

DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

WSRC-MS--92-227

DE92 016889

CORE MELT PROGRESSION AND CONSEQUENCE ANALYSIS METHODOLOGY DEVELOPMENT IN SUPPORT OF THE SAVANNAH RIVER REACTOR PSA (U)

by

K. R. O'Kula and D. A. Sharp

Westinghouse Savannah River Company
Savannah River Site
Aiken, South Carolina 29808

and

C. N. Amos, K. C. Wagner, and D. R. Bradley

Science Applications International Corporation
2109 Air Park Road S. E.
Albuquerque, NM 87106

JUL 1 6 1992

A paper proposed for presentation at the
Probabilistic Safety Assessment International Topical Meeting
Clearwater Beach, FL
January 27 - 29, 1993

and for publication in the proceedings

The information contained in this abstract was developed during the course of work done under Contract No. DE-AC09-89SR18035 with the U.S. Department of Energy. By acceptance of this paper the publisher and/or recipient acknowledges the U.S. Government's right to retain a nonexclusive, royalty-free license in and to any copyright covering this paper, along with the right to reproduce and to authorize others to reproduce all or part of the copyrighted paper.

MASTER
DISTRIBUTION OF THIS DOCUMENT IS UNLIMITED

**CORE MELT PROGRESSION AND CONSEQUENCE ANALYSIS
METHODOLOGY DEVELOPMENT IN SUPPORT OF THE SAVANNAH
RIVER REACTOR PSA**

by

K. R. O'Kula and D. A. Sharp

Westinghouse Savannah River Company
Safety Technology Section
992W-1 Savannah River Site
Aiken, South Carolina 29803

C. N. Amos, K. C. Wagner, and D. R. Bradley

Science Applications International Corporation
2109 Air Park Road S.E.
Albuquerque, NM 87106

DOES NOT CONTAIN
UNCLASSIFIED CONTROLLED
NUCLEAR INFORMATION

Reviewing
Official: Kevin O'Kula
Kevin R. O'Kula, Manager
Risk & Source Term Technology
Group/Safety Technology Section

Date: 6-2-92

Summary of a paper proposed for presentation and publication at the
Probabilistic Safety Assessment International Topical Meeting
Clearwater Beach, Florida
January 27-29, 1993

This paper was prepared in connection with work done under Contract No. DE-AC09-89SR18035 with the U.S. Department of Energy. By acceptance of this paper, the publisher and/or recipient acknowledges the U.S. Government's right to retain a nonexclusive, royalty-free license in and to any copyright covering this paper, along with the right to reproduce and to authorize others to reproduce all or part of the copyrighted paper.

**CORE MELT PROGRESSION AND CONSEQUENCE ANALYSIS
METHODOLOGY DEVELOPMENT IN SUPPORT OF THE
SAVANNAH RIVER REACTOR PSA**

K. R. O'Kula and D. A. Sharp
Safety Technology Section
992W-1 Westinghouse Savannah River Company
Aiken, South Carolina 29803

C. N. Amos, K. C. Wagner, and D. R. Bradley
Science Applications International Corporation
2109 Air Park Road, S. E.
Albuquerque, New Mexico 87106

INTRODUCTION

A three-level Probabilistic Safety Assessment (PSA) of production reactor operation has been underway since 1985 at the U. S. Department of Energy's Savannah River Site (SRS). The goals of this analysis are to: (1) analyze existing margins of safety provided by the heavy-water reactor (HWR) design challenged by postulated severe accidents; (2) compare measures of risk to the general public and onsite workers to guideline values, as well as to those posed by commercial reactor operation; and (3) develop the methodology and database necessary to prioritize improvements to engineering safety systems and components, operator training, and engineering projects that contribute significantly to improving plant safety. PSA technical staff from the Westinghouse Savannah River Company (WSRC) and Science Applications International Corporation (SAIC) have performed the assessment despite two obstacles: (1) a variable baseline plant configuration and power level; and (2) a lack of technically applicable code methodology to model the SRS reactor conditions. This paper discusses the detailed effort necessary to modify the requisite codes before accident analysis insights for the risk assessment were obtained.

Although the Level 1 PSA SRS methods for analysis of severe accident initiators and binning into plant damage states are similar to that available for commercial plants, the Level 2/3 portion of the analysis required code revision in virtually every aspect of the overall model. Modifications of key light-water reactor (LWR) codes had to be accomplished before integrated phenomenological assessments supporting an Accident Progression Event Tree could be finalized. Several accident and consequence analysis codes to predict primary system thermal hydraulics, fission product transport, confinement system thermal hydraulics, molten core-concrete interactions (MCCI), molten fuel coolant interactions (MFCI) and ex-plant consequence determination are discussed in this paper, along with associated model changes, the chief insights developed as a result of the analysis, and the extent of applicability elsewhere in the DOE complex.

METHODOLOGY

The modified computer codes necessary to support quantification of the in-plant Level 2 risk study are discussed initially. Next, revisions to the ex-plant consequence analysis model for onsite workers is summarized.

Phenomenology of postulated reactor accidents and the accompanying core melt progression is profoundly different in SRS reactors than in LWR counterparts. Most significantly, zircalloy-clad uranium dioxide fuel, high temperature-high pressure primary system conditions and containment parameters, will lead to fission product barrier challenges markedly different from those in a production reactor with aluminum alloy, uranium-aluminum fuel, low temperature-low pressure primary conditions operating with confinement. In the SRS PSA, integrated analysis tools were developed in three stages to provide temperature and pressure estimates, and later, fission product source terms, corresponding to severe accident scenarios. CONTEMPT4¹ was applied initially in a 1987 scoping analysis of confinement response. Heat loads were computed outside of the code and then incorporated in the analysis as tabular input to model core debris and structural sources of deposited energy. The second generation of analysis in 1989 - 1990 included the ability to model coupled thermal-hydraulic/aerosol/fission product behavior as part of CONTAIN/SR code. CONTAIN/SR was the primary tool used to support severe accident analysis in the 1990 Environmental Impact Statement for continued reactor operation at SRS and is tailored for fan/filter modeling based on CONTAIN 1.10.² By 1991, a more realistic filter compartment model and the ability to perform hundreds of sensitivity analyses to support quantification of the Level 2 APET led to adoption of the MELCOR/SR code as the primary tool supporting the SRS Level 2 PSA.³ Additional demands for phenomenological insights due to MCCI and MFCI in SRS reactors required special-purpose models by SNL and the University of Wisconsin, respectively. The core debris-concrete interactions were estimated with a CORCON version that included aluminum and silicon species aerosols. The steam explosion tool allowed molten aluminum - coolant interactions to be predicted in terms of energetic yield, and steam and hydrogen over-pressures.

The MACCS analyses are conducted in a manner similar to the recent light-water reactor risk study⁴. However, the production reactor assessment is notably different in two key areas: (1) the presence of a large tritium source term component; (2) the requirement to estimate occupational risk to a large nearby workforce. The first difference is included in the MACCS analysis with the addition of a tenth fission product transport group as part of the source term with wet and dry deposition characteristics. The second difference required implementation of an modified MACCS model for modeling evacuation of the onsite worker population. The onsite analysis uses a model limiting evacuees to exit in a few preferential directions from the affected reactor. Thus the SRS PSA uses two MACCS models, one for calculation of consequences to the general public, and another for determination of the onsite worker consequences. Both calculations are based on MACCS 1.5.5-7 Table 1

summarizes the major codes modified to support the integrated, phenomenological, and ex-plant consequence analysis for the SRS PSA.

SUMMARY

Differences between LWR and SRS production reactors demanded modification of methodology required to perform the Level 2/3 PSA at Savannah River. Ultimately, six computational tools were tailored to predict the in-plant response to, and the ex-plant consequences of hypothetical severe accidents. The resulting SRS PSA is based on the results obtained from the code enhancements. SNL supplied four of the methodologies, and was responsible for the model adequacy and functional acceptability review of three of the codes. Although the modified codes undergird the Level 2/3 PSA analysis at Savannah River, applicability throughout the DOE complex is broad.

Table 1.
 Major Accident Analysis Codes Modified
 Savannah River Site Reactor Probabilistic Safety Assessment (1985 - 1992)

<u>Code</u>	<u>Authoring Institution/Assistance</u>	<u>Modification(s)</u>
Integrated Analysis Codes		
CONTEMPT4	Brookhaven National Laboratory SAIC/Marietta	Intercompartment Flow Criteria; Heat Load Model Executed As Auxillary
CONTAIN/SR	Sandia National Laboratories WSRC & SNL	Limited Filter Compartment Model; Fan Model
MELCOR/SR	Sandia National Laboratories SAIC-Albuquerque	Detailed Filter Compartment Model; Fan Model
Phenomenological Analysis Codes		
CORCON	Sandia National Laboratory WSRC & SNL	Al and Si Chemistry Species Added; Decay Power Tables For U/Al Debris
Non-Equilib. Parametric Model	University of Wisconsin	Mixing, Propagation, Expansion Phase
Ex-Plant Consequence Analysis		
MACCS	Sandia National Laboratories	Evacuation Model For DOE Reservation Worker Population

REFERENCES

1. C. C. Lin et al., *CONTEMPT4/MOD4/A Multicompartment Containment System Analysis Program*, NUREG/CR-3716, BNL-NUREG-51754, Brookhaven National Laboratory, (March 1984).
2. K. K. Murata et al., *User's Manual For CONTAIN 1.1: A Computer Code For Severe Nuclear Reactor Accident Containment Analysis*, NUREG/CR-5026, SAND87-12309, Sandia National Laboratories, Albuquerque, NM, (November, 1989).
3. MELCOR/SR.
4. U. S. Nuclear Regulatory Commission, *Severe Accident Risks: An Assessment for Five U. S. Nuclear Power Plants*, NUREG-1150 (December 1990).
5. Chanin, D. I., J. L. Sprung, L. T. Ritchie, and H-N Jow, *MELCOR Accident Consequence Code System (MACCS), User's Guide*, Vol. 1, NUREG/CR-4691, SAND-86-1562, Sandia National Laboratories, Albuquerque, NM, (February, 1990).
6. Jow, H-N, J. L. Sprung, J. A. Rollstin, L. T. Ritchie, and D. I. Chanin, *MELCOR Accident Consequence Code System (MACCS), Model Description*, Vol. 2, NUREG/CR-4691, SAND-86-1562, Sandia National Laboratories, Albuquerque, NM, (February, 1990).
7. Rollstin, J. A., D. I. Chanin, and H-N Jow, *MELCOR Accident Consequence Code System (MACCS), Programmer's Reference Manual*, Vol. 3, NUREG/CR-4691, SAND-86-1562, Sandia National Laboratories, Albuquerque, NM, (February, 1990).

END

DATE
FILMED

12/15/92

