#4	11-30-93	12/2/93	502	1027	1055	489.4	2.1	2.2	✓	TP#4	(20071227)
12-2-93	RFL-SS- 2350			402	3512	7750	375.2	9.4	2.1	✓	TP#4	(20071227)
2-11-94	TP#4	11-30-93	12/2/93	500	4637	1007	375.2	12.4	2.7	✓	TP#4	(20071227)
12-2-93	RFL-SS- 2351			504	979.5	824.7	398.4	2.5	2.1	✓	TP#5	(20071227)
2-11-94	TP#5	11-30-93	12/2/93	504	804.7	901.4	398.4	2.0	2.3	✓	TP#5	(20071227)
12-2-93	RFL-SS- 2352			404	2645	1001	406.1	6.5	2.5	✓	TP#5	(20071227)
2-11/94	TP#5	11-30-93	12/2/93	402	3881	801.1	406.1	9.6	2.0	✓	TP#5	(20071227)
12-2-93	RFL-SS- 2353			506	891.8	815.1	608	1.5	1.3	✓	TP#20	(20071227)
12-2-93	TP #20	12-1-93	12-3-93	564	748.3	928.6	517	1.3	1.6	✓	TP#20	(20071227)
12-2-93	RFL-SS- 2354			406	1131	914.3	603	1.9	1.5	✓	TP#20	(20071227)
12-2-93	TP #20-DUP	12-1-93	12-3-93	564	1197	5658	567	2.1	1.0	✓	TP#20	(20071227)
12-2-93	RFL-SS- 2355			508	1156	767.1	645	1.8	1.2	✓	TP#20	(20071227)
12-2-93	TP #20	12-1-93	12-3-93	431	1633	731.4	601	2.7	1.2	✓	TP#20	(20071227)
12-2-93	RFL-SS- 2356			408	1367	844.6	622	2.2	1.4	✓	TP#20	(20071227)
12-2-93	TP#20-DUP	12-1-93	12/3/93	406	1136	705.3	580	2.0	1.2	✓	TP#20	(20071227)

 Site Correction Factor = 1.8

 VP Correction Factor (if applicable) = 2.0

 Count Time = 500 sec., unless otherwise noted

Site HP Manager

 REVIEWED BY: John H. Tietz



SITE NAME RIFLE, CO.

OCS SAMPLE LOG

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COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-226 pCi/g INITIAL/COH, 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH ≤ 15cm > 15cm	TECH INITIAL 20 DAY	COMMENTS
12/2/93	RFL-SS-2367			520	8476	930.2	542	16 ^{15.6} 15.6	1.7		✓	TP#21
12/28/93	TP#21-Dup	12/1/93	12/3/93	564	13112	1199	497	23	2.4	✓	DRC	3-4' Screened
12/2/93	RFL-SS-2368			420	2809	696.6	604	4.7	1.2		✓	TP#21
12/27/93	TP#21	12/1/93	12/3/93	441	5751	838.2	535	11	1.7	✓	DRC	4-5' Screened
12/2/93	RFL-SS-2369			522	3129	805.5	671	4.7	1.2		✓	TP#21
12/27/93	TP#21-Dup	12/1/93	12/3/93	562	5112	872.6	600	9.5	1.5	✓	DRC	4-5' Screened
12/2/93	RFL-SS-2370			422	414.4	618.2	616	0.67	1.0		✓	TP#32 Bkg
12/27/93	TP#32	12/2/93	12/3/93	417	745.2	635.6	579	1.3	1.1		DRC	0-1' Screened
12/2/93	RFL-SS-2371			524	277.7	853.4	655	1.0	1.3		✓	TP#32 Bkg
12/27/93	TP#32	12/2/93	12/3/93	408	701	636	609	1.2	1.0	✓	DRC	0-1' Screened
12/2/93	RFL-SS-2372			424	383.8	635.6	639	0.60	0.99		✓	TP#32 Bkg
12/27/93	TP#32	12/2/93	12/3/93	414	562	653	595	0.94	1.10	✓	DRC	1-2' Screened
12/2/93	RFL-SS-2373			526	465.9	920.6	761	0.70	1.4		✓	TP#32 Bkg
12/27/93	TP#32	12/2/93	12/3/93	420	861.5	766.3	596	1.4	1.3	✓	DRC	2-3' Screened
12/2/93	RFL-SS-2374			426	432.2	696.6	631	0.68	1.1		✓	TP#32 Bkg
12/27/93	TP#32	12/2/93	12/3/93	425	864.4	714.0	541	1.5	1.2	✓	DRC	1-2' Screened
12/2/93	RFL-SS-2375			528	649.5	863.0	644g	1.0	1.3		✓	TP#32 Bkg
12/30/93	TP#32	12/2/93	12/6/93	400	773.9	687.9	579	1.3	1.2	✓	✓	2-3' Screened
12/2/93	RFL-SS-2376			428	420.1	705.3	709	0.59	0.99		✓	TP#32 Bkg
12/27/93	TP#32	12/2/93	12/3/93	429	666.0	879.5	607	1.1	1.4	✓	DRC	3-4' Screened

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY: *K. M. Linsell*
Site HP Manager

Site HP Manager

VP Correction Factor (if applicable) = 0.0

Count Time = 500 SEC. unless otherwise noted

REVIEWED BY:

A.O.

11/8

COUNT DATE INITIAL	LOCATION	SAMPLED	DATE	SEAL'D	DATE	OC's #	BL-214	20 DAY INITIAL	DEPTH	TECH	TECH	COMMENTS						
12/2/93	RFL-SS-3377	TP#32	12/2/93	530	157.8	680.8	703	412	588	557	598	.98	.93	1	0.97	TP#32	TP#32	3-4', SCUBA
12/2/93	RFL-SS-3378	TP#32	12/2/93	430	197.5	888.2	759								1.2	TP#32	TP#32	3-4', SCUBA
12/2/93	RFL-SS-3379	TP#32	12/2/93	532	720.6	757.6	800	0.90	0.95						1.1	TP#32	TP#32	4-5', SCUBA
12/2/93	RFL-SS-3380	TP#32	12/2/93	432	197.0	783.4	687	0.29	1.1						1.1	TP#32	TP#32	4-5', SCUBA
12/2/93	RFL-SS-3381	TP#33	12/2/93	534	462.5	968.5	754	0.61	1.3						1.1	TP#33	TP#33	4-7', SCUBA
12/2/93	RFL-SS-3382	TP#33	12/2/93	434	721.3	853.3	716	1.0	1.0						1.2	TP#33	TP#33	4-7', SCUBA
12/2/93	RFL-SS-3383	TP#33	12/2/93	536	435.8	728.8	774	0.56	0.94						1.3	TP#33	TP#33	4-7', 8', SCUBA
12/2/93	RFL-SS-3384	TP#33	12/2/93	437	557.1	863.0	652.	0.52	0.85	1.3					1.6	TP#33	TP#33	4-7', 8', SCUBA
12/2/93	RFL-SS-3385	TP#33	12/2/93	538	307.3	930.3	728	0.42	1.3						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3386	TP#33	12/2/93	438	386.5	1228	695	5.6	5.6	1.8					1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3387	TP#33	12/2/93	449	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3388	TP#33	12/2/93	450	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3389	TP#33	12/2/93	451	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3390	TP#33	12/2/93	452	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3391	TP#33	12/2/93	453	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3392	TP#33	12/2/93	454	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3393	TP#33	12/2/93	455	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3394	TP#33	12/2/93	456	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3395	TP#33	12/2/93	457	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3396	TP#33	12/2/93	458	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3397	TP#33	12/2/93	459	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3398	TP#33	12/2/93	460	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3399	TP#33	12/2/93	461	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3400	TP#33	12/2/93	462	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3401	TP#33	12/2/93	463	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3402	TP#33	12/2/93	464	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3403	TP#33	12/2/93	465	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3404	TP#33	12/2/93	466	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3405	TP#33	12/2/93	467	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3406	TP#33	12/2/93	468	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3407	TP#33	12/2/93	469	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3408	TP#33	12/2/93	470	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3409	TP#33	12/2/93	471	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3410	TP#33	12/2/93	472	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3411	TP#33	12/2/93	473	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3412	TP#33	12/2/93	474	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3413	TP#33	12/2/93	475	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3414	TP#33	12/2/93	476	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3415	TP#33	12/2/93	477	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3416	TP#33	12/2/93	478	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3417	TP#33	12/2/93	479	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3418	TP#33	12/2/93	480	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3419	TP#33	12/2/93	481	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3420	TP#33	12/2/93	482	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3421	TP#33	12/2/93	483	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3422	TP#33	12/2/93	484	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3423	TP#33	12/2/93	485	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3424	TP#33	12/2/93	486	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3425	TP#33	12/2/93	487	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3426	TP#33	12/2/93	488	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3427	TP#33	12/2/93	489	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3428	TP#33	12/2/93	490	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3429	TP#33	12/2/93	491	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3430	TP#33	12/2/93	492	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3431	TP#33	12/2/93	493	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3432	TP#33	12/2/93	494	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3433	TP#33	12/2/93	495	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3434	TP#33	12/2/93	496	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3435	TP#33	12/2/93	497	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3436	TP#33	12/2/93	498	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3437	TP#33	12/2/93	499	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33	4-7', 8', 9', SCUBA
12/2/93	RFL-SS-3438	TP#33	12/2/93	500	615.8	933.2	632	0.8	1.8						1.6	TP#33	TP#33</td	

SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214	Tl-208	MASS	Ra-228	Th-232	DEPTH	TECH.	COMMENTS
					INITIAL 20 DAY	pCi INITIAL 20 DAY	INITIAL 20 DAY	(grams) WET DRY	pCi/g INITIAL/CORR. 20 DAY	pCi/g INITIAL 20 DAY	<15cm >15cm	
12-2-93	RFL-SS-2397	12-1-93	12/3/93	550	1249	1017	741	1.6	1.3		✓	TP #24 Screened
12/29/93	TP #24			502	1357	1208	612.5	21.0	1.8	✓	✓	4-5 Dup
12-2-93	RFL-SS-2398			450	5661	975.2	681	8.3	1.4		✓	TP #25
12-29-93	TP #25	12-1-93	12-3-93	444	6798	1010	575	12	1.8	✓	DRC	9-10 Screened
12-2-93	RFL-SS-2399			552	4659	151	759	6.1	1.5		✓	TP #25 Screened
12-28-93	TP #25	12-1-93	12-3-93	472	5952	975.2	638	8.5	1.5	✓	DRC	9-10 Dup
12-2-93	RFL-SS-2400	12-1-93	1	452	1700	600.8	776	2.2	.77		✓	TP #26
2-11-94	TP #26		12-6-93	506	1288	786.3	648	2.0	1.2	✓	WW	8-9.5
12-2-93	RFL-SS-2401	12-1-93	10/3/93	554	3698	1218	665	5.6	1.8		✓	TP #28
12/29/93	TP #28			512	6348	939.8	610	10.4	1.5	✓	✓	0-1
12-2-93	RFL-SS-2402	12-1-93	12/3/93	556	5404	911.1	732	.74	1.2		✓	TP #28
12-28-93	TP #28			404	7855	975.2	607	13	1.6	✓	DRC	1-2' Screened
12-2-93	RFL-SS-2403	12-1-93	12-3-93	454	4606	731.4	735	6.3	1.0		✓	TP #28 Dup
12-28-93	TP #28 Dup			476	7042	1149	611	12	1.9	✓	DRC	1-2' Screened
12-2-93	RFL-SS-2404	12-1-93	12/3/93	558	2593	1160	728	3.6	1.6		✓	TP #28
12/29/93	TP #28			414	4077	983.9	592	6.9	1.7	✓	✓	2-3' Screened
12-2-93	RFL-SS-2405	12-1-93	12/3/93	456	2415	466.5	740	3.3	1.3		✓	TP #28 Dup
12/29/93	TP 28			500	4348	930.2	608	7.2	1.5	✓	✓	2-3' Screened
12-2-93	RFL-SS-2406	12-1-93	12/3/93	560	60783	3347	618	9.8	5.4		✓	TP 29
12/29/93	TP 29			508	103280	4229	555	186	7.6	✓	✓	0-1' Screened

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY: 
Site HP Manager



SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE <u>INITIAL</u> <u>20 DAY</u>	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214 pCi <u>INITIAL</u> <u>20 DAY</u>	Tl-208 pCi <u>INITIAL</u> <u>20 DAY</u>	MASS (gram) WET DRY	Ra-226 pCi/g <u>INITIAL</u> / <u>CORR.</u> <u>20 DAY</u>	Th-232 pCi/g <u>INITIAL</u> <u>20 DAY</u>	DEPTH <u><15cm</u> <u>>15cm</u>	TECH. <u>INITIAL</u> <u>20 DAY</u>	COMMENTS
12-2-93	RFL-SS-2407	12-1-93	12/3/93	488	67566	3344	740	91	4.5		✓	TP 29 DUP
12/29/93	TP 29 DUP			402	114497	4787	643	173	7.4	✓	✓	0-1' SCREENED
12-2-93	RFL-SS-2408	12-1-93	12/3/93	502	35228	2100	690	51	3.0		✓	TP 29
12/29/93	TP 29			514	60950	3174	618	99	5.1	✓	✓	1-2' SCREENED
12-2-93	RFL-SS-2409	12-1-93	12/3/93	460	32065	2064	662	48	3.1		✓	TP 29 DUP
12/29/93	TP 29			504	57491	7397	596	96	4.0	✓	✓	1-2' SCREENED
12-2-93	RFL-SS-2410	12-1-93	12/3/93	564	41989	2608	705	60	3.7		✓	TP 29
12/29/93	TP 29			416	74697	3344	651	115	5.1	✓	✓	2-3' SCREENED
12-2-93	RFL-SS-2411	12-1-93	12/3/93	462	47500	2438	721	66	3.4		✓	TP 29 DUP
12/29/93	TP 29 DUP			516	83609	3519	639	131	5.5	✓	✓	2-3' SCREENED
12-2-93	RFL-SS-2412	12-1-93	12-3-93	566	9550	1410	557	17	2.5		✓	TP 30
12-27-93	TP 30			455	17634	1132	516	34	2.2	✓	✓	0-1'
12-2-93	RFL-SS-2413	12-1-93	12-3-93	464	2386	8707	567	46	1.5		✓	TP 30
12-27-93	TP 30			518	6150	1130	543	11	2.2	✓	✓	1-2'
12-2-93	RFL-SS-2414	12-1-93	12-3-93	568	34583	2014	468	74	4.3		✓	TP 30
12-27-93	TP 30			560	68812	2603	292	236	8.9	✓	✓	2-3'
12-2-93	RFL-SS-2415	12-1-93		466	518.5	8533	390	13	2.2		✓	TP 25, COMPOSIT 6.5-7.5'
12-2-93	TP 25, COMPOSIT 6.5-7.5'											
12-2-93	RFL-SS-2416	12-1-93	12-2-93	510	2615	8151	419	6.2	1.9		✓	TP 27 COMPOSIT 9-12'
2-11-94	TP 27			400	3714	7140	419	9.3	1.7	✓	WW	

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec. unless otherwise noted

REVIEWED BY:

John M. Fossell
Site HP Manager

SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-226 pCi/g INITIAL/CORR 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-3-93	RFL-SS- 2417			400 31550	2020	572	55	3.5	✓		✓	Tp #30
12/30/93	Tp #30	12-1-93	12/6/93	500 54683	2417	384	142	6.3	✓			3-4'
12-3-93	RFL-SS- 2418			500 2244	795.4	565	4.0	1.4	✓		✓	Tp #30
12/30/93	Tp #30	12-1-93	12/6/93	402 4714	992.6	501	9.8	2.0	✓			'4-5' Screened
12-3-93	RFL-SS- 2419			402 2878	870.7	579	5.0	1.5	✓		✓	Tp #30
12-28-93	Tp #30	12-1-93	12-6-93	402 6879	696.4	510	13	1.4	✓	✓	DRC	4-5' Screened
12-3-93	RFL-SS- 2420			502 2829	863.0	626	4.5	1.4	✓		✓	Tp #30
12/30/93	Tp #30	12-1-93	12/6/93	502 8360	834.3	533	16.0	1.6	✓			5-6' Screened
12-3-93	RFL-SS- 2421			404 2400	731.4	651	3.7	1.1	✓		✓	Tp #30
12/28/93	Tp #30	12-1-93	12-6-93	418 6679	731.4	553	12	1.3	✓	✓	DRC	5-6' Dup Screened
12-3-93	RFL-SS- 2422			504 7290	1036	686	11	1.5	✓		✓	Tp #30
12/30/93	Tp #30	12-1-93	12/6/93	404 17045	1628	564	30	2.9	✓			6-7' Screened
12-3-93	RFL-SS- 2423			406 6232	453.4	647	9.6	1.5	✓		✓	Tp #30
12-28-93	Tp #30	12-1-93	12-6-93	524 16410	51-3-73	1247	542	30	2.3	✓	✓	DRC
12-3-93	RFL-SS- 2424			506 2129	891.8	729	2.9	1.2	✓		✓	Tp #30
12/30/93	Tp #30	12-1-93	12/6/93	504 2640	853.4	602	4.4	1.4	✓			7-8' Screened
12-3-93	RFL-SS- 2425			408 2294	757.5	687	3.3	1.1	✓		✓	Tp #30 Screened
12-28-93	Tp #30	12-1-93	12-6-93	420 3430	674.2	569	6.0	1.2	✓	✓	DRC	7-8-8' Dup
12-3-93	RFL-SS- 2426			508 17004	1793	676	25	2.7	✓		✓	
12/30/93	Tp #30	12-1-93	12/6/93	406 26641	1715	513	52	3.3	✓			8-9' Screened

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY: John K. Ferrell
Site HP Manager



SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214 pCi INITIAL 20 DAY	Ti-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-226 pCi/g INITIAL/CORR 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-3-93	RFL-SS-2427			410	16055	1283	681	24	1.9		PU	TP #30 Screened
12-28-93	TP #30	12-1-93	12-6-93	510	24590	1477	521	47	2.9	✓	ORC	3'-9' Dup.
12-3-93	RFL-SS-2428			510	7341	1045	580	13	1.9		PU	TP #19
12/30/93	TP #19	12-1-93	12/6/93	506	19013	1467	460	41	3.2	✓	BS	0'-1'
12-3-93	RFL-SS-2429			412	532.1	1158	606	.88	1.9		PU	TP #19 *
12/30/93	TP #19	12-1-93	12/6/93	408	1087	1106	549	2.0	2.0	✓	BS	2'-3'
12-3-93	RFL-SS-2430			512	6820	815.1	509	1.4	1.4		PU	TP #19
12/30/93	TP #19	12-1-93	12/6/93	508	1126	661.7	531	2.1	1.2	✓	BS	1'-2'
12-3-93	RFL-SS-2431			414	2174	957.8	643	3.4	1.5		PU	TP #19
12/30/93	TP #19	12-1-93	12/6/93	410	4017	1132	560	7.3	2.1	✓	BS	3 1/2 - 4 1/2
12-3-93	RFL-SS-2432			514	1880	949.3	630	3.0	1.5		PU	TP #19
12-28-93	TP #19	12-1-93	12-6-93	430	3738	1019	534	7.1	1.7	✓	ORC	3 1/2 - 4 1/2 Dup.
12-3-93	RFL-SS-2433			416	2604	844.6	572	4.6	1.5		PU	TP #19
12/30/93	TP #19	12-1-93	12/6/93	510	4870	843.9	513	9.5	1.6	✓	BS	4 1/2 - 5 1/2
12-3-93	RFL-SS-2434			516	2459	1036	553	4.4	1.9		PU	TP #19
12-28-93	TP #19	12-1-93	12-6-93	522	4954	632.7	493	10	1.3	✓	ORC	4 1/2 - 5 1/2 Dup
12-3-93	RFL-SS-2435			418	1602	1036	658	2.4	1.6		PU	TP #19
12-27-93	TP #19	12-1-93	12-6-93	445	3471	1123	589	5.9	1.9	✓	ORC	5 1/2 - 6 1/2
12-3-93	RFL-SS-2436			518	1915	1112	661	2.9	1.7		PU	TP #19
12-28-93	TP #19	12-1-93	12-6-93	428	3528	835.7	592	6.0	1.4	✓	ORC	5 1/2 - 6 1/2 Dup

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec. unless otherwise noted

REVIEWED BY:

Site HP Manager

SITE NAME RIFLE, CO.

OCS SAMPLE LOG

INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-226 pCi/g INITIAL/CORR. 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-3-93	RFL-SS-2437			420	719.7	731.4	55.3	1.3	1.3		PU	TP # 11
12-27-93	TP # 11	12-2-93	12-6-93	443	435.3	1036	46.8	0.93	2.2	✓	DRC	3' - 4'
12-3-93	RFL-SS-2438			520	4922	1486	66.6	2.4	2.2		PU	TP # 11
12/30/93	TP # 11	12-2-93	12/6/93	412	8584	1176	535	16.0	2.2	✓	PU	4' - 5'
12-3-93	RFL-SS-2439			422	1856	949.1	650	2.9	1.5		PU	TP # 11
12/30/93	TP # 11	12-2-93	12/6/93	512	3309	882.2	507	6.5	1.7	✓	PU	5' - 6'
12-3-93	RFL-SS-2440			522	928	132.3	782	1.2	1.7		PU	TP # 11, Screened
12-27-93	TP # 11	12-2-93	12-6-93	447	1527	1350	644	2.4	2.1	✓	DRC	6' - 7'
12-3-93	RFL-SS-2441			424	1283	905.6	753	1.7	1.2		PU	TP # 11, Screened
12-28-93	TP # 11	12-2-93	12-6-93	422	1715	1025	614	2.8	1.7	✓	DRC	6' - 7' Dup
12-3-93	RFL-SS-2442			524	1030	997.3	761	1.4	1.3		PU	TP # 11, Screened
12/30/93	TP # 11	12-2-93	12/6/93	414	1980	1297	604	3.2	2.1	✓	PU	7' - 8'
12-3-93	RFL-SS-2443			426	1738	792.4	762	2.3	1.0		PU	TP # 11, Screened
12/30/93	TP # 11	12-2-93	12/6/93	514	2233	1017	621	3.6	1.6	✓	PU	7' - 8' Dup
12-3-93	RFL-SS-2444			526	733.0	911.0	830	.98	1.1		PU	TP # 11, Screened
12/30/93	TP # 11	12-2-93	12/6/93	416	1408	1080	692	2.0	1.6	✓	PU	8' - 9'
12-3-93	RFL-SS-2445			428	1141	870.7	812	1.4	1.1		PU	TP # 11, Screened
12-28-93	TP # 11	12-2-93	12-6-93	514	1457	930.2	677	2.2	1.3	✓	DRC	8' - 9' Dup
12-3-93	RFL-SS-2446			528	3010	1036	795	3.8	1.3		PU	TP # 11, Screened
12/30/93	TP # 11	12-2-93	12/6/93	516	4737	815.1	669	7.1	1.2	✓	PU	9' - 10'

Site Correction Factor = 1.9

VP Correction Factor (if applicable) = 9.1

Count Time = 500 sec., unless otherwise noted

REVIEWED BY: *Robert F. Finch*
Site HP Manager



SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-226 pCi/g INITIAL/CORR. 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH ≤15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-3-93	RFL-SS-2447			430	2543	588.2	727	3.5	1.2		✓	TP # 11 Screened
12-28-93	TP # 11	12-2-93	12-6-93	512	4350	949.3	613	7.1	1.5	✓	DEC	9-10' Dup
12-3-93	RFL-SS-2448			530	37026	2215	666	56	3.3		✓	TP # 15
12/30/93	TP # 15	12-2-93	12/6/93	418	83688	4049	500	167	8.1	✓	✓	0-1'
12-3-93	RFL-SS-2449		12-2-93	432	138630	6017	588	236	10		✓	TP # 15
12/30/93	TP # 15		12/6/93	518	268600	11191	484	555	23	✓	✓	1-2'
12-3-93	RFL-SS-2450		12-2-93	532	120690	5399	587	205	9.2		✓	TP # 15
12/30/93	TP # 15		12/6/93	420	232430	9639	494	471	20.	✓	✓	2-3'
12-3-93	RFL-SS-2451		12-2-93	434	27267	1393	565	48	2.5		✓	TP 15
12/30/93	TP 15		12/6/93	520	59645	2791	467	128	6.0	✓	✓	3-4'
12-3-93	RFL-SS-2452		12-2-93	534	1484	1064	661	2.2	1.6		✓	TP 15
12-27-93	TP 15		12-6-93	518	4433	815.1	513	8.6	1.6	✓	DEC	4-5'
12-3-93	RFL-SS-2453		12-2-93	436	1441	896.9	708	2.0	1.3		✓	TP 15
12/30/93	TP 15		12/6/93	422	1900	940.4	537	3.5	1.8	✓	✓	5-6'
12-3-93	RFL-SS-2454		12-2-93	536	666.3	891.9	763	.87	1.2		✓	TP 15
12/30/93	TP 15		12/6/93	522	1114	786.3	583	1.9	1.3	✓	✓	6-7'
12-3-93	RFL-SS-2455		12-2-93	438	492.0	835.9	688	.72	1.2		✓	TP 15
12/30/93	TP 15		12/6/93	424	551.4	775.0	516	1.1	1.5	✓	✓	7-8'
12-3-93	RFL-SS-2456		12-2-93	538	4938	853.4	681	7.3	1.3		✓	TP 15
12/30/93	TP 15		12/6/93	524	8433	843.9	531	16.	1.6	✓	✓	8-9'

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec. unless otherwise noted

REVIEWED BY: John H. Fennell
Site HP Manager

SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SCALED	OCS #	Bi-214	TI-208	MASS (gram) WET DRY	Ra-228 pCi/g INITIAL/CORR. 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
					INITIAL 20 DAY	pCi INITIAL 20 DAY						
12-3-93	RFL-SS-2457 TP#15	12-2-93	12/6/93	440	4037	853.3	747	5.4	1.1		✓	TP#15
12/30/93				426	6650	1263	612	11	2.1	✓	✓	9-10'
12-3-93	RFL-SS-2458 TP#15	12-2-93	12/6/93	540	731.1	882.2	663	1.1	1.3		✓	TP#15
12/30/93				526	1061	959.8	533	2.0	1.8	✓	✓	10-11'
12-3-93	RFL-SS-2459 TP#15	12-2-93	12/6/93	442	978.4	809.8	799	1.2	1.0		✓	TP#15
12/30/93				428	1452	1071	674	2.2	1.6	✓	✓	12'-13' Screened #4
12-3-93	RFL-SS-2460 TP#15	12-2-93	12-6-93	542	3050	997.3	831	3.7	1.2		✓	TP#15
12-27-93				546	5323	891.8	675	7.9	1.3	✓	DRC	11'-12' Screened #4
12-3-93	RFL-SS-2461 TP#15-DUP	12-2-93	12-6-93	444	796.2	931.7	767	1.0	1.2		✓	TP#15
12-28-93				520	1726	1007	623	2.8	1.6	✓	DRC	11'-12' Screened #4
12-3-93	RFL-SS-2462 TP#15-DUP	12-2-93	12-6-93	544	1474	939.8	808	1.8	1.2		✓	TP#15
12-28-93				426	1796	705.3	633	2.6	1.0	✓	DRC	12'-13' Screened #4
12-3-93	RFL-SS-2463A TP#4	12-3-93	12/6/93	446	4372	1228	775	5.6	1.6		✓	TP#4
12/29/93				448	5420	849.5	635	8.5	1.4	✓	✓	11'-12' Screened
12-3-93	RFL-SS-2464 TP#4-DUP	12-3-93	12-6-93	546	5027	1534	771	6.5	2.0		✓	TP#4
12-28-93				502	6977	1199	636	11	1.9	✓	DRC	11'-12' Screened
12-3-93	RFL-SS-2465A TP#4	12-3-93	12/6/93	448	8482	1358	694	12	2.0		✓	TP#4
12/29/93				518	10823	1122	619	17	1.8	✓	✓	12'-13' Screened
12-3-93	RFL-SS-2466A TP#4-DUP	12-3-93	12-6-93	548	8563	1026	673	13	1.5		✓	TP#4
12-28-93				424	10088	1010	600	17	1.7	✓	DRC	12'-13' Screened

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY: *J. L. M. Espejel*

Site HP Manager

TE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #		Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-226 pCi/g INITIAL/CORR. 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
				INITIAL 20 DAY	20 DAY								
2-3-93	RFL-SS-2467A			450	3259	1219	654	6.1	1.9	40	TP#4		
2/29/93	TP#4	12-3-93	12/6/93	420	5282	896.9	574	9.2	1.6	✓	L	13'-14'	Screened
2-3-93	RFL-SS-2468A			550	5132	1036	731	7.0	1.4	40	TP#4		
2-28-93	TP#4-DUP	12-3-93	12-6-93	414	7071	923.0	642	11	1.4	✓	DR	13'-14'	Screened
2-3-93	RFL-SS-2469A			452	1143	905.6	611	1.9	1.5	40	TP#4		
2/29/93	TP#4	12-3-93	12/6/93	520	1815	767.1	565	3.2	1.4	✓	L	14'-15'	Screened
2-3-93	RFL-SS-2470A			552	1651	1064	729	2.3	1.5	40	TP#4		
2-28-93	TP#4-DUP	12-3-93	12-6-93	416	2466	775.0	581	4.2	1.3	✓	DR	14'-15'	Screened
2-3-93	RFL-SS-2471A			454	962.1	1045	718	1.3	1.5	40	TP#4		
2/29/93	TP#4	12-3-93	12/6/93	422	1264	722.7	651	1.9	1.1	✓	L	15'-16'	Screened
2-3-93	RFL-SS-2472A			554	1071	1055	669	1.6	1.6	40	TP#4		
12-28-93	TP#4-DUP	12-3-93	12-6-93	516	1500	1343	633	2.4	2.1	✓	DR	15'-16'	Screened
12-3-93	RFL-SS-2473A			456	979.5	923.0	823	1.2	1.1	40	TP#4		
2/29/93	TP#4	12-3-93	12/6/93	522	1668	758.4	697	2.4	1.1	✓	L	16'-17'	Screened
12-3-93	RFL-SS-2474A			556	968.4	1045	854	1.1	1.2	40	TP#4		
12-28-93	TP#4-DUP	12-3-93	12-6-93	508	1519	960.0	719	2.1	1.3	✓	DR	16'-17'	Screened
12-3-93	RFL-SS-2475			458	633.6	966.5	519	1.2	1.9	40	TP#31		
2/30/93	TP#31	12-3-93	12/6/93	528	707.9	690.4	456	1.6	1.5	✓	L	0'-1'	Background
12-3-93	RFL-SS-2476			558	514.5	1074	471	1.1	2.3	40	TP#31		
12/30/93	TP#31	12-3-93	12/6/93	430	445.7	1097	409	1.1	2.7	✓	L	1'-2'	Background

to Correction Factor = 1.8

P Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY: *Paul K. Conrad*
Site HP Manager

FOR INFORMATION ONLY

OCS SAMPLE LOG

RIFLE, CO.

SITE NAME	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET/DRY	Ra-226 pCi/g INITIAL/20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-3-93	RFL-SS-2477	12-3-93	12/6/93	460	117.6	116.7	421	42	2.8		PU	TP #31
12/30/93	TP #31	12-3-93	12/6/93	530	515.8	911.0	353	1.5	216	✓	PU	2-3' Background
12-3-93	RFL-SS-2478			560	293.4	1026	450	.65	2.3		PU	TP #31
12/30/93	TP #31	12-3-93	12/6/93	432	606.7	844.6	392	1.5	2.2	✓	PU	3-4' Background
12-3-93	RFL-SS-2479			462	352.0	1062	541	.70	2.0		PU	TP #31
12/30/93	TP #31	12-3-93	12/6/93	532	847.8	792	481	1.8	1.5	✓	PU	4-5' Background
12-3-93	RFL-SS-2480			562	675.6	1007	681	.99	1.5		PU	TP #31
12/30/93	TP #31	12-3-93	12/6/93	434	377.2	1019	617	1.62	1.7	✓	PU	5-6' Background
12-3-93	RFL-SS-2481			464	381.2	923.0	605	.50	1.5		PU	TP #31
12/30/93	TP #31	12-3-93	12/6/93	534	472.8	896.8	544	0.76	1.6	✓	PU	6-7' Background
12-3-93	RFL-SS-2482			564	114.1	114.1	716	.89	1.6		PU	TP #31
12/30/93	TP #31	12-3-93	12/6/93	436	104.1	1097	667	0.91	1.6	✓	PU	7-8' Background
12-3-93	RFL-SS-2483			466	562.1	1036	635	.82	1.5		PU	TP #31
12/29/93	TP #31-Dup	12-3-93	12/6/93	436	832.8	618.2	636	1.3	0.97	✓	PU	7-8' Background
12-3-93	RFL-SS-2484			566	512.0	1132	806	.64	1.4	✓	PU	TP #31
12/30/93	TP #31	12-3-93	12/6/93	536	556.7	968.5	727	0.77	1.3	✓	PU	8-9' Background
12-3-93	RFL-SS-2485			468	626.1	1045	829	.75	1.3		PU	TP #31
12-11-94	TP #31-Dup	12-3-93	12/6/93	404	981.2	949.1	750	1.3	1.3	✓	PU	8-9' Background
12-3-93	RFL-SS-2486			568	744.6	786.3	730	.95	1.0		PU	TP #31
12/30/93	TP #31-Dup	12-3-93	12/6/93	438	385.4	853.2	593	0.65	1.4	✓	PU	8-9' Background
												9-10' Background

Site Correction Factor = 1.8
 VP Correction Factor (if applicable) = 2.0
 Count time = 500 sec., unless otherwise noted

REVIEWED BY: John C. Ladd
 Count time = 500 sec., unless otherwise noted

Site HP Manager



MK-FEI SON COMPANY
A MORRISON JUDSEN COMPANY



CWM Federal Environmental Services, Inc.

SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-226 pCi/g INITIAL/CORR. 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-3-93	RFL-SS-2487			470	533.4	838.2	828	0.64	1.1			Tp #31 Screened
12/29/93	Tp #31 - Dup	12-3-93	12/6/93	424	501.3	687.9	708	0.71	0.97	✓		9'-10' Background
12-3-93	RFL-SS-2488			570	771.8	853.4	701	1.1	1.2			Tp #31 Screened
12/30/93	Tp #31	12-3-93	12/6/93	538	489.6	767.1	598	0.82	1.3	✓		10'-11' Background
12-3-93	RFL-SS-2489			472	755.8	844.6	691	1.1	1.2			Tp #31 Screened
12/30/93	Tp #31 - Dup	12-3-93	12/6/93	440	593.8	923	605	0.98	1.5	✓		10'-11' Background
12-3-93	RFL-SS-2490			572	474.7	939.8	800	.59	1.2			Tp #31 Screened
12/30/93	Tp #31 - Dup	12-3-93	12/6/93	540	410.1	1045	688	.61	1.5	✓		11'-12' Background
12-3-93	RFL-SS-2491			474	940.9	318.5	777	1.2	1.1			Tp #31 Screened
12/30/93	Tp #31 - Dup	12-3-93	12/6/93	442	684.9	975.2	683	1.0	1.4	✓		11'-12' Background
12-3-93	RFL-SS-2492			574	802.2	604.1	450	1.8	1.3			Tp #2
12/29/93	Tp #2	12-3-93	12/6/93	524	939.6	527.4	423	2.2	1.2	✓		0'-1'
12-3-93	RFL-SS-2493			476	773.1	966.5	605	1.3	1.6			Tp #2
12/29/93	Tp #2	12-2-93	12/6/93	426	634.9	888.2	563	1.1	1.6	✓		1'-2'
12-3-93	RFL-SS-2494			576	910.3	1132	415	2.2	2.7			Tp #2
12-27-93	Tp #2	12-2-93	12-6-93	433	707.4	931.7	378	1.9	2.5	✓	ORC	2'-3'
12-3-93	RFL-SS-2495			478	555.4	835.9	383	1.5	2.2			Tp #2
12/29/93	Tp #2	12-2-93	12/6/93	526	1056	700.0	353	3.0	2.0	✓		3'-4'
12-3-93	RFL-SS-2496			578	549.1	786.3	439	1.3	1.8			Tp #2
12/29/93	Tp #2	12-2-93	12/6/93	542	394.6	883.2	412	0.97	2.2	✓		4'-5'

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY:

Site HP Manager

John P. Farrel

SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214	Tl-208	MASS (gram) WET DRY	Ra-226 pCi/g INITIAL/CORR. 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
					INITIAL 20 DAY	pCi INITIAL 20 DAY						
12-3-93	RFL-SS-2497			480	466.6	931.7	521	.90	1.8			Tp#2
12/30/93	Tp#2	12-2-93	12/6/93	444	529.9	931.7	462	1.1	2.0	✓		5'-6'
12-3-93	RFL-SS-2498			580	315.3	939.8	616	.51	1.5			Tp#2
12/29/93	Tp#2	12-2-93	12/6/93	428	546.3	696.6	555	0.98	1.3	✓		6'-7'
12-3-93	RFL-SS-2499			482	463.7	883.2	556	.83	1.6			Tp#2
12/29/93	Tp#2	12-2-93	12/6/93	528	1139	556.2	505	2.3	1.1	✓		7'-8'
12-3-93	RFL-SS-2500			582	665.5	832.2	556	1.2	1.6			Tp#2
12/29/93	Tp#2	12-2-93	12/6/93	430	745.1	781.4	507	1.5	1.4	✓		3'-4'
12-3-93	RFL-SS-2501			484	618.7	879.5	708	.96	1.2			Tp#2
12/29/93	Tp#2	12-2-93	12/6/93	530	878.5	652.1	637	1.4	1.0	✓		9'-10'
12-3-93	RFL-SS-2502			554	533.8	767.1	586	1.0	1.3			Tp#2
12/30/93	Tp#2	12-2-93	12/6/93	584	385.5	920.6	564	0.59	1.6	✓		10'-11'
12-3-93	RFL-SS-2503			486	696.7	1158	693	1.0	1.7			Tp#2
12/29/93	Tp#2	12-2-93	12/6/93	432	831.9	925.6	644	1.3	1.4	✓		11'-12' Screened
12-3-93	RFL-SS-2504			586	532.8	353.4	643	.82	1.3			Tp#2
2-11-94	Tp#2-Dup	12-2-93	12/6/93	406	1039	966.5	604	1.7	1.6	✓	WW	11-12' Screened
12-6-93	RFL-SS-2505			400	520.3	783.7	608	.86	1.3			Tp#2
12/29/93	Tp#2	12-2-93	12/6/93	536	806.2	920.6	574	1.4	1.6	✓		12'-13' Screened
12-6-93	RFL-SS-2506			500	620.3	949.3	613	1.0	1.5			Tp#2
12/29/93	Tp#2-Dup	12-2-93	12/7/93	534	1132	938.4	577	2.0	1.3	✓		12'-13' Screened

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY:

Site HP Manager



SITE NAME RIFLE, CO.

OCS SAMPLE LOG

INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS		Bi-214	Th-208	MASS	Ra-226	Th-232	DEPTH	TECH	COMMENTS
				INITIAL	20 DAY	pCi	pCi	grams	pCi/g	INITIAL/CORR.	20 DAY	pCi/g	INITIAL
12-6-93	RFL-SS-2507			402	803.7	949.1	673		1.2	1.4		PU	TP#2
12/29/93	TP#2	12-2-93	12/7/93	438	747.8	870.7	619		1.2	1.4	✓	SL	13'-14' Screened
12-6-93	RFL-SS-2508			502	571.7	1064	691		.83	1.5		PU	TP#2
12/29/93	TP#2-DUP	12-2-93	12/7/93	4538	1132	834.3	642		1.8	1.3	✓	SL	13'-14' Screened
12-6-93	RFL-SS-2509			404	844.6	896.9	673		1.3	1.3		PU	TP#2
12/29/93	TP#2	12-2-93	12/7/93	440	707.3	1123	618		1.1	1.8	✓	SL	14'-15' Screened
12-6-93	RFL-SS-2510			504	744.9	968.5	607		1.2	1.6		PU	TP#2
12/29/93	TP#2-DUP	12-2-93	12/7/93	540	971.9	911.0	553		1.8	1.6	✓	SL	14'-15' Screened
12-6-93	RFL-SS-2511			406	716.6	975.2	631		1.1	1.5		PU	TP#2
12/29/93	TP#2	12-2-93	12/7/93	442	641.2	888.2	573		1.1	1.6	✓	SL	15'-16' Screened
12-6-93	RFL-SS-2512			506	845.0	863.8	672		1.3	1.3		PU	TP#2
12/29/93	TP#2-DUP	12-2-93	12/7/93	542	867.4	1227	616		1.4	2.0	✓	SL	15'-16' Screened
12-6-93	RFL-SS-2513			408	581.7	1045	597		1.0	1.8		RME	TP#2
12/29/93	TP#2	12-2-93	12/7/93	444	571.9	818.5	523		1.0	1.6	✓	SL	16'-17' Screened
12-6-93	RFL-SS-2514			508	521.5	891.8	468		1.1	1.9		RME	TP#2
12/29/93	TP#2-DUP	12-2-93	12/7/93	544	561.0	843.9	410		1.4	2.1	✓	SL	16'-17' Screened
12-6-93	RFL-SS-2515			410	726.9	1036	730		1.0	1.4		RME	TP#2
12/29/93	TP#2	12-2-93	12/7/93	446	732.1	1115	647		1.1	1.7	✓	SL	17'-18' Screened
12-6-93	RFL-SS-2516			510	428.6	997.3	660		.65	1.5		RME	TP#2
12/29/93	TP#2-DUP	12-2-93	12/7/93	546	919.7	891.8	583		1.6	1.5	✓	SL	17'-18' Screened

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec. unless otherwise noted

REVIEWED BY: J. L. L. (John L. Fine)
Sito HP Manager

RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

SITE NAME	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	DI-214 pCi INITIAL 20 DAY	TI-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	RA-226 pCi/g INITIAL 20 DAY	TH-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH	COMMENTS
12-6-93	RFL-SS-2517	12/29/93	12/2-93	4112	1628.7	8829.5	240	9.2	1.2	✓	Rece	18'-19' screened
12-6-93	RFL-SS-2518	12-2-93	12/2/93	4448	1092.6	601	1.8	1.7	✓	✓	Rece	TP#2
12-6-93	RFL-SS-2519	12-2-93	12/2/93	512	438.9	267.1	584	7.5	1.3	✓	Rece	18'-19' screened
12-6-93	RFL-SS-2520	12-2-93	12/2/93	4114	201.3	240.1	500	1.4	1.5	✓	Rece	TP#3
12-6-93	TP#3	12-2-93	12/2/93	450	601.6	766.3	444	1.4	1.7	✓	Rece	TP#3
12-6-93	TP#3	12-2-93	12/2/93	514	250.5	480.8	465	1.6	1.5	✓	Rece	TP#3
12-6-93	TP#3	12-2-93	12-7-93	427	314.4	531.2	401	2.0	1.3	✓	Rece	TP#3
12-6-93	RFL-SS-2521	12-2-93	12/2/93	416	359.7	740.1	438	2.0	1.7	✓	Rece	TP#3
12-6-93	TP#3	12-2-93	12/2/93	550	791.1	824.7	393	2.0	2.1	✓	Rece	TP#3
12-6-93	RFL-SS-2522	12-2-93	12/2/93	514	194.8	905.5	506	3.8	1.6	✓	Rece	TP#3
12-6-93	TP#3	12-2-93	12-2-93	452	453.2	766.2	463	9.8	1.7	✓	Rece	TP#3
12-6-93	RFL-SS-2523	12-2-93	12/2/93	418	433.9	722.7	492	.88	1.5	✓	Rece	TP#3
12-6-93	TP#3	12-2-93	12/2/93	552	656.5	949.3	445	1.5	2.1	✓	Rece	TP#3
12-6-93	RFL-SS-2524	12-2-93	12/2/93	518	722.0	767.1	601	1.3	1.3	✓	Rece	TP#3
12-6-93	TP#3	12-2-93	12/2/93	420	622.7	905.6	651	.97	1.4	✓	Rece	TP#3
12-6-93	RFL-SS-2525	12-2-93	12/2/93	554	831.5	786.3	593	1.4	1.3	✓	Rece	TP#3
12-6-93	TP#3	12-2-93	12-2-93	520	871.4	834.3	630	1.4	1.3	✓	Rece	TP#3
12-6-93	RFL-SS-2526	12-2-93	12/2/93	456	766.3	865.0	570	1.3	1.5	✓	Rece	TP#3
12-6-93	TP#3	12-2-93	12/2/93	456	766.3	865.0	570	1.3	1.5	✓	Rece	TP#3

Site Correction Factor = 1.8
 VP Correction Factor (if applicable) = 2.0
 Count Time = 500 SEC. unless otherwise noted

REVIEWED BY: John E. Tamm

Site HP Manager



SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214	Tl-208	MASS	Ra-228	Th-232	DEPTH	TECH	COMMENTS
					INITIAL 20 DAY	pCi INITIAL 20 DAY	pCi INITIAL 20 DAY	(grams) WET DRY	pCi/g INITIAL/20 DAY	pCi/g INITIAL 20 DAY	<15cm 20 DAY	
12-6-93	RFL-SS-2527			422	628.4	983.9	647	.97	1.5		RMC	TP#3
12/29/93	TP#3	12-2-93	12/1/93	556	681.2	719.2	576	1.2	1.2	✓	R	10'-11'
12-6-93	RFL-SS-2528			622	535.7	978.1	685	.78	1.4		RMC	TP#3
12/29/93	TP#3	12-2-93	12/1/93	458	723.7	792.4	592	1.2	1.3	✓	R	11'-12'
12-6-93	RFL-SS-2529			424	659.1	870.7	619	1.1	1.4		RMC	TP#3
12/29/93	TP#3	12-2-93	12/1/93	558	783.2	815.	543	1.4	1.5	✓	R	12'-13'
12-6-93	RFL-SS-2530			524	695.5	805.5	586	1.2	1.4		RMC	TP#3
12/29/93	TP#3	12-2-93	12/1/93	460	431.2	116.7	509	0.85	2.3	✓	R	13'-14'
12-6-93	RFL-SS-2531			426	643.6	827.2	663	.97	1.3		RMC	TP#3
12/29/93	TP#3	12-2-93	12/1/93	560	719.3	920.6	598	1.2	1.5	✓	R	14'-15'
12-6-93	RFL-SS-2532			526	502.3	1074	664	.76	1.6		RMC	TP#3
12/29/93	TP#3	12-2-93	12/1/93	462	644.7	870.7	549	1.1	1.6	✓	R	15'-16'
12-6-93	RFL-SS-2533			428	682.0	1028	724	.94	1.4		RMC	TP#3
12/29/93	TP#3	12-2-93	12/1/93	562	1029	719.2	642	1.6	1.1	✓	R	16'-17'
12-6-93	RFL-SS-2534			528	608.1	978.1	591	1.0	1.7		RMC	TP#3
12/29/93	TP#3	12-2-93	12/1/93	464	505.2	844.6	527	0.96	1.6	✓	R	17'-18'
12-6-93	RFL-SS-2535			430	539.8	888.2	661	.82	1.3		RMC	TP#3
12/29/93	TP#3	12-2-93	12/1/93	564	1012	872.6	592	1.7	1.5	✓	R	18'-19' screened
12-6-93	RFL-SS-2536			530	529.2	387.7	697	.76	.56		RMC	TP#3
12/29/93	TP#3 DUP	12-2-93	12/1/93	434	534.7	809.8	624	0.86	1.3	✓	R	18'-19' screened

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec. unless otherwise noted

REVIEWED BY:

John H. Fennell
Site HP Manager

FOR INFORMATION ONLY

ITE NAME RIFLE, CO.

OCS SAMPLE LOG

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214	Ti-208	MASS (grams)	Ra-228	Th-232	DEPTH	TECH	COMMENTS
					INITIAL 20 DAY	pCi INITIAL 20 DAY	pCi INITIAL 20 DAY	WET DRY	pCi/g INITIAL/CONT. 20 DAY	pCi/g INITIAL 20 DAY	<15cm	
2-6-93	RFL-SS-2537			432	224.7	1001	820	.88	1.2		RMC	TP#3
2/27/93	TP#3	12-2-93	12/7/93	466	690.1	957.8	746	0.93	1.3	✓	✓	19'-20' screened
2-6-93	RFL-SS-2538			532	474.8	1208	870	.55	1.4		RMC	TP#3
2/27/93	TP#3 DUP	12-2-93	12/6/93	532	13.3	863	785	1.6	1.1	✓	✓	19'-20' screened
2-6-93	RFL-SS-2539			434	548.6	231.4	754	.23	.97		RMC	TP#3
2/27/93	TP#3	12-2-93	12/7/93	467	690.1	957.8	746	0.93	1.3	✓	✓	20'-21' screened
2-6-93	RFL-SS-2540			534	636.5	882.2	731	.87	1.2		RMC	TP#3 DUP
12/29/93	TP#3 DUP	12-2-93	12/7/93	468	534.0	896.9	616	0.87	1.5	✓	✓	20'-21' screened
2-6-93	RFL-SS-2541			436	324.4	696.6	440	2.0	1.6		RMC	TP#7
2/30/93	TP#7	12-2-93	12/7/93	446	546.8	801.1	353	1.5	2.3	✓	✓	14'-15'
2-6-93	RFL-SS-2542			536	862.8	815.1	577	1.5	1.4		RMC	TP#7
12-27-93	TP#7	12-2-93	12-7-93	536	1344	939.8	449	3.0	2.1	✓	✓	15'-16' screened
2-6-93	RFL-SS-2543			438	670.1	748.8	618	1.1	1.2		RMC	TP#7
12/29/93	TP#7 DUP	12-2-93	12/7/93	568	943.5	738.4	481	2.0	1.5	✓	✓	15'-16' screened
2-6-93	RFL-SS-2544			538	3378	930.2	735	4.6	1.3		RMC	TP#7
12-27-93	TP#7	12-2-93	12-7-93	552	3667	748.0	617	5.9	1.2	✓	✓	16'-17' screened
2-6-93	RFL-SS-2545			440	3893	975.2	756	5.1	1.3		RMC	TP#7
12/29/93	TP#7 DUP	12-2-93	12/7/93	470	5222	1237	638	8.2	1.9	✓	✓	16'-17' screened
2-6-93	RFL-SS-2546			540	9549	1218	801	12	1.5		RMC	TP#7
12/30/93	TP#7	12-2-93	12/7/93	546	11601	1160	686	17	1.7	✓	✓	17'-18' screened

Site Correction Factor = 1.8

TP Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY: Robert K. Finsel

Site HP Manager



SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	Bi-214 pCi INITIAL 20 DAY	Ti-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-226 pCi/g INITIAL/CORR. 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-6-93	RFL-SS-2547			442	11519	1280	809	14	1.6		B	TP#2 screened
12/29/93	TP#7 DUP	12-2-93	12/7/93	570	14105	1112	693	20	1.6		B	17'-18' DUP
12-6-93	RFL-SS-2548			448	73263	3030	465	158	6.5		B	TP#6 COMPOSITE
	TP#6	11/30/93									✓	20-25'
12-6-93	RFL-SS-2549			548	1001	1084	559	1.8	1.9		B	TP#19 COMPOSITE
	TP#19	12/3/93									✓	3.6'-5.5'
12-6-93	RFL-SS-2550			450	1957	653.1	648	3.0	1.0		B	TP#20 COMPOSITE
	TP#20	12-3-93										
12-6-93	RFL-SS-2551			550	2243	863.0	561	4.0	1.5		B	TP#20 COMPOSITE
	12-6-93 KC TP#20 20	12-1-93									✓	1'-5'
12-6-93	RFL-SS-2552			452	980.4	548.6	637	1.5	.860		B	TP#21 COMPOSITE
	TP#21	12-1-93									✓	1'-5'
12-6-93	RFL-SS-2553			562	12270	1458	648	19	2.3		B	TP#21 COMPOSITE
	TP#21	12-3-93										
12-6-93	RFL-SS-2554			454	452.8	818.5	648	.70	1.3		B	TP#22 COMPOSITE
	TP#22	12/3/93										
12-6-93	RFL-SS-2555			554	929.3	930.6	608	1.5	1.5		B	TP#24 COMPOSITE
	TP#24	12/3/93										
12-6-93	RFL-SS-2556			456	787.9	1193	772	1.0	1.5		B	TP#25 COMPOSITE
	TP#25	12/3/93									✓	6.5'-8.5'

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY:

John H. Fornich
Site HP Manager

FOR INFORMATION ONLY

TE NAME RIFLE, CO.

OCS SAMPLE LOG

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214	Tl-208	MASS	Ra-226	Th-232	DEPTH	TECH	COMMENTS
					INITIAL 20 DAY	pCi INITIAL 20 DAY	pCi INITIAL 20 DAY	(grams) WET DRY	pCi/g INITIAL/CORR. 20 DAY	pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	INITIAL 20 DAY
2-6-93	RFL-SS-2557			586	810.7	1064	524	1.5	2.0			TP#25 Composite
	TP#25	12-1-93								✓		7.5' - 8.5'
2-6-93	RFL-SS-2558			458	1234	844.6	538	2.3	1.6			TP#25 Composite
	TP#25	12-1-93								✓		9'-10'
2-6-93	RFL-SS-2559			558	1229	958.9	635	1.9	1.5			TP#27 Composite
	TP#27	12-3-93								✓		9.5' - 11'
2-6-93	RFL-SS-2560			460	957.6	879.5	678	1.4	1.3			TP#28 Composite
	TP#28	12-3-93										
2-6-93	RFL-SS-2561			560	877.5	2014	410	92.1	4.9			TP#29 Composite
	TP#29	12-3-93										
2-6-93	RFL-SS-2562			572	1425.5	1112	732	19	1.5			
2-30-93	493	12-6-93	12-7-93	448	2078.4	1811	676	31	2.7	✓		
2-6-93	RFL-SS-2563	12-6-93		464	274.7	905.6	519	0.53	1.7			TP#2
	TP#2	12-6-93								✓		13'-16' Composite
2-7-93	RFL-SS-2564	12-6-93		564	450.4	997.3	586	0.77	1.7			TP#1
	TP#1	12-6-93								✓		15'-17' Composite
2-7-93	RFL-SS-2565			466	1028.4	933.9	543	1.2	1.8			TP#15
	TP#15	12-6-93										Composite
2-7-93	RFL-SS-2566			566	327.2	728.8	519	0.63	1.4			TP#26
	TP#26	12-6-93										Composite

ite Correction Factor = 1.8

'P Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY: Robert P. Fennell
Site HP Manager



SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # <u>INITIAL</u> 20 DAY	Bi-214 pCi <u>INITIAL</u> 20 DAY	Tl-208 pCi <u>INITIAL</u> 20 DAY	MASS (grams) <u>WET</u> <u>DRY</u>	Ra-226 pCi/g <u>INITIAL/COFFL</u> 20 DAY	Th-232 pCi/g <u>INITIAL</u> 20 DAY	DEPTH <u><15cm</u> <u>>15cm</u>	TECH <u>INITIAL</u> 20 DAY	COMMENTS
12-7-93	RFL-SS-2567			468	1922	809.8	604	3.0	1.3		RMC	TP#30
	TP#30	12-6-93								✓		4.5'-7.5' Composite
12-8-93	RFL-SS-2568			424	489.7	801.1	578.3	0.85	1.4		RMC	Composite
	BKG Pit	12-7-93									—	BKG Pit
12-8-93	RFL-SS-2569			524	926.9	623.3	530.7	1.8	1.2		RMC	TP#4
	TP#4	12-7-93									—	Composite
12-8-93	RFL-SS-2570			426	555.1	539.9	436.2	1.3	1.2		RMC	TP#3
	TP#3	12-7-93									—	Composite
12-8-93	RFL-SS-2571			526	309.3	776.7	491.3	.63	1.6		RMC	TP#5
	TP#5	12-7-93									—	Composite
12-8-93	RFL-SS-2572			428	579.3	618.2	462.0	1.3	1.5		RMC	TP#11
	TP#11	12-7-93									—	Composite
12-8-93	RFL-SS-2573			528	259.1	343.3	476.0	160	7.2		RMC	TP#7
	TP#7	12-7-93									—	Composite
12/9/93	RFL-SS-2574			400	1372	626.9	446	3.1	1.4		R	TP#1 -4 MOIST
12/30/93	TP#1	12/6/93	12/9/93	450	1528	870.7	446	3.4	2.0	✓	R	15-17' composite
12/9/93	RFL-SS-2575			500	521.2	918.1	433	1.2	2.3		R	TP#2 -4 MOIST
12/30/93	TP#2	12/6/93	12/9/93	550	42.8	891.8	433	0.95	2.1	✓	R	13-16' composite
12/9/93	RFL-SS-2576			402	921.0	609.5	460	3.0	1.3		R	TP#3 18-21' -4 moist
1-3-94	TP#3	12/7/93	12/9/93	500	624.7	1093	460	1.4	2.4	✓	R	Composite

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY: Robert H. Fornal

Site HP Manager

FOR INFORMATION ONLY

OCS SAMPLE LOG

ITE NAME RIFLE, CO.

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Re-228 pCi/g INITIAL/CORR. 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
				INITIAL 20 DAY	INITIAL 20 DAY	INITIAL 20 DAY	INITIAL/CORR. 20 DAY	INITIAL 20 DAY	INITIAL 20 DAY	INITIAL 20 DAY	INITIAL 20 DAY	
2/9/93	RFL-SS-2577			502	2339	805.1	442	5.3	1.8			TP#4 -4 moist
1/3/93 94	TP#4	12/7/93	12/9/93	518	2948	1074	442	6.7	2.4	✓		11-16' composite
2/9/93	RFL-SS-2578			404	885.8	653.1	427	2.1	1.5			TP#5 -4 moist
1-3-94	TP#5	12/7/93	12/9/93	400	1172	757.5	427	2.7	1.8	✓		16-21' composite
2/9/93	RFL-SS-2579			504	73891	3360	419	154.3	6.8			TP#7 -4 moist
1/3/94	TP#7	12/7/93	12/9/93	402	100310	4476	479	209.4	9.3	✓		11-21' composite
2/9/93	RFL-SS-2580			406	1061	809.8	417	2.5	1.9			TP#11 -4 moist
1/3/94	TP#11	12/7/93	12/9/93	502	1072	978.1	417	2.6	2.3	✓		composite
2/9/93	RFL-SS-2581			506	1563	786.3	525	3.0	1.5			TP#15 -4 moist
1/3/94	TP#15	12/6/93	12/9/93	504	2978	911.0	525	5.7	1.7	✓		10-13' composite
2/9/93	RFL-SS-2582			408	1698	757.5	456	3.7	1.7			TP#19 -4 moist
1/3/94	TP#19	12/2/93	12/9/93	404	3612	949.1	456	7.9	2.1	✓		3.5'-5.5' composite
2/9/93	RFL-SS-2583			508	2774	949.3	500	5.9	1.9			TP#20 -4 moist
1/3/94	TP#20	12/2/93	12/9/93	506	5162	968.5	500	10.3	1.9	✓		composite
2/9/93	RFL-SS-2584			410	10559	940.4	456	23	2.1			TP#21 -4 moist
1/3/94	TP#21	12/6/93	12/9/93	406	19350	1724	456	40	3.8	✓		composite
2/9/93	RFL-SS-2585			510	838.3	958.9	582	1.4	1.6			TP#22 -4 moist
1/3/94	TP#22	12/6/93	12/9/93	508	1020	872.6	582	1.8	1.5	✓		composite
2/9/93	RFL-SS-2586			412	565.3	696.7	495	1.1	1.4			TP#24 -4 moist
1/3/94	TP#24	12/11/93	12/9/93	408	1214	1115	495	2.5	2.3	✓		composite

Site Correction Factor = 1.8

HP Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY: *J. Hunt, Jr. email*

Site HP Manager

RIFLE, CO.
OCS SAMPLE LOG

SITE NAME	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214 PCI INITIAL 20 DAY	Tl-208 PCI INITIAL 20 DAY	RA-228 PCI/g INITIAL 20 DAY	Th-232 PCI/g INITIAL 20 DAY	DEPTH <15cm	DEPTH >15cm	TECH INITIAL 20 DAY	COMMENTS
12/9/93	RFL-SS-2587	12/1/93	12/9/93	5/2	12/8	497.3	553	2.2	1.8	✓	TP#25	-4' moist
1/3/94	TP#25			410	2232	975.2	553	4.0	1.8	✓	TP#26	-4' moist
12/9/93	RFL-SS-2588			414	799.3	687.9	526	1.5	1.3	✓	TP#26	-4' moist
1/3/94	TP#26	12/6/93	12/9/93	510	1104	863.0	526	2.1	1.6	✓	TP#27	-4' moist
12/9/93	RFL-SS-2589			514	658.5	795.9	583	1.1	1.4	✓	TP#27	-4' moist
1/3/94	TP#27	12/6/93	12/9/93	512	899.4	911.0	583	1.5	1.6	✓	TP#27	-4' moist
12/9/93	RFL-SS-2590			416	3456.6	2620	417	83	4.8	✓	TP#29	-4' moist
1/3/94	TP#29	12/6/93	12/9/93	412	6206.6	3100	417	149	7.4	✓	TP#29	-4' moist
12/9/93	RFL-SS-2591			516	130.1	786.3	507	1.4	1.6	✓	TP#30	-4' moist
1/3/94	TP#30	12/6/93	12/9/93	514	1117	1007	507	2.2	2.0	✓	TP#30	-4' moist
12/9/93	RFL-SS-2592			418	859.7	740.1	633	1.4	1.2	✓	TP#32	con sy
1/3/94	TP#32	12/8/93	12/9/93	414	819.3	896.9	633	1.3	1.4	✓	TP#32	con sy
12/9/93	RFL-SS-2593			518	557.1	642.5	422	1.1	1.3	✓	TP#33	con sy
1/3/94	TP#33	12/8/93	12/9/93	516	511.3	767.1	492	1.0	1.6	✓	TP#33	con sy
12/9/93	RFL-SS-2594			420	794.6	809.8	464	1.7	1.7	✓	TP#34	-4' moist
1/3/94	TP#34	12/7/93	12/9/93	416	790.7	1237	464	1.7	2.7	✓	TP#34	-4' moist
12/9/93	RFL-SS-2595			426	1237	783.7	490	2.5	1.6	✓	TP#35	-4' moist
1/3/94	TP#35	12/6/93	12/13/93	418	2096	1238	448	4.7	2.7	✓	TP#35	-4' moist
12/9/93	RFL-SS-2596			526	1416	853.4	494	2.9	1.7	✓	TP#36	2 of 2
1/3/94	TP#36	12/6/93	12/13/93	420	2077	748.8	453	4.6	1.7	✓	TP#36	2 of 2
12/9/93	RFL-SS-2597			526	1416	853.4	494	2.9	1.7	✓	TP#37	2 of 2
1/3/94	TP#37	12/6/93	12/13/93	420	2077	748.8	453	4.6	1.7	✓	TP#37	2 of 2

Site Correction Factor = 1.8
 VP Correction Factor (if applicable) = 2.0
 Count Time = 500 sec. unless otherwise noted

REVIEWED BY: John L. Fennell
 SITE HP Manager

ITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT	DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) Wt/L DLY	Rs-226 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH	COMMENTS
3/9/93	RFL-SS- 2597	TP# 2	12/6/93	12/13/93	1278	503.0	809.8	495	1.0	1.6		TP #2	1' 08 2
1/3/94	RFL-SS- 2598	TP# 2	12/6/93	12/13/93	520	566.5	911.0	452	1.3	2.0	✓		13'-16' Rust Comp.
1/2/93	RFL-SS- 2599	TP# 2	12/6/93	12/13/93	528	583.7	767.1	515	1.1	1.5		TP#2	2' 07 2
1/3/94	RFL-SS- 2599	TP# 3	12/6/93	12/13/93	524	789.1	709.6	473	1.7	1.5			13'-16' Rust Comp.
1/2/93	RFL-SS- 2600	TP# 3	12/7/93	12/13/93	430	965.2	801.1	488	2.0	1.6		TP#3	1' 08 2
1/3/94	RFL-SS- 2601	TP# 3	12/7/93	12/13/93	424	1036	714.0	432	2.4	1.7	✓		18'-21' Rust Comp.
1/2/93	RFL-SS- 2601	TP# 4	12/7/93	12/13/93	531	698.8	757.6	511	1.4	1.5		TP#3	2' 08 2
1/3/94	RFL-SS- 2602	TP# 4	12/7/93	12/13/93	426	1285	748.8	450	2.9	1.7	✓		18'-21' Rust Comp.
1/2/93	RFL-SS- 2603	TP# 4	12/7/93	12/13/93	432	2593	975.2	484	5.4	2.0		TP#4	1' 03 2
1/3/94	RFL-SS- 2604	TP# 4	12/7/93	12/13/93	526	4244	537.0	463	9.2	1.2	✓		11'-16' Rust Comp.
1/2/93	RFL-SS- 2604	TP# 4	12/7/93	12/13/93	532	3101	642.5	479	6.5	1.3		TP#4	3' 03 2
1/3/94	RFL-SS- 2605	TP# 5	12/7/93	12/13/93	428	4287	809.8	453	9.5	1.8			11'-16' Rust Comp.
1/2/93	RFL-SS- 2605	TP# 5	12/7/93	12/13/93	438	747.2	957.8	528	1.4	1.8	✓	TP#5	1 of 2
1/3/94	RFL-SS- 2604	TP# 5	12/7/93	12/13/93	528	869.3	805.5	476	1.8	1.7	✓		16'-21' Rust Comp.
1/2/93	RFL-SS- 2605	TP# 5	12/7/93	12/13/93	532	699.0	671.3	503	1.4	1.3	✓	TP#5	2 of 2
1/3/94	RFL-SS- 2605	TP# 7	12/7/93	12/13/93	440	73019	4058	539	1.35	7.5	✓	TP#7	1 of 2
1/2/93	RFL-SS- 2606	TP# 7	12/7/93	12/13/93	530	10024	4306	485	2.0	8.9	✓		11'-21' Rust Comp.
1/3/94	RFL-SS- 2606	TP# 7	12/7/93	12/13/93	540	73183	3280	527	1.39	6.2	✓	TP#7	2 of 2
1/2/93	RFL-SS- 2607	TP# 7	12/7/93	12/13/93	432	99355	3527	474	210	7.4	✓		11'-21' Rust Comp.

100 Correction Factor = 1.8
 Count time = 500 sec., unless otherwise noted

REVIEWED BY:

Site HP Manager

John T. French

SITE NAME RIFLE, CO.

COS SAMPLE LOG

FOR INFORMATION ONLY

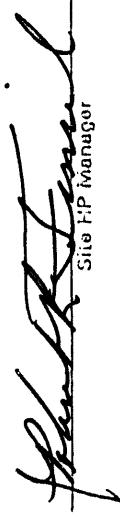
COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	COS #	3-214 PC INITIAL 20 DAY	71-20a PC INITIAL 20 DAY	MASS (prem.) %V/I DRY	Re-226 PC/I INITIAL 20 DAY	Th-232 PC/I INITIAL 20 DAY	DEPTH cm >15cm 20 DAY	TECH Rue TP#11 10' 2	COMMENTS
12-9-93	RFL-SS-2607	12-7-93	12/13/93	4112	9981	222.7	486	2.1	1.5		Rue TP#11 10' 2	
1/3/94	TP#11	12-7-93	12/13/93	5321	1227	930.2	4472	2.8	2.1		Rue TP#11 10' 2	
12-9-93	RFL-SS-2608			51/2	1084	76.7	465	2.3	1.7		Rue TP#11 10' 2	
1/3/94	TP#11	12-7-93	12/13/93	434	1461	975.2	423	3.3	2.3		Rue TP#11 10' 2	
12-9-93	RFL-SS-2609			444	1440	79.4	553	2.6	1.4		Rue TP#15 10' 2	
1/3/94	TP#15	12-6-93	12/13/93	534	2253	901.4	507	5.4	1.8		Rue TP#15 10' 2	
12-9-93	RFL-SS-2610			544	1706	671.3	501	3.4	1.3		Rue TP#15 10' 2	
1/3/94	TP#15	12-6-93	12/13/93	436	2880	714.0	460	6.3	1.6		Rue TP#15 10' 2	
12-9-93	RFL-SS-2611			446	2058	944.6	493	4.2	1.7		Rue TP#19 10' 2	
1/3/94	TP#19	12-2-93	12/13/93	536	3158	815.1	459	6.9	1.8		Rue TP#19 10' 2	
12-9-93	RFL-SS-2612			546	1965	8334.3	483	4.1	1.7		Rue TP#19 10' 2	
1/3/94	TP#19	12-2-93	12/13/93	542	2698	39.8	450	6.0	2.1		Rue TP#20 10' 2	
12-9-93	RFL-SS-2613			444	3774	592.1	622	7.2	1.1		Rue TP#20 10' 2	
1/3/94	TP#20	12-2-93	12/13/93	544	4898	1087	489	10.0	2.1		Rue TP#20 10' 2	
12-9-93	RFL-SS-2614			548	3957	748.0	557	7.1	1.3		Rue TP#20 10' 2	
1/3/94	TP#20	12-2-93	12/13/93	444	4875	870.7	520	9.4	1.7		Rue TP#21 10' 2	
12-9-93	RFL-SS-2615			450	11532	1280	540	2.1	2.4		Rue TP#21 10' 2	
1/3/94	TP#21	12-6-93	12/13/93	446	9101	1316	498	38	2.8		Rue TP#21 10' 2	
12-9-93	RFL-SS-2616			550	12280	1017	544	23	1.9		Rue TP#21 10' 2	
1/3/94	TP#21	12-6-93	12/13/93	546	19679	1381	502	39	2.8		Rue TP#21 10' 2	

1.8

 VP Correction Factor (if applicable) = 2.0
 Count Time = 500 sec., unless otherwise noted

REVIEWED BY:

Site HP Manager



FOR INFORMATION ONLY

SITE NAME RIFLE, CO.

CGS SAMPLE LOG

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCB # INITIAL 20 DAY	Bi-214 pCi INITIAL 20 DAY	Ti-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Rn-220 pCi/g INITIAL/COAL 20 DAY	Rn-232 pCi/g INITIAL 20 DAY	DEPTH 15cm 18cm	TECH INITIAL 20 DAY	COMMENTS
2-9-93	RFL-SS-2617			452	936.3	844.6	623	1.5	1.4		RnC	TP#22 1 of 2
3/94	TP#22	12-6-93	12/13/93	448	1066	801.1	548	1.9	1.5	✓	R	4'-7' Rust Comp
2-9-93	RFL-SS-2618			552	1330	680.8	719	1.8	.95		RnC	TP#22 2 of 2
1/3/94	TP#22	12-6-93	12/13/93	548	1382	786.3	634	2.2	1.2	✓	R	4'-7' Rust Comp
2-9-93	RFL-SS-2619			454	1131	626.9	548	2.1	1.1		RnC	TP#24 1 of 2
1/3/94	TP#24	12-1-93	12/13/93	450	1454	818.5	505	2.9	1.6	✓	R	2.5'-5' Rust Comp
2-9-93	RFL-SS-2620			554	1007	632.9	554	1.8	1.1		RnC	TP#24 2 of 2
1/3/94	TP#24	12-1-93	12/13/93	550	1384	632.9	509	2.7	1.2	✓	R	2.5'-5' Rust Comp
2-9-93	RFL-SS-2621			456	1430	731.4	634	2.3	1.2		RnC	TP#25 1 of 2
1/3/94	TP#25	12-1-93	12/13/93	552	2160	738.4	571	3.8	1.3	✓	R	6.5'-8.5' Rust Comp
2-9-93	RFL-SS-2622			556	938.7	1036	539	1.7	1.9		RnC	TP#25 2 of 2
1/3/94	TP#25	12-1-93	12/13/93	452	2110	862.0	487	4.3	1.8	✓	R	6.5'-8.5' Rust Comp
2-9-93	RFL-SS-2623			458	618.4	635.6	544	1.1	1.2		RnC	TP#26 1 of 2
1/3/94	TP#26	12-6-93	12/13/93	554	1086	709.6	514	2.1	1.4	✓	R	8'-9.5' Rust Comp
2-9-93	RFL-SS-2624			558	902.6	680.8	537	1.7	1.3		RnC	TP#26 2 of 2
1/3/94	TP#26	12-6-93	12/13/93	454	1086	896.9	508	2.1	1.8	✓	R	8'-9.5' Rust Comp
2-9-93	RFL-SS-2625			460	1009	679.2	637	1.6	1.1		RnC	TP#27 1 of 2
1/3/94	TP#27	12-3-93	12/13/93	556	1122	795.9	572	2.0	1.4	✓	R	9.5'-11' Rust Comp
2-9-93	RFL-SS-2626			560	627.5	941.3	579	1.1	1.6		RnC	TP#27 2 of 2
1/3/94	TP#27	12-3-93	12/13/93	456	798.5	870.7	580	1.5	1.7	✓	R	9.5'-11' Rust Comp

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY:

Robert F. Sennil

Site HP Manager

SITE NAME: RIFLE, CO.

C-233 SAMPLE LOG

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	DCS #	Bi-214 PCi INITIAL 20 DAY	Tl-203 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Re-226 pCi/g INITIAL 20 DAY	1n-232 pCi/g INITIAL 20 DAY	DEPTH ≤ 15cm > 15cm	TECH	COMMENTS
12-4-93	RFL-SS-2627			462	1285	2488	462	2.7	1.6		Puc	TP#28 1 of 2
13/94	TP#28	12-9-93	12/13/93	558	2269	8247	442	5.1	1.9		TP#28	0'-45' Post Comp
12-4-93	RFL-SS-2628			562	1962	9781	557	3.5	1.8		Puc	TP#28 2 of 2
13/94	TP#28	12-9-93	12/13/93	458	2189	1202	510	4.3	2.4		TP#28	0'-45' Post Comp
12-9-93	RFL-SS-2629			464	30354	2064	498	77	4.1		Puc	TP#29 1 of 2
13/94	TP#29	12-6-93	12/13/93	470	64696	2699	460	141	5.9		TP#29	0'-3' Post Comp
12-9-93	RFL-SS-2630			564	40256	1891	493	83	3.7		Puc	TP#29 2 of 2
13/94	TP#29	12-6-93	12/13/93	570	67840	3030	458	148	6.6		TP#29	0'-3' Post Comp
12-9-93	RFL-SS-2631			566	1209	548.6	590	2.1	.93		Puc	TP#30 1 of 2
13/94	TP#30	12-6-93	12/13/93	572	1238	795.9	566	2.2	1.4		TP#30	4.5'-7.5' Post Comp
12-9-93	RFL-SS-2632			568	892.2	891.8	540	1.8	1.2		Puc	TP#32 1 of 2
13/94	TP#30	12-6-93	12/13/93	472	1484	879.5	518	2.9	1.7		TP#32	4.5'-7.5' Post Comp
12-9-93	RFL-SS-2633			468	667.9	740	473	1.4	1.5		Rug	TP#32 1 of 2
13/94	TP#32	12-9-93	12/13/93	574	536.9	546.6	460	1.2	1.2		Rug	0'-4' Post Comp
12-9-93	RFL-SS-2634			568	302.1	772.7	482	.62	1.6		Rug	TP#32 2 of 2
13/94	TP#32	12-9-93	12/13/93	474	510.4	827.2	469	1.1	1.8		TP#32	0'-4' Post Comp
12-9-93	RFL-SS-2635			470	530.7	708.8	521	1.0	1.4		Rug	TP#33 1 of 2
13/94	TP#33	12-9-93	12/13/93	576	631.0	546.6	488	1.3	1.1		Rug	0'-4' Post Comp
12-9-93	RFL-SS-2636			570	470.4	709.6	486	.97	1.5		Rug	TP#33 2 of 2
13/94	TP#33	12-9-93	12/13/93	476	421.3	626.9	454	0.93	1.4		Rug	0'-4' Post Comp

 Site Correction Factor = 1.8

 VP Correction Factor (if applicable) = 2.0

 Count Time = 500 Sec., unless otherwise noted

Site Manager

REVIEWED BY:

John J. Lavelle

FOR INFORMATION ONLY

CCE SAMPLE LOG

SITE NAME RIFLE, CO.

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SCALED	CCS :	3-214 pCi INITIAL 20 DAY	3-203 pCi INITIAL 20 DAY	MASS (gram) WET DRY	AL-220 pCi/g INITIAL/CONC. 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH ≤15cm ≥15cm	TECH INITIAL 20 DAY	COMMENTS
12-9-93	RFL-SS-2637	93	4/22	561.2	822.2	483	1.2	1.7	1.7	1.7	1.7	Pneu PKG 1 of 2
1/3/94	TP# BKG	12-7-93	12-13-93	578	706.1	757.6	1.6	1.7	1.7	1.7	1.7	7-12' Rust Cor.
	RFL-SS-2638	1/3/94	5/22	862.6	901.4	523	1.7	TP# BKG 2 of 2	1.7	1.7	1.7	TP# BKG 2 of 2
2-9-93	TP# BKG	12-7-93	12-13-93	478	1039	862.0	2.2	1.8	1.8	1.8	1.8	7-12' Rust Cor.
1/3/94	TP# BKG	12-11/93	406	34918	2055	505	6.8	4.1	4.1	4.1	4.1	TP# 29 0-1'
1/10/93	RFL-SS- 2639	12-13-93	12-13-93	554	56401	2532	505	11.2	5.0	5.0	5.0	TAC Sample
1/10/94	TP# 29	12/1/93	SD6	11247	1074	561	20.	1.9	1.9	1.9	1.9	TP# 29 1-2'
1/2/10/93	RFL-SS- 2640	12-13-93	12-13-93	454	20115	1768	561	3.6	3.2	3.2	3.2	TAC Sample
1/10/94	TP# 29	12/1/93	408	32618	1698	354	59.0	3.1	3.1	3.1	3.1	TP# 29 2-3'
1/2/10/93	RFL-SS- 2641	12/1/93	12-13-93	558	55305	2503	554	100	4.5	4.5	4.5	TAC Sample
1/10/94	TP# 29	12/1/93	422	1672	87446	471	3.5	1.8	1.8	1.8	1.8	TP# 28 0-15'
12/10/93	RFL-SS- 2642	12/1/93	12/10/93	480	2434	766.3	471	5.4	1.6	1.6	1.6	Complaint
1/3/94	TP# 28	12/1/93	522	4345	623.3	461	1.1	1.6	1.6	1.6	1.6	TP# 32
1/2/10/93	RFL-SS- 2643	12/1/93	12/10/93	580	710.9	460.3	401	1.8	1.1	1.1	1.1	TP# 33
1/3/94	TP# 32	12/1/93	424	451.1	992.4	491	0.92	1.6	1.6	1.6	1.6	TP# 33
1/2/10/93	RFL-SS- 2644	12/1/93	12/10/93	582	593.2	527.4	491	1.2	1.1	1.1	1.1	TP# 33
1/3/94	TP# 33	12/1/93	450	19091	13.5	803	24.0	1.6	1.6	1.6	1.6	TP# 33
1/2/15/93	RFL-SS- 2645	12/1/5/93	446	26094	1881	803	32.6	2.3	2.3	2.3	2.3	TP# 4
1/5/94	TP# 4	12/1/5/93	500	19051.0	8539	805	337.0	10.6	10.6	10.6	10.6	TP# 6
12/15/93	RFL-SS- 2646	12/15/93	448	218120	7480	805	271	9.3	9.3	9.3	9.3	24-25' THC
1/5/94	TP# 6	12/15/93	12/16/93	446	26094	1881	803	32.6	2.3	2.3	2.3	TP# 6

Site Correction Factor = 1.8
 VP Correction Factor (if applicable) = 2.0
 Cont. Time = 500 sec. unless otherwise noted

REVIEWED BY:
 Site Manager

John J. French
 Site Manager

FOR INFORMATION ONLY
OCS SAMPLE LOG
SITE NAME RIFLE, CO.

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	Bi-214 PCI INITIAL 20 DAY	Ti-203 PCI INITIAL 20 DAY	MASS (gram) WET DRY	Ra-226 PCI/6 INITIAL/COH4; 20 DAY	Th-232 PCI/6 INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12/15/93	RFL-SS-2647	12/15/93	12/16/93	402	6780	8271.2	155	9.0	1.1			17-18'
1/5/94	TP#7			546	9534	939.8	755	13	1.2			TP#7 TAC
12/15/93	RFL-SS-2648			503	1720	1611	809	21.2	2.0			8-9'
1/5/94	TP#30	12/16/93		548	45157	2206	809	56	2.7			TD#30 TAC
12/16/93	RFL-SS-2649A			400	1767	853.3	498	3.5	1.7			A-914 CPTM
1/6/94		12/17/93	514	3664	1064	46e	7.9	2.3				B-N.W.
12/16/93	RFL-SS-2650A			500	883.0	979.9	522	1.7	1.5			A-1040 CPTM
1/6/94		12/17/93	508	697.4	1007	480	1.5	2.1				Area B-Fence Line
12/16/93	RFL-SS-2651A			402	1656	801.1	430	3.9	1.9			
1/6/94		12/17/93	408	4240	661.8	363	12	1.8	1.5			
12/16/93	RFL-SS-2652A			502	587.4	901.4	498	1.2	1.8			B-N.W.
1/6/94		12/17/93	510	715.9	700.0	464	1.5	1.5				△ 912 CPTM
12/16/93	RFL-SS-2653A			404	2631	879.5	452	5.8	1.9			
1/6/94		12/16/93	458	4819	983.9	452	11	2.2				△ 1350 CPTM
12/16/93	RFL-SS-2654A			504	773.9	968.5	517	1.5	1.9			
1/6/94		12/17/93	410	970.4	496.3	459	2.1	1.1	1.1			△ 1610 CPTM
12/16/93	RFL-SS-2655A			406	639.6	766.3	595	1.1	1.3			B-N.W.
1/6/94		12/17/93	512	352.6	863.0	573	0.62	1.5				△ 1550 CPTM
12/16/93	RFL-SS-2656A			506	247.0	1084	493	1.5	2.2			B-N.W.
1/6/94		12/17/93	412	423.5	757.5	463	0.91	1.6	1.6			△ 712 CPTM

 Site Correction Factor = 1.8 VP Correction Factor (if applicable) = 2.0

 Count Time = 500 sec. unless otherwise noted

 REVIEWED BY: John S. Clegg

Site HP Manager

2149 - 2450 to avoid confusion with duplicate sample # ID numbers assign

**DATE
FILMED**

10/20/94

END