

1 of 5

NEMS Industrial Module Documentation Report

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1. Introduction

Purpose of this Report

This report documents the objectives, analytical approach, and development of the National Energy Modeling System (NEMS) Industrial Demand Model. The report catalogues and describes model assumptions, computational methodology, parameter estimation techniques, and model source code.

This document serves three purposes. First, it is a reference document providing a detailed description of the NEMS Industrial Model for model analysts, users, and the public. Second, this report meets the legal requirement of the Energy Information Administration (EIA) to provide adequate documentation in support of its statistical and forecast reports (*Public Law 93-275, section 57(b)(1)*). Third, it facilitates continuity in model development by providing documentation from which energy analysts can undertake model enhancements, data updates, and parameter refinements as future projects.

Model Summary

The NEMS Industrial Demand Model is a dynamic accounting model, bringing together the disparate industries and uses of energy in those industries, and putting them together in an understandable and cohesive framework. The Industrial Model generates mid-term (up to the year 2010) forecasts of industrial sector energy demand as a component of the NEMS integrated forecasting system. From the NEMS system, the Industrial Model receives fuel prices, employment data, and the value of output of industrial activity. Based on the values of these variables, the Industrial Model passes back to the NEMS system estimates of consumption by fuel types.

The NEMS Industrial Model estimates energy consumption by energy source (fuels and feedstocks) for 26 manufacturing and 6 nonmanufacturing industries. The manufacturing industries are further subdivided into the energy-intensive manufacturing industries and non-energy-intensive manufacturing industries. The energy-intensive industries are modeled through the use of a detailed process flow accounting procedure, whereas the non-energy-intensive, as well as the nonmanufacturing industries, are modeled through econometrically based equations. The industrial model forecasts energy consumption at the nine Census division levels; energy consumption at the Census division level is allocated by using State Energy Data System (SEDS) data and the shares remain constant.

Each industry is modeled as three separate but interrelated components consisting of the process/assembly component (PA), the buildings component (BLD), and the boiler/steam/cogeneration component (BSC). The BSC component satisfies steam demand from the PA and BLD components. In some industries, the PA component produces byproducts that are consumed in the BSC component. For the energy-intensive industries, the PA component is broken down into the major production processes or end uses.

Archival Media

As of this writing, the model has not been officially archived. The model will be archived on IBM 3090 mainframe magnetic tape storage as part of the National Energy Modeling System production runs used to generate the Annual Energy Outlook 1994.

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Organization of this Report

Chapter 2 of this report discusses the purpose of the NEMS Industrial Demand Model, detailing its objectives, input and output quantities, and the relationship of the Industrial Model to the other modules of the NEMS system. Chapter 3 of the report describes the rationale behind the Industrial Model design, providing insights into further assumptions utilized in the model development process to this point. Chapter 3 also reviews alternative industrial sector modeling methodologies drawn from existing literature. Chapter 4 details the model structure. The first section in the chapter provides a flow diagram of the model. The second section provides a description of the principal model subroutines, including the key computations performed and equations solved in each subroutine.

The Appendices to this report provide supporting documentation for the Industrial Model. Appendix A lists and defines the input data used to generate parameter estimates and endogenous forecasts from the Industrial Model, along with the parameter estimates and the outputs of most relevance to the NEMS system and the model evaluation process. A table referencing the equation(s) in which each variable appears is also provided in Appendix A. Appendix B contains a mathematical description of the algorithms used in the Industrial Model, including model equations and variable transformations. Appendix C is a bibliography of reference materials used in the development process. Appendix D consists of a model abstract. Appendix E lists the input data and estimation methods for deriving the input data.

2. Model Purpose

Model Objectives

The NEMS Industrial Demand Model was designed to forecast industrial energy consumption by fuel type and Standard Industrial Classification (SIC). The Industrial Model generates mid-term (up to the year 2010) forecasts of industrial sector energy demand as a component of the NEMS integrated forecasting system. From the NEMS system, the Industrial Model receives fuel prices, employment data, and the value of output for industrial activity. All dollar values are expressed in 1987 dollars. Based on the values of these variables, the Industrial Model passes back to the NEMS system estimates of fuel consumption for seventeen main fuels (including feedstocks and renewables) for each of 32 SIC industry groups. The Industrial Model forecasts energy consumption at the four Census region levels; energy consumption is allocated to the Census division level based on SEDS data, with the shares remaining constant.

The NEMS Industrial Model is an annual energy forecasting model; as such, it does not model seasonal variations in fuel demand or fuel prices, for example. The model was designed primarily for use in applications such as the Annual Energy Outlook and other applications that examine mid-term energy-economy interactions.

The model can also be used to examine various policy, environmental, and regulatory initiatives. For example, energy consumption per dollar of output is, in part, a function of energy prices. Therefore, the effect on industrial energy consumption of policies that change relative fuel prices can be analyzed endogenously in the model. Currently, industrial carbon emissions are explicitly accounted for in the model as a function of fuel consumption.

To a lesser extent, the Industrial Model can endogenously analyze specific technology programs or energy standards regulations. The model distinguishes among the energy-intensive

manufacturing industries, the non-energy-intensive manufacturing industries, and the non-manufacturing industries. The unit energy consumption in the non-energy-intensive industries is modeled econometrically as a function of relative fuel price ratios and an autonomous trend. Consequently, the Industrial Model does not currently have the capability to model detailed technologies or processes for these industries.

A process flow approach, represented by their major production processes or end uses, is used to model the energy-intensive industries. This approach provides considerable detail about how energy is consumed in that particular industry. Even using this approach, however, the process flows are modeled at a high degree of aggregation. Therefore, technologies or processes at the same level of aggregation as the model can be endogenously analyzed by changing the relevant unit energy consumption values for those technologies or processes. For example, the model can analyze changes at the level of a blast furnace or a pulping process. To model technologies or processes at a lower level of aggregation, off-line analysis can be performed, and the results incorporated into the model through the use of engineering judgment.

Relationship between the Industrial Model and Other NEMS Models

Table 1 shows the Industrial Model inputs from and outputs to other NEMS modules. Note that all inter-module interactions must pass through the system module.

Table 1. Interaction With Other NEMS Modules

| INPUTS | From Module |
|--|---------------------------|
| Controlling information (iteration count, present year, number of years to be modeled, convergence switch, etc.) | System |
| Electricity prices | Electricity Market Module |
| Natural gas prices | Natural gas supply |
| Steam coal prices Metallurgical coal prices | Coal supply |
| Distillate oil prices Residual oil prices LPG prices Motor gasoline prices Petrochemical feedstock prices Asphalt and road oil prices Other petroleum prices | Petroleum Market Module |
| Value of output Employment | Macro |

| INPUTS | From Module |
|---|-------------------------|
| Refinery consumption of: Natural gas Steam coal Distillate oil Residual oil LPG Still gas Petroleum coke Other petroleum Refinery consumption of fuels to cogenerate electricity: Natural gas Steam coal Residual oil Biomass Refinery electricity consumption: Purchased electricity Cogenerated electricity Electricity sold to the grid Refinery consumption of renewables | Petroleum Market Module |

Table 1. Interaction with Other NEMS Modules, cont.

| OUTPUTS | To Module |
|--|---------------------------|
| Industrial consumption of: Purchased electricity Natural gas Steam coal Metallurgical coal Net coal coke imports Distillate oil Residual oil LPG Motor gasoline Kerosene Petrochemical feedstocks Still gas Petroleum coke Other petroleum | Supply Modules |
| Consumption of renewables: Biomass Hydropower Solar/wind/geothermal/etc. | System |
| Nonutility generation: Cogeneration of electricity Electricity sales to the grid and own use | Electricity Market Module |
| Carbon emissions | System |

3. Model Rationale

Theoretical Approach

Introduction

The NEMS Industrial Model can best be characterized as a dynamic accounting model, because its architecture attempts to bring together the disparate industries and uses of energy in those industries, and put them together in an understandable and cohesive framework. This explicit understanding of the current uses of energy in the industrial sector is used as the framework from which to base the dynamics of the model.

One of the overriding characteristics in the industrial sector is the extensiveness and the heterogeneity of industries, products, equipment, technologies, processes, and energy uses. Adding to this heterogeneity is that the industrial sector as defined at EIA includes not only manufacturing, but also agriculture, mining, and construction. These disparate industries range widely from highly energy-intensive activities to non-energy-intensive activities. Industries are modeled at a disaggregate level so that changes in composition of the products produced will not significantly offset accounting of energy consumption. Other industrial modeling approaches have either lumped together these very different activities across industries or users, or they have been so disaggregate as to require extensive resources for data development and for running the model.

Modeling Approach

There are a number of considerations that have been taken into account in building the industrial model. These considerations have been identified largely through experience with the current

and previous EIA models and with various EIA analyses, through communication and association with other modelers and analysts, and through literature review. The primary considerations are listed below.

- The industrial model incorporates three major industry categories, consisting of energy-intensive manufacturing industries, non-energy-intensive manufacturing industries, and nonmanufacturing industries. The level and type of modeling and the attention to detail is different for each. Manufacturing disaggregation is at least at the 2-digit SIC level, with some further disaggregation of the more energy-intensive industries.
- Each industry is modeled as three separate but interrelated components, consisting of boilers/steam/cogeneration (BSC), buildings (BLD) and process/assembly (PA) activities.
- The model uses a vintaged capital stock accounting framework that models energy use in new additions to the stock and in the existing stock. The existing stock is retired based on retirement rates for each industry.
- The energy-intensive industries are modeled with a structure that explicitly describes the major process flows or major consuming uses in the industry.
- Technology penetration at the level of major processes in each energy-intensive industry is based upon engineering judgment. A second relationship provides additional energy conservation due to the effect of changes in energy prices.
- The model structure accommodates several industrial sector activities including: fuel switching, cogeneration, renewables consumption, recycling, byproduct

consumption, and carbon emissions. The principal model calculations are performed at the four Census region levels and aggregated to a national total.

- The implementation of the model is being phased, beginning with the basic accounting structure and with relatively simple behavioral relationships. Features and enhancements will be added over time, as needed or appropriate for specific analyses.

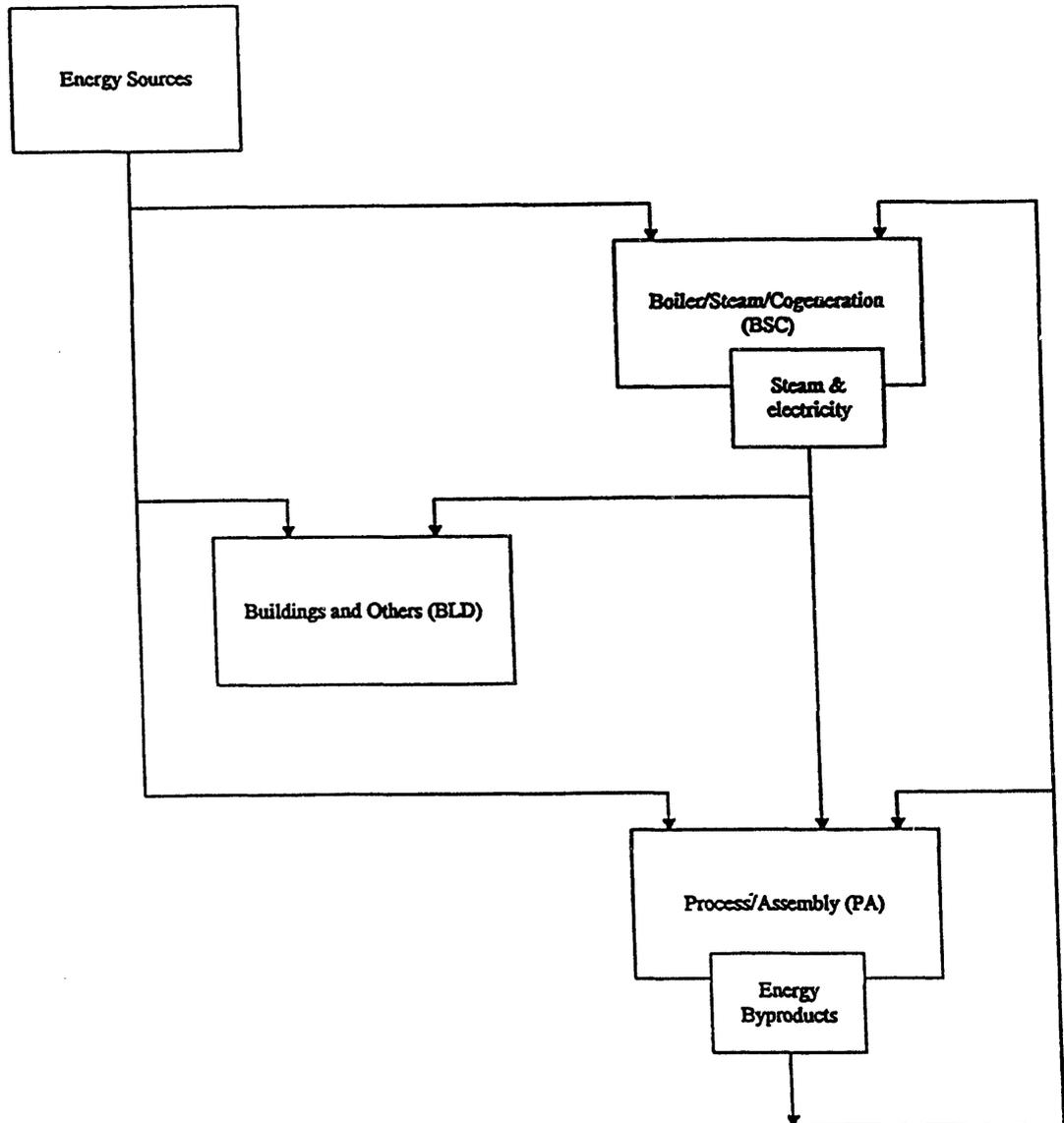
Fundamental Assumptions

The industrial sector consists of a wide variety of heterogeneous industries. The Industrial Model classifies these industries into three groups by Standard Industrial Classification (SIC) - energy-intensive industries, non-energy-intensive industries, and non-manufacturing industries. There are eight energy-intensive manufacturing industries modeled; seven of them are modeled in the industrial model. They are as follows: food and kindred products (SIC 20); paper and allied products (SIC 26); bulk chemicals (SIC's 281, 282, 286, and 287); glass and glass products (SIC's 321, 322, and 323); hydraulic cement (SIC 324); blast furnaces and basic steel products (primarily SIC's 331, 332, etc.); and primary aluminum (primarily SIC's 3334, 3341, 3353, 3354, 3355, etc.). Petroleum refining (SIC 2911) is modeled in detail in a separate module of NEMS, and the projected energy consumption is included in the manufacturing total. The forecast for Oil and Gas (SIC 1311) lease and plant and cogeneration consumption are exogenous to the Industrial model, but endogenous to the NEMS modeling system.

Each industry is modeled as three separate but interrelated components consisting of the process/assembly component (PA), the buildings component (BLD) and the boiler/steam/cogeneration component (BSC). (See Figure 1). The BSC component satisfies the steam demand from the PA and BLD components. For the energy-intensive industries, the PA component is broken down into the major production processes or end uses.

Figure 1. Industrial Model Components

The flow of energy among the three industrial model components follows the arrows.



Energy consumption in the NEMS Industrial Model is primarily a function of the level of industrial economic activity. Industrial economic activity in the NEMS system is measured by the dollar value of output produced by each SIC industry group. The value of output for the Industrial Model by SIC is provided by the NEMS MACRO Module. As the level of industrial economic activity increases, the amount of energy consumed to produce the relevant industrial products typically increases at a slower rate.

The amount of energy consumption reported by the Industrial Model is also a function of vintage of the capital stock that produces the output. It is assumed that new vintage stock will consist of state-of-the-art technologies that are relatively more energy efficient than the average efficiency of the existing capital stock. Consequently, the amount of energy required to produce a unit of output using new capital stock is less than that required by the existing capital stock. The energy intensity of the new capital stock relative to 1990 capital stock is reflected in the parameter of the Technology Possibility Curve estimated for each of the energy-intensive industries. These curves are based on engineering judgment of the likely future path of energy intensity changes.

The energy intensity of the existing capital stock also is assumed to decrease over time, but not as rapidly as new capital stock. The decline is due to retrofitting and replacement of equipment due to normal wear and tear. The net effect is that over time the amount of energy required to produce a unit of output declines. Although total energy consumption in the industrial sector is projected to increase, overall energy intensity is projected to decrease.

Energy consumption in buildings is assumed to grow at the same rate as employment in that industry. Energy consumption in the BSC is assumed to be a function of the steam and electricity requirements of the other two components.

Industry Disaggregation

Table 2 identifies the industry groups to be modeled in the industrial sector along with their Standard Industrial Classification¹ (SIC) code coverage. These industry groups have been chosen for a variety of reasons. The primary consideration is the distinction between energy-intensive industry groups (or large energy consuming industry groups) and non-energy-intensive industry groups. The energy-intensive industries are modeled in more detail, with aggregate process flows. The industry categories are also to be as consistent as possible with the categories which are available from the Manufacturing Energy Consumption Survey (MECS).² Table 2 identifies 6 nonmanufacturing industries and 26 manufacturing industries. Within the manufacturing industries, the seven most energy-intensive industries are modeled in greater detail in the Industrial Demand Model. Refining (SIC 2911), also an energy-intensive industry, is modeled elsewhere in NEMS.

Energy Sources Modeled

The NEMS Industrial Model estimates energy consumption for the 32 SIC industries by energy source (fuels and feedstocks) for 17 energy types. The major energy sources (fuels) modeled in the Industrial Model are:

- Electricity
- Natural Gas

¹The Standard Industrial Classification (SIC) codes have been modified at various points in time, leading to occasional difficulties with tracking specific industries over time. In general this is not a problem, but does lead to some difficulties with matching some databases, including the National Energy Accounts.

²All the two digit industries can be made consistent with the published tables in MECS, but the published MECS tables do not have subcategories (below 2 digit) that add up to their industry total. Moreover, in cases where there are subcategories, MECS uses a fairly specific 4-digit industry which is typically at a lower level of detail than that which is desired for the industrial model. This makes for some difficulty with coordination. There can be coordination at the 2-digit level.

Table 2. Industry Categories for the EIA Industrial Model^a

| | Level of Modeling |
|---|----------------------|
| Nonmanufacturing Industries | |
| Agricultural Production - Crops (SIC 01) | Aggregate |
| Other Agriculture including Livestock (SIC 02, 07, 08, 09) | Aggregate |
| Coal Mining (SIC 11, 12) | Aggregate |
| Oil and Gas Mining (SIC 13) | Part External |
| Metal and Other Non-metallic Mining (SIC 10, 14) | Aggregate |
| Construction (SIC 15, 16, 17) | Aggregate |
| Manufacturing Industries | |
| Food and Kindred Products (SIC 20) | Detailed |
| Tobacco Products (SIC 21) | Aggregate |
| Textile Mill Products (SIC 22) | Aggregate |
| Apparel and Other Textile Products (SIC 23) | Aggregate |
| Lumber and Wood Products (SIC 24) | Aggregate |
| Furniture and Fixtures (SIC 25) | Aggregate |
| Paper and Allied Industries (SIC 26) | Detailed |
| Printing and Publishing (SIC 27) | Aggregate |
| Chemicals and Allied Products (SIC 28) | - |
| Bulk Chemicals (SIC 281, 282, 286, and 287) | Detailed |
| Other Chemicals and Allied Products (SIC 283, 284, 285, 289) | Aggregate |
| Petroleum and Coal Products (SIC 29) | - |
| Petroleum Refining (SIC 2911) | External |
| Asphalt, Coal and Miscellaneous Products (SIC 295, 299) | Aggregate |
| Rubber and Miscellaneous Plastic Products (SIC 30) | Aggregate |
| Leather and Leather Products (SIC 31) | Aggregate |
| Stone, Clay and Glass Products (SIC 32) | - |
| Glass and Glass Products (SIC 321, 322, 323) | Detailed |
| Cement, Hydraulic (SIC 324) | Detailed |
| Other Stone and Clay Products (SIC 325, 326, 327, 328, 329) | Aggregate |
| Primary Metals Industries (SIC 33) | - |
| Blast Furnace & Basic Steel Products (primarily SIC 331, 332, etc.) | Detailed |
| Primary Aluminum (primarily SIC 3334, 3341, 3353, 3354, 3355, etc.) | Detailed |
| Other Primary Metals Products (SIC 333-336, 339, with above exceptions) | Aggregate |
| Fabricated Metal Products (SIC 34) | Aggregate |
| Industrial Machinery and Equipment (SIC 35) | Aggregate |
| Electronic & Other Electric Equipment (SIC 36) | Aggregate |
| Transportation Equipment (SIC 37) | Aggregate |
| Instruments and Related Products (SIC 38) | Aggregate |
| Miscellaneous Manufacturing Industries (SIC 39) | Aggregate |

^aNot all possible SIC numbers are used in the SIC classification scheme. For example, there is no SIC 03, 04, 05 or 06. There are also difficulties with the definition of some of the categories for use in the industrial model. For example, the most difficult category is primary aluminum. It is defined in the SIC classification as a four-digit industry under primary metals, but this represents only part of what is generally understood to be the aluminum industry. This four-digit code does not represent the manufacture of alumina from bauxite which is a significant energy consumer. The alumina activity is in the chemical industry under SIC 2819.

- Steam Coal
- Distillate Oil
- Residual Oil
- LPG for heat and power
- Other Petroleum
- Renewables
- Motor Gasoline

Other energy sources that are used in specific industries are also modeled:

- Natural Gas Feedstock
- Coking Coal (including net imports)
- LPG Feedstock
- Petrochemical Feedstocks
- Asphalt and Road Oil
- Still Gas
- Petroleum Coke
- Other Petroleum Feedstocks

In the model, byproduct fuels are always consumed before purchased fuels.

Key Computations

The key computations of the Industrial Model are the Unit Energy Consumption (UEC) estimates made for each SIC industry group. UEC is defined as the amount of energy required to produce one dollar's worth of output. The overall modeling approach posits a *putty/clay* process of investment to determining UEC's. This means that before a piece of equipment or industrial process is installed, the factor inputs may be freely variable. Thus, the combination of energy

and other factor inputs will be chosen to minimize costs (for a given output level) based on the current price expectations. However, after installation the capital has become clay, and factor proportions cannot be changed without additional investment. This characterization of the industrial expansion process leads to the notion that the existing capital stock has limited variation of input ratios of energy versus other factors, but when new capital is added the input ratios are freely variable. Distinguishing between the characteristics of the process when new capital equipment is put into place and the characteristics of the process with existing capital equipment is done with a vintage-based accounting procedure.

The modeling approach incorporates technical change in the production process to achieve lower energy intensity. Autonomous technical change can be envisioned as a learning-by-doing process for existing technology. As experience is gained with a technology, the costs of production decline. Autonomous technical change is the most important source of technical change in the industrial sector. The reason is that few industrial innovations are adopted solely because of their energy consumption characteristics; industrial innovations are adopted for a combination of factors, many of which are hard to quantify. These factors include process changes to improve product quality, changes made to improve productivity, or changes made in response to the competitive environment. These strategic decisions are not readily amenable to economic or engineering modeling at the level of disaggregation in the Industrial Model (For example, see [67]).

Modeling the changes to UEC is one of the main features of the Industrial Model. The methodology for performing the estimation differs, however, both among the components of the model and between the energy-intensive and non-energy-intensive industries. The following sections describe the methodology for each of the components in more detail.

Buildings Component UEC

Buildings are estimated to account for 3 percent of energy consumption in manufacturing industries [30]. (In non-manufacturing industries, building energy consumption is assumed to be negligible.) This estimate is based on a combination of an ISTUM model run and a study on industrial building energy use prepared by Hagler-Bailly [49]. In reality, however, there is very little actual data on which to base accurate estimates. Consequently, the modeling approach is a parsimonious one. Energy consumption in industrial buildings is assumed to grow at the same rate as employment in that industry. This assumption appears to be reasonable since lighting and HVAC are used primarily for the convenience of humans rather than machines.

Estimates of 1990 manufacturing sector (SIC 20-39) building UEC's are presented in Table E-1 in Appendix E. The subroutines and equations used to forecast industrial buildings energy consumption are shown on page B-4 in Appendix B.

Process and Assembly Component UEC

The process and assembly component accounted for the largest share of direct energy consumption for heat and power in 1990 - 54 percent. Of the total, natural gas accounts for 33 percent, electricity for 29 percent, and byproducts 20 percent of the total [30].

Estimation of the PA component UEC's differs according to whether the industry is an energy-intensive industry or a non-energy-intensive industry. UEC's for the non-energy-intensive industries are estimated using econometric techniques. For the energy-intensive industries, the econometric estimates are replaced by engineering data relating energy consumption to the product flow through the process steps in each industry. In addition, engineering judgment is also used to characterize autonomous change in the energy-intensive industries through the use

of Technology Possibility Curves. Each of these methods is discussed in the following sections. The subroutines and equations for the PA component begin on page B-5 in Appendix B.

Non-Energy-Intensive Industry UEC Estimation

The formulation to estimate UEC's for the non-energy-intensive industries incorporates price-induced energy intensity changes and autonomous efficiency trends in a single economically motivated equation. The resulting equation shows that the change in UEC results from a combination of autonomous and price-induced technical change. One process operates on the existing stock (or technology). It is expected that small but measurable efficiency gains can be obtained even with the existing technology. The other process operates through the incorporation of new technology and current price expectations in the production process.

The price-induced technical change can be represented as a function of price changes.³ The autonomous change is somewhat more problematical. However, one may argue that as equipment using the current technology undergoes maintenance and refurbishing that the tendency is to incorporate the latest version of the equipment being replaced. Usually, the latest versions consume energy somewhat differently. The autonomous trend can be represented as a function of cumulative output from existing technology. The resulting equation takes the following form:

$$\frac{UEC_{f,t}}{UEC_{f,1958}} = \alpha \left(\frac{P_{f,t}}{P_{f,1958}} \right)^{\beta_f} * \left(\frac{\sum_{i=1958}^{t-1} Q_i}{Q_{1958}} \right)^{\beta_2} \quad (1)$$

³A similar formulation is found in [87].

where:

| | | |
|----------------|---|--|
| $UEC_{f,t}$ | = | Unit energy consumption for fuel f in year t , |
| $UEC_{f,1958}$ | = | Unit energy consumption for fuel f in year 1958, |
| $P_{f,t}$ | = | Price of fuel f in year t , in 1987 dollars, |
| $P_{f,1958}$ | = | Price of fuel f in year 1958, in 1987 dollars, |
| Q_{1958} | = | Output in year 1958, in 1987 dollars, |
| Q_i | = | Output in year i . |

The α parameter captures the effects of influences on the UEC that are not specified in the model.

In double log form, this formulation leads to estimated elasticities as follows:

$$LN\left(\frac{UEC_{f,t}}{UEC_{f,1958}}\right) = LN \alpha + \beta_f LN\left(\frac{P_{f,t}}{P_{f,1958}}\right) + \beta_2 LN\left(\frac{\sum_{i=1958}^{t-1} Q_i}{Q_{1958}}\right) + \epsilon \quad (2)$$

The estimated β_f and β_2 would then represent the UEC elasticity for price-induced and autonomous change, respectively. The β_f are expected to be less than zero, but β_2 may be positive or negative. Similar UEC elasticities are estimated for natural gas, petroleum products, and coal. The baseline (1988) PA component UEC values for the non-manufacturing and the non-energy-intensive manufacturing industries are given in Appendix E Table E-2.A. and Table E-2.B., respectively. The regression parameter estimates (β_f and β_2) that are used in the model to modify the baseline UEC values and the statistical properties of these estimators are given in Table E-15 in Appendix E. In Table E-15, β_2 is identified by RCUMOUT. Obviously, not all

variables appear in each equation. The consumption, output, and price input data for the regressions can be found in Appendix E Tables E-22A through E-22D.

Energy-Intensive Industry UEC Estimation

For the seven most energy-intensive industries, energy consumption for the PA component is modeled according to the process flows in that industry. The industries are food and kindred products, paper and allied products, blast furnaces and basic steel products, primary aluminum, bulk chemicals, hydraulic cement, and glass and glass products industries. (Petroleum refining is also a major energy consuming industry but it is being modeled elsewhere in NEMS.)

To derive energy use estimates for the process steps, the production process for each industry was first decomposed into its major steps, and then the engineering and product flow relationships among the steps were specified. The process steps for the seven industries were analyzed according to one of the following methodologies:

Methodology 1. Developing a process flowsheet and estimates of energy use by process step. This was applicable to a number of industries where the process flows could be fairly well defined for a single broad product line by unit process step (blast furnace and basic steel products, primary aluminum, hydraulic cement, glass and glass products, and paper and allied products).

Methodology 2. Developing end use estimates by generic process units as a percent of total use in the PA component. This was especially applicable where the diversity of end products and unit process is extremely large (food and kindred products, and bulk chemicals).

In both methodologies, major components of end use are identified by process for various energy sources:

- Fuels;
- Electricity (valued at 3412.0 Btu/Kwh);
- Steam; and
- Non-fuel energy sources.

The following sections present a more detailed discussion of the process steps and unit energy consumption estimates for each of the energy-intensive industries. The data tables showing the estimates are presented in Appendix E, and are referenced in the text as appropriate. The process steps are model inputs with the variable name *INDSTEPNAME*, and are also listed on page A-59 of this report.

Food and Kindred Products (SIC 20)

The food and kindred products industry is the largest (with the exception of transportation, SIC 37) of the twenty manufacturing industry sectors with regard to the value of annual shipments. The energy use profile has been divided into the nine sectors according to the food industry's 3-digit SICs: SIC 201, Meat Products; SIC 202, Dairy Products; SIC 203, Preserved Fruits and Vegetables; SIC 204, Grain Mill Products; SIC 205, Bakery Products; SIC 206, Sugar and Confectionery Products; SIC 207, Fats and Oils; SIC 208, Beverages; and SIC 209, Miscellaneous Foods and Kindred Products.

The 1992 Arthur D. Little supplement to "Energy Use for Industry" served as a basis for the 1988 values. Since the ADL supplement was based on 1985 data, the values were estimated for 1988 by multiplying by a ratio of 1988 MECS data to 1985 MECS data. The portion of "other electricity" reported in the ADL supplement (January 1992) which can be attributed to the BLD component was subtracted using proportions from EIA 1988 data. The UEC for the PA component of the food and kindred products industry is expressed in terms of trillion Btu per billion dollars of output.

The food and kindred products industry consumed approximately 996 trillion Btus of energy in 1988 [43]. Energy use in the food and kindred products industry for the PA Component was estimated on the basis of end-use in four major categories:

- Steam or hot water;
- Direct fuel used in a process such as in grain drying or directly fired ovens;
- Electrical energy used in refrigeration; and
- Other electric energy.

Figure 2 portrays the PA component's end-use energy flow for the food and kindred products industry. The UEC's estimated for this industry are provided in Table E-3, Appendix E. Note that the steam/hot water use shown in the table represents the energy content of steam that is used in the industry sub-sector (i.e., boiler losses and efficiencies are not included in these tables). The dominant end-use was steam (and hot water), which accounted for 57 percent of the total energy consumption. Direct fuel use made up about 21 percent. Electric energy was primarily used for motors, pumps and drives, contributing 18 percent of the energy consumption and refrigeration accounting for about 4 percent.

Paper and Allied Products (SIC 26)

The paper and allied products industry's principal processes involve the conversion of domestic wood fiber to pulp, and then paper and board to consumer products that are generally targeted at the domestic marketplace. Aside from dried market pulp, which is sold as a commodity product to both domestic and international paper and board manufacturers, the industry produces a full line of paper and board products. Figure 3 illustrates the major process steps for all pulp and paper manufacturing. The wood is prepared by removing the bark and chipping the whole tree into small pieces. Pulping is the process in which the fibrous cellulose in the wood is

Figure 2. Food and Kindred Products Industry End-Use Flow

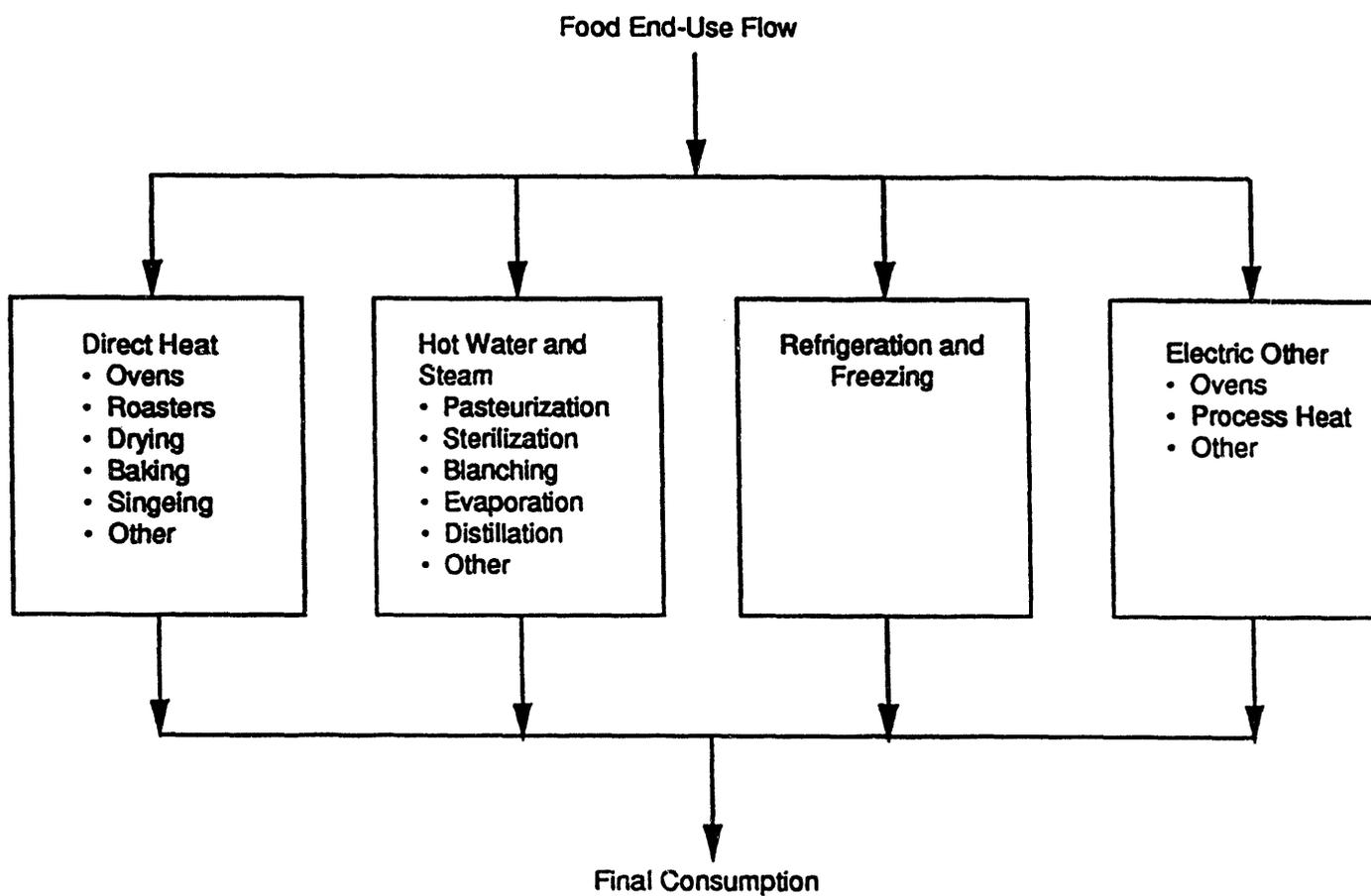
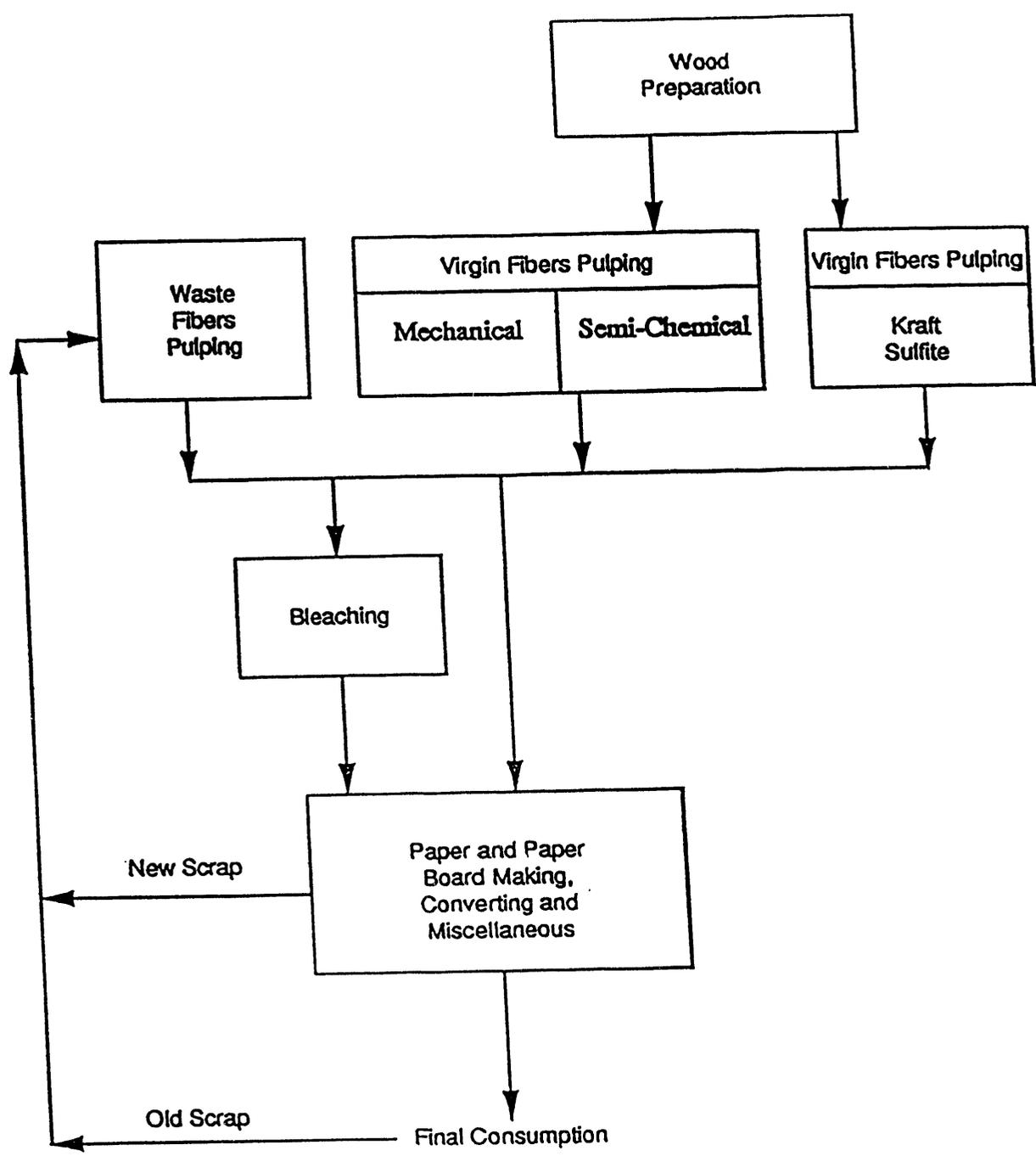


Figure 3. Paper and Allied Products Industry Process Flow



removed from the surrounding lignin. Pulping can be conducted with a chemical process (e.g., Kraft, sulfite) or a mechanical process. (In addition, a semi-chemical process is also available.) The pulping step also includes processes such as drying, liquor evaporation, effluent treatment and miscellaneous auxiliaries. Bleaching is required to produce white paper stock.

Paper and paperboard making takes the pulp from the above processes and makes the final paper and paper board products. The manufacturing operations after pulp production are similar for each of the paper end-products even though they have different desired characteristics imparted by the feedstocks (fibers furnished) and specific processes used, i.e. texture, strength, whiteness. The processes in the paper-making step include papermaking, converting/packaging, coating/redrying, effluent treatment and other miscellaneous processes.

In 1988, a total of 76 million tons of paper and paperboard products were produced. The major paper products include woodfree printing paper, groundwood printing paper, newsprint paper, tissue paper and packaging paper. The major paper board products include kraft paperboard, corrugating medium and recycled paperboard. Of the total 76 million tons of product, 62 percent were produced from kraft chemical process, 5 percent from semi-chemical, 25 percent from waste fibers and 8 percent from mechanical (groundwood). The average unit energy consumption estimated for this industry is slightly over 28 million Btu/ton of final product. The unit energy use estimates for this industry are provided in Table E-4, Appendix E. The largest component of this energy use is in the paper and paper board making process step and kraft pulping step, accounting for 40 percent each. The three types of kraft pulp (bleached, unbleached and market) were combined and presented as a weighted average. Use of recycled paper as the feedstock for the waste fiber pulping step was also taken into account.

Of the four pulping processes, it was assumed in the model that capacity additions would be in the following proportions: kraft pulping - 58.6 percent waste fiber pulping - 36.8 percent; semi-chemical pulping - 2.8 percent; and mechanical pulping - 1.7 percent [31]. The regional distribution for each technology is shown in Table E-17 in Appendix E.

Bulk Chemical Industry (SIC 281, 282, 286, and 287)

The bulk chemical sector is very complex. Industrial inorganics and industrial organics are the basic chemicals, while plastics, agricultural chemicals, and other chemicals are either intermediates or final products. The chemical industry is estimated to consume 21 percent (4.4 quadrillion Btu) of the total energy consumed in the manufacturing sector. This industry also is a major energy feedstock user and a major cogenerator of electricity.

The complexity of the bulk chemical industry, with its wide variety of products and use of energy as both a fuel and feedstock, has led to an end-use modeling approach. The unit energy consumption in the PA component for the bulk chemical industry is shown in Table E-5 in Appendix E. The end-use flow for the industry is shown in Figure 4. From an energy use viewpoint, four 3-digit SIC sectors dominate the bulk chemical industry:

SIC 281, Industrial Inorganic Chemicals;

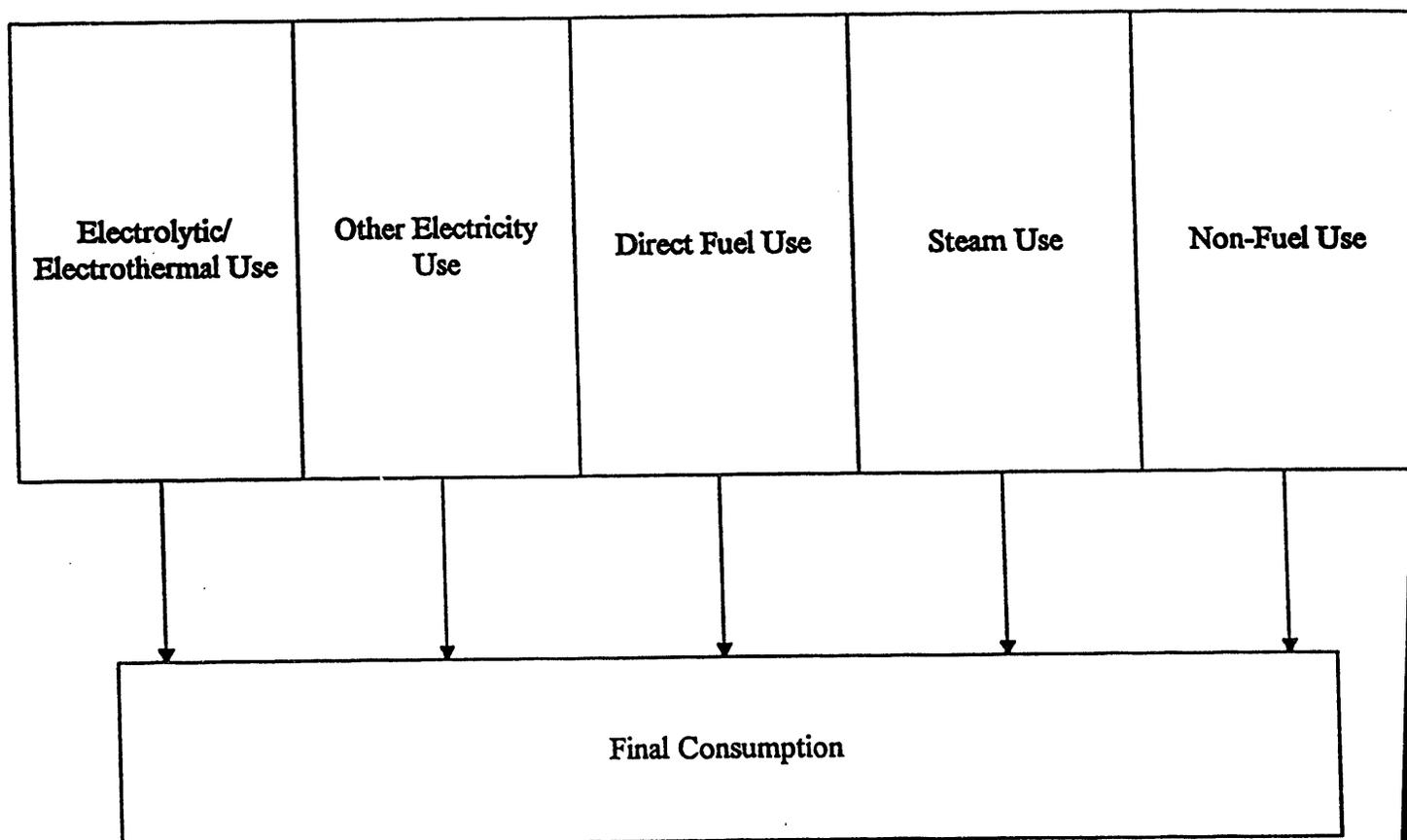
SIC 282, Plastic Materials and Resins;

SIC 286, Industrial Organic Chemicals, which can be produced from a variety of feedstocks; and

SIC 287, Agricultural Chemicals.

Of the 25 top energy consuming chemicals, five were inorganic chemicals. *Chemical and Engineering News* (4/90) listed four of these five substances among the top 50 for production in 1988. One hundred billion pounds of chlorine, sodium hydroxide, sodium carbonate (Trona,) and oxygen were produced in 1988 alone. Sulfuric acid and calcined gypsum were also produced in significant quantities (84.28 and 34.55 billion lbs, respectively) in 1988.

Figure 4. Bulk Chemical Industry End-Use Flow



These five chemicals alone accounted for the use of 507 trillion Btu in 1988, representing 32 percent of the chemical industry being studied. The energy consumption in the bulk chemicals industry was fairly evenly divided between the four major end uses. Steam made up 34 percent, electricity made up 24 percent and electrolytic and direct fuels each contributed 21 percent [31].

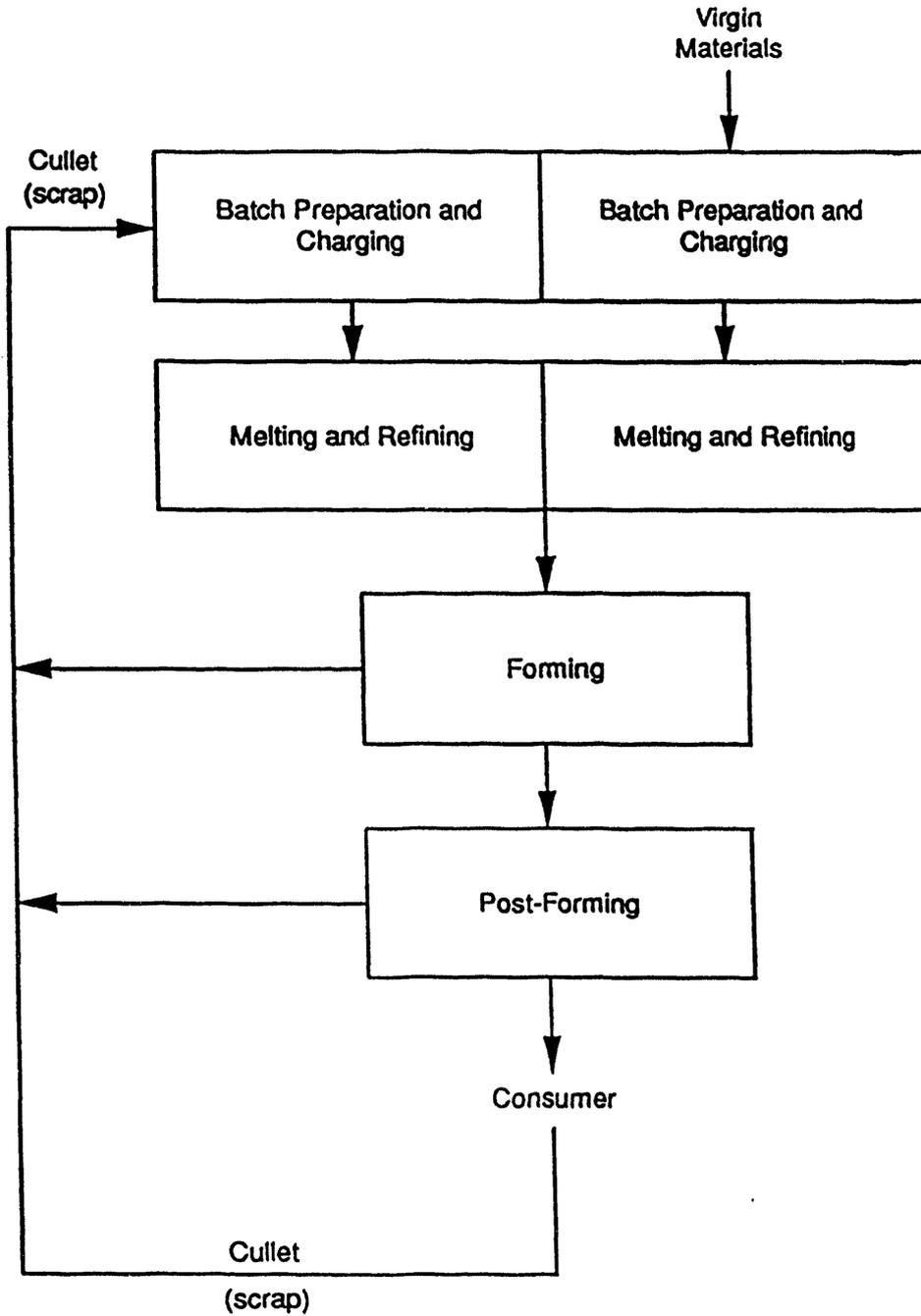
Glass and Glass Products Industry (SIC 321, 322, 323)

The energy use profile has been developed for the total glass and glass products industry, SIC 321, 322, and 323. The glassmaking process contains four process steps: batch preparation, melting/refining, forming and post-forming. Figure 5 provides an overview of the process steps involved in the glass and glass products industry. While scrap (cullet) and virgin materials are shown separately, this is done to separate energy requirements for scrap versus virgin material melting. In reality, glassmakers generally mix cullet with the virgin material.

In 1988, the glass and glass product industry produced approximately 19 million tons of glass products. As noted by the Department of Commerce, this 19 million tons consists of 4.3 million tons of flat glass, 10.8 million tons of container glass, 1.8 million tons of pressed and blown glass, and 2.4 million tons of fiberglass.

The glass and glass product industry consumed approximately 270 trillion Btus of energy in 1988 as identified in the *1988 Manufacturing Consumption Survey*. This accounts for 28 percent of the total energy consumed in the stone, clay and glass industry. The fuel consumed is predominantly for direct fuel use; there is very little steam raising. This direct fuel is used mainly in furnaces for melting. Table E-6 in Appendix E shows the unit energy consumption values for each process step. The unit consumption energy values are presented in MMBtu per ton of process step product.

Figure 5. Glass and Glass Products Industry Process Flow



Hydraulic Cement Industry (SIC 324)

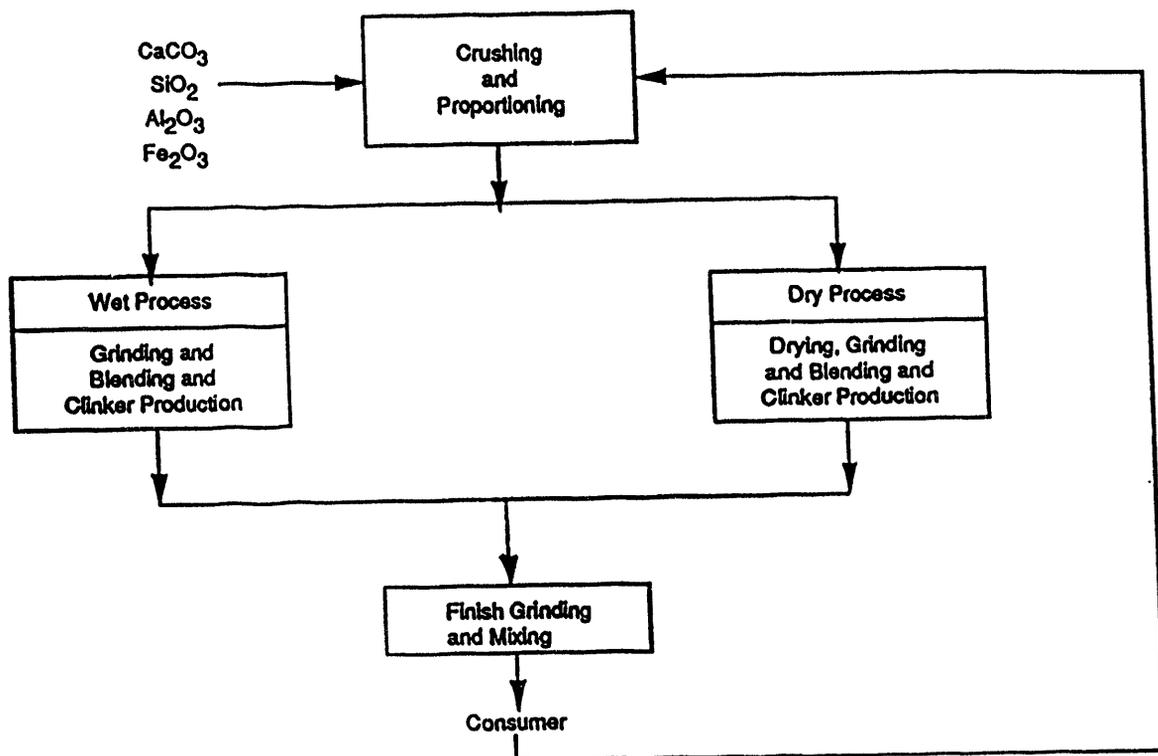
The hydraulic cement industry uses raw materials from quarrying and mining operations which are sent through crushing and grinding mills and then converted to clinker in the clinker producing step. This clinker is then ground to produce cement. The industry produces cement by two major processes: the long-wet process and the dry process. The dry process is less energy-intensive than the wet process. As a result, the long-wet process is obsolescent, and it is projected in the model that all new plants will be based on the dry process. Figure 6 provides an overview of the process steps involved in the hydraulic cement industry.

The Portland Cement Association noted that in 1988 the hydraulic cement industry produced 76.9 million tons of cement, of which 73.3 million or 95 percent was Portland cement with the remaining 3.6 million tons being masonry cement. Since cement is the primary binding ingredient in concrete mixtures, it is used in virtually all types of construction. As a result, the U.S. demand for cement is highly sensitive to the levels of construction activity. The wet process accounted for 34 percent of production, while the dry process accounted for about 60 percent, with the difference being accounted for by imported clinker (6 percent).

The hydraulic cement industry exhibits one of the highest unit energy consumption values (MMBtu/dollar value of output) in the U.S. industrial sector. The industry consumed approximately 454 trillion Btus of energy in 1988 as identified in the *1988 Manufacturing Consumption Survey*. This accounts for 47 percent of the energy consumed in the stone, clay and glass industry. Direct fuel, used in clinker-producing kilns, accounted for 89 percent of the total energy consumption, with the remaining 11 percent attributed to electricity. The electricity consumed is used to operate crushing and grinding equipment, materials handling equipment, machine drives and pumps and fans.

The wet process requires significantly larger amounts of energy which can be largely attributed to fuels used to dry the feed. While wet grinding is known to require less energy than dry

Figure 6. Hydraulic Cement Industry Process Flow



grinding, the entire wet process has longer kilns, requiring greater energy use than the dry process to drive them. Higher air flows, larger pollution control devices, and generally older facilities lead to slightly larger estimated electric energy use for the wet process.

The UEC values for each process in the hydraulic cement industry are shown in Table E-6, Appendix E. As noted previously, it is assumed that all new hydraulic cement capacity will be based on the dry process. The regional distribution of hydraulic cement production processes is presented in Table E-17 in Appendix E.

Blast Furnace and Basic Steel Products Industry (SIC 331, 332, etc.)

The blast furnace and basic steel products industry includes the following six major process steps:

- Agglomeration;
- Cokemaking;
- Iron Making;
- Steel Making;
- Steelcasting; and
- Steelforming.

Steel manufacturing plants can be divided into two major classifications: integrated and non-integrated. The classification is dependent upon the number of the above process steps that are performed in the facility. Integrated plants perform all the process steps, whereas non-integrated plants, in general, perform only the last three steps.

For the Industrial Demand Model, a process flow was developed to classify the above six process steps into the five process steps around which unit energy consumption values were

estimated. Figure 7 shows the process flow diagram used for the analysis. The agglomeration step was not considered because it is not part of the SIC 33 (it is part of mining). Iron ore and coal are the basic raw materials which are used to produce iron. A simplified description of a very complex industry is provided below.

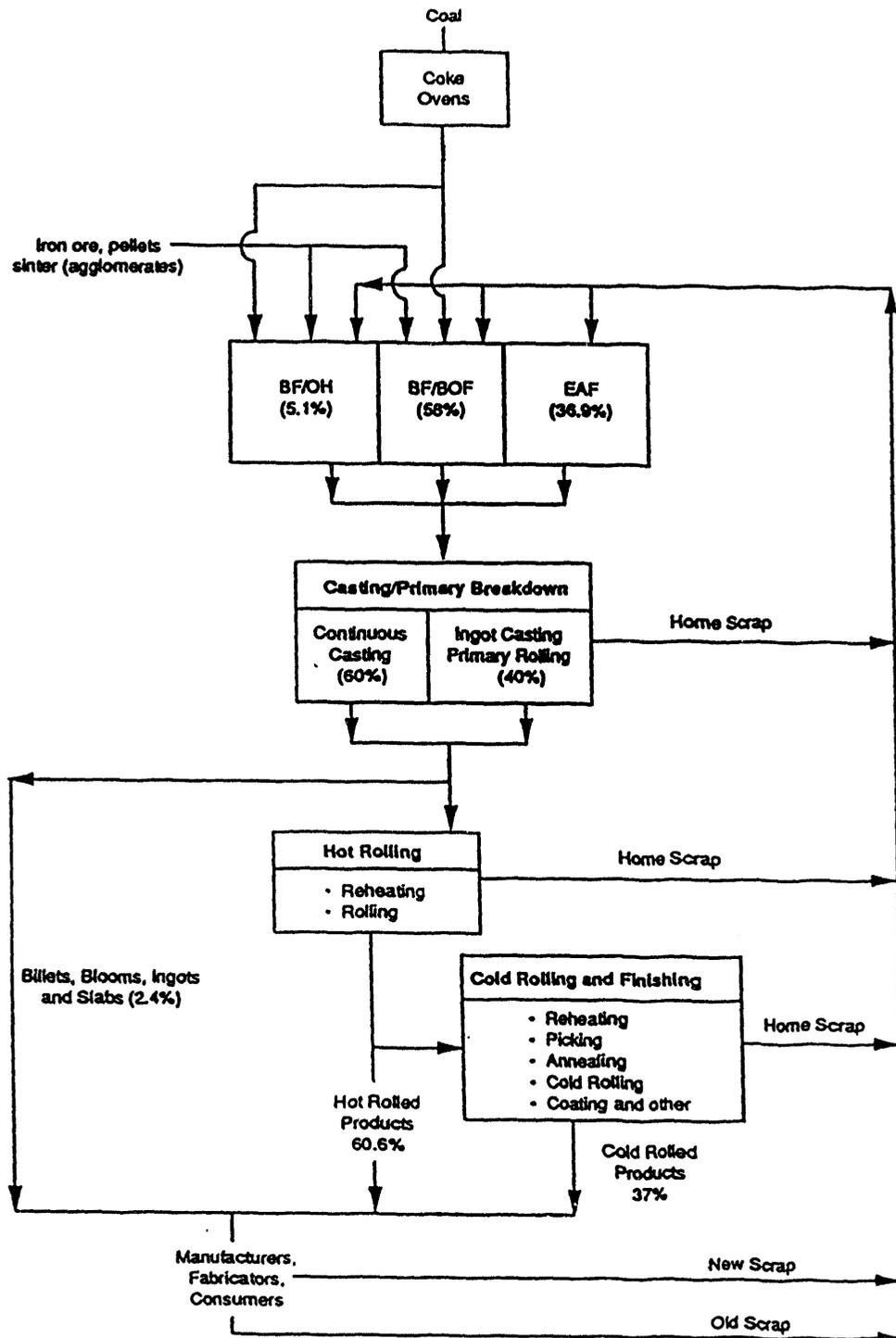
Iron is produced in the Blast Furnace (BF), which is then charged into a Basic Oxygen Furnace (BOF) or Open Hearth (OH) to produce raw steel. The OH now is becoming obsolete; however, it was used to some extent in 1988. The Electric Arc Furnace (EAF) is utilized to produce raw steel from an all steel scrap charge.

The raw steel is cast into ingots, blooms, billets or slabs, some of which are marketed directly (e.g., forging grade billets). The majority is further processed ("hot rolled") into various mill products. Some of these are sold as hot rolled mill products, while some are further cold rolled to impart surface finish or other desirable properties.

In 1988, the U.S. steel industry produced nearly 100 million tons of raw steel utilizing the BF/OH, BF/BOF and the EAF. Taking process yields into account, the total amount of product shipments was approximately 85 million tons. The EAF accounted for 37 percent of the raw steel production, whereas the BF/BOF accounted for 58 percent and the BF/OH for 5 percent. Continuous casting was utilized for 60 percent of the products, and ingot casting for 40 percent. Final consumption was made up of about 2.4 percent ingot, billets, blooms, and slabs, 37 percent cold rolled products, and 60.6 percent hot rolled products.

Table E-8 in Appendix E summarizes UEC estimates by process step and energy type for the blast furnace and basic steel products industry. The largest category for energy use is coal, followed by liquid and gas fuels. Coke ovens and blast furnace also generate a significant amount of byproduct fuels (denoted by a negative number in Table E-8) which are used throughout the steel plant. For the integrated producers, it is assumed in the model that all new

Figure 7. Blast Furnace and Basic Steel Products Industry Process Flow



NOTE: Percentages in boxes indicate market usage of process by estimated tonnage throughputs.

capacity additions will be the blast furnace/basic oxygen furnace technology; open hearth furnaces are obsolete and no new open hearths will be built. The regional distribution of steel-making technologies is presented in Table E-17, Appendix E.

Primary Aluminum Industry (SIC 3334)

The U.S. primary aluminum industry consist of two majors sectors: the primary aluminum sector, which is largely dependent on imported bauxite and alumina as raw materials; and the secondary sector, which is largely dependent on the collection and processing of aluminum scrap. The primary and secondary aluminum industries generally cater to different markets. Traditionally, the primary industry bought little scrap and supplied wrought products, including sheet, plate and foil. The secondary industry is scrap-based and supplies foundries that produce die, permanent mold, and sand castings. In the past decade, the primary producers have been moving aggressively into recycling aluminum, especially used beverage cans, into wrought products. Figure 8 provides an overview of the process steps involved in the aluminum industry.

The primary aluminum industry modeled in the Industrial Model generally accounts for the energy used in SIC 3334, alumina refineries and primary aluminum smelters. In the future, the following SIC's will also be explicitly accounted for:

- SIC 3353: Aluminum sheet, plate, and foil;
- SIC 3354: Aluminum extruded products;
- SIC 3355: Aluminum rolling and drawing, n.e.c.; and
- SIC 3341: Secondary Aluminum.

Domestic aluminum production plus aluminum ingot imports resulted in about 6.6 million tons of semi-fabricated product shipments from U.S. plants. Secondary (scrap-based)

operations added another 1.05 million tons. Total shipments were about 7.6 million tons. The primary industry produced approximately 4.3 million tons of aluminum products in 1988.

The UEC estimates developed around the process steps shown in the process flow diagram are presented in Table E-10 in Appendix E. As shown in the table, the alumina smelting process is the most energy-intensive of the four process steps. The primary form of energy used is electricity, which accounts for 58 percent of the total, with fuel accounting for 35 percent and steam accounting for 7 percent. The majority of the fuel for processing alumina and aluminum is used in kilns, furnaces and ovens. The regional distribution of smelters in the primary aluminum Industry is presented in Table E-17 in Appendix E.

Boiler, Steam, Cogeneration Component Share

The boiler, steam, cogeneration (BSC) component consumes energy to meet the steam demands from the other two components and to provide internally generated electricity to the buildings and process and assembly components. The boiler component consumes fuels and renewable energy to produce the steam and, in appropriate situations, cogenerate electricity. The subroutines and equations for the BSC component begin on page B-32 in Appendix B.

The boiler component is estimated to consume 44 percent of total industrial energy consumption. Within the BSC component, natural gas accounts for 35 percent, coal 14 percent, and petroleum products 8 percent. Most of the remainder (38 percent) is accounted for by waste or byproduct consumption. The basis of these estimates is Dun & Bradstreet's Major Industrial Plant Database (MIPD) for 1989. No other data from which to derive estimates exist for the BSC component. Estimates of 1990 BSC component shares are presented in Table E-10 in Appendix E.

The steam demand from the PA and BLD components is passed to the BSC component, which then applies a heat rate and fuel share elasticities to compute the required energy consumption. The heat rate is estimated from MECS and the MIPD. The fuel share elasticities for the BSC component are from [25], and are presented in Table E-11 in Appendix E. The estimates were used for both the energy-intensive and non-energy-intensive industries.

Cogeneration (the generation of electricity and steam) has been a standard practice in the industrial sector for many years. The cogeneration model within the Industrial Model is an econometrically estimated set of recursive equations in log-log form. The first equation relates on-site electricity generation to industrial steam demand. The second equation then relates industrial electricity generation for own use to total electricity generated.

Parameter estimates for the cogeneration model are based on regressions from a panel of pooled time series and cross sectional data. The data source is EIA Form EI-867, consisting of data from approximately 400 cogenerators over the years 1989 to 1991. The regression results are presented in Table E-16, Appendix E.

Technology Possibility Curves and Relative Energy Intensities

Future energy improvements were estimated for old (retrofit) and new processes/plants. The data used to determine the energy savings was obtained from:

DOE reports;

DOE memorandum - "Review of Industrial Technologies";

Selected industry contacts;

Arthur D. Little, Inc. in-house sources; and

Other readily available data sources (included in the bibliography).

The energy improvements for old plants as a group consist of gradual improvements due to housekeeping/energy conservation measures, retrofit of selected technologies, and the closure of older facilities leaving the more efficient plants in the "operating pool". The energy savings for old processes/plants were estimated using data available in the above sources and engineering judgment on how much energy conservation savings were reasonably achievable in each industry. The estimated annual energy savings values for energy conservation measures are modest (up to 0.5 percent per year).

The above data sources also were used to estimate the unit energy consumption values for the state-of-the-art (SOA) and advanced technologies. SOA technologies are the latest proven technologies that are available at the time there is a commitment made to build a new plant. These values were then compared to the unit energy consumption values for 1988 to develop a relative energy intensity (REI). Relative energy intensity is defined as ratio of energy use in a new or advanced process compared to 1988 average energy use. Time frame estimates are also provided for when these improvements will take place (see Table E-12, Appendix E).

The savings shown in the appendix for the listed technologies represent savings over "average" 1988 energy use and SOA energy use. The latter increases are due to the gradual commercialization of advanced technologies. Advanced technologies are ones which are still under development and will be available at some time in the future. Where a range is shown for the savings, it was assumed that the lower end of the savings range would start to be realized in the beginning of the time frame, the midpoint of the savings would be realized at the end of the time frame, and the upper end of the savings range would not be realized until 10 or more years after the time frame shown. An energy savings range is most often given when multiple technologies will be becoming available in the future for the same process step or product line. The savings range represents engineering judgment of the most likely achievable savings. In these instances, it is uncertain which specific technologies will be implemented, but it is reasonably certain that at least one of these technologies or a similar technology is likely to be

successful. It is also recognized that in some instances thermodynamic limits are being approached which will prevent further significant improvements in energy savings.

The improvements for new plants assumes the plant has been built with the SOA technologies available for that process. SOA technologies are the latest proven technologies that are available at the time there is a commitment made to build the plant. A second and often more important set of substantial improvements are often realized when advanced technologies become available for a certain process. Often one sees a number of technologies being developed and it is difficult to ascertain which specific technologies will be successful. Some judgment is necessary as to the potential for energy savings and the likelihood for such savings to be achieved. All the energy improvement values are based on 1988 energy usage.

Additionally, even SOA technologies and advanced technologies can at times be expected to show improvements once developed as the process is debottlenecked, optimal residence times and temperatures are found, and better energy recovery techniques are installed. Depending on the process, these are factored into the projections as slow improvements ranging from zero to about 0.5 percent/year. However, once a process is installed in a new plant, it is assumed that its energy use per unit of output remains constant. Old plants, however, are assumed to be able to economically justify some retrofits and for other reasons listed above, to show slow improvements over time in their unit energy use. Based on engineering judgment, it is assumed that by 2015, old processes (1988 stock) still operating can achieve up to 50 percent of the energy savings of SOA technology [31]. Thus, if SOA technology has an REI of 0.80, old processes in the year 2015 will have an REI of 0.90.

With a few exceptions (noted as appropriate in Appendix E), it was assumed that the REI for all energy sources decrease in proportion to the total. Thus, if the total REI for a new technology is 0.90, it was assumed that the relative energy intensity for natural gas, oil, coal, or electricity are all 0.9. When the new technology uses a very different energy mix than the existing technology, it is so noted.

The methodology described above was applied by Arthur D. Little , Inc. The initial results for a process step in an industry consist of a scatter of points where the Y-axis is the REI and the X-axis is time from 1990 to 2015. Thus, the scatter might indicate that the REI is 0.9 in 1997, 0.8 in 1999, and 0.5 in 2007. As a convenience for modeling purposes, a least squares line was fitted through these points (using natural logarithms) so that the resulting slope coefficient (i.e., the TPC) could be used rather than a step function. (The TPCs are given in Appendix E. However, since there is no particular meaning to measures of fit for this exercise, they are not given in Appendix E.)

Table E-13 in Appendix E lists the REI's for old and new plants, by process step, for the seven energy-intensive industries. The REI is defined as the ratio of energy use in a new or advanced process compared to the 1988 old plant average energy use which has been normalized to a value of 1.0. The list of SOA and advanced technologies considered in the analysis is presented in Table E-12, Appendix E.

Where the relative amounts of different energy sources changes with time, a separate equation was estimated for each energy source. The procedure for calculating UEC's over time includes establishing the energy sources used as a fraction of the total for each process step, as shown in Table E-14 in Appendix E.

Assumptions

Capital Stock and Vintaging

Industrial energy consumption is affected by increased energy efficiency in new and old plants, the growth rate of the industry, and the retirement rate for old plants. The efficiency changes are captured in the β_i estimated in equation 2, and the rate of growth is given by the

Macroeconomic module. (Retirement rates from the Census Bureau and vintaging information are very sketchy.) At present, the capital stock is grouped into three vintages: old, middle, and new. The old vintage consists of capital in production prior to 1991 and is assumed to retire at a fixed rate each year. Middle vintage capital is that which is added from 1991 through the lag of the forecast year. New production is added in the forecast years when existing production is less than the output forecasted by the NEMS Regional Macroeconomic Model. Capital additions during the forecast horizon are retired in subsequent years at the same rate as the pre-1991 capital stock. The retirement rates used in the Industrial Model for the various industries are listed in Table E-18 in Appendix E.

Renewable Fuels

Renewable fuels are modeled in the same manner as all other fuels in the industrial model. Renewable fuels are modeled both in the PA component and the BSC component. The primary renewable fuels consumed in the industrial sector are pulping liquor, a byproduct of the chemical pulp process in the paper industry, and wood. Hydropower is also modeled in the industrial model, while geothermal, solar thermal, photovoltaic, wind and municipal solid waste are estimated in the NEMS Renewable Energy Module.

Recycling

With projected higher landfill costs, regulatory emphasis on recycling, and potential cost savings, recycling of post-consumer scrap is likely to grow. Projecting such growth, however, is highly dependent on assessing how regulations will be developed, the growth of the economy, and quality related issues dealing with recycled materials. To assess the potential for recycling in the industrial sector, industry experts were canvassed to obtain the best judgment on the future of recycling for the Paper and Allied Products and Blast Furnace and Basic Steel Products

industries. The estimates obtained for these industries are shown in Table E-19 in Appendix E.

Legislative Implications

The Energy Policy Act of 1992 (EPACT) and the Clean Air Act Amendments of 1990 (CAA) contain several implications for the industrial model. These implications fall into three categories: coke oven standards, efficiency standards for boilers, furnaces and electric motors, and industrial process technologies. The industrial model assumes the leakage standards for coke oven doors do not reduce the efficiency of producing coke, or increase unit energy consumption. The industrial model uses heat rates of 1.25 (80 percent efficiency) and 1.22 (82 percent efficiency) for gas and oil burners respectively [32]. These efficiencies meet the EPACT standards. The standards for electric motors call for an increase of 10 percent efficiency. The industrial model incorporates a 10 percent savings for SOA motors increasing to 20 percent savings in 2015. Given the time lag in the legislation and the expected lifetime of electric motors, no further adjustments are necessary to meet the EPACT standards for electric motors. The industrial model incorporates the necessary reductions in unit energy consumption for the energy-intensive industries.

Emissions

Industrial emissions are modeled for total carbon. The emissions factors [43] that are utilized to compute the emissions levels are consistent with those used throughout NEMS. The factors are assumed to be constant throughout the forecast horizon. The carbon emission factors used in the model are presented in Table E-20 in Appendix E.

Fuel Switching

In the Industrial Model, seasonal fuel switching is not considered because it is an annual model. Most observable fuel switching is seasonal and is difficult or impossible to detect with annual data. In the BSC component, all natural gas consumption is interruptible, i.e., switchable. Presumably, most of the switching that occurs here is seasonal and unobservable with annual data and prices. Fuel switching is implemented in the model by allowing the share of fuels in existing boilers to shift based on the short-run fuel share elasticities discussed above.

Benchmarking

The 1990 Industrial Model energy demand forecasts are benchmarked to actual 1990 and 1991 State Energy Data System (SEDS) values to ensure that the model forecasts for 1990 coincides with the SEDS consumption data. The benchmark factors are based on the ratio of the SEDS value of consumption for each fuel to the consumption calculated by the model at the census division level. (The average of the benchmark factors for 1990 and 1991 is applied to all future years.) The difference in energy consumption between the benchmarked consumption and forecasted model consumption is accounted for in the "Other Industry" category. Benchmarking is accomplished in Subroutine IBSEDS, described on page 120.

Alternative Approaches

This section discusses the previous EIA industrial model, as well as other industrial modeling approaches that are currently in use or have been recommended for use at EIA.

Previous EIA Industrial Model

The previous EIA industrial model used an econometric approach based on historical patterns of individual fuel and electricity uses in a variety of manufacturing and nonmanufacturing industries [44]. When the model was originally constructed, the time frame of the forecasting was for the next 10 years and provided the appropriate requirements. These requirements consisted primarily of forecasting and not of policy and technology analysis. Subsequently, the forecasting time frame was extended to 20 years and the econometric modeling approach became less appropriate.

The Intermediate Future Forecasting System (IFFS) industrial model estimates the consumption of each fuel or electricity in each of 11 industries independently, by using historical data from the period 1958 through 1985. Each of these energy consumption equations uses independent variables consisting of value of industry output, energy prices, and the lagged (one time period) level of energy consumption. For a relatively short forecast period of time, these equations can perform very well. However, they are lacking in substitution effects, not only in terms of the overall production function and the factor inputs of capital, labor and materials, but also in terms of substitution between various forms of energy. In general, the price estimations did not provide for significant cross price coefficients. In addition, the equations were estimated in log-linear transformations which can cause problems in a long-term forecast. Moreover, the lagged consumption terms can cause accumulating problems if they start going off on the wrong track. One further difficulty with the IFFS model is the insufficient ability of the model to address and assess new policies and/or issues and discrete changes in industry.

The primary advantages of the NEMS model are that:

- The model uses all available data and at the industry specific level as much as possible.

- The model is sensitive in expected directions and degrees to changes in energy prices and to changes in the level of industry output.
- The model equations are directly explainable and understandable and the relationships are straightforward and intuitive.

The model also includes additional algorithms or inputs for nonutility generation of electricity, consumption of renewable energy, and calibration and benchmarking.

Other Approaches to Modeling Industrial Energy Consumption

A variety of models are used to provide energy forecasts of one type or another in the industrial sector. Many of these models are not exclusively industrial models, but rather are macroeconomic models that pay particular attention to energy and to energy consumption sectors. Most industrial sector energy models can be categorized according to certain general characteristics. Several categories are shown in Table 3. These categories identify whether the model is (1) a basic econometric model, (2) an hybrid econometric model with technology and/or process information, (3) an hybrid accounting model with economic relationships and with technology and/or process information, (4) an industry process model with economic relationships, (5) an interindustry and/or macroeconomic model, or (6) an input-output model. The categories are a very rough description of the content of the models and may not be very satisfactory in all cases. Not all these categories are clearly defined and some models may overlap portions of several categories.

Table 3. Other Industrial Energy Models

Basic Econometric

PC-IM (IFFS EIA Model)

PURHAPS Model (Former EIA Model)

INDEPTH Level 1 (EPRI)

Hybrid Econometric

DEMO-PSM

INRAD (Argonne)

LIEF (Marc Ross and Roland Hwang)

Hybrid Accounting

FOSSIL-1 and FOSSIL-2 (AES)

Peck/Bosch/Weyant Vintage Model

Industry Process

INDEPTH Level 2 (EPRI)

ISTUM-1, ISTUM-2 and ISTUM-PC

ICE and IFCAM (EEA)

ORIM (Oak Ridge)

Interindustry/Macroeconomic

Data Resources, Inc. (also Wharton Econometrics)

Hudson/Jorgenson (also Jorgenson/Wilcoxon DGEM)

Input/Output

LIFT (INFORUM at University of Maryland)

Energy Indexes (Short-term analysis)

The hybrid econometric and hybrid accounting types of models are those of most interest for the EIA industrial sector modeling. In most of the cases, the models that are discussed represent only the manufacturing sector part of the industrial sector. There are not many established models that have been created to model energy use in the agriculture, mining and/or construction industries (one notable exception is the ISTUM model).

Each of these models has its own particular approach to modeling industrial energy consumption (several use similar approaches). The approaches used and their advantages and disadvantages are discussed below. It should be kept in mind that the overall objective here is to determine the appropriate approach to be used in the new EIA industrial energy model. To that end, there are a number of unstated criteria and objectives that will be implied in the discussion. In addition, each model is discussed only in terms of what can be learned from it with respect to designing the modeling approach here at EIA.

Energy Intensity Indexes

The most basic approach to modeling industrial energy consumption consists of using an index of energy consumption relative to value of output (an index of energy intensity). This approach can be extended by including prices in the index. This approach can be very useful in the very short term, in a period of time when industry structure, the production function and processes and technologies are fixed. Industry consumption changes at essentially the rate of industry output.

Individual Econometric Energy Equations

On the other hand, over a longer period of time, the relationship between energy consumption and industry output does not remain constant. The changing relationship can be modeled with the use of estimated coefficients. The IFFS industrial model is an example of this approach [44]. In this case, an equation is estimated over historical data, and it identifies a relationship between energy consumption for a single fuel and the value of output in the industry and energy prices. The equation can be specified in a variety of ways and estimated using a number of tools including ordinary least squares, two-stage least squares, or seemingly-unrelated regression. The equation can include a time-trend or lagged endogenous variable to represent technology trends

and capital stock adjustments. However, no matter what is done, the equation still represents the circumstances over the historical period and is not necessarily appropriate for a longer-term forecast. It depends upon the extent to which it is assumed that the equation is specified properly, that data are not missing, that the data used in the estimation is good and appropriate, and that the future relationships will remain the same as in the historical period. Moreover, the equation does not capture the production function relationships that economic theory assigns such a high value.

Production Function Based Econometric Models

A wide variety of industrial models are based upon the idea of a production function or its dual, a cost function, and run the gamut from single industry models to economy-wide models. A previous EIA model, PURHAPS, is one example of this type of approach [40]. The PURHAPS model looked at the production function in an implicit manner, modeling the factor share for energy based upon the prices of all the factors, a technology trend and lagged prices of energy.

The production function in these models can be specified in a wide variety of ways, with alternate considerations concerning the relationships among the factor shares. Equation 4 shows the basic form for a production function. The basic relationship is that for a two-factor production function in which the output is a function of inputs of capital and labor. This basic relationship can be extended to other factors of production, such as materials and other variables which may or may not be specified, such as technology.

$$q = f(v_1, \dots, v_n) \quad (3)$$

where: q is the production level, and

v_i are factor usages.

The primary idea behind the production function is that production occurs according to some technical production "recipe", in which "factors" of production are brought together to produce output. There are certain engineering relationships among the variables that allow them to be brought together in an efficient manner to produce the product. It is important to note that the production function, as typically explained, is a micro concept. It applies to the technical relationships within the smallest economic units, such as small, well-defined processes. There are often significant problems when the concept is taken to a more aggregate level, such as an aggregate process, a firm, a plant or an industry [50].

The production function provides a technical relationship and the cost function that is the dual to the production function provides the economic relationship. An example of a cost function is shown in equation 5. The economic objective of the firm is to minimize this cost function.

$$TC = P_1 v_1 + \dots + P_n v_n \quad (4)$$

where: TC is total cost,
 P_i are factor prices, and
 v_i are factor usages.

Using a variety of mathematical forms, the relationships among the capital, labor, and materials variables in the production function can be specified in various ways with their specific characteristics. There are a variety of standard forms for production functions that have been used at various times throughout the literature (for discussions, see [31], [50], [85]). Some of the more prominent of these major variations include the original Cobb-Douglas, which is a special case of a more general class of production functions, the Constant Elasticity of

Substitution (CES) production functions. Following from these are the Translog [24] and the Generalized Leontief [33].

The total energy equation (the primary equation) in the PURHAPS model (as noted above) is basically a cost function. It assumes that production will be organized in an efficient manner, so that any one factor (energy in this case) can be solved for based upon the relative prices of all the factors of production. This is a common and reasonable assumption. The two major assumptions being made are that the substitution relationships among factor prices remain constant and that the factors are homogeneous enough so that they can be categorized in an aggregate fashion. In practical terms, the assumptions are also being made that the equations properly specify the relationships (missing or misspecified variables), that the coefficients from the historical estimations represent the future and that the exogenous forecasts upon which the forecast is based are good.

The Danish Production Sector Model uses a number of hybrid features [71], including the use of a vintage approach to address the path of adjustment and the modeling of detailed decision making chains (a systems dynamics approach) for each of the factors of production including capital and labor. The model uses a production function approach but uses only capital and labor in the production function (along with a technology time trend) and identifies a type of capital used for energy conservation.

The INDEPTH (Industrial End-Use Planning Methodology) Level 1 models [63] consist of a series of industrial energy models for individual manufacturing industries. For each of the manufacturing industries, alternative standard econometric approaches for modeling energy consumption using a production function are used. The INDEPTH Level 1 models were developed for the Electric Power Research Institute (EPRI) for the use of the EPRI member utilities in assessing the extent and nature of the utilities' industrial electricity demand. For this reason, the models are schematics into which the member utilities can insert the particular details and data of their own industrial demand. In addition, the emphasis of the models is on the

modeling of electricity energy demand. In the alternative INDEPTH formulations, the detailed information contained in the firm's production function and explicit cost minimization calculations is summarized by two functions. These are the cost function and the factor demand equations (from the production function). These empirical equations implicitly reflect the decisions that go into equipment choices and production processes as input prices and output demand change. As in econometric models of this type, there is no explicit accounting for the equipment and processes. The relationships are estimated over historical data. The advantages are that the models are rooted in good economic theory and that they can be estimated directly from historical data (although there are some problems with the availability of data). The disadvantages are that the relationships could not be valid too far into the future and that there is no explicit treatment of capital adjustment (vintages) or of technology.

Interindustry and/or Macroeconomic Models

A series of models continue to implement the production function approach but extend the modeling out beyond the boundaries of the industrial sector in order to cover all of the interactions among the entire economy. There are a number of approaches that can be used to do this, but an overriding characteristic is that the models capture some sense of the flows of economic activity from one sector to another. (A "sector" is being used as a general term indicating anything from large entities such as households, government and business, to small entities such as specific industries or types of households.) These can be explicit material flows or accounting for expenditures or payments between sectors.⁴ These are not explicitly industrial models, but rather have an industrial sector (or sectors) as parts of the model. Another

⁴ These models can range from small, less than 10-equation models, to very large and detailed models with large numbers of sectors with a thousand or more equations. In the context of this paper, however, the emphasis is primarily upon those models which pay some attention to the industrial sector as a distinct entity. Obviously, there is always more detail that can be added to these models, for example regional flows and as economies become more international in scope, international flows.

overriding characteristic is that these models attempt to solve for a economy-wide general economic equilibrium.

There are analogues relating to the sectoral interrelationships and the equilibrium modeling between these models and the IFFS [44]. The IFFS is designed as an energy model, so the sectors consist of energy sectors, rather than overall economic sectors. The interactions between the sectors in IFFS are in terms of energy flows, while that in the macroeconomic and interindustry models are in terms of overall economic activity and/or materials flows (of which energy could be one). Since the overall interest in IFFS is in energy activity, the economy is modeled as a separate sector. In the macroeconomic and interindustry models, there is no real distinction made between the economic sectors and other sectors; it is all one piece and simultaneous. Consequently, the equilibrium in the macroeconomic and interindustry models is theoretically represented as a true, general equilibrium (although it could be imperfectly represented). The equilibrium in IFFS is an approximation to a general equilibrium solution, to the extent that the macroeconomic sector is capturing the interindustry flows that are implied in all the energy sectors. This is a reasonable representation in the mid-term, but as the time horizon extends and industry structure changes in significant ways, there may be some difficulties with its representation as a general equilibrium solution. Because of these overall linkages, it would be difficult to separate the industrial energy sector from the overall macroeconomic or interindustry model in a sensible fashion.⁵ There are also difficulties in the other "direction" of trying to use the economic portion of an overall macroeconomic or interindustry model (particularly for the interindustry model) as the economic module in an energy system such as IFFS or the NEMS system.

⁵ A distinction is made between the industrial energy sector and the overall industrial sector economy. At EIA, when we refer to the industrial sector, we are referring to the energy activity. The overall industrial sector economy is a much more extensive and complex entity, consisting of not only energy and energy processes, but all capital, labor and materials decision making that go with it.

The Data Resources, Inc. (DRI) model is a good example of a macroeconomic model and it is currently being used in EIA for economic modeling. This model is based upon the equilibrium between the production-side and consumption-side expenditures in the economy along with (hundreds of) equations that provide significant relationships among the sectors. Another example is the macroeconomic model of Wharton Econometrics. The industrial sector in each of these models lacks detail, especially for energy.

The Hudson/Jorgensen model and the Jorgensen/Wilcoxon Dynamic General Equilibrium Model (DGEM) both have much more detailed industrial sectors which are based quite explicitly upon a production function/cost function approach. There are several industries represented, with production functions based upon flows of capital, labor, materials and energy. One primary characteristic of these models is the interdependence among the sectors (or industries) in the economy. Although these models have more detail, they are not strictly energy models and typically energy is a small part of the model. In addition, these models do not use any explicit representations of how energy is used, but rather rely upon the simplifying concept of aggregate production functions along with other simplifying assumptions relating to full employment and the substitutability of factors of production.

Input-Output Models

An input-output model is distinguished by the accounting for the flows of outputs from one industry to be used as inputs in other industries. Because of this interindustry dependence, any set of "correct" output flows from industry must be the same as all the input requirements in the economy (including to other sectors and outside the economy). Technically, the input-output analysis is not a general equilibrium analysis because although the interdependence of the various industries and the correct flow of product is the critical factor, this satisfies the technical relationships rather than the market based relationships. Additional cost factors can be brought into the analysis to solve for a general equilibrium. Typically, there are also simplifying

assumptions that must be made for the input-output analysis, including that each industry produces homogeneous products, industries use fixed input ratios and production in each industry is subject to constant returns to scale.

The Long-term Interindustry Forecasting Tool (LIFT) from INFORUM at the University of Maryland [57] is a hybrid of a large macroeconomic model and a 78-sector input-output model. This provides for a theoretically satisfying general economic equilibrium along with the technical relationships for the flows among industries. This model is mentioned here because there has been some interest in using features from it for the macroeconomic modeling at EIA. The difficulty would be in separating out the macroeconomic part of the model from the energy parts for all the sectors (residential, commercial, transportation and industrial) including the energy production and conversion sectors. As has been discussed earlier, the separation which is made at EIA is somewhat artificial, but useful so that a great deal of detail can be built into the energy aspects of demand and supply. In reality, these are simultaneous and therefore it is difficult to separate them in a model like LIFT which has been built with them together.

Industrial Process Models

Industrial process models generally take a bottom-up approach to modeling energy use in the industrial sector. Individual processes, technologies or equipment are represented in the model. In the forecast, as new processes, technologies or equipment are to be added to the capital base, the model makes choices from among various options by competing the processes, technologies or equipment on an economic basis. There are a number of difficulties associated with building a process model for models for the entire industrial sector, the first of which is that they require vast amounts of knowledge and resources. The resources have simply not been available nor are they expected to become available. In some cases, the approach has been to consider a process model for only a specific industry or for a specific energy source. In addition, the extensiveness of these models make them very complex so that they are not typically accessible

or transparent. The common developmental approach is to have experts with engineering backgrounds do a variety of studies to determine the various current and potential processes, technologies or equipment and to characterize each with a variety of economic factors such as capital cost, operating costs, maintenance costs, energy costs, lifetime, and others. These characteristics are used in various algorithms to make choices among the processes based upon economic decision making rules.

However, the industrial sector is very complex and capital stock decisions are made with a wide variety of motivations; these are the subject of much of the entire field of industrial organization in economics (see [85] for a discussion of this and several of the following points). A simple minimization of life-cycle cost may not be an appropriate rule. Moreover, there can be any number of other attributes associated with the process, technology or equipment that are externalities in the decision process or which are more important than the strictly economic variables. It may be more straightforward to characterize the decision making rules in an energy industry such as electric utilities, where the product is much more homogeneous, knowledge is and has been more available, the processes, technologies or equipment are better understood and in many cases a public utility commission mandates the rules to be used in decision making.

An additional difficulty in the industrial sector is that there is no clear way to know whether the characterization of the future processes, technologies and equipment has captured all possibilities. The characterization may be imperfect with respect to the processes available for competition or with respect to the attributes associated with that process. This can be a very significant problem and can imply that any error associated with this means that there really is no need to fine-tune anything else. It has been suggested that this is a common error and that it will typically cause the model to underestimate the potential for conservation of energy [85].

Another problem with using a process model to model energy is that energy is usually a small part of the capital choice decision. Even in some energy-intensive industries, energy can still be only a small part of the capital choice decision. For example, it has been suggested that the

penetration of continuous casting in the blast furnace and basic steel products industry, which saves very large amounts of energy, was motivated not by the desire to save industrial energy, but by the opportunity it provides for quality control. Another example is that future movements away from chemical pulping to mechanical pulping in the paper industry are not driven by energy economics but by environmental considerations. This choice also largely drives the extent of renewables consumption in the paper industry, because the single largest category of renewables is pulping liquor from the chemical pulping process. Recycling in the paper industry also has a significant influence upon the pulping process choices and on the amount of bleaching. Even if all the economic attributes of the processes could be determined, strict life-cycle costing does not capture all these non-economic considerations in an economic algorithm.

It is also difficult to assess the quality of the details of a process model, because there is typically no information about the details beyond the data that was put together for the model. The model can be assessed on an overall basis, but this does not provide any insight on whether the extra details have helped to provide better forecasts. Other models that are constructed on an overall basis can also provide forecasts. In general, an assessment of the 1977 ISTUM-1 model at a fairly aggregate level over the period 1977 to 1990 did not seem to indicate that the model performed particularly well, even on an overall basis.⁶

The ISTUM model is an industrial process-level model which was developed in the mid to late 1970's [38]. The model is very large and extensive and requires a vast data base of technologies. The original development effort was over an extended period of time and at least one stage utilized the equivalent of about two dozen full-time personnel. ISTUM is the seminal industrial process model and is perhaps the best known. Parts of ISTUM have been updated in various ways (the details are not clear) by Energy and Environmental Analysis, Inc. (EEA) into ISTUM-2 [37] and they occasionally run the model for various analyses, primarily for an annual forecast by the Gas Research Institute. Some industries in ISTUM have been redone for use on

⁶ The 1977 ISTUM model that begins forecasting in 1977 (its base year is 1976) was acquired by this office and was run over the historical period to 1990 using historical prices and historical level of output. The results were mixed.

the IBM PC, most notably the paper industry in British Columbia, Canada [58]. It is not anticipated that ISTUM would be used directly for the new EIA industrial model, but some of the detail that is available in ISTUM might be used to help provide information for the new EIA model.

The INDEPTH Level 2 model is also an industrial process-level model and was developed for the EPRI [28, 36]. It consists of an extremely detailed examination of 25 principal industrial production processes and the activities that make up each process. The model was developed with the intention that it would be used by electric utilities interested in how the introduction of new technologies and production processes would affect the electricity demand of their manufacturing clients. Along these lines, the model does not attempt to provide coverage for all of the manufacturing sector industries at a national level, nor does it pay significant attention to modeling other than for electricity. While the INDEPTH Level 2 model could be used to represent an industry, it is so process-specific that the most likely use would be to model actual or idealized plants operated by an electric utility's customers. The INDEPTH system has never received a high degree of acceptance among utility planning staffs as the EPRI residential and commercial models have. In part this may have been because most utilities had developed other in-house modeling approaches to forecasting industrial demand, and in part it may have been due to the cumbersome data requirements that are needed to do justice to the INDEPTH system's full capabilities.⁷

Apparently, the INDEPTH models are being phased out by EPRI and a set of industrial end-use models named INFORM, developed by Regional Economic Research, Inc. (RER) for EPRI, are being used instead. The model's end uses include motors, process heating, process drying and curing, melting, welding and cutting, electrolytic processes, lighting, HVAC and miscellaneous. For each end use, INFORM examines three sets of market decisions. These are fuel and

⁷ This information is based on the DAC report referred to above. Apparently, both INDEPTH Level 1 and INDEPTH Level 2 models have been used by only 3 utilities with only 1 significant user of Level 2.

technology decisions, which determine market shares; efficiency choices, which account for competition among efficiency options; and usage levels, which reflect production levels.

The Oak Ridge Industrial Model (ORIM) [83, 84], the Industrial Combustion Emissions (ICE) and the IFCAM models are older, process-type models that actually use a lot of hybrid features. They are apparently not being currently used. ORIM uses a mix of features of both top-down and bottom-up models, dealing with very generic energy services, manufacturing services and technologies. Although the technologies are generic, the data requirements are still extensive. The model also uses a vintage accounting structure. The Industrial Regional Activity and Energy Demand Model (INRAD) was used by Argonne National Laboratory to model industrial activity and energy demand for the National Acid Precipitation Assessment Program (NAPAP) studies [15].

Hybrid Econometric and Hybrid Accounting Models

This class of models is expected to have the most relevance to the new EIA industrial model. They consist of various equations and relationships that are implemented on an accounting structure.

The Long-Term Industrial Energy Forecasting (LIEF) model has been in development over the last few years [85]. There are several characteristics of this new model which strongly influenced the development of the new EIA industrial model (LIEF covers only the manufacturing sector). The first task of this model is to properly disaggregate the manufacturing sector according to output growth rates and energy intensities so that the way that energy is used can be properly accounted for. The point is made that disaggregation into the 2-digit SICs is not satisfactory for long-term forecasting. The problem is not that there are too few 2-digit sectors, but that they are improperly aggregated for energy analysis. The idea is to reorganize

the manufacturing sector into 4 to 10 sectors based upon energy intensity and output growth rates (the current version is organized into 4 sectors).

The long-term, real energy intensity forecasting technique used by LIEF rests on a sequence of three major decision areas: 1) the choice of the fundamental production process, which is autonomous in the sense that it is not sensitive to energy prices, 2) the choice of energy-related technologies which are sensitive to energy price, and 3) the operational decisions which are more of a short-term nature and not of interest in long-term forecasting. The choice of energy-related technologies in the model uses the conservation supply curve (CSC) as the basic analytical tool. However, the procedures used to estimate or characterize the CSC relationship are not based upon detailed lists of technologies, but rather are based on statistical estimation. In this forecasting sequence, the model uses variables other than price, which provide useful policy-analysis handles. Sectoral energy intensities are principally related to autonomous (price-independent) time trends, and to energy prices, implicit capital recovery factors, slope and intercept parameters for the CSCs and the rate of penetration of conservation technologies.

The NEMS Industrial Demand Model shares the concern with the proper disaggregation and accounting for energy use in the industrial sector. In addition, the model shares and borrows from major concepts, including the idea that choice of fundamental process change is autonomous (not price related) and the use of a conservation supply curve or something similar for energy intensity changes that is not necessarily built up from a detailed list of technologies. The basic model equation also recognizes the distinction between energy consumed in new equipment versus that of existing equipment and this basic idea is expected to be extended in the EIA model with a full vintage structure. Finally, it is desired that the overall feeling of accessibility, transparency and familiarity that the authors associate with LIEF, will also be associated with the EIA industrial model.

The industrial energy demand model described in [78] is a relatively straightforward structural representation for industrial energy use. The primary features of the model are that it is based

on production-function-like concepts (explicitly considering the prices of all input factors), considers the long-term substitution potential between fossil fuels and electricity (using relative prices) and incorporates vintaging of the existing capital stock in making energy consumption decisions. The model has been exercised and estimated for the primary metals industry based upon input data over the period 1958 through 1982. The major features of this model are also concerns in the new EIA industrial model and have influenced its development. The idea that the vintage of the capital stock impacts significantly upon the way that energy can be consumed in industry is carried through into the new model which is designed as a "putty-clay" representation.

The FOSSIL2 industrial sector model was constructed in 1985 by Applied Energy Services for the DOE Office of Policy, Planning and Analysis [9]. The industrial sector model is based on an end-use engineering process approach, but works at a very high level of aggregation (no industry disaggregation). This makes it necessary to exogenously input overall changes in industry composition and product/process shifts. However, the model does maintain some sense of vintage and models 4 types of energy service demands (such as boilers, process heat, machine drive/electrolytic and feedstocks). The distinction between energy consumption in new versus existing equipment and between components such as BSC and PA uses is carried through into the NEMS Industrial Demand Model.

4. Model Structure

Flow Diagrams

Figure 9 presents the calculational flow for the NEMS Industrial Demand Model. The figure shows each of the model subroutines and the corresponding data inputs and outputs, as appropriate. The following section provides the solution algorithms for the model.

Figure 9. Module Calculational Flow

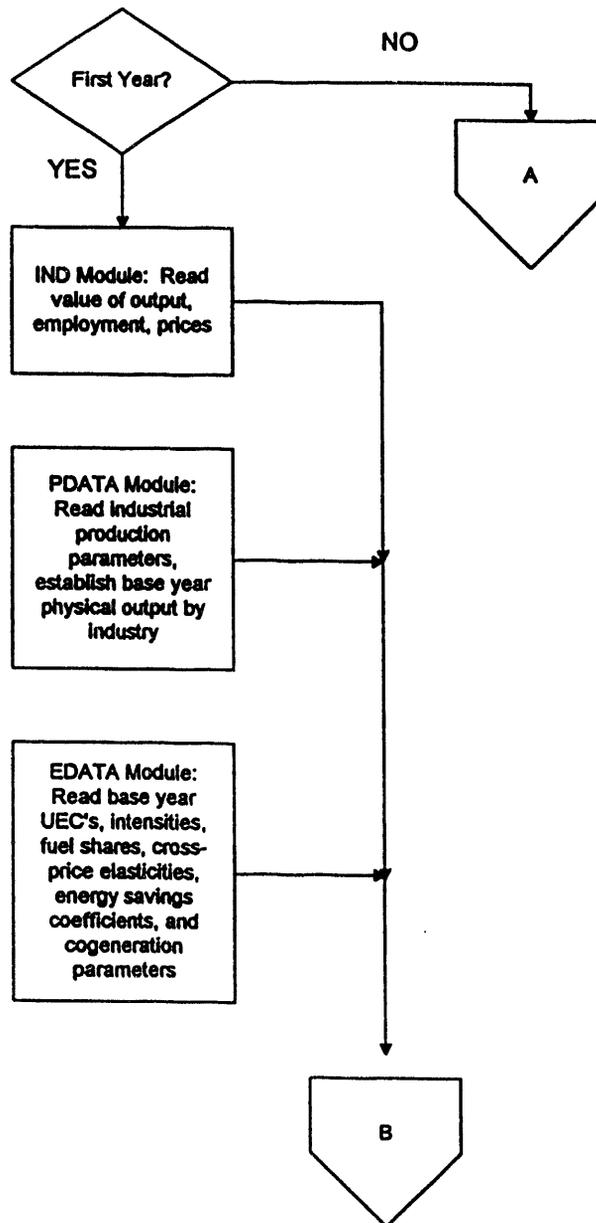


Figure 9. Module Calculational Flow, cont.

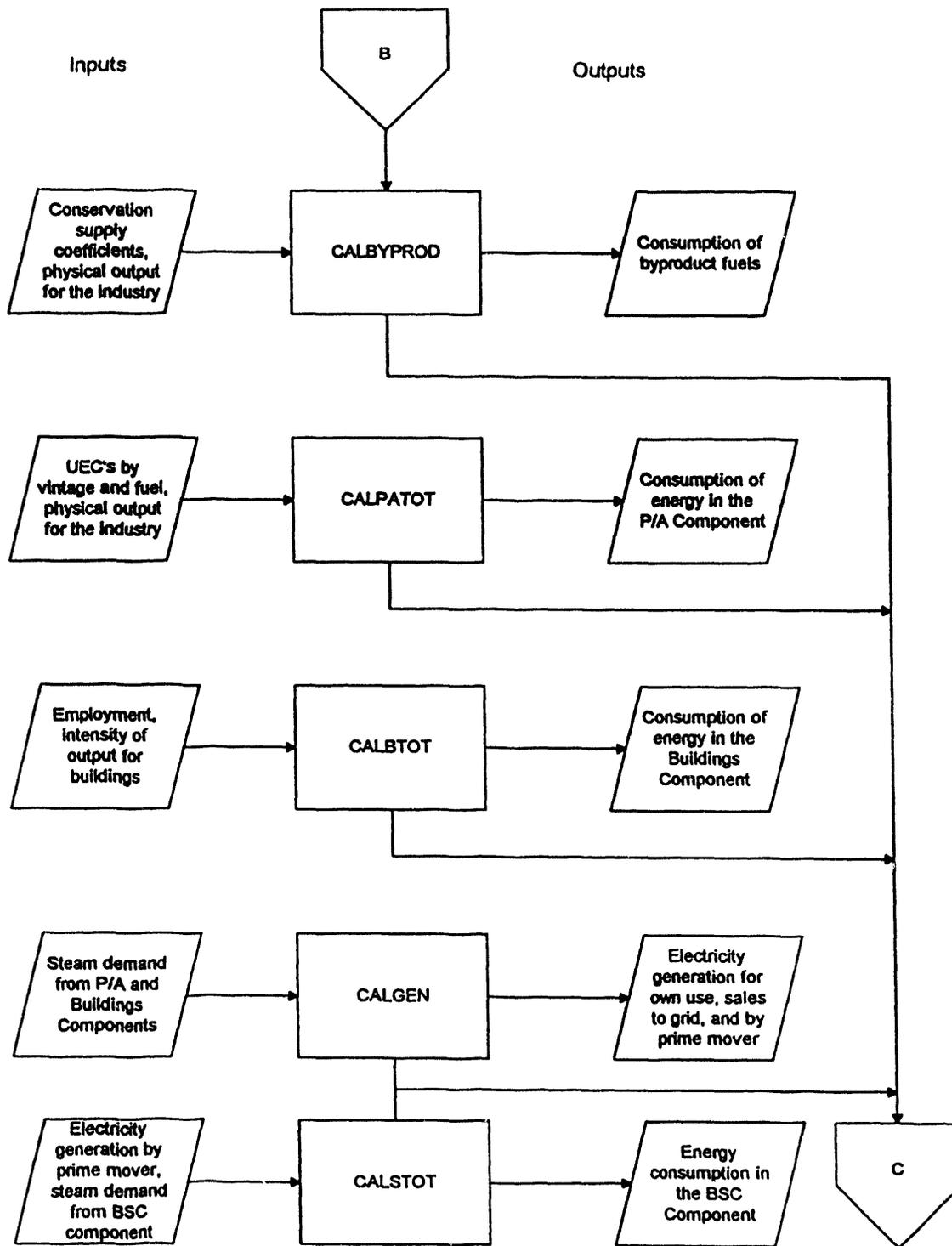


Figure 9. Module Computational Flow, cont.

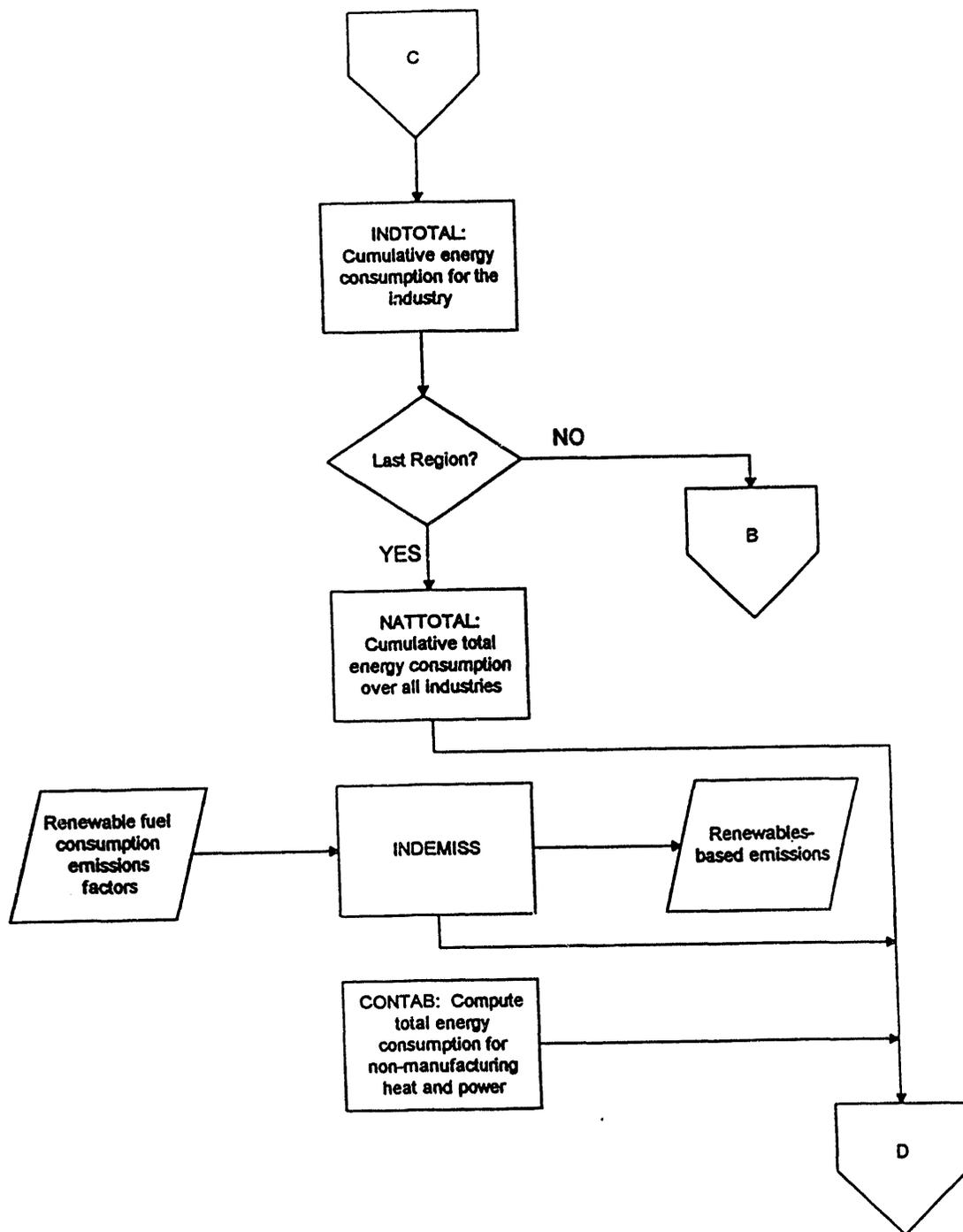


Figure 9. Module Computational Flow, cont.

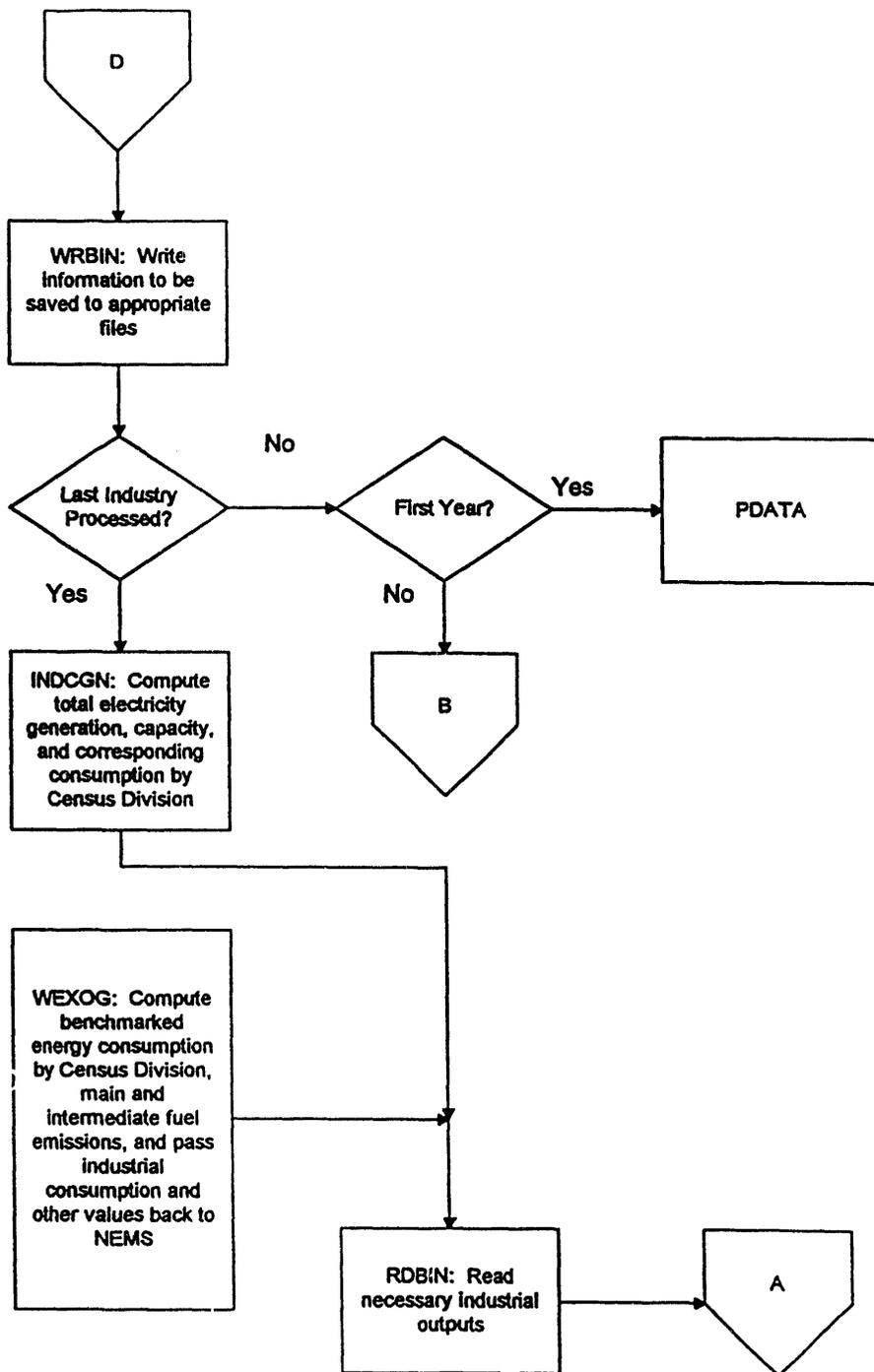
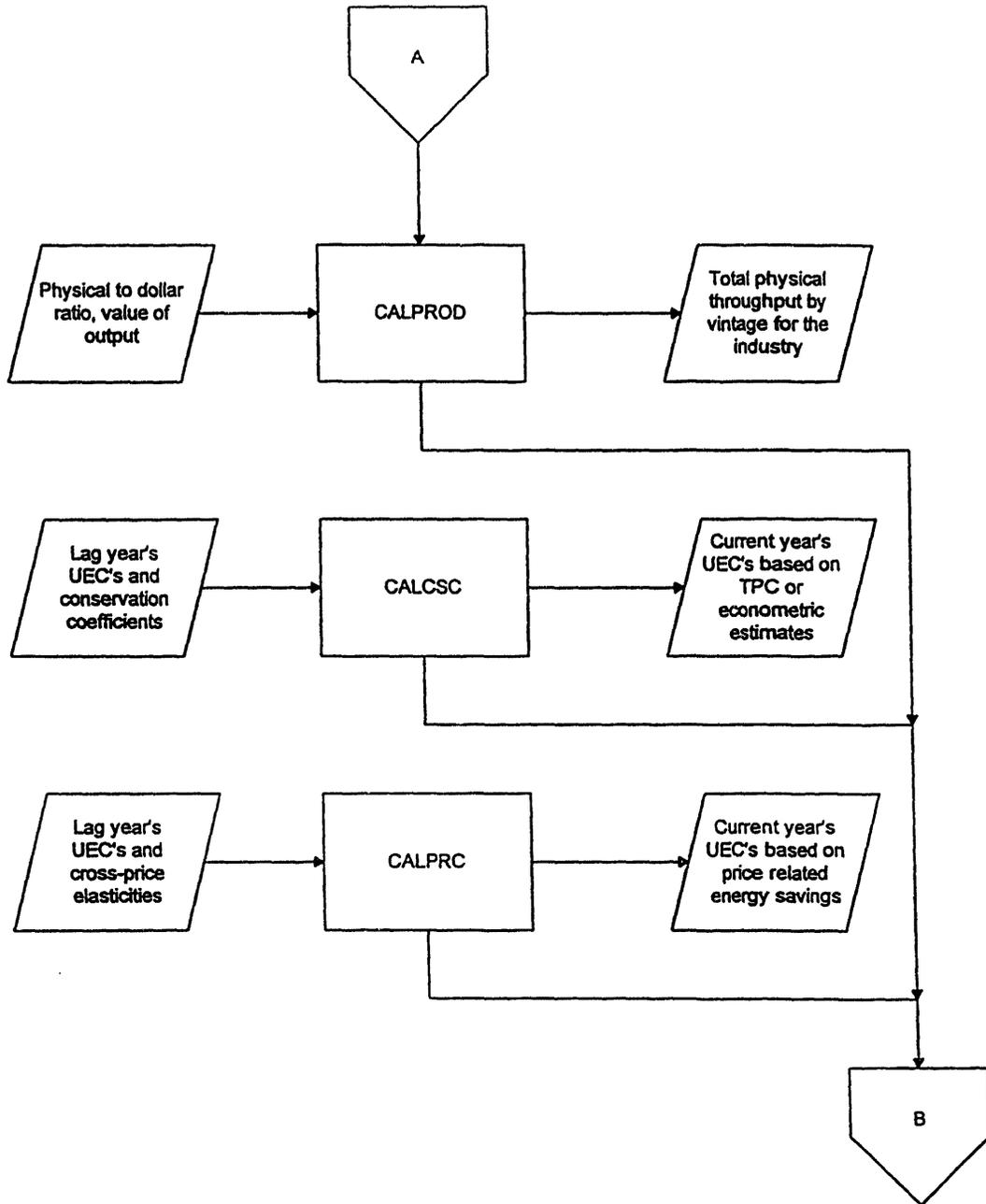


Figure 9. Module Calculational Flow, cont.



Subroutines and Equations

This section provides the solution algorithms for the Industrial Model. The order in which the equations are presented follows the logic of the FORTRAN source code very closely to facilitate an understanding of the code and its structure. In several instances, a variable name will appear on both sides of an equation. This is a FORTRAN programming device that allows a previous calculation to be updated (for example, multiplied by a factor) and re-stored under the same variable name.

IND

IND is the main industrial subroutine called by NEMS. This subroutine retrieves data for gross output for both the manufacturing and non-manufacturing industries from the NEMS Macroeconomic (MACRO) model. Employment is also obtained from the MACRO model for each non-agricultural industry. Prices for the various fuels as well as the previous year's consumption are obtained from NEMS COMMON blocks. For the first model year, consumption is obtained from the *State Energy Data System 1990* (SEDS). Because data for the industrial model are available only for the four Census regions, the energy prices obtained from NEMS, available for each of the nine Census divisions, are combined using a weighted average of the fuel prices in each of the four Census regions as shown in the following equation for the first model year. A similar weighted average is used for all other model years, however, the previous year's consumption is used rather than 1990 SEDS consumption.

$$PRCX_{elec,r} = \frac{\sum_{d=1}^{NUM_r} DPRCX_{elec,r} \times QSELIN_{d,1990}}{\sum_{d=1}^{NUM_r} QSELIN_{d,1990}} \quad (5)$$

where:

$$\begin{aligned} PRCX_{elec,r} &= \text{Price for electricity in Census region } r, \\ NUM_r &= \text{Number of Census divisions in Census region } r, \end{aligned}$$

| | | |
|-------------------|---|---|
| $DPRCX_{elec,d}$ | = | Price of electricity in Census division d , and |
| $QSELIN_{d,1990}$ | = | SEDS consumption of electricity in Census division d in 1990. |

Prices for biomass and steam are not available from NEMS. The price for biomass is assumed to be 2.0 dollars per MMBtu for all Census regions. The price of steam is an average of the prices of natural gas, coal, and residual oil. IND calls two subroutines: ISEAM, the subroutine that guides the industrial model calculations, and WEXOG, the subroutine that reports the results back to NEMS.

ISEAM

ISEAM controls all of the industrial model calculations. It opens external files for debugging, binary files for restarting on successive iterations and forecast years, and the input data files. In the first model year and only on the first iteration, ISEAM calls two subroutines: RCNTRL and INDEMISI to read the control file and emissions input file. ISEAM then calls REXOG to read in exogenous inputs on each model run. For the first model year, ISEAM calls the following subroutines for each Census region within each industry: PDATA, EDATA, CALBYPROD, CALPATOT, CALBTOT, CALGEN, CALSTOT, and INDTOTAL. After the forecast for the last Census region for a particular industry has been calculated, the following three subroutines are called: NATTOTAL, INDEMISS, and CONTAB. After the first model year, ISEAM calls two subroutines, RDBIN to read the restart files, and MODCAL to carry out model calculations. After all model calculations have been completed, ISEAM calculates industry totals and saves information to the restart files in the subroutine WRBIN. Finally, after each industry has been processed, ISEAM calls the subroutine INDCGN to report industrial cogeneration estimates to NEMS.

Subroutine RCNTRL

RCNTRL reads data from the input file INDRUN. This file contains internal control variables for the industrial model. Data in this file come from a series of questions the user is asked at the beginning of a run. The data consists of indicator variables for subroutine tracing, debugging, writing summary tables, calculating unit energy consumption using technology possibility curve (TPC) parameters, calculating unit

energy consumption using price elasticities, including imports and exports in the model, and benchmarking. This file also contains the beginning model year, the ending model year, the number of industries to be modeled, and input file names.

Subroutine INDEMISI

INDEMISI reads emission factors from an input file. Uncontrolled emissions factors for each fuel, expressed in metric tons per million Btu, are read in for each of the following pollutants: carbon, carbon monoxide, carbon dioxide, methane, sulfur dioxide, nitrogen oxide, volatile organic compounds (VOC), and particulates. Controlled emissions factors for each fuel, expressed in fractional terms, are also read in from the input file for each of the pollutants. Fractional sulfur contents are obtained for each fuel for use in calculating emissions of SO_x . Currently, only the carbon emissions are reported.

Subroutine REXOG

REXOG prepares exogenous data obtained from the NEMS MACRO model for use in the industrial model. Dollar value of output and employment are aggregated over the appropriate Census divisions to obtain data at the Census region level. Employment data is obtained from NEMS at the two digit SIC level. Therefore, for several industries modeled in the industrial model, employment data must be shared out between industries at the same two digit SIC level. In particular, the chemical industry (SIC 28) is grouped into bulk chemicals (SICs 281, 282, 286, and 287) and other chemical. Employment for the petroleum industry must be shared out between refining and all other petroleum. The stone, clay, and glass industry and the primary metals industry also require sharing out of employment data.

Subroutine PDATA

PDATA is the subroutine that reads in data for the process and assembly component of the model. For each region in each industry, the following data is read from the ENPROD input file: industry name, industry code⁸, Census region, number of process steps, an indicator variable indicating the units of unit energy consumption (physical or dollar units), value of production, and cumulative output. For each process step, the following data is read from the input file: process step number, number of links, the process steps linked to the current step, physical throughput to each process step, the retirement rate, and process step name.

Note that only the energy-intensive industries have steps. However, two industries, food and kindred products and bulk chemicals, do not have linkages among steps because the steps represent end-uses (e.g., refrigeration and freezing in the food and kindred products industry). As a result, the downstep throughput for food and kindred products and bulk chemicals is equal to one. A linkage is defined as a link between more than one process step. For example, in the paper and allied products industry, the wood preparation process step is linked to the virgin fibers pulping process step. The down-step throughput is the fraction of total throughput for an industry at a process step if it is linked to the final consumption. If the process step is linked to another process step, then the down-step throughput is the fraction of the linked process step plus the fraction of final consumption. The following example illustrates this procedure.

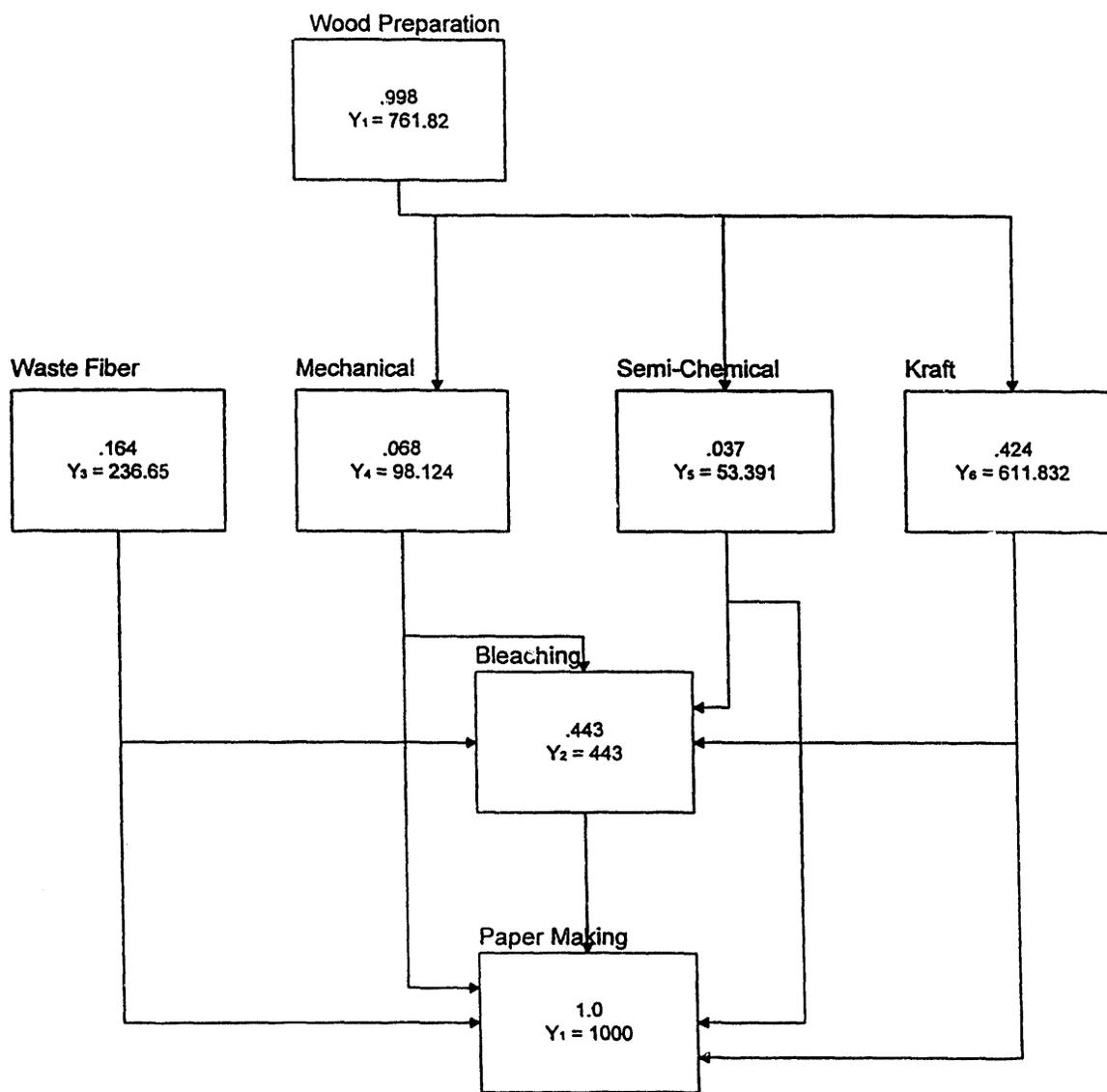
Figure 10 shows the process flow for the paper and allied products industry. The algebraic representation is as follows:

Let:

- $Y_1 \equiv$ Number of tons of paper to be produced.
- $Y_2 \equiv$ Number of tons of material to go through the bleaching process.
- $Y_3 \equiv$ Number of tons of material to go through the waste fiber pulping process.
- $Y_4 \equiv$ Number of tons of material to go through the mechanical pulping process.

⁸This industry code is the industrial model code, not the SIC code.

Figure 10. Paper and Allied Products Industry Process Flow



$Y_5 \equiv$ Number of tons of material to go through the semi-mechanical pulping process.

$Y_6 \equiv$ Number of tons of material to go through the Kraft pulping process.

$Y_7 \equiv$ Number of tons of material to go through the wood preparation process.

Then, we have the following:

$Y_1 =$ Some value of output, in tons (from the MACRO Module).

$Y_2 = 0.443 Y_1$

$Y_3 = 0.164 Y_1 + 0.164 Y_2$

$Y_4 = 0.068 Y_1 + 0.068 Y_2$

$Y_5 = 0.037 Y_1 + 0.037 Y_2$

$Y_6 = 0.424 Y_1 + 0.424 Y_2$

$Y_7 = 0.998 Y_4 + 0.998 Y_5 + 0.998 Y_6$

If $Y_1 = 1,000$ tons of paper to be produced, then $Y_2 = 443$, $Y_3 = 236.65$, $Y_4 = 98.124$, $Y_5 = 53.391$, $Y_6 = 611.836$, and $Y_7 = 761.82$.

The papermaking process is as follows. We need 761.82 tons of output from the wood preparation process and 236.65 tons of output from the waste fiber pulping process. Of the 761.82 tons of material, 98.124 tons flow through mechanical pulping, 53.391 tons into semi-mechanical pulping, and 611.832 tons into the Kraft pulping process. 443 tons from the sum of output of the waste fiber, mechanical, semi-mechanical, and Kraft pulping processes goes through the bleaching process. This 443 tons along with the remainder of the output from each process goes to the final stage in papermaking.

Physical throughput is obtained for two vintages, old and new. Old vintage is considered to be any capital installed in 1990 or earlier. Middle vintage includes installations from 1991 to the lag of the current forecast year. New vintage includes any capital installed in the current forecast year.

PDATA forms the ratio of physical output to 1990 value of output for the energy-intensive industries with the exception of the food and kindred products and bulk chemical industries. This constant ratio is applied to physical output in subsequent years. The physical output value PHDRAT is converted to a ratio with the same name.

$$PHDRAT = \frac{PHDRAT}{PRODVX_{i,r}} \quad (6)$$

where:

| | | |
|-----------------------------|---|---|
| <i>PHDRAT</i> | = | Ratio of physical units to value of output, and |
| <i>PRODVX_{i,r}</i> | = | Value of output for industry <i>i</i> in Census region <i>r</i> . |

If the Unit Energy Consumption (UEC) is in physical units, then the following equation is used.

$$PRODX_{i,r} = PHDRAT \times PRODVX_{i,r} \quad (7)$$

where:

| | | |
|-----------------------------|---|--|
| <i>PRODX_{i,r}</i> | = | Output in physical units for industry <i>i</i> in Census region <i>r</i> , |
| <i>PHDRAT</i> | = | Ratio of physical units to value of output, and |
| <i>PRODVX_{i,r}</i> | = | Value of output for industry <i>i</i> in Census region <i>r</i> . |

If the UEC is in dollar units, then the following equation is used.

$$PRODX_{i,r} = PRODVX_{i,r} \quad (8)$$

where:

| | | |
|-----------------------------|---|---|
| <i>PRODX_{i,r}</i> | = | Value of output for industry <i>i</i> in Census region <i>r</i> , and |
| <i>PRODVX_{i,r}</i> | = | Value of output for industry <i>i</i> in Census region <i>r</i> . |

If the current process step is linked to final consumption (i.e., if there are no intermediate steps between the current step and final output), then the following equation is used:

$$PRODSUM_{s,l} = PRODFLOW_{old,s,l} \times PRODX_{i,r} \quad (9)$$

where:

| | | |
|----------------------|---|--|
| $PRODSUM_{s,l}$ | = | Amount of throughput used at process step s through link l , |
| $PRODFLOW_{old,s,l}$ | = | Down-step throughput to process step s linked by link l for old vintage, and |
| $PRODX_{i,r}$ | = | Output for industry i in Census region r . |

Note that PRODFLOW is a parameter that represents the relative production throughput to a subsequent production step in the energy-intensive industries. The linkage parameter indicates which production step is involved.

If the current process step is linked to one or more intermediate process steps, then the following equation is used:

$$PRODSUM_{s,l} = PRODFLOW_{old,s,l} \times PRODCUR_{total,IP} \quad (10)$$

where:

| | | |
|----------------------|---|---|
| $PRODSUM_{s,l}$ | = | Amount of throughput used at process step s through link l , |
| $PRODFLOW_{old,s,l}$ | = | Down-step throughput to process step s linked by link l for old vintage, and |
| $PRODCUR_{total,IP}$ | = | Current production at process step IP linked to process step s through link l for all vintages. |

In either case, the total production at each process step is determined through the following equation:

$$PRODCUR_{total,s} = \sum_{l=1}^{NTMAX_s} PRODSUM_{s,l} \quad (11)$$

where:

- $PRODCUR_{total,s}$ = Current production at process step s for all vintages,
- $NTMAX_s$ = Number of links at process step s , and
- $PRODSUM_{s,l}$ = Amount of throughput used at process step s through link l .

Subroutine EDATA

EDATA reads energy related data from the input file ENPROD. For each process step, the number of fuels used at the process step and the number of byproducts are obtained from ENPROD. For each fuel type within each process step, initial unit energy consumption (UEC), an intercept term for use in econometric equations, technology possibility curve (TPC) coefficient, and cross price elasticities are read in for both old and new vintage. EDATA reads in similar data for each byproduct fuel for each process step. The values for UEC, TPC coefficient, and cross price elasticities for new vintage are assigned to the variables for middle vintage.

This subroutine is also responsible for reading energy data for the buildings component. The number of fuels used for lighting, either none or one for electricity, is obtained as well as the initial UEC. The same information is obtained for heating, ventilation, and cooling (HVAC). There are three fuels considered for HVAC, electricity, natural gas, and steam.

Data for the boiler/steam/cogeneration (BSC) component is obtained through the EDATA subroutine. The number of non-byproduct fuels consumed in the BSC component is read in as well as boiler fuel shares, cross price elasticities, and the boiler efficiencies for each fuel. Boiler shares are normalized to sum to one. The number of byproduct fuels consumed in the BSC component is read in. Several variables are read concerning cogeneration of electricity, including initial steam demand, 1990 total electricity generation and generation for own use, and capacity utilization. Regression parameter estimates are read for steam demand and generation. Four prime movers, internal combustion engines, combustion turbines, steam turbines, and renewables are considered in the industrial model. For each prime mover, a share of total generation, a heat rate, and an efficiency are read from the input file.

Subroutine CALBYPROD

The industrial model consumes all byproduct fuels prior to purchasing any fuels. This subroutine calculates the energy savings or the current location on the technology possibility curve (TPC) based on the current year's industry production and the previous year's industry production for each process step, fuel, and old and new vintage as shown in the following equation. Currently, only the paper and allied products industry has a TPC for byproducts. For all other industries the UEC remains unchanged.

$$BYPCSCCUR_{v,f,s} = \left[\frac{PRODCUR_{total,s}}{PRODLAG_{total,s}} \right]^{BYPCSC_{v,f,s}} \quad (12)$$

| | | |
|---------------------|---|---|
| $BYPCSCCUR_{v,f,s}$ | = | Current energy savings for byproduct fuel f at process step s for vintage v , |
| $PRODCUR_{total,s}$ | = | Current production at process step s for all vintages, |
| $PRODLAG_{total,s}$ | = | Lagged production at process step s for all vintages, and |
| $BYPCSC_{v,f,s}$ | = | Byproduct technology possibility curve coefficient for byproduct fuel f at process step s for vintage v . |

The energy savings for middle vintage is a weighted average (by production) of the current year's energy savings for new vintage and the previous year's energy savings for middle vintage.

$$BYPCSCCUR_{mid,f,s} = \frac{(PRODCUR_{new,s} \times BYPCSCCUR_{new,f,s}) + (PRODCUR_{mid,s} \times BYPCSCLAG_{mid,f,s})}{PRODCUR_{new,s} + PRODCUR_{mid,s}} \quad (13)$$

where:

- $BYPCSCCUR_{mid,f,s}$ = Current energy savings for byproduct fuel f at process step s for mid vintage,
- $PRODCUR_{new,s}$ = New production at process step s ,
- $BYPCSCCUR_{new,f,s}$ = Current energy savings for byproduct fuel f at process step s for new vintage,
- $PRODCUR_{mid,s}$ = Existing production at process step s for mid vintage, and,
- $BYPCSCLAG_{mid,f,s}$ = Lagged location on the byproduct technology possibility curve for byproduct fuel f at process step s for middle vintage.

CALBYPROD calculates the rate of byproduct energy produced for each process step, fuel, and vintage shown in the following equation. This value is based on the previous year's rate of production and the current energy savings for each vintage.

$$BYPINT_{v,f,s} = BYPINTLAG_{v,f,s} \times BYPCSCCUR_{v,f,s} \quad (14)$$

where:

- $BYPINT_{v,f,s}$ = Rate of byproduct energy production for byproduct fuel f at process step s for vintage v ,
- $BYPINTLAG_{v,f,s}$ = Lagged rate of byproduct energy production for byproduct fuel f at process step s for vintage v , and

$BYPCSCCUR_{v,f,s}$ = Current energy savings for byproduct fuel f at process step s for vintage v .

The byproduct rate of production is used to calculate the quantity of byproduct energy produced by multiplying total production at the process step by the production rate.

$$BYPQTY_{v,f,s} = PRODCUR_{v,s} \times BYPINT_{v,f,s} \quad (15)$$

where:

$BYPQTY_{v,f,s}$ = Byproduct energy production for byproduct fuel f at process step s for vintage v ,

$PRODCUR_{v,s}$ = Production at process step s for vintage v , and

$BYPINT_{v,f,s}$ = Rate of byproduct energy production for byproduct fuel f at process step s for vintage v .

The byproduct rate of production is then converted from million Btu to trillion Btu. Byproduct production is subdivided into three categories: main fuels, intermediate fuels, and renewable fuels.

Byproduct production for each group of fuels is determined by summing byproduct production over the individual process steps for each fuel and vintage as shown below for main byproduct fuels. The equations for intermediate and renewable fuels are similar.

$$ENBYPM_{f,v} = \sum_{s=1}^{MPASTP} BYPQTY_{v,f,s} \quad (16)$$

where:

$ENBYPM_{f,v}$ = Byproduct energy production for main byproduct fuel f for vintage v ,

$MPASTP$ = Number of process steps, and

$BYPQTY_{v,f,s}$ = Byproduct energy production for byproduct fuel f at process step s for vintage v .

Subroutine CALPATOT

CALPATOT calculates the total energy consumption from the process and assembly component. In the first model year, this subroutine calls CALINTER to calculate an intercept term for further use in econometric equations. Note that CALINTER does not apply to the energy-intensive industries. Energy consumption at each process step is determined by multiplying the current production at that particular process step by the unit energy consumption (UEC) for that process step. Energy consumption is calculated for each fuel and vintage using the following equation.

$$ENPQTY_{v,f,s} = PRODCUR_{v,s} \times ENPINT_{v,f,s} \quad (17)$$

where:

$$\begin{aligned} ENPQTY_{v,f,s} &= \text{Consumption of fuel } f \text{ at process step } s \text{ for vintage } v, \\ PRODCUR_{v,s} &= \text{Production at process step } s \text{ for vintage } v, \text{ and} \\ ENPINT_{v,f,s} &= \text{Unit energy consumption of fuel } f \text{ at process step } s \text{ for} \\ &\quad \text{vintage } v. \end{aligned}$$

Four energy products that are used for non-fuel purposes are modeled differently. These products are asphalt and road oil, liquid petroleum gas feedstocks, petrochemical feedstocks, and natural gas feedstocks. For the construction industry, the consumption of asphalt and road oil for all model years after 1990 is determined through the following equation.

$$ENPQTY_{v,asp,s} = ENPINT_{v,asp,s} \times PRODZERO_{v,s} + 0.4 \times [PRODCUR_{v,s} - PRODZERO_{v,s}] \quad (18)$$

where:

$$ENPQTY_{v,asp,s} = \text{Consumption of asphalt and road oil at process step } s \text{ for} \\ \text{vintage } v,$$

| | | |
|--------------------|---|--|
| $ENPINT_{v,asp,s}$ | = | Unit energy consumption of asphalt and road oil at process step s for vintage v , |
| $PRODZERO_{v,s}$ | = | 1990 production at process step s for vintage v for the construction industry, and |
| $PRODCUR_{v,s}$ | = | Production at process step s for vintage v . |

For all years after 1990, feedstock consumption in the bulk chemical industry is computed as shown below for natural gas feedstocks. Equations for liquid petroleum gas feedstocks and petrochemical feedstocks are similar.

$$ENPQTY_{v,ngf,s} = ENPINT_{r,ngf,s} \times PRODZERO_{v,s} + 0.25 \times (PRODCUR_{v,s} - PRODZERO_{v,s}) \quad (19)$$

where:

| | | |
|--------------------|---|--|
| $ENPQTY_{v,ngf,s}$ | = | Consumption of natural gas feedstock at process step s for vintage v , |
| $ENPINT_{v,ngf,s}$ | = | Unit energy consumption of natural gas feedstock at process step s for vintage v , |
| $PRODZERO_{v,s}$ | = | 1990 production at process step s for vintage v for the construction industry, and |
| $PRODCUR_{v,s}$ | = | Production at process step s for vintage v . |

Consumption of each fuel is converted to trillion Btu. Energy consumption is subdivided into main fuels, intermediate fuels, and renewable fuels. Main fuels include the following:

- electricity consumed in the PA or BLD components,
- core and non-core natural gas,
- natural gas feedstocks,
- steam coal,
- coking coal (including net coke imports),
- residual oil,

- distillate oil,
- liquid petroleum gas for heat and power,
- liquid petroleum gas for feedstocks,
- motor gasoline,
- still gas,
- petroleum coke,
- asphalt and road oil,
- petrochemical feedstocks,
- other petroleum feedstocks, and
- other petroleum.

Intermediate fuels include the following:

- steam,
- coke oven gas,
- blast furnace gas,
- other byproduct gas,
- waste heat, and
- coke.

Renewable fuels include the following:

- hydropower,
- biomass--wood,
- biomass--pulping liquor,
- geothermal,
- solar,
- photovoltaic,
- wind, and
- municipal solid waste.

Energy consumption for the three fuel groups is determined for each fuel by summing over the process steps as shown below for main fuels. The equations for intermediate and renewable fuels are similar.

$$ENPMQTY_f = \sum_{s=1}^{MPASTP} ENPQTY_{total,f,s} \quad (20)$$

where:

| | | |
|----------------------|---|---|
| $ENPMQTY_f$ | = | Consumption of main fuel f in the process/assembly component, |
| $MPASTP$ | = | Number of process steps, and |
| $ENPQTY_{total,f,s}$ | = | Consumption of fuel f at process step s for all vintages. |

Energy consumption for coke imports is calculated as the difference between coke consumption and coke production. In the current industrial model, coke is consumed only in the blast furnace/basic oxygen furnace process step in the blast furnace and basic steel products industry. Coke is produced only in the coke oven process step in the blast furnace and basic steel products industry. The equation for net coke imports is shown below.

$$ENPMQTY_{coke} = ENPIQTY_{coke} - \left[PRODCUR_{total,co} \times \frac{24.8}{10^6} \right] \quad (21)$$

where:

| | | |
|------------------|---|--|
| $ENPMQTY_{coke}$ | = | Consumption of coke imports in the process/assembly component, |
|------------------|---|--|

| | | |
|----------------------|---|--|
| $ENPIQTY_{coke}$ | = | Consumption of coke in the process/assembly component, |
| $PRODCUR_{total,co}$ | = | Current production at the coke oven process step for all vintages, and |
| $24.8/10^6$ | = | Conversion factor, where there are 24.8 million btu per short ton of coke converted to trillion Btu. |

Subroutine CALINTER

CALINTER calculates an intercept term used to calculate unit energy consumption (UEC) by an econometric approach. The intercept calibrates projected consumption for the base year to actual consumption. The non-energy-intensive industries, with a few exceptions, utilize an econometric equation to estimate UECs. (The energy-intensive industries, with the exception of the feedstock process step in the bulk chemical industry, use an approach developed by Arthur D. Little (ADL) to estimate unit energy consumption.) For each fuel, an intercept term is calculated in CALINTER based on the UEC, cumulative output, own-price elasticities, and cross price elasticities. The purpose of the intercept term is to calibrate the results for the first model year. The intercept term is calculated for old vintage in the following equation. The intercept for new vintage is assumed to equal the intercept for old vintage. An intercept term is not required for middle vintage calculations.

$$EINTER_{old,f,s} = \frac{ENPINT_{old,f,s}}{[CUMOUT88]^{BCSC_{old,f,s}} \times \prod_{i=1}^{11} [WPRC_i]^{BELAS_{old,f,s,i}}} \quad (22)$$

where:

| | | |
|--------------------|---|--|
| $EINTER_{old,f,s}$ | = | Intercept at process step s for fuel f for old vintage, |
| $ENPINT_{old,f,s}$ | = | Unit energy consumption of fuel f at process step s for old vintage, |

| | | |
|----------------------------------|---|---|
| <i>CUMOUT88</i> | = | Cumulative output through the year 1988, |
| <i>BCSC_{old,f,s}</i> | = | Energy savings coefficient at process step <i>s</i> for fuel <i>f</i> and old vintage, |
| <i>WPRC_t</i> | = | Price for fuel <i>t</i> in 1987 dollars, and |
| <i>BELAS_{old,f,s,t}</i> | = | Own price elasticity at process step <i>s</i> for fuel <i>f</i> for old vintage, and cross price elasticity at process step <i>s</i> for fuel <i>f</i> and fuel <i>t</i> for old vintage. |

Subroutine CALBTOT

CALBTOT calculates the total energy consumption for buildings. The energy consumption for buildings is calculated for two building uses, lighting and HVAC. Total energy consumption is determined for electricity, natural gas, and steam by multiplying industry employment by the building unit energy consumption as shown in the following equation.

$$ENBQTY_{e,f} = EMPLX_{i,r} \times ENBINT_{e,f} \quad (23)$$

where:

| | | |
|-----------------------------|---|--|
| <i>ENBQTY_{e,f}</i> | = | Consumption of fuel <i>f</i> for building end use <i>e</i> , |
| <i>EMPLX_{i,r}</i> | = | Employment for industry <i>i</i> in Census region <i>r</i> , and |
| <i>ENBINT_{e,f}</i> | = | Unit energy consumption of fuel <i>f</i> for building end use <i>e</i> . |

Subroutine CALGEN

CALGEN calculates electricity generation and the quantity of steam used to generate electricity. The following two equations calculate the total demand for electricity and steam. The total demand for electricity is determined by summing the electricity consumed in the PA component and in the BLD

component (no electricity is consumed in boilers). Total steam demand is calculated in the same manner as electricity demand.

$$ELDEM = ENPMQTY_{elec} + ENBQTY_{total,elec} \quad (24)$$

where:

- ELDEM* = Total electricity demand from process/assembly and buildings,
- ENPMQTY_{elec}* = Consumption of electricity in the process/assembly component, and
- ENBQTY_{total,elec}* = Consumption of electricity for all building end uses.

$$STEMCUR = ENBQTY_{hvac,steam} + ENPIQTY_{steam} \quad (25)$$

where:

- STEMCUR* = Total steam demand,
- ENBQTY_{hvac,steam}* = Consumption of steam for HVAC, and
- ENPIQTY_{steam}* = Consumption of steam in the process/assembly component.

Total electricity generation is based on an econometric equation (see Appendix E). To utilize the regression parameters, an intercept term must be calculated on the first call to CALGEN. The intercept is the natural log of the ratio of 1990 generation to the predicted value for the current year based on the regression parameters.

$$GINTER = \ln \left[\frac{GEN90}{STEMCUR_{90}^{GSTEAM}} \right] \quad (26)$$

where:

| | | |
|-----------------------------|---|--|
| <i>GINTER</i> | = | Intercept term for electricity generation, |
| <i>GEN90</i> | = | 1990 generation of electricity, |
| <i>STEMCUR₉₀</i> | = | Total steam demand for 1990, and |
| <i>GSTEAM</i> | = | Steam demand coefficient. |

Electricity generation is then determined through the equation shown below based on the intercept term and an estimated parameter for steam demand.

$$ELGEN_{total} = e^{GINTER} \times STEMCUR^{GSTEAM} \quad (27)$$

where:

| | | |
|------------------------------|---|--|
| <i>ELGEN_{total}</i> | = | Electricity generation for all prime movers, |
| <i>GINTER</i> | = | Intercept for electricity generation, |
| <i>STEMCUR</i> | = | Total steam demand, and |
| <i>GSTEAM</i> | = | Steam demand coefficient. |

Generation of electricity is converted from Btu to megawatt hours. Capacity for electric generation is determined from total generation of electricity and input data on capacity utilization. The following equation calculates capacity for electric generation.

$$ELCAP = \frac{ELGEN_{total} \times 10^9}{GENUTIL \times 3412.0 \times 365.25 \times 24.0} \quad (28)$$

where:

| | | |
|------------------------------|---|---|
| <i>ELCAP</i> | = | Capacity for electricity generation, |
| <i>ELGEN_{total}</i> | = | Electricity generation from all prime movers, |
| <i>GENUTIL</i> | = | Capacity utilization for cogeneration, |
| 3412.0 | = | Conversion factor, 3412.0 Btu per kilowatthour, |
| 365.25 | = | Number of days per year, |
| 24.0 | = | Number of hours per day, and |
| 10 ⁹ | = | Conversion factor to convert to megawatts. |

Electricity generation for own use is based on an econometric equation (see Appendix E). An intercept term is calculated on the first call to CALGEN. This intercept is based on 1990 own use generation, total electricity generation, and a parameter estimate for own use generation.

$$OINTER = \ln \left[\frac{OWN90}{(ELGEN_{total})^{OGEN}} \right] \quad (29)$$

where:

| | | |
|------------------------------|---|---|
| <i>OINTER</i> | = | Intercept for own use generation, |
| <i>OWN90</i> | = | 1990 electricity generation for own use, |
| <i>ELGEN_{total}</i> | = | Electricity generation from all prime movers, and |
| <i>OGEN</i> | = | Own use generation coefficient. |

Electricity generation for own use is then calculated from the following equation.

$$ELOWN = e^{OINTER} \times ELGEN_{total}^{OGEN} \quad (30)$$

where:

| | | |
|------------------------------|---|---|
| <i>ELOWN</i> | = | Electricity generation for own use, |
| <i>OINTER</i> | = | Intercept for own use generation, |
| <i>ELGEN_{total}</i> | = | Electricity generation from all prime movers, and |
| <i>OGEN</i> | = | Own use generation coefficient. |

Electricity generation for sales to the grid is calculated as the difference between total generation and generation for own use. Electricity generation is calculated for each of the four prime movers based on the share of total generation for each prime mover as shown below.

$$ELGEN_m = ELGEN_{total} \times GENEQPSHR_m \quad (31)$$

where:

| | | |
|------------------------------|---|--|
| <i>ELGEN_m</i> | = | Electricity generation from prime mover <i>m</i> , |
| <i>ELGEN_{total}</i> | = | Electricity generation from all prime movers, and |
| <i>GENEQPSHR_m</i> | = | Share of generation for prime mover <i>m</i> . |

Total industrial cogeneration for sales to the grid and own use and total capacity for generation are incremented as the processing of each industry is completed.

Subroutine CALSTOT

CALSTOT calculates total fuel consumption in the BSC component. Fuel consumption for non-steam turbines is calculated by multiplying electricity generation by internal combustion engines and combustion turbines by the appropriate heat rates. The equation for internal combustion engines is presented below

and a similar equation is used for combustion turbines. (Note that $ELGEN_{ICE}$ is calculated in CALGEN where it is one of the prime movers.) CALSTOT also calls the subroutine FUELBOIL. FUELBOIL calculates total fuel consumption in boilers and steam turbines.

$$ICEFUEL = ELGEN_{ice} \times \frac{GENEQPHTRT_{ice}}{3412.0} \quad (32)$$

where:

- $ICEFUEL$ = Fuel consumption for electricity generation from internal combustion engines,
- $ELGEN_{ice}$ = Electricity generation from internal combustion engines,
- $GENEQPHTRT_{ice}$ = Heat rate for internal combustion engines, and
- 3412.0 = Conversion factor to convert from Kwh to Btu.

Steam generated from cogeneration of electricity, shown below for internal combustion turbines, is determined through the efficiency for each prime mover obtained from the input file. A similar equation exists for combustion turbines.

$$ICESTEAM = (ICEFUEL - ELGEN_{ice}) \times GENEQPSTEFF_{ice} \quad (33)$$

where:

- $ICESTEAM$ = Cogeneration of steam from internal combustion engines,
- $ICEFUEL$ = Fuel consumption for electricity generation from internal combustion engines,
- $ELGEN_{ice}$ = Electricity generation from internal combustion engines, and
- $GENEQPSTEFF_{ice}$ = Efficiency for internal combustion engines.

Steam generated from boilers is calculated as the difference between total steam demand and the quantity of steam generated from internal combustion engines and combustion turbines.

$$BOILSTEAM = STEMCUR - (ICESTEAM + GCTSTEAM) \quad (34)$$

where:

| | | |
|------------------|---|--|
| <i>BOILSTEAM</i> | = | Steam generated from boilers, |
| <i>STEMCUR</i> | = | Total steam demand, |
| <i>ICESTEAM</i> | = | Cogeneration of steam from internal combustion engines, and |
| <i>GCTSTEAM</i> | = | Cogeneration of steam from combustion turbines. |

Fuel consumption in steam turbines and boilers is processed in the subroutine FUELBOIL called by CALSTOT. The four fuels considered for cogeneration are coal, oil, natural gas, and renewables/other. The fuels consumed for cogeneration are calculated by summing fuel consumption over fuels for each of the four prime movers. It is assumed that all coal and renewables consumed for cogeneration are consumed in steam turbines. Internal combustion engines are assumed to consume only distillate oil, and all combustion turbines use natural gas. The following equation is the computation of consumption of distillate oil for cogeneration. The equations for the other fuels are similar.

$$CGFUEL_{oil,total,r} = STFUEL_{oil} + ICEFUEL \quad (35)$$

where:

| | | |
|--------------------------------------|---|--|
| <i>CGFUEL</i> _{oil,total,r} | = | Consumption of distillate oil for cogeneration of electricity for all uses in Census region <i>r</i> , |
| <i>STFUEL</i> _{oil} | = | Consumption of distillate oil in steam turbines, and |
| <i>ICEFUEL</i> | = | Fuel consumption for electricity generation from internal combustion engines. |

The total fuel consumption for cogeneration is shared between generation for own use and sales to the grid based on the proportion of total generation allotted to each use. The following equation calculates fuel consumption for own use generation. Fuel consumption for sales to the grid is calculated as the difference between total fuel consumption for all uses and fuel consumption for own use generation.

$$CGFUEL_{f,own,r} = CGFUEL_{f,total,r} \times \left[\frac{ELOWN}{ELGEN_{total}} \right] \quad (36)$$

where:

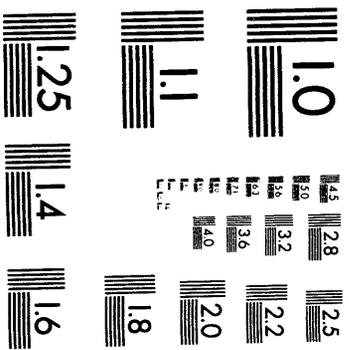
- $CGFUEL_{f,own,r}$ = Consumption of fuel f for cogeneration of electricity for own use in Census region r ,
- $CGFUEL_{f,total,r}$ = Consumption of fuel f for cogeneration of electricity for all uses in Census region r ,
- $ELOWN$ = Electricity generation for own use, and
- $ELGEN_{total}$ = Electricity generation from all prime movers.

Total industrial fuel use for cogeneration is incremented after each industry is processed.

Subroutine FUELBOIL

FUELBOIL calculates total fuel consumption in boilers and steam turbines. An average intensity, shown below, is determined from boiler fuel shares and the unit energy consumption to generate steam.

$$AVGINT = \sum_{f=1}^{IFSMAX} BSSHR_f \times ENSINT_f \quad (37)$$



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where:

| | | |
|---------------------------|---|--|
| <i>AVGINT</i> | = | Average intensity, |
| <i>IFSMAX</i> | = | Number of fuels consumed in the BSC component, |
| <i>BSSHR_f</i> | = | Share of total fuel consumption in the BSC component for fuel <i>f</i> , and |
| <i>ENSINT_f</i> | = | Intensity of fuel <i>f</i> in the BSC component. |

The quantity of steam generated by byproduct fuels is determined by dividing the byproduct energy produced by the unit energy consumption for each main, intermediate, and renewable fuel.

$$BYPSTM = \sum_{f=1}^{IFSBYPM} \frac{BYPBSCM_f}{BYSINT_f} + \sum_{f=1}^{IFSBIPI} \frac{BYPBSCI_f}{BYSINT_f} + \sum_{f=1}^{IFSBIYPR} \frac{BYPBSCR_f}{BYSINT_f} \quad (38)$$

where:

| | | |
|----------------------------|---|---|
| <i>BYPSTM</i> | = | Amount of steam generated from all byproduct fuels, |
| <i>IFSBYPM</i> | = | Number of byproduct main fuels, |
| <i>BYPBSCM_f</i> | = | Byproduct consumption of main fuel <i>f</i> in the BSC component, |
| <i>BYSINT_f</i> | = | Intensity for byproduct fuel <i>f</i> consumed in the BSC component, |
| <i>IFSBIPI</i> | = | Number of byproduct intermediate fuels, |
| <i>BYPBSCI_f</i> | = | Byproduct consumption of intermediate fuel <i>f</i> in the BSC component, |
| <i>IFSBIYPR</i> | = | Number of byproduct renewable fuels, and |
| <i>BYPBSCR_f</i> | = | Byproduct consumption of renewable fuel <i>f</i> in the BSC component. |

The following equation calculates the quantity of steam to be generated from purchased fuels. The quantity of steam to be generated from purchased fuels is the difference between the amount of steam consumed in boilers and the amount of steam generated from all byproduct fuels.

$$STEMCURF = STEMCUR - BYPSTM \quad (39)$$

where:

| | | |
|-----------------|---|---|
| <i>STEMCURF</i> | = | Amount of steam to be generated from purchased fuels, |
| <i>STEMCUR</i> | = | Total steam demand, and |
| <i>BYPSTM</i> | = | Amount of steam generated from all byproduct fuels. |

The total quantity of fuel consumed to generate steam is calculated below from the total steam demand from purchased fuels, the average intensity, and boiler fuel shares.

$$ENSQTY_f = STEMCURF \times AVGINT \times BSSHR_f \quad (40)$$

where:

| | | |
|---------------------------|---|--|
| <i>ENSQTY_f</i> | = | Consumption of fuel <i>f</i> to generate steam, |
| <i>STEMCURF</i> | = | Amount of steam to be generated from purchased fuels, |
| <i>AVGINT</i> | = | Average intensity, and |
| <i>BSSHR_f</i> | = | Share of total fuel consumption in the BSC component for fuel <i>f</i> . |

The amount of fuel consumed in the BSC component must be adjusted to exclude the amount of diesel used in internal combustion engines as shown in the following equation. A similar equation exists to exclude natural gas consumed in combustion turbines.

$$ENSQTY_f = ENSQTY_f - ICEFUEL \quad (41)$$

where:

$ENSQTY_f$ = Consumption of fuel f to generate steam, and
 $ICEFUEL$ = Fuel consumption for electricity generation from internal combustion engines.

The amount of each fuel and byproduct consumed in steam turbines is determined by fuel shares, total generation from steam turbines, and the heat rate for steam turbines. The following equation calculates the fuel consumption in steam turbines. A similar equation exists for byproduct fuel consumption in steam turbines.

$$STFUEL_f = \left[\frac{ENSQTY_f}{\sum_{f=1}^{IFSMAX} ENSQTY_f + \sum_{f=1}^{IFSBYP} BYSQTY_f} \right] \times ELGEN_{st} \times \frac{GENEQPHTRT_{st}}{3412.0} \quad (42)$$

where:

$STFUEL_f$ = Consumption of fuel f in steam turbines,
 $ENSQTY_f$ = Consumption of fuel f to generate steam,
 $IFSMAX$ = Number of fuels consumed in the BSC component,
 $IFSBYP$ = Number of byproducts consumed in the BSC component,
 $BYSQTY_f$ = Consumption of byproduct fuel f in the BSC component,
 $ELGEN_{st}$ = Electricity generation from steam turbines,

$GENEQPHTRT_{st}$ = Heat rate for steam turbines, and
 3412.0 = Conversion factor to convert from kilowatt hours to Btu.

Subroutine INDTOTAL

The consumption estimates derived in the PA, BSC, and BLD components are combined in INDTOTAL to produce an overall energy consumption figure for each industry. The consumption estimates include byproduct consumption for each of the main, intermediate, and renewable fuels. Only electricity, natural gas, and steam include consumption from buildings. For all fuels except electricity and natural gas, the following equation is used.

$$QTYMAIN_{f,r} = ENPMQTY_f + ENBQTY_{total,f} + ENSQTY_f + BYPBSCM_f \quad (43)$$

where:

$QTYMAIN_{f,r}$ = Consumption of main fuel f in Census region r ,
 $ENPMQTY_f$ = Consumption of main fuel f in the PA component,
 $ENBQTY_{total,f}$ = Consumption of fuel f for all building end uses,
 $ENSQTY_f$ = Consumption of fuel f to generate steam, and
 $BYPBSCM_f$ = Byproduct consumption of main fuel f to generate electricity from the BSC component.

Consumption of electricity is defined as purchased electricity only, therefore, electricity generation for own use is removed from the consumption estimate.

$$QTYMAIN_{elec,r} = ENPMQTY_{elec} + ENBQTY_{total,elec} - ELOWN \quad (44)$$

where:

| | | |
|-----------------------|---|---|
| $QTYMAIN_{elec,r}$ | = | Consumption of purchased electricity in Census region r , |
| $ENPMQTY_{elec}$ | = | Consumption of electricity in the PA component, |
| $ENBQTY_{total,elec}$ | = | Consumption of electricity for all building end uses, and |
| $ELOWN$ | = | Electricity generated for own use. |

Subroutine NATTOTAL

After processing all four Census regions for an industry, NATTOTAL computes a national industry estimate of energy consumption. This subroutine also computes totals over all fuels for main, intermediate, and renewable fuels. Total consumption for the entire industrial sector for each main, intermediate, and renewable fuel is determined by aggregating as each industry is processed as shown in the following equation.

$$TQMAIN_{f,r} = \sum_{i=1}^{INDMAX} QTYMAIN_{f,r} \quad (45)$$

where:

| | | |
|-----------------|---|--|
| $TQMAIN_{f,r}$ | = | Total consumption for main fuel f in Census region r , |
| $INDMAX$ | = | Number of industries, and |
| $QTYMAIN_{f,r}$ | = | Consumption of main fuel f in Census region r . |

Subroutine INDEMISS

INDEMISS is the subroutine that calculates emissions for each industry. Emissions are calculated for each of the following pollutants: carbon, carbon monoxide, carbon dioxide, methane, sulfur dioxide, nitrogen oxide, volatile organic compounds, and particulates. Emissions for each fuel and pollutant are based on uncontrolled and controlled emissions factors. Emissions are calculated for the main fuels and renewable fuels. No emission calculations are necessary for intermediate fuels. The equation below calculates emissions for each renewable fuel. Emissions from renewable fuels are calculated similarly. Currently, only carbon emissions have been implemented.

$$EMIRENW_{f,p,r} = QTYRENW_{f,r} \times UNCONTEMISSFACT_{f,p} \times EMISSCONTROLFAC_{f,p} \quad (46)$$

where:

| | | |
|-------------------------|---|---|
| $EMIRENW_{f,p,r}$ | = | Emissions of pollutant p from renewable fuel f in Census region r , |
| $QTYRENW_{f,r}$ | = | Consumption of renewable fuel f in Census region r , |
| $UNCONTEMISSFACT_{f,p}$ | = | Uncontrolled emission factor for pollutant p using fuel f , and |
| $EMISSCONTROLFAC_{f,p}$ | = | Emissions control factor for pollutant p using fuel f . |

For emissions of SO_x , the following equation is used.

$$EMIRENW_{f,sox,r} = EMIRENW_{f,sox,r} \times SULFURCONT_f \quad (47)$$

where:

| | | |
|---------------------|---|--|
| $EMIRENW_{f,sox,r}$ | = | Emissions of SO_x from renewable fuel f in Census region r , and |
| $SULFURCONT_f$ | = | Sulfur content of fuel f . |

Total emissions from all renewable fuels and emissions from the industrial sector are calculated in the two equations below.

$$TOTEMIS_{renw,p,r} = \sum_{f=1}^8 EMIRENW_{f,p,r} \quad (48)$$

where:

| | | |
|----------------------|---|---|
| $TOTEMIS_{renw,p,r}$ | = | Total emissions of pollutant p from renewables in Census region r , and |
| $EMIRENW_{f,p,r}$ | = | Emissions of pollutant p from renewable fuel f in Census region r . |

$$TEMISR_{f,p,r} = \sum_{i=1}^{INDMAX} EMIRENW_{f,p,r} \quad (49)$$

where:

| | | |
|-------------------|---|--|
| $TEMISR_{f,p,r}$ | = | Total emissions of pollutant p for renewable fuel f in Census region r , |
| $INDMAX$ | = | Number of industries, and |
| $EMIRENW_{f,p,r}$ | = | Emissions of pollutant p from renewable fuel f in Census region r . |

Subroutine CONTAB

CONTAB is responsible for reporting consumption values for the energy-intensive industries and energy consumption for heat and power for non-energy-intensive industries. Energy consumption for

manufacturing heat and power is computed by summing total consumption of each fuel over all the manufacturing industries. The consumption for heat and power will include consumption from the energy-intensive industries. The following fuels are considered for manufacturing heat and power: electricity, natural gas except for feedstock and lease and plant gas, steam coal, coking coal, net coke imports, residual oil, distillate oil, liquid petroleum gas, still gas, petroleum coke, other petroleum and total renewables. The following equation calculates consumption of main fuels for manufacturing heat and power. A similar equation exists for renewable fuels.

$$TMANHP_f = \sum_{i=7}^{INDMAX} \sum_{fg=1}^{NUM_{fg}} QTYMAIN_{f,total} \quad (50)$$

where:

| | | |
|---------------------|---|---|
| $TMANHP_f$ | = | Total manufacturing consumption of fuel f for heat and power, |
| $INDMAX$ | = | Number of industries, |
| NUM_{fg} | = | Number of fuels in fuel group fg , and |
| $QTYMAIN_{f,total}$ | = | Consumption of main fuel f in all Census regions. |

Energy consumption for non-manufacturing heat and power is considered separately from the manufacturing industries. Fuels considered for non-manufacturing heat and power include: electricity, natural gas, steam coal, residual oil, distillate oil, liquid petroleum gas, motor gasoline, renewables and other petroleum. A consumption table is also produced for miscellaneous feedstocks. All industries are included here and the following fuels are considered: natural gas feedstocks, liquid petroleum gas feedstocks, asphalt and road oils, petrochemical feedstocks, lubes and waxes, and other petroleum feedstocks.

A consumption table for each of the energy-intensive industries is produced in CONTAB. Consumption figures are reported for each of the fuels used in each particular industry. There is a total renewables

fuel group for each energy-intensive industry. Consumption for the chemical industry includes bulk chemicals and the non-energy-intensive industry other chemicals. The equation below calculates consumption of main fuels in the food and kindred products industry. All other energy-intensive industries have similar equations.

$$TFOODCON_f = \sum_{f=1}^{NUM_{fg}} QTYMAIN_{f,total} \quad (51)$$

where:

| | | |
|---------------------|---|--|
| $TFOODCON_f$ | = | Total consumption of fuel f in the food and kindred products industry, |
| NUM_{fg} | = | Number of fuels in fuel group fg , and |
| $QTYMAIN_{f,total}$ | = | Consumption of main fuel f for all Census regions. |

Subroutine WRBIN

WRBIN writes data for each industry to a binary file. Two different binary files are created. The first contains variables and coefficients that do not change over years, but change over industries. This binary file also contains data that do not change over years, but change over processes. The second binary file contains data that change from year to year.

Subroutine INDCGN

After all industries and regions have been processed, INDCGN calculates industrial cogeneration variables to report to NEMS. Two files are opened to read existing capacity for 1990 and 1991 and planned capacity for the years 1992 to 1996. The first file reads year, existing capacity, Census region, and fuel type for the following four fuels: coal, oil, natural gas, and other. The second file reads planned

capacity for the years 1992 to 1996, Census division, SIC, prime mover, year, and fuel type. Existing capacity for 1990 and 1991 and planned capacity for 1992 through 1996 are shared out between own use and sales to the grid based on the ratio of own use generation to total generation of electricity.

Existing capacity was shared from Census regions to Census divisions based on the electricity share for each Census division from 1990 SEDS. For 1990 and 1991, the following equation is used for own use generation. A similar equation exists for generation for sales to the grid.

$$CAPD_{d,y,f,own,pl} = \left[\frac{ELOTOT_r}{ELOTOT_r + ELSTOT_r} \right] \times CAPREG_{r,y,f,total} \times DIVSHARE_d \quad (52)$$

where:

| | | |
|------------------------|---|---|
| $CAPD_{d,y,f,own,pl}$ | = | Existing or planned capacity for cogeneration of electricity for own use for Census division d using fuel f in year y , |
| $ELOTOT_r$ | = | Total industrial electricity generation for own use in Census region r , |
| $ELSTOT_r$ | = | Total industrial electricity generation for sales to the grid in Census region r , |
| $CAPREG_{r,y,f,total}$ | = | Existing capacity for cogeneration of electricity for all uses for Census region r using fuel f in year y , and |
| $DIVSHARE_d$ | = | Electricity share for Census division d . |

For the years 1992 through 1996, the capacity for each Census division is augmented with the planned capacity for each Census division, fuel, use, and year. The following equation is the equation for own use and the equation for sales to the grid is similar.

$$CAPD_{d,y,f,own,pl} = CAPD_{d,y-1,f,own,pl} + \left[\frac{ELOTOT_r}{ELOTOT_r + ELSTOT_r} \right] \times CAPDIV_{d,y,f,total,pl} \quad (53)$$

where:

$CAPD_{d,y,f,own,pl}$ = Existing or planned capacity for cogeneration of electricity for own use in Census division d using fuel f in year y ,

$CAPD_{d,y-1,f,own,pl}$ = Existing or planned capacity for cogeneration of electricity for own use in Census division d using fuel f in year $y-1$,

$ELOTOT_r$ = Total industrial electricity generation for own use in Census region r ,

$ELSTOT_r$ = Total industrial electricity generation for sales to the grid in Census region r , and

$CAPDIV_{d,y,f,total,pl}$ = Planned capacity for electricity generation for all uses for Census division d using fuel f in year y .

The following equation calculates fuel consumption for each Census division.

$$DIVFUEL_{d,f,u} = GENTOT_{f,u,r} \times DIVSHARE_d \quad (54)$$

where:

$DIVFUEL_{d,f,u}$ = Consumption of fuel f for cogeneration of electricity for use u in Census division d ,

$GENTOT_{f,u,r}$ = Total consumption of fuel f for cogeneration of electricity for use u in Census region r , and

$DIVSHARE_d$ = Electricity share for Census division d .

Total generation, generation for own use, and generation for sales to the grid are shared from Census regions to the Census divisions. The shares are 1990 electricity shares for each Census division from

the *State Energy Data System 1990* (SEDS). Capacity for own use generation and generation for sales to the grid are also shared from Census regions to Census divisions. Own use generation and generation for sales to the grid are converted from trillion Btu to gigawatt hours. Capacity for own use and sales to the grid are converted to megawatts. The following equation computes capacity for own use. A similar equation is used to calculate capacity for sales to the grid.

$$CAPGW_{d,f,own,pl} = ELCTOT_r \times \left[\frac{ELOTOT_r}{ELOTOT_r + ELSTOT_r} \right] \times DIVSHARE_d \times \left[\frac{DIVFUEL_{d,f,own}}{DIVFUEL_{d,total,own}} \right] \quad (55)$$

where:

| | | |
|-------------------------|---|--|
| $CAPGW_{d,f,own,pl}$ | = | Existing or planned capacity for cogeneration of electricity for own use using fuel f in Census division d , |
| $ELCTOT_r$ | = | Capacity for industrial electricity generation in Census region r , |
| $ELOTOT_r$ | = | Total industrial electricity generation for own use in Census region r , |
| $ELSTOT_r$ | = | Total industrial electricity generation for sales to the grid in Census region r , |
| $DIVSHARE_d$ | = | Electricity share for Census division d , |
| $DIVFUEL_{d,f,own}$ | = | Consumption of fuel f for cogeneration of electricity for own use in Census division d , and |
| $DIVFUEL_{d,total,own}$ | = | Consumption of all fuels for cogeneration of electricity for own use in Census division d . |

The following equation calculates electric generation for own use.

$$GENGWH_{d,f,own} = ELOTOT_r \times DIVSHARE_d \times \left[\frac{DIVFUEL_{d,f,own}}{DIVFUEL_{d,total,own}} \right] \times \frac{10^6}{3412.0} \quad (56)$$

where:

| | | |
|-------------------------|---|---|
| $GENGWH_{d,f,own}$ | = | Cogeneration of electricity for own use using fuel f in Census division d , |
| $ELOTOT_r$ | = | Total industrial electricity generation for own use in Census region r , |
| $DIVSHARE_d$ | = | Electricity share for Census division d , |
| $DIVFUEL_{d,f,own}$ | = | Consumption of fuel f for cogeneration of electricity for own use in Census division d , |
| $DIVFUEL_{d,total,own}$ | = | Consumption of all fuels for cogeneration of electricity for own use in Census division d , and |
| $10^6/3412.0$ | = | Conversion factor to convert trillion Btu to megawatts. |

For the years 1990 to 1996, planned capacity is obtained from the following equation and unplanned capacity is set equal to zero.

$$CAPGW_{d,f,u,pl} = CAPD_{d,y,f,u,pl} \quad (57)$$

where:

| | | |
|---------------------|---|--|
| $CAPGW_{d,f,u,pl}$ | = | Existing or planned capacity for cogeneration of electricity for use u using fuel f in Census division d , and |
| $CAPD_{d,y,f,u,pl}$ | = | Existing or planned capacity for cogeneration for use u in Census division d using fuel f in year y . |

For all years after 1996, if the previous year's capacity for electricity generation is less than or equal to the current year's capacity, then the following equation calculates planned capacity.

$$CAPGW_{d,f,u,pl} = CAPD_{d,y-1,f,u,pl} + [CAPGW_{d,f,u,pl} - CAPGWLAG_{d,y,f,u,pl}] \quad (58)$$

where:

| | | |
|-----------------------|---|---|
| $CAPGW_{d,f,u,pl}$ | = | Planned capacity for cogeneration of electricity for use u using fuel f in Census division d , |
| $CAPD_{d,y-1,f,u,pl}$ | = | Existing or planned capacity for cogeneration for use u using fuel f in Census division d in year $y-1$, |
| $CAPGW_{d,f,u,pl}$ | = | Planned capacity for cogeneration of electricity for use u using fuel f in Census division d , and |
| $CAPGWLAG_{d,f,u,pl}$ | = | Lagged planned capacity for cogeneration of electricity for use u using fuel f in Census division d . |

If the previous year's capacity is greater than the current year's capacity, then the following equation is used.

$$CAPGW_{d,f,u,pl} = CAPD_{d,y-1,f,u,pl} \quad (59)$$

where:

| | | |
|-----------------------|---|--|
| $CAPGW_{d,f,u,pl}$ | = | Planned capacity for cogeneration of electricity for use u using fuel f in Census division d , and |
| $CAPD_{d,y-1,f,u,pl}$ | = | Existing or planned capacity for cogeneration of electricity for use u using fuel f in Census division d in year $y-1$. |

Subroutine WEXOG

WEXOG is the subroutine that reports variables to NEMS. All consumption values calculated at the regional level must be shared to the Census division level. The shares, computed in the following equation, are based on 1990 SEDS fuel consumption data. In the first and second model year, this subroutine calls IBSEDS to calculate benchmark factors for consumption.

$$FUELSHARE_{elec,d} = \frac{QSELIN_{d,1990}}{NUM_r \sum_{d=1} QSELIN_{d,1990}} \quad (60)$$

where:

| | | |
|----------------------|---|---|
| $FUELSHARE_{elec,d}$ | = | Share of consumption of electricity in Census division d , |
| $QSELIN_{d,1990}$ | = | SEDS consumption of electricity in Census division d in 1990, and |
| NUM_r | = | Number of Census divisions in Census region r . |

The shares for renewable fuels, calculated through the following equation, are based on the value of output from the paper and lumber industries since most renewable fuel consumption occurs in these industries.

$$DSRENEW_{f,d} = \frac{OUTIND_{13,d} + OUTIND_{11,d}}{NUM_r \sum_{d=1} (OUTIND_{13,d} + OUTIND_{11,d})} \quad (61)$$

where:

| | | |
|-----------------|---|--|
| $DSRENW_{f,d}$ | = | Share of output for renewable fuel f in Census division d , |
| $OUTIND_{13,d}$ | = | Gross value of output for the paper and allied products industry in Census division d , |
| $OUTIND_{11,d}$ | = | Gross value of output for the lumber and wood products industry in Census division d , and |
| NUM_r | = | Number of Census divisions in Census region r . |

Energy consumption for each main and renewable fuel is computed by multiplying the consumption computed by the model at the Census region level by the appropriate Census division share.

$$DQMAIN_{f,d} = TQMAIN_{f,r} \times FUELSHARE_{f,d} \quad (62)$$

where:

| | | |
|-------------------|---|---|
| $DQMAIN_{f,d}$ | = | Consumption of main fuel f in Census division d , |
| $TQMAIN_{f,r}$ | = | Total consumption of main fuel f in Census region r , and |
| $FUELSHARE_{f,d}$ | = | Share of consumption of fuel f in Census division d . |

Petroleum refineries lease and plant natural gas use, and fuels consumed for cogeneration in the oil and gas industry are not modeled explicitly in the industrial model. However, energy consumption from these industries is accounted for in total consumption from the industrial sector. Therefore, computed energy consumption values must be augmented by fuels consumed by refineries. In particular, the following fuels are consumed by refineries: electricity, natural gas, steam coal, residual oil, distillate oil, liquid petroleum gas, still gas, petroleum coke, and other petroleum. The following equation computes industrial consumption of natural gas for each Census division. All other fuels have similar equations with refinery consumption and oil and gas consumption included only where appropriate.

$$BMAIN_{ng,d} = \left[\sum_{f=3}^5 DQMAIN_{f,d} \right] + QNGRF_{d,y} + \sum_{u=1}^2 CGOGQ_{d,y,ng,u} \quad (63)$$

where:

| | | |
|--------------------|---|---|
| $BMAIN_{ng,d}$ | = | Consumption of natural gas in Census division d , |
| $DQMAIN_{f,d}$ | = | Consumption of natural gas fuel f in Census division d , |
| $QNGRF_{d,y}$ | = | Natural gas consumed by petroleum refining industry in Census division d in year y , and |
| $CGOGQ_{d,y,ng,u}$ | = | Consumption of natural gas from cogeneration of electricity for use u in enhanced oil recovery in Census division d in year y . |

Also accounted for in WEXOG are the supply of coal liquids and coal gases as shown in the following equation for industrial coal consumption.

$$BMAIN_{coal,d} = DQMAIN_{coal,d} + QCLRF_{d,y} + COPRCLQ_{d,y} + COPRCLG_{d,y} + \sum_{u=1}^2 CGOGQ_{d,y,coal,u} \quad (64)$$

where:

| | | |
|----------------------|---|--|
| $BMAIN_{coal,d}$ | = | Consumption of coal in Census division d , |
| $DQMAIN_{coal,d}$ | = | Consumption of coal in Census division d , |
| $QCLRF_{d,y}$ | = | Coal consumed by petroleum refining industry in Census division d in year y , |
| $COPRCLQ_{d,y}$ | = | Supply of coal liquids in Census division d in year y , |
| $COPRCLG_{d,y}$ | = | Supply of coal gases in Census division d in year y , and |
| $CGOGQ_{d,y,coal,u}$ | = | Consumption of coal from cogeneration of electricity for use u in enhanced oil recovery in Census division d in year y . |

After all industrial consumption has been accounted for, the resulting values are benchmarked to SEDS consumption values that are calculated in the subroutine IBSEDS. Consumption of renewable fuels are benchmarked to the values in the Annual Energy Review June 1993.

$$OTHIND_{f,d} = \left[BMAIN_{f,d} \times \frac{\sum_{y=1}^{MSEDYR} BENCHFAC_{f,d}}{2.0} \right] - BMAIN_{f,d} \quad (65)$$

where:

- $OTHIND_{f,d}$ = Consumption of fuel f for "other industry" in Census division d ,
- $BMAIN_{f,d}$ = Consumption of fuel f in Census division d ,
- $MSEDYR$ = Index of SEDS years, and
- $BENCHFAC_{f,d}$ = Benchmark factor for fuel f in Census division d .

Benchmarked consumption values are then passed into the appropriate variables for reporting to NEMS. The following equation calculates consumption of electricity. Equations for other fuels are similar.

$$QELIN_{d,y} = BMAIN_{elec,d} + OTHIND_{elec,d} \quad (66)$$

where:

- $QELIN_{d,y}$ = Industrial consumption of electricity in Census division d in year y ,
- $BMAIN_{elec,d}$ = Consumption of electricity in Census division d , and
- $OTHIND_{elec,d}$ = Consumption of electricity for "other industry" in Census division d .

The following two equations represent the consumption of core and non-core natural gas.

$$QGFIN_{d,y} = [BMAIN_{ng,d} + OTHIND_{ng,d}] \times \left[\frac{DQMAIN_{cng,d} + DQMAIN_{fds,d}}{BMAIN_{ng,d}} \right] \quad (67)$$

where:

- $QGFIN_{d,y}$ = Industrial consumption of core natural gas in Census division d in year y ,
- $BMAIN_{ng,d}$ = Consumption of natural gas in Census division d ,
- $OTHIND_{ng,d}$ = Consumption of natural gas for "other industry" in Census division d ,
- $DQMAIN_{cng,d}$ = Consumption of core natural gas in Census division d , and
- $DQMAIN_{fds,d}$ = Consumption of feedstock natural gas in Census division d .

$$QGIIN_{d,y} = (BMAIN_{ng,d} + OTHIND_{ng,d}) - QGFIN_{d,y} \quad (68)$$

where:

- $QGIIN_{d,y}$ = Industrial consumption of non-core natural gas in Census division d in year y ,
- $BMAIN_{ng,d}$ = Consumption of natural gas in Census division d ,
- $OTHIND_{ng,d}$ = Consumption of natural gas for "other industry" in Census division d , and
- $QGFIN_{d,y}$ = Industrial consumption of core natural gas in Census division d in year y .

Consumption of total petroleum is calculated as follows.

$$QTPIN_{d,y} = \sum_{f=6}^{15} BMAIN_{f,d} + OTHIND_{f,d} \quad (69)$$

where:

| | | |
|----------------|---|--|
| $QTPIN_{d,y}$ | = | Industrial consumption of total petroleum in Census division d in year y , |
| $BMAIN_{f,d}$ | = | Consumption of fuel f in Census division d , and |
| $OTHIND_{f,d}$ | = | Consumption of fuel f for "other industry" in Census division d . |

Industrial consumption of biomass is calculated in the following equation.

$$QBMIN_{d,y} = \left[\sum_{f=2}^3 DQRENW_{f,d} \right] + \left[\sum_{u=1}^2 CGOGQ_{d,y,bm,u} \right] + QBMRF_{d,y} \quad (70)$$

where:

| | | |
|--------------------|---|---|
| $QBMIN_{d,y}$ | = | Industrial consumption of biomass in Census division d in year y , |
| $DQRENW_{f,d}$ | = | Consumption of renewable fuel f in Census division d , |
| $CGOGQ_{d,y,bm,u}$ | = | Consumption of biomass from cogeneration of electricity for use u in enhanced oil recovery in Census division d in year y , and |
| $QBMRF_{d,y}$ | = | Biomass consumed by petroleum refining industry in Census division d in year y . |

Consumption of total renewables is calculated through the following equation.

$$QTRIN_{d,y} = QHOIN_{d,y} + QBMIN_{d,y} + QGEIN_{d,y} + QSTIN_{d,y} + QPVIN_{d,y} + QWIIN_{d,y} + QMSIN_{d,y} \quad (71)$$

where:

| | | |
|---------------|---|--|
| $QTRIN_{d,y}$ | = | Industrial consumption of total renewables in Census division d in year y , |
| $QHOIN_{d,y}$ | = | Industrial consumption of hydropower in Census division d in year y , |
| $QBMIN_{d,y}$ | = | Industrial consumption of biomass in Census division d in year y , |
| $QGEIN_{d,y}$ | = | Industrial consumption of geothermal in Census division d in year y , |
| $QSTIN_{d,y}$ | = | Industrial consumption of solar thermal in Census division d in year y , |
| $QPVIN_{d,y}$ | = | Industrial consumption of photovoltaic in Census division d in year y , |
| $QWIIN_{d,y}$ | = | Industrial consumption of wind in Census division d in year y , and |
| $QMSIN_{d,y}$ | = | Industrial consumption of municipal solid waste in Census division d in year y . |

Currently, only biomass (including pulping liquor) and hydropower are implemented in the model.

Variables pertaining to industrial cogeneration of electricity including generation for own use and sales to the grid, capacity, and fuel consumption are also passed to the appropriate NEMS variables. Cogeneration data from the refining and oil and gas industries are included in the industrial cogeneration data passed to NEMS as shown in the following equation for capacity. Similar equations are used to incorporate refining and oil and gas cogeneration for own use and sales to the grid as well as fuel consumption.

$$CGINDCAP_{d,y,f,u,pl} = CAPGW_{d,f,u,pl} + CGRECAP_{d,y,f,u,pl} + CGOGCAP_{d,y,f,u} \quad (72)$$

where:

- $CGINDCAP_{d,y,f,u,pl}$ = Industrial planned capacity for cogeneration for use u using fuel f in Census division d in year y ,
- $CAPGW_{d,f,u,pl}$ = Existing or planned capacity for cogeneration of electricity for use u using fuel f in Census division d ,
- $CGRECAP_{d,y,f,u,pl}$ = Refinery planned capacity for cogeneration for use u using fuel f in Census division d in year y , and
- $CGOGCAP_{d,y,f,u,pl}$ = Oil and gas planned capacity for cogeneration for use u using fuel f in Census division d in year y .

Total consumption is calculated below.

$$CGINDQ_{d,y,f,u} = DIVFUEL_{d,f,u} + CGREQ_{d,y,f,u} + CGOGQ_{d,y,f,u} \quad (73)$$

where:

- $CGINDQ_{d,y,f,u}$ = Industrial consumption of fuel f for cogeneration of electricity for use u in Census division d in year y ,
- $DIVFUEL_{d,f,u}$ = Consumption of fuel f for cogeneration of electricity for use u in Census division d ,
- $CGREQ_{d,y,f,u}$ = Consumption of fuel f from cogeneration of electricity for use u in refineries in Census division d in year y , and
- $CGOGQ_{d,y,f,u}$ = Consumption of fuel f from cogeneration of electricity for use u in enhanced oil recovery in Census division d in year y .

Consumption values for manufacturing heat and power must be augmented by fuels purchased for refineries before passing to NEMS as shown in the following equation.

$$MANHP_{elec,y} = TMANHP_{elec} + QELRF_{d,y} \quad (74)$$

where:

| | | |
|------------------|---|--|
| $MANHP_{elec,y}$ | = | Consumption of electricity for manufacturing heat and power in year y , |
| $TMANHP_{elec}$ | = | Total manufacturing consumption of electricity for heat and power, and |
| $QELRF_{d,y}$ | = | Electricity consumed by petroleum refining industry in Census division d in year y . |

Consumption of natural gas, coal, residual, distillate, liquid petroleum gas, still gas, petroleum coke, and others are calculated in a similar fashion.

Consumption for non-manufacturing heat and power is adjusted to include consumption from oil and gas mining.

$$NONHP_{f,y} = TNONHP_f + \sum_{u=1}^2 CGOGQ_{total,y,f,u} \quad (75)$$

where:

| | | |
|-----------------------|---|---|
| $NONHP_{f,y}$ | = | Consumption of fuel f for non-manufacturing heat and power in year y , |
| $TNONHP_f$ | = | Total non-manufacturing consumption of fuel f for heat and power, and |
| $CGOGQ_{total,y,f,u}$ | = | Consumption of fuel f from cogeneration of electricity for use u in enhanced oil recovery in all Census divisions in year y . |

Consumption for miscellaneous feedstocks in each of the energy-intensive industries are passed to the appropriate variables for usage by NEMS. Emissions are computed based on the benchmarked values shown below.

$$DEMIMAIN_{f,p,d} = [BMAIN_{f,d} + OTHIND_{f,d}] \times UNCONTEMISSFACT_{f,p} \times EMISSCONTROLFAC_{f,p} \quad (76)$$

where:

| | | |
|-------------------------|---|--|
| $DEMIMAIN_{f,p,d}$ | = | Emissions of pollutant p from main fuel f in Census division d , |
| $BMAIN_{f,d}$ | = | Consumption of main fuel f in Census division d , |
| $OTHIND_{f,d}$ | = | Consumption of fuel f from other industry in Census division d , |
| $UNCONTEMISSFACT_{f,p}$ | = | Uncontrolled emission factor for pollutant p using fuel f , and |
| $EMISSCONTROLFAC_{f,p}$ | = | Emissions control factor for pollutant p using fuel f . |

Emissions for natural gas and liquid petroleum gas must be adjusted to remove feedstocks as shown in the following two equations.

$$DEMIMAIN_{ng,p,d} = (BMAIN_{ng,d} + OTHIND_{ng,d}) - (BENCHFAC_{ng,d} \times DQMAIN_{ng,d}) + (BENCHFAC_{ng,d} \times QLPIN_{d,y} \times UNCONTEMISSFACT_{cng,p} \times EMISSCONTROLFAC_{cng,p}) + (BENCHFAC_{ng,d} \times DQMAIN_{ng,d} \times UNCONTEMISSFACT_{fng,p} \times EMISSCONTROLFAC_{fng,p}) \quad (77)$$

where:

| | | |
|---------------------|---|--|
| $DEMIMAIN_{ng,p,d}$ | = | Emissions of pollutant p from natural gas in Census division d , |
|---------------------|---|--|

| | | |
|---------------------------|---|--|
| $BMAIN_{ng,d}$ | = | Consumption of natural gas in Census division d , |
| $OTHIND_{ng,d}$ | = | Consumption of natural gas from other industry in Census division d , |
| $BENCHFAC_{ng,d}$ | = | Benchmark factor for natural gas in Census division d , |
| $DQMAIN_{ng,d}$ | = | Consumption of natural gas in Census division d , |
| $QLPIN_{d,y}$ | = | Industrial consumption of lease and plant natural gas in Census division d in year y , |
| $UNCONTEMISSFACT_{cng,p}$ | = | Uncontrolled emission factor for pollutant p using core natural gas, |
| $EMISSCONTROLFAC_{cng,p}$ | = | Emissions control factor for pollutant p using core natural gas, |
| $UNCONTEMISSFACT_{fng,p}$ | = | Uncontrolled emission factor for pollutant p using feedstock natural gas, and |
| $EMISSCONTROLFAC_{fng,p}$ | = | Emissions control factor for pollutant p using feedstock natural gas. |

$$\begin{aligned}
 DEMIMAIN_{lp,p,d} = & ((BMAIN_{lp,d} + OTHIND_{lp,d}) - (BENCHFAC_{lp,d} \times DQMAIN_{lp,d})) \quad (78) \\
 & \times (UNCONTEMISSFACT_{lp,p} \times EMISSCONTROLFAC_{lp,p}) + \\
 & (BENCHFAC_{lp,d} \times DQMAIN_{lp,d} \times UNCONTEMISSFACT_{lp,p} \times EMISSCONTROLFAC_{lp,p})
 \end{aligned}$$

where:

| | | |
|---------------------|---|--|
| $DEMIMAIN_{lp,p,d}$ | = | Emissions of pollutant p from liquid petroleum gas in Census division d , |
| $BMAIN_{lp,d}$ | = | Consumption of liquid petroleum gas in Census division d , |
| $OTHIND_{lp,d}$ | = | Consumption of liquid petroleum gas from "other industry" in Census division d , |

| | | |
|------------------------------|---|---|
| $BENCHFAC_{lp,g,d}$ | = | Benchmark factor for liquid petroleum gas in Census division d , |
| $DQMAIN_{lp,g,d}$ | = | Consumption of liquid petroleum gas in Census division d , |
| $UNCONTEMISSFACT_{lp,ghp,p}$ | = | Uncontrolled emission factor for pollutant p using liquid petroleum gas for heat and power, |
| $EMISSCONTROLFAC_{lp,ghp,p}$ | = | Emissions control factor for pollutant p using liquid petroleum gas for heat and power, |
| $UNCONTEMISSFACT_{lp,gf,p}$ | = | Uncontrolled emission factor for pollutant p using liquid petroleum gas for feedstocks, and |
| $EMISSCONTROLFAC_{lp,gf,p}$ | = | Emissions control factor for pollutant p using liquid petroleum gas for feedstocks. |

For emissions of SO_x the following equation is used. Currently, only carbon emissions have been implemented.

$$DEMIMAIN_{f,p,d} = DEMIMAIN_{f,p,d} \times SULFURCONT_f \quad (79)$$

where:

| | | |
|--------------------|---|--|
| $DEMIMAIN_{f,p,d}$ | = | Emissions of pollutant p from main fuel f in Census division d , and |
| $SULFURCONT_f$ | = | Sulfur content of fuel f . |

Emissions for renewables are calculated by the equation below.

$$DEMIRENW_{f,p,d} = TEMISR_{f,p,r} \times DSRENW_{f,d} \quad (80)$$

where:

- $DEMIRENW_{f,p,d}$ = Emissions of pollutant p from renewable fuel f in Census division d ,
- $TEMISR_{f,p,r}$ = Total emissions of pollutant p from renewable fuel f in Census region r , and
- $DSRENEW_{f,d}$ = Consumption of renewable fuel f in Census division d .

Emissions are calculated through the following equations. Emissions of methane and particulates are assigned a value of zero.

$$EMINCX_{fp,d,y} = \sum_{f=1}^{NUM_{fg}} DEMIMAIN_{fp,d} \quad (81)$$

where:

- $EMINCX_{fp,d,y}$ = Emissions of pollutant p from fuel f in Census division d in year y ,
- NUM_{fg} = Number of fuels in fuel group fg , and
- $DEMIMAIN_{fp,d}$ = Emissions of pollutant p from main fuel f in Census division d .

$$EMINC_{fp,y} = \frac{EMINCX_{fp,total,y}}{10^6} \quad (82)$$

where:

- $EMINC_{fp,y}$ = Industrial emissions of pollutant p from fuel f in year y ,

$EMINCX_{f,p,total,y}$ = Emissions of pollutant p from fuel f in all Census divisions in year y , and

10^6 = Conversion factor to convert to million metric tons.

Subroutine IBSEDS

IBSEDS calculates benchmark factors for consumption. The benchmark factors are based on the ratio of SEDS consumption of the fuel to the consumption calculated by the industrial model.

$$BENCHFAC_{f,d} = \frac{SEDSIND_{f,d}}{BMAIN_{f,d}} \quad (83)$$

where:

$BENCHFAC_{f,d}$ = Benchmark factor for fuel f in Census division d ,

$SEDSIND_{f,d}$ = SEDS consumption of fuel f in Census division d , and

$BMAIN_{f,d}$ = Consumption of main fuel f in Census division d .

The benchmark factor for biomass is computed as follows.

$$BENCHFAC_{bm,d} = \frac{BIOFUELS_d}{\sum_{f=2}^3 DQRENW_{f,d}} \quad (84)$$

where:

$BENCHFAC_{bm,d}$ = Benchmark factor for biomass in Census division d ,

| | | |
|----------------|---|--|
| $BIOFUELS_d$ | = | Consumption of biofuels in Census division d , and |
| $DQRENW_{f,d}$ | = | Consumption of renewable fuel f in Census division d . |

A category labeled "Other Industry" is computed as the difference between the benchmarked consumption and the modeled consumption.

$$OTHIND_{f,d} = (BENCHFAC_{f,d} \times BMAIN_{f,d}) - BMAIN_{f,d} \quad (85)$$

where:

| | | |
|------------------|---|---|
| $OTHIND_{f,d}$ | = | Consumption of fuel f for "other industry" in Census division d , |
| $BENCHFAC_{f,d}$ | = | Benchmark factor for fuel f in Census division d , and |
| $BMAIN_{f,d}$ | = | Consumption of main fuel f in Census division d . |

Subroutine RDBIN

RDBIN is called by the main industrial subroutine ISEAM on model runs after the first model year. This subroutine reads the previous year's data from the binary files. The previous year's values are assigned to lagged variables for price, value of output, and employment. The previous year's UECs, TPC coefficients, price elasticities, and intercepts are read into the variables for initial UEC, TPC, price elasticity, and intercept. Process specific data is read into either a lagged variable or an initial estimate variable. Three cumulative variables are calculated in this subroutine for future use. A cumulative output variable, a cumulative UEC, and a cumulative production variable are computed for each fuel and process step.

MODCAL

MODCAL performs like the main industrial subroutine ISEAM in all years after the first model year. In subsequent years, no data must be read from the input files, however, UECs and TPC coefficients must be adjusted to reflect the new model year, whereas the first model year uses only initial estimates of these values. MODCAL calls the following subroutines: CALPROD, CALCSC, CALPRC, CALPATOT, CALBYPROD, CALBTOT, CALGEN, CALBSC, CALSTOT, INDTOTAL, NATTTOTAL, INDEMISS, and CONTAB. Similar to the functioning of ISEAM, the subroutines NATTTOTAL, INDEMISS, and CONTAB are called only after the last region for an industry has been processed.

Subroutine CALPROD

CALPROD determines the throughput for production flows for the process and assembly component. Existing old and middle vintage production is adjusted by the retirement rate of capital through the following equations for the manufacturing industries.

$$PRODCUR_{old,s} = [PRODCUR_{old,s} + IDLCAP_{old,s}] \times (1 - PRODRETR_s) \quad (86)$$

where:

| | | |
|-------------------|---|---|
| $PRODCUR_{old,s}$ | = | Existing production for process step s for old vintage, |
| $IDLCAP_{old,s}$ | = | Idle production at process step s for old vintage, and |
| $PRODRETR_s$ | = | Retirement rate at process step s . |

$$PRODCUR_{mid,s} = (PRODCUR_{mid,s} + PRODCUR_{new,s}) \times (1 - PRODRETR_s) \quad (87)$$

where:

| | | |
|-------------------|---|--|
| $PRODCUR_{mid,s}$ | = | Existing production at process step s for mid vintage, |
| $PRODCUR_{new,s}$ | = | Production at process step s for new vintage, |
| $PRODRETR_s$ | = | Retirement rate at process step s . |

For the non-manufacturing industries, the following two equations are used for old vintage and middle vintage production.

$$PRODCUR_{old,s} = PRODCUR_{old,s} + IDLCAP_{old,s} \quad (88)$$

where:

| | | |
|-------------------|---|--|
| $PRODCUR_{old,s}$ | = | Existing production at process step s for old vintage, and |
| $IDLCAP_{old,s}$ | = | Idle production for process step s for old vintage. |

$$PRODCUR_{mid,s} = PRODCUR_{mid,s} + PRODCUR_{new,s} \quad (89)$$

where:

| | | |
|-------------------|---|--|
| $PRODCUR_{mid,s}$ | = | Existing production at process step s for mid vintage, and |
| $PRODCUR_{new,s}$ | = | Production at process step s for new vintage. |

Total production throughput for the industry is calculated. If the initial UEC is in physical units, the value of output for the current year is multiplied by the fixed ratio of physical units to value of output calculated on the first model run in the subroutine PDATA.

$$PRODX_{i,r} = PHDRAT \times PRODVX_{i,r} \quad (90)$$

where:

| | | |
|----------------|---|---|
| $PRODX_{i,r}$ | = | Value of output in physical units for industry i in Census region r , |
| $PHDRAT$ | = | Ratio of physical units to value of output, and |
| $PRODVX_{i,r}$ | = | Value of output for industry i in Census region r . |

If the initial UEC is in dollar units, then the current year's value of output is used to determine total production throughput.

For each process step that is linked to final consumption, then the total production throughput is calculated by the following procedure:

1. The total production throughput for all vintages is calculated in the following equation by multiplying the down-step throughput to the process step by the value of output.

$$PRODCUR_{total,s} = PRODFLOW_{old,s,l} \times PRODX_{i,r} \quad (91)$$

where:

| | | |
|----------------------|---|---|
| $PRODCUR_{total,s}$ | = | Production at process step s for all vintages, |
| $PRODFLOW_{old,s,l}$ | = | Down-step throughput to process step s by link l for old vintage, and |
| $PRODX_{i,r}$ | = | Value of output for industry i in Census region r . |

2. If the total production throughput for all vintages is greater than the existing old and middle vintage production, then new production must be added. The new production becomes the difference between the total production throughput for all vintages and existing production.

$$PRODCUR_{new,s} = PRODCUR_{total,s} - PRODCUR_{old,s} - PRODCUR_{mid,s} \quad (92)$$

where:

- $PRODCUR_{new,s}$ = New production at process step s for new vintage,
 $PRODCUR_{total,s}$ = Total production at process step s for all vintages,
 $PRODCUR_{old,s}$ = Existing production at process step s for old vintage, and
 $PRODCUR_{mid,s}$ = Existing production at process step s for mid vintage.

Middle vintage production is unaltered.

3. If the total production throughput for all vintages equals existing production, then no new production is installed and middle vintage production is unaltered.
4. If the total production throughput for all vintages is less than existing production, then no new production capacity is installed. Idle production becomes the difference between total production throughput for all vintages and existing production. Idle production is determined through the following equation.

$$IDLCAP_{old,s} = PRODCUR_{old,s} + PRODCUR_{mid,s} - PRODCUR_{total,s} \quad (93)$$

where:

- $IDLCAP_{old,s}$ = Idle production for process step s for old vintage,
 $PRODCUR_{old,s}$ = Existing production at process step s for old vintage,
 $PRODCUR_{mid,s}$ = Existing production at process step s for mid vintage, and
 $PRODCUR_{total,s}$ = Production at process step s for all vintages.

Old vintage production is then reduced by the following equation:

$$PRODCUR_{old,s} = PRODCUR_{old,s} - IDLCAP_{old,s} \quad (94)$$

where:

$$\begin{aligned}
 PRODCUR_{old,s} &= \text{Existing production at process step } s \text{ for old vintage, and} \\
 IDLCAP_{old,s} &= \text{Idle production for process step } s \text{ for old vintage.}
 \end{aligned}$$

If the process step is not linked to final consumption, then the following procedure determines production for the process step:

1. If no new production has been added, then the total production for the current process step is augmented by multiplying the down-step throughput by the total production throughput of the final consumption. This is shown in the following two equations.

$$PRODSUM_{new,s,l} = PRODCUR_{total,IP} \times PRODFLOW_{old,s,l} \quad (95)$$

where:

$$\begin{aligned}
 PRODSUM_{new,s,l} &= \text{Amount of throughput used at process step } s \text{ through} \\
 &\quad \text{link } l \text{ for new vintage,} \\
 PRODCUR_{total,IP} &= \text{Production at process step } IP \text{ linked to process step } s \\
 &\quad \text{through link } l \text{ for all vintages, and} \\
 PRODFLOW_{old,s,l} &= \text{Down-step throughput to process step } s \text{ linked by link } l \\
 &\quad \text{for old vintage.}
 \end{aligned}$$

$$PRODCUR_{total,s} = PRODCUR_{total,s} + PRODSUM_{new,s,l} \quad (96)$$

where:

$$PRODCUR_{total,s} = \text{Production at process step } s \text{ for all vintages, and}$$

$PRODSUM_{new,s,l}$ = Amount of throughput used at process step s through link l for new vintage.

If the current link is the last link for the process step, then there is no new capital installed. Production for old vintage becomes the difference between the total for all vintages and the production for middle vintage.

$$PRODCUR_{old,s} = PRODCUR_{total,s} - PRODCUR_{mid,s} \quad (97)$$

where:

$PRODCUR_{old,s}$ = Existing production at process step s for old vintage,
 $PRODCUR_{total,s}$ = Production at process step s for all vintages, and
 $PRODCUR_{mid,s}$ = Existing production at process step s for mid vintage.

If the production for old vintage is less than zero, then all of the old and part of the middle vintage production is retired. If the production for middle vintage is less than zero, then the remaining middle vintage production is retired.

2. If new production is added, then production is augmented by multiplying the down-step throughput to the current process step through the current link as shown in the equations below.

$$PRODSUM_{new,s,l} = PRODCUR_{new,JP} \times PRODFLOW_{new,s,l} \quad (98)$$

where:

$PRODSUM_{new,s,l}$ = Amount of throughput used at process step s through link l for new vintage,

$PRODCUR_{new,IP}$ = Production at process step IP linked to process step s through link l for new vintages, and

$PRODFLOW_{new,s,l}$ = Down-step throughput to process step s linked by link l for new vintage.

$$PRODCUR_{new,s} = PRODCUR_{new,s} + PRODSUM_{new,s,l} \quad (99)$$

where:

$PRODCUR_{new,s}$ = Production at process step s for new vintage, and

$PRODSUM_{new,s,l}$ = Amount of throughput used at process step s through link l for new vintage.

If the current link is the last link for the process step, then middle vintage production is unaltered.

If the new production at the first process step is not zero, then the total production at a particular process step is determined by summing the production for old, middle, and new vintage.

Subroutine CALCSC

CALCSC is called to update unit energy consumption. CALCSC calls one of three subroutines, CALCSC1, CALCSC2, or CALCSC3 depending on the type of approach for a particular fuel, process step, and industry. CALCSC1 maintains constant UECs. CALCSC2 applies the econometric approach for non-energy-intensive industries. CALCSC3 applies the engineering approach for energy-intensive industries.

Subroutine CALCSC1

CALCSC1 updates UECs based on the previous year's UEC. Unit energy consumption for each fuel, process step, and vintage is updated in the equation below. This approach yields constant UECs over time.

$$ENPINT_{v,f,s} = ENPINTLAG_{v,f,s} \quad (100)$$

where:

$ENPINT_{v,f,s}$ = Unit energy consumption of fuel f at process step s for vintage v , and

$ENPINTLAG_{v,f,s}$ = Lagged unit energy consumption of fuel f at process step s for vintage v .

Subroutine CALCSC2

CALCSC2 updates UECs through an econometrically estimated equation. Energy savings, or the location on the technology possibility curve, is calculated in the following equation for old and new vintage and is based on the total cumulative output raised to the coefficient.

$$CSCCUR_{v,f,s} = [CUMOUT_{total,s}]^{BCSC_{v,f,s}} \quad (101)$$

where:

$CSCCUR_{v,f,s}$ = Current energy savings at process step s for fuel f for vintage v ,

- $CUMOUT_{total,s}$ = Cumulative output, from 1958 through the lag of the current year, at process step s for all vintages, and
- $BCSC_{v,f,s}$ = Energy savings coefficient at process step s for fuel f and vintage v .

As noted on page 121, CUMOUT is calculated in RDBIN.

The unit energy consumption for old and new vintage is calculated by multiplying the intercept term calculated in CALINTER by the current energy savings.

$$ENPINT_{v,f,s} = EINTER_{v,f,s} \times CSCCUR_{v,f,s} \quad (102)$$

where:

- $ENPINT_{v,f,s}$ = Unit energy consumption of fuel f at process step s for vintage v ,
- $EINTER_{v,f,s}$ = Intercept at process step s for fuel f for vintage v , and
- $CSCCUR_{v,f,s}$ = Current energy savings at process step s for fuel f for vintage v .

The UEC for middle vintage is computed in the following equation as the ratio of the cumulative unit energy consumption to cumulative production for new vintage, i.e., it is simply the weighted average UEC.

$$ENPINT_{mid,f,s} = \frac{SUMPINT_{f,s}}{CUMPROD_{new,s}} \quad (103)$$

where:

| | | |
|--------------------|---|--|
| $ENPINT_{mid,f,s}$ | = | Unit energy consumption of fuel f at process step s for mid vintage, |
| $SUMPINT_{f,s}$ | = | Cumulative unit energy consumption of fuel f at process step s , and |
| $CUMPROD_{new,s}$ | = | Cumulative production at process step s for new vintage. |

As noted on page 121, the cumulative variables are calculated in RDBIN.

Subroutine CALCSC3

CALCSC3 computes UECs according to an approach suggested by Arthur D. Little (ADL). The energy savings for old and new vintage is calculated below as the exponential of the TPC coefficient multiplied by a yearly index.

$$CSCCUR_{v,f,s} = e^{BCSC_{v,f,s} \times (CURIYR - 1)} \quad (104)$$

where:

| | | |
|------------------|---|---|
| $CSCCUR_{v,f,s}$ | = | Current energy savings ($0 < \text{fraction} < 1$) at process step s for fuel f for vintage v , |
| $BCSC_{v,f,s}$ | = | Energy savings coefficient at process step s for fuel f and vintage v , and |
| $CURIYR$ | = | Current year index. |

The unit energy consumption for old and new vintage is computed as in CALCSC2 by multiplying the current energy savings by the intercept. In a few process steps, fuel shares are expected to change over time due to technology changes. These process steps are cold rolling, blast furnaces, and electric arc furnaces in the blast furnace and basic steel products industry and dry process clinker in the hydraulic

cement industry. The following equation calculates the unit energy consumption of electricity in the cold rolling process step. Similar equations exist for other fuels used in cold rolling and for the blast furnace/basic oxygen furnace process step (see Table E-8, Appendix E).

$$ENPINT_{new,elec,s} = EINTER_{new,elec,s} \times CSCCUR_{new,elec,s} \times \frac{1}{0.20} \left[0.20 + \frac{(0.21 - 0.20) \times (CURIYR - 1)}{25} \right] \quad (105)$$

where:

- $ENPINT_{new,elec,s}$ = Unit energy consumption of electricity at process step s for new vintage,
- $EINTER_{new,elec,s}$ = Intercept at process step s for electricity for new vintage,
- $CSCCUR_{new,elec,s}$ = Current energy savings at process step s for electricity and new vintage, and
- $CURIYR$ = Current year index.

The UECs for middle vintage are calculated as in CALCSC2 and shown below, by the ratio of cumulative UEC to cumulative production for all process steps and industries, i.e., the weighted average UEC.

$$ENPINT_{mid,f,s} = \frac{SUMPINT_{f,s}}{CUMPROD_{new,s}} \quad (106)$$

where:

- $ENPINT_{mid,f,s}$ = Unit energy consumption of fuel f at process step s for middle vintage,
- $SUMPINT_{f,s}$ = Cumulative unit energy consumption of fuel f at process step s , and
- $CUMPROD_{new,s}$ = Cumulative production at process step s for new vintage.

Subroutine CALPRC

CALPRC is called to update unit energy consumption based on price parameters. CALPRC calls one of the three subroutines CALPRC1, CALPRC2, or CALPRC3, depending on the approach to be taken. CALPRC1 assumes unit energy consumption is constant. CALPRC2 uses an econometric equation to update UECs. CALPRC3 is currently not implemented.

Subroutine CALPRC1

The unit energy consumption is unaltered by CALPRC1.

Subroutine CALPRC2

CALPRC2 calculates unit energy consumption based on price related conservation using an econometric equation. Average prices for each fuel are calculated to accommodate the equation. Price based energy savings is calculated below as the product of the average price of a particular fuel raised to each cross price elasticity for both old and new vintage.

$$PRCCUR_{v,f,s} = \prod_{t=1}^{11} [WPRC_t]^{BELAS_{v,f,s,t}} \quad (107)$$

where:

| | | |
|-------------------|---|---|
| $PRCCUR_{v,f,s}$ | = | Current energy savings based on price for fuel f at process step s for vintage v , |
| $WPRC_t$ | = | Price for fuel t in 1987 dollars, and |
| $BELAS_{v,f,s,t}$ | = | Own price elasticity at process step s for fuel f for old vintage and cross price elasticity at process step s for fuel f and fuel t for old vintage. |

Unit energy consumption is then computed by multiplying the unit energy consumption by the price based energy savings.

$$ENPINT_{v,f,s} = ENPINT_{v,f,s} \times PRCCUR_{v,f,s} \quad (108)$$

where:

$ENPINT_{v,f,s}$ = Unit energy consumption of fuel f at process step s for vintage v , and

$PRCCUR_{v,f,s}$ = Current energy savings based on price for fuel f at process step s for vintage v .

Subroutine CALBSC

CALBSC calculates boiler fuel shares for the current year. Boiler fuel shares are based on the previous year's boiler fuel share, the ratio of the current year's price to the previous year's price, and cross price elasticities as shown in the following two equations.

$$BSSHR_f = BSSHRLAG_f \times \left[\frac{PRCX_{f,r}}{PRCXLAG_f} \right]^{BSSHRE_f} \times \left[\frac{PRCX_{ng,r}}{PRCXLAG_{ng}} \right]^{BSSHRNG_f} \times \left[\frac{PRCX_{oil,r}}{PRCXLAG_{oil}} \right]^{BSSHROIL_f} \times \left[\frac{PRCX_{coal,r}}{PRCXLAG_{coal}} \right]^{BSSHRCL_f} \quad (109)$$

where:

$BSSHR_f$ = Share of total fuel consumption in the BSC component for fuel f ,

$BSSHRLAG_f$ = Lagged boiler share for fuel f ,

$PRCX_{f,r}$ = Price for fuel f in Census region r ,

| | | |
|--------------|---|---|
| $PRCXLG_f$ | = | Lagged price for fuel f , |
| $BSSHRE_f$ | = | Own price elasticity for fuel f , |
| $BSSHRNG_f$ | = | Cross price elasticity of natural gas with fuel f , |
| $BSSHROIL_f$ | = | Cross price elasticity of oil with fuel f , and |
| $BSSHRCL_f$ | = | Cross price elasticity of steam coal with fuel f . |

The boiler shares are normalized to make sure that when less of a particular fuel is consumed in the boiler, that the same amount is picked up by some other fuel.

$$BSSHR_f = \frac{BSSHR_f}{IFSMAX \sum_{f=1} BSSHR_f} \quad (110)$$

where:

| | | |
|-----------|---|---|
| $BSSHR_f$ | = | Share of total fuel consumption in the BSC component for fuel f , and |
| $IFSMAX$ | = | Number of fuels consumed in the BSC component. |

Appendix A. Data Sources, Input Parameters, Model Variables

Introduction

This appendix describes the module inputs, module parameters, and output variables for the Industrial model. A list of the subscripts used in variable definitions and equations is provided in Table A-1. The variable list in Table A-2 references the module inputs, module parameters, and module outputs. Each item is accompanied by its definition as well as its dimensions.

Table A-3 categorizes each item listed in Table A-2 as "Module Inputs", "Module Parameters", "Calculated Variable", or "Module Outputs". This table also lists the equation reference to link variables in Table A-2 to the equations represented in Appendix B. Table A-3 provides the units of measurement where applicable for each variable.

The remainder of this appendix contains supporting discussion on the input data, including the sources of the data and any transformations occurring offline.

Table A-1. Subscript Definitions

| Subscript | Definition | Possible values |
|-----------|------------------|---|
| <i>d</i> | Census division | <i>d</i> = 1, ..., 9 |
| <i>e</i> | Building end use | <i>e</i> = 1 lighting 2 HVAC |
| <i>f</i> | Fuel | <p>Main fuels</p> <p><i>f</i> = 1 electricity 2 cogenerated electricity 3 core natural gas 4 non-core natural gas 5 feedstock natural gas 6 lease and plant natural gas 7 steam coal 8 coking coal 9 net coke imports 10 residual oil 11 distillate oil 12 liquid petroleum gas for heat and power 13 liquid petroleum gas for feedstocks 14 motor gasoline 15 still gas 16 petroleum coke 17 asphalt and road oil 18 lubes and waxes 19 petrochemical feedstocks 20 kerosene 21 other petroleum feedstocks 22 other petroleum</p> <p>Intermediate fuels</p> <p><i>f</i> = 1 steam 2 coke oven gas 3 blast furnace gas 4 other byproduct gas 5 waste heat 6 coke</p> <p>Renewable fuels</p> <p><i>f</i> = 1 hydropower 2 biomass-wood 3 biomass-pulping liquor 4 geothermal 5 solar 6 photovoltaic 7 wind 8 municipal solid waste</p> |

| Subscript | Definition | Possible values |
|-----------|--|--|
| <i>i</i> | Industry | <i>i</i> = 1 agriculture - crops 2 agriculture - other 3 coal mining 4 oil and gas mining 5 metal and other non-metallic mining 6 construction 7 food and kindred products 8 tobacco products 9 textile mill products 10 apparel and other textile products 11 lumber and wood products 12 furniture and fixtures 13 paper and allied products 14 printing and publishing 15 bulk chemicals 19 other chemicals and allied products 20 petroleum refining 21 asphalt and miscellaneous coal products 22 rubber and miscellaneous plastics products 23 leather and leather products 24 glass and glass products 25 cement, hydraulic 26 other stone, clay, and glass products 27 blast furnace and basic steel products 28 primary aluminum 29 other primary metals 30 fabricated metals 31 industrial machinery 32 electronic and other electric equipment 33 transportation equipment 34 instruments and related products 35 miscellaneous manufacturing industries |
| <i>l</i> | Link | <i>l</i> = 1, ..., NTMAX _{<i>i</i>} |
| <i>m</i> | Prime mover | <i>m</i> = 1 internal combustion engine 2 combustion turbine 3 steam turbine 4 renewables |
| <i>p</i> | Pollutant | <i>p</i> = 1 carbon 2 carbon monoxide 3 carbon dioxide 4 methane 5 sulfur dioxide 6 nitrogen oxide 7 volatile organic compounds 8 particulates |
| <i>r</i> | Census region | <i>r</i> = 1, ..., 4 |
| <i>s</i> | Process step | <i>s</i> = 1, ..., MPASTP |
| <i>t</i> | Fuel type for cross price elasticities | <i>t</i> = 1 own price 2 electricity 3 natural gas 4 steam coal 5 petroleum oil 6 motor gasoline 7 asphalt 8 other petroleum 9 liquid petroleum gas 10 distillate oil 11 residual oil |

| Subscript | Definition | Possible values |
|-----------|--------------------------------|--|
| u | Use of cogenerated electricity | $u =$ 1 sales to the grid 2 own use |
| v | Vintage | $v =$ 1 old 2 middle 3 new |
| y | Year | $y =$ 1990,...,2010 |

Table A-2. NEMS Industrial Sector Model Variables

| Model Variable | Definition and Dimensions | Page Reference |
|-----------------------|---|--|
| <i>ALUMCON</i> | Consumption of fuel <i>f</i> from the primary aluminum industry in year <i>y</i> | A-22, B-95 |
| <i>AVGINT</i> | Average intensity | 92, 94, A-19, B-42, B-44 |
| <i>BCSC</i> | Energy savings coefficient at process step <i>s</i> for fuel <i>f</i> and vintage <i>v</i> | 84, 130, 131, A-19, A-25, A-42, B-18, B-19, B-31 |
| <i>BELAS</i> | Own price elasticity at process step <i>s</i> for fuel <i>f</i> for vintage <i>v</i> and cross price elasticity at process step <i>s</i> for fuel <i>f</i> and fuel <i>t</i> for vintage <i>v</i> | 84, 134, A-19, A-27, B-30, B-31 |
| <i>BENCHFAC</i> | Benchmark factor for fuel <i>f</i> in Census division <i>d</i> | 110, 116, 117, 121, A-19, B-87, B-96, B-97, B-100, B-101 |
| <i>BIOFUELS</i> | Consumption of biofuels in Census division <i>d</i> | 121, A-19, B-101 |
| <i>BMAIN</i> | Consumption of main fuel <i>f</i> in Census division <i>d</i> | 108 to 111, 116, 117, 120, 121, A-19, B-82 to B-88, B-95 to B-97, B-100, B-101 |
| <i>BOILSTEAM</i> | Steam generated from boilers | 90, A-19, B-39 |
| <i>BSSHR</i> | Share of total fuel consumption in the BSC component for fuel <i>f</i> | 92, 94, 134, A-16, A-28, B-43, B-44, B-47, B-48 |
| <i>BSSHRCL</i> | Cross price elasticity for steam coal with fuel <i>f</i> | 135, A-19, A-29, B-47 |
| <i>BSSHRE</i> | Own price elasticity for fuel <i>f</i> | 135, A-19, A-31, B-47 |
| <i>BSSHRLAG</i> | Lagged boiler share for fuel <i>f</i> | 135, A-19, B-47 |
| <i>BSSHRNG</i> | Cross price elasticity for natural gas with fuel <i>f</i> | 135, A-19, A-33, B-47 |
| <i>BSSHROIL</i> | Cross price elasticity for oil with fuel <i>f</i> | 135, A-19, A-35, B-47 |
| <i>BYPBSCI</i> | Byproduct consumption of intermediate fuel <i>f</i> in the BSC component | 93, A-19, B-43 |
| <i>BYPBSCM</i> | Byproduct consumption of main fuel <i>f</i> in the BSC component | 93, 96, A-19, B-43, B-67 |
| <i>BYPBSCR</i> | Byproduct consumption of renewable fuel <i>f</i> in the BSC component | 93, A-19, B-43, B-67 |
| <i>BYPCSC</i> | Byproduct technology possibility curve coefficient for byproduct fuel <i>f</i> at process step <i>s</i> for vintage <i>v</i> | 76, A-19, A-37, B-61 |
| <i>BYPCSCCUR</i> | Current energy savings for byproduct fuel <i>f</i> at process step <i>s</i> for vintage <i>v</i> | 76 to 78, A-19, B-61, B-62 |
| <i>BYPCSCLAG</i> | Lagged energy savings for byproduct fuel <i>f</i> at process step <i>s</i> for vintage <i>v</i> | 77, A-19, B-62 |

| Model Variable | Definition and Dimensions | Page Reference |
|------------------|--|---|
| <i>BYPINT</i> | Rate of byproduct energy production for byproduct fuel <i>f</i> at process step <i>s</i> for vintage <i>v</i> | 77, 78, A-16, A-38, B-62, B-63 |
| <i>BYPINTLAG</i> | Lagged rate of byproduct energy production for byproduct fuel <i>f</i> at process step <i>s</i> for vintage <i>v</i> | 78, A-19, B-62 |
| <i>BYPQTY</i> | Byproduct energy production for byproduct fuel <i>f</i> at process step <i>s</i> for vintage <i>v</i> | 78, 79, A-19, B-63 to B-65 |
| <i>BYPSTM</i> | Amount of steam generated from all byproduct fuels | 92, 93, A-19, B-43, B-44 |
| <i>BYSINT</i> | Intensity for byproduct fuel <i>f</i> consumed in the BSC component | 93, A-16, A-39, B-43 |
| <i>BYSQTY</i> | Consumption of byproduct fuel <i>f</i> in the BSC component | 95, A-19, B-45, B-46 |
| <i>CAPD</i> | Existing or planned capacity for cogeneration of electricity for use <i>u</i> in Census division <i>d</i> using fuel <i>f</i> in year <i>y</i> | 101, 102, 105, 106, A-19, B-50, B-51, B-53, B-56, B-57 |
| <i>CAPDIV</i> | Planned capacity for electricity generation for use <i>u</i> in Census division <i>d</i> using fuel <i>f</i> in year <i>y</i> | 102, A-20, B-51 |
| <i>CAPGW</i> | Planned or unplanned capacity for cogeneration of electricity for use <i>u</i> using fuel <i>f</i> in Census division <i>d</i> | 103, 105, 106, 113, A-20, B-54 to B-57, B-90 |
| <i>CAPGWL</i> | Lagged planned or unplanned capacity for cogeneration of electricity for use <i>u</i> using fuel <i>f</i> in Census division <i>d</i> | 105, A-20, B-56 |
| <i>CAPREG</i> | Existing or planned capacity for cogeneration of electricity for use <i>u</i> in Census region <i>r</i> using fuel <i>f</i> in year <i>y</i> | 102, A-16, A-40, B-49, B-50 |
| <i>CEMENTCON</i> | Consumption of fuel <i>f</i> by the hydraulic cement industry in year <i>y</i> | A-22, B-94 |
| <i>CGFUEL</i> | Consumption of fuel <i>f</i> for cogeneration of electricity for use <i>u</i> in Census region <i>r</i> | 91, A-20, B-39 to B-42 |
| <i>CGINDCAP</i> | Industrial capacity for cogeneration for use <i>u</i> using fuel <i>f</i> in Census division <i>d</i> in year <i>y</i> | 113, A-22, B-90 |
| <i>CGINDGEN</i> | Industrial cogeneration of electricity for use <i>u</i> using fuel <i>f</i> in Census division <i>d</i> in year <i>y</i> | A-22, B-91 |
| <i>CGINDQ</i> | Industrial consumption of fuel <i>f</i> for cogeneration of electricity for use <i>u</i> in Census division <i>d</i> in year <i>y</i> | 114, A-22, B-91 |
| <i>CGOGCAP</i> | Oil and gas capacity for cogeneration for use <i>u</i> using fuel <i>f</i> in Census division <i>d</i> in year <i>y</i> | 113, A-16, B-90 |
| <i>CGOGGEN</i> | Oil and gas cogeneration of electricity for use <i>u</i> using fuel <i>f</i> in Census division <i>d</i> in year <i>y</i> | A-16, B-91 |
| <i>CGOGQ</i> | Consumption of fuel <i>f</i> from cogeneration of electricity for use <i>u</i> in enhanced oil recovery in Census division <i>d</i> in year <i>y</i> | 108, 109, 112, 114, 115, A-16, B-83, B-84, B-89, B-91, B-92 |

| Model Variable | Definition and Dimensions | Page Reference |
|-----------------|---|--|
| <i>CGRECAP</i> | Refinery capacity for cogeneration for use u using fuel f in Census division d in the year y | 113, A-16, B-90 |
| <i>CGREGEN</i> | Refinery cogeneration of electricity for use u using fuel f in Census division d in year y | A-16, B-91 |
| <i>CGREQ</i> | Consumption of fuel f from cogeneration of electricity for use u in refineries in Census division d in year y | 114, A-16, B-91 |
| <i>CHEMCON</i> | Consumption of fuel f by the chemical industry in year y | A-23, B-93 |
| <i>COPRCLG</i> | Supply of coal gases in Census division d in year y | 109, A-16, B-83 |
| <i>COPRCLQ</i> | Supply of coal liquids in Census division d in year y | 109, A-16, B-83 |
| <i>CSCCUR</i> | Current energy savings at process step s for fuel f for vintage v | 129 to 132, A-20, A-48, B-17 to B-29 |
| <i>CUMOUT</i> | Cumulative output, from 1958 through the lag of the current year, at process step s for all vintages | 130, A-20, B-17 |
| <i>CUMOUT88</i> | Cumulative output through the year 1988 | 84, A-16, A-41, B-31 |
| <i>CUMPROD</i> | Cumulative production at process step s for vintage v | 131, 132, A-20, B-18, B-29 |
| <i>DEMIMAIN</i> | Emissions of pollutant p from main fuel f in Census division d | 115 to 119, A-20, B-95 to B-98 |
| <i>DEMIRENW</i> | Emissions of pollutant p from renewable fuel f in Census division d | 118, A-20, B-98, B-99 |
| <i>DIVFUEL</i> | Consumption of fuel f for cogeneration of electricity for use u in Census division d | 103, 104, 114, A-20, B-52 to B-55, B-91 |
| <i>DIVSHARE</i> | Electricity share for Census division d | 102 to 104, A-16, B-50, B-52 to B-55 |
| <i>DQMAIN</i> | Consumption of main fuel f in Census division d | 107 to 111, 116, 117, A-20, B-81 to B-86, B-88, B-96, B-97 |
| <i>DQRENW</i> | Consumption of renewable fuel f in Census division d | 112, 121, A-20, B-82, B-89, B-101 |
| <i>DSRENW</i> | Share of output for renewable fuel f in Census division d | 107, 118, A-20, A-42, B-81, B-82, B-98 |
| <i>EINTER</i> | Intercept at process step s for fuel f for vintage v | 84, 130, 132, A-16, A-42, A-48, B-18 to B-30 |
| <i>ELCAP</i> | Capacity for electricity generation | 87, A-20, B-34, B-37 |
| <i>ELCTOT</i> | Capacity for industrial electricity generation in Census region r | 103, A-20, B-37, B-48, B-54, B-55 |
| <i>ELDEM</i> | Total electricity demand from process/assembly and buildings | 85, A-20, B-32 |
| <i>ELGEN</i> | Electricity generation from prime mover m | 86 to 91, 95, A-20, B-33 to B-35, B-37, B-38, B-41, B-45 |
| <i>ELTOT</i> | Total industrial electricity generation for own use in Census region r | 102 to 104, A-20, B-36, B-48, B-50, B-51, B-53 to B-55 |

| Model Variable | Definition and Dimensions | Page Reference |
|------------------------|---|--|
| <i>ELOWN</i> | Electricity generation for own use | 88, 91, 96, A-20, B-35, B-36, B-40, B-65 |
| <i>ELSALE</i> | Electricity generation for sales to the grid | A-20, B-35, B-36 |
| <i>ELSTOT</i> | Total industrial electricity generation for sales to the grid in Census region <i>r</i> | 102, 104, A-20, B-36, B-49 to B-51, B-54, B-55 |
| <i>EMINC</i> | Industrial emissions of pollutant <i>p</i> from fuel <i>f</i> in year <i>y</i> | 119, A-23, B-99 |
| <i>EMINCC</i> | Industrial emissions of pollutant <i>p</i> in Census division <i>d</i> in year <i>y</i> | A-20, B-100 |
| <i>EMINCX</i> | Emissions of pollutant <i>p</i> from fuel <i>f</i> in Census division <i>d</i> in year <i>y</i> | 119, A-20, B-98 to B-100 |
| <i>EMIRENW</i> | Emissions of pollutant <i>p</i> from renewable fuel <i>f</i> in Census region <i>r</i> | 97 to 99, A-20, B-71 to B-73 |
| <i>EMISSCONTROLFAC</i> | Emission control factor for pollutant <i>p</i> using fuel <i>f</i> | 98, 116 to 118, A-16, A-44, B-71, B-95 to B-97 |
| <i>EMPIND</i> | Employment for industry <i>i</i> in Census division <i>d</i> | A-16, B-60 |
| <i>EMPLX</i> | Employment for industry <i>i</i> in Census region <i>r</i> | 84, A-20, B-4, B-60, B-61 |
| <i>ENBINT</i> | Unit energy consumption of fuel <i>f</i> for building end use <i>e</i> | 85, A-16, A-45, B-4 |
| <i>ENBQTY</i> | Consumption of fuel <i>f</i> for building end use <i>e</i> | 84, 85, 96, A-20, B-4, B-32, B-65 to B-67 |
| <i>ENBYPI</i> | Byproduct energy production for intermediate byproduct fuel <i>f</i> for vintage <i>v</i> | A-20, B-64 |
| <i>ENBYPM</i> | Byproduct energy production for main fuel <i>f</i> for vintage <i>v</i> | 79, A-20, B-64 |
| <i>ENBYPR</i> | Byproduct energy production for renewable byproduct fuel <i>f</i> for vintage <i>v</i> | A-20, B-65 |
| <i>ENPINT</i> | Unit energy consumption of fuel <i>f</i> at process step <i>s</i> for vintage <i>v</i> | 79, 80, 84, 129 to 134, A-16, A-47, B-5, B-6, B-17 to B-31 |
| <i>ENPINLAG</i> | Lagged unit energy consumption of fuel <i>f</i> at process step <i>s</i> for vintage <i>v</i> | 129, A-20, A-47, B-17 |
| <i>ENPIQTY</i> | Consumption of intermediate fuel <i>f</i> in the PA component | 83, 85, A-20, B-9, B-32, B-67 |
| <i>ENPMQTY</i> | Consumption of main fuel <i>f</i> in the PA component | 82, 83, 85, 95, 96, A-21, B-8, B-9, B-32, B-66 |
| <i>ENPQTY</i> | Consumption of fuel <i>f</i> at process step <i>s</i> for vintage <i>v</i> | 79, 80, 82, A-21, B-5 to B-9 |
| <i>ENPRQTY</i> | Consumption of renewable fuel <i>f</i> in the PA component | A-21, B-9, B-67 |
| <i>ENSINT</i> | Intensity of fuel <i>f</i> in the BSC component | 92, A-16, A-49, B-43 |
| <i>ENSQTY</i> | Consumption of fuel <i>f</i> to generate steam | 94 to 96, A-21, B-44 to B-46, B-66, B-67 |
| <i>FOODCON</i> | Consumption of fuel <i>f</i> by the food and kindred products industry in year <i>y</i> | A-23, B-93 |

| Model Variable | Definition and Dimensions | Page Reference |
|--------------------|---|---|
| <i>FUELSHARE</i> | Share of consumption for fuel <i>f</i> in Census division <i>d</i> | 106, 108, A-21, B-82 |
| <i>GCTFUEL</i> | Fuel consumption for electricity generation from combustion turbines | A-21, B-37, B-38, B-40, B-45, B-46 |
| <i>GCTSTEAM</i> | Cogeneration of steam from combustion turbines | 90, A-21, B-38, B-39 |
| <i>GEN90</i> | 1990 generation of electricity | 86, A-16, A-50, B-33 |
| <i>GENEQPHTRT</i> | Heat rate for prime mover <i>m</i> | 89, 95, A-16, A-51, B-37, B-45 |
| <i>GENEQPSHR</i> | Share of generation for prime mover <i>m</i> | 88, A-16, A-52, B-36 |
| <i>GENEQPSTEFF</i> | Efficiency for prime mover <i>m</i> | 90, A-16, A-53, B-38 |
| <i>GENGWH</i> | Cogeneration of electricity for use <i>u</i> using fuel <i>f</i> in Census division <i>d</i> | 104, A-21, B-53, B-54, B-57, B-91 |
| <i>GENTOT</i> | Total consumption of fuel <i>f</i> for cogeneration of electricity for use <i>u</i> in Census region <i>r</i> | 103, A-21, B-42, B-49, B-52 |
| <i>GENUTIL</i> | Capacity utilization for cogeneration | 87, A-16, A-54, B-34 |
| <i>GINTER</i> | Intercept for electricity generation | 86, A-21, B-33 |
| <i>GLASSCON</i> | Consumption of fuel <i>f</i> by the glass and glass products industry in year <i>y</i> | A-23, B-94 |
| <i>GSTEAM</i> | Steam demand coefficient | 86, A-19, A-55, B-33 |
| <i>ICEFUEL</i> | Fuel consumption for electricity generation from internal combustion engines | 89 to 91, 94, A-21, B-37 to B-39, B-45, B-46 |
| <i>ICESTEAM</i> | Cogeneration of steam from internal combustion engines | 89, 90, A-21, B-38, B-39 |
| <i>IDLCAP</i> | Idle production for process step <i>s</i> for vintage <i>v</i> | 122, 123, 125, 126, A-21, B-10, B-11, B-13 |
| <i>IDVAL</i> | Units of value of production | A-16, A-56 |
| <i>IFBYP</i> | Number of byproducts consumed at process step <i>s</i> | A-17, B-64 |
| <i>IFMAX</i> | Number of fuels consumed at process step <i>s</i> | A-17, B-8 |
| <i>IFSBYP</i> | Number of byproducts consumed in the BSC component | 95, A-17, B-45, B-46 |
| <i>IFSBYPI</i> | Number of byproduct intermediate fuels | 93, A-21, B-43 |
| <i>IFSBYPM</i> | Number of byproduct main fuels | 93, A-21, B-43 |
| <i>IFSBYPR</i> | Number of byproduct renewable fuels | 93, A-21, B-43 |
| <i>IFSMAX</i> | Number of fuels consumed in the BSC component | 92, 95, 135, A-17, B-42, B-45, B-46, B-48 |
| <i>INDDIR</i> | Industry code | A-17, A-57 |
| <i>INDMAX</i> | Number of industries | 97, 99, 100, A-17, B-36, B-37, B-42, B-73 to B-75 |
| <i>INDNAME</i> | Industry name | A-17 |
| <i>INDNUM</i> | Industry index number | A-17 |
| <i>INDREG</i> | Census region for the industry | A-17 |

| Model Variable | Definition and Dimensions | Page Reference |
|-----------------------|--|---|
| <i>INDSTEPNAME</i> | Step name for process step <i>s</i> | A-17, A-59 |
| <i>IPASTP</i> | Process step linked to process step <i>s</i> by link <i>l</i> | A-17 |
| <i>ISTP</i> | Process step number | A-17 |
| <i>ITYPE</i> | Equation type for fuel <i>f</i> at process step <i>s</i> | A-17, A-62 |
| <i>MANHP</i> | Consumption of fuel <i>f</i> for manufacturing heat and power in year <i>y</i> | 114, A-23, B-92 |
| <i>MC_MFGO</i> | Gross value of output for manufacturing industry <i>i</i> in Census division <i>d</i> in year <i>y</i> | A-17, B-58 |
| <i>MC_NMFGO</i> | Gross value of output for non-manufacturing industry <i>i</i> in Census division <i>d</i> in year <i>y</i> | A-17, B-58 |
| <i>MISCFD</i> | Consumption of miscellaneous fuels and feedstocks <i>f</i> in year <i>y</i> | A-23, B-92 |
| <i>MPASTP</i> | Number of process steps | 79, 82, A-3, A-17, B-8, B-9, B-64, B-65 |
| <i>MSEDYR</i> | Index of SEDS years | 109, A-17, B-86 |
| <i>NONHP</i> | Consumption of fuel <i>f</i> for non-manufacturing heat and power in year <i>y</i> | 115, A-23, B-92 |
| <i>NSTEP</i> | Process step number | A-17 |
| <i>NTMAX</i> | Number of links for process step <i>s</i> | 75, A-3, A-17, B-104 |
| <i>OGEN</i> | Own use generation coefficient | 88, A-19, A-63, B-34, B-35 |
| <i>OINTER</i> | Intercept for own use generation | 88, A-21, B-34, B-35 |
| <i>OTHIND</i> | Consumption of fuel <i>f</i> for "other industry" in Census division <i>d</i> | 109 to 111, 116, 117, 121, A-21, B-86, B-87, B-88, B-95 to B-97, B-101, B-102 |
| <i>OUTIND</i> | Gross value of output for industry <i>i</i> in Census division <i>d</i> | 107, A-21, B-58, B-60, B-80 |
| <i>OWN90</i> | 1990 electricity generation for own use | 88, A-17, A-64, B-34 |
| <i>PAPERCON</i> | Consumption for fuel <i>f</i> by the paper and allied products industry in year <i>y</i> | A-23, B-93 |
| <i>PCLIN</i> | Industrial price of steam coal for Census division <i>d</i> in year <i>y</i> | A-17 |
| <i>PDSIN</i> | Industrial price of distillate for Census division <i>d</i> in year <i>y</i> | A-17 |
| <i>PELIN</i> | Industrial price of electricity for Census division <i>d</i> in year <i>y</i> | A-17 |
| <i>PGFIN</i> | Industrial price of core natural gas in Census division <i>d</i> in year <i>y</i> | A-17 |
| <i>PGIIN</i> | Industrial price of non-core natural gas in Census division <i>d</i> in year <i>y</i> | A-17 |
| <i>PHDRAT</i> | Ratio of physical units to value of output | 73, 124, A-17, A-65, B-11, B-102 |
| <i>PKSIN</i> | Industrial price of kerosene in Census division <i>d</i> in year <i>y</i> | A-17 |

| Model Variable | Definition and Dimensions | Page Reference |
|-----------------|---|---|
| <i>PLGIN</i> | Industrial price of liquid petroleum gas in Census division <i>d</i> in year <i>y</i> | A-17 |
| <i>PLPIN</i> | Industrial price of lease and plant fuel in Census division <i>d</i> in year <i>y</i> | A-17 |
| <i>PMGIN</i> | Industrial price of metallurgical coal in Census division <i>d</i> in year <i>y</i> | A-17 |
| <i>PMGIN</i> | Industrial price of motor gasoline in Census division <i>d</i> in year <i>y</i> | A-17 |
| <i>PNGIN</i> | Industrial price of natural gas in Census division <i>d</i> in year <i>y</i> | A-17 |
| <i>POTIN</i> | Industrial price of other petroleum in Census division <i>d</i> in year <i>y</i> | A-17 |
| <i>PRCCUR</i> | Current energy savings based on price for fuel <i>f</i> at process step <i>s</i> for vintage <i>v</i> | 133, 134, A-21, B-30 |
| <i>PRCX</i> | Price for fuel <i>f</i> in Census region <i>r</i> | 69, 135, A-21, B-47, B-59 |
| <i>PRCXLG</i> | Lagged price of fuel <i>f</i> | 135, A-21, B-47 |
| <i>PRLIN</i> | Industrial price of low sulfur residual fuel in Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>PRODCUR</i> | Production at process step <i>s</i> for vintage <i>v</i> | 74 to 80, 83, 122 to 128, A-21, B-5, B-6, B-9 to B-16, B-61 to B-63, B-103, B-104 |
| <i>PRODFLOW</i> | Down-step throughput to process step <i>s</i> linked by link <i>l</i> for vintage <i>v</i> | 74, 124, 126, 128, A-18, A-66, B-12, B-14, B-16, B-103, B-104 |
| <i>PRODLG</i> | Lagged production at process step <i>s</i> and vintage <i>v</i> | 76, A-21, B-61 |
| <i>PRODRETR</i> | Retirement rate at process step <i>s</i> | 122, 123, A-18, A-67, B-10 |
| <i>PRODSUM</i> | Amount of throughput used at process step <i>s</i> through link <i>l</i> for vintage <i>v</i> | 74, 75, 126 to 128, A-21, B-14, B-16, B-103, B-104 |
| <i>PRODVX</i> | Value of output for industry <i>i</i> in Census region <i>r</i> | 73, 124, A-18, B-11, B-12, B-60, B-102, B-103 |
| <i>PRODX</i> | Output in either physical units or dollar units for industry <i>i</i> in Census region <i>r</i> | 73, 74, 124, A-21, B-11, B-12, B-102, B-103 |
| <i>PRODZERO</i> | 1990 production at process step <i>s</i> for vintage <i>v</i> | A-21, B-5, B-6 |
| <i>PRSIN</i> | Industrial price of residual fuel in Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>PTPIN</i> | Industrial price of all petroleum in Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>QASIN</i> | Industrial consumption of asphalt and road oil for Census division <i>d</i> in year <i>y</i> | A-23 |
| <i>QBMIN</i> | Industrial consumption of biomass for Census division <i>d</i> in year <i>y</i> | 112, A-23, B-89, B-90 |
| <i>QBMRF</i> | Biomass consumed by the petroleum refining industry in Census division <i>d</i> in year <i>y</i> | 112, A-18, B-89 |
| <i>QCIIN</i> | Industrial net coke imports for Census division <i>d</i> in year <i>y</i> | A-23 |

| Model Variable | Definition and Dimensions | Page Reference |
|----------------|--|-----------------------------|
| <i>QCLIN</i> | Industrial consumption of steam coal for Census division <i>d</i> in year <i>y</i> | A-23 |
| <i>QCLRF</i> | Coal consumed by the petroleum refining industry in Census division <i>d</i> in year <i>y</i> | 109, A-18, B-83 |
| <i>QDSIN</i> | Industrial consumption of distillate for Census division <i>d</i> in year <i>y</i> | A-23 |
| <i>QDSRF</i> | Distillate consumed by the petroleum refining industry in Census division <i>d</i> in year <i>y</i> | A-18, B-84 |
| <i>QELIN</i> | Industrial consumption of electricity in Census division <i>d</i> in year <i>y</i> | 110, A-23, B-60, B-87 |
| <i>QELRF</i> | Electricity consumed by the petroleum refining industry in Census division <i>d</i> in year <i>y</i> | 114, A-18, B-74, B-82, B-92 |
| <i>QGEIN</i> | Industrial consumption of geothermal for Census division <i>d</i> in year <i>y</i> | 112, A-23, B-90 |
| <i>QGFIN</i> | Industrial consumption of core natural gas in Census division <i>d</i> in year <i>y</i> | 110, 111, A-23, B-87, B-88 |
| <i>QGFRF</i> | Refinery consumption of core natural gas for Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>QGIIN</i> | Industrial consumption of non-core natural gas for Census division <i>d</i> in year <i>y</i> | 111, A-23, B-88 |
| <i>QGIRF</i> | Refinery consumption of non-core natural gas for Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>QHGIN</i> | Industrial consumption of hydropower for Census division <i>d</i> in year <i>y</i> | 112, A-23, B-89 |
| <i>QKSIN</i> | Industrial consumption of kerosene for Census division <i>d</i> in year <i>y</i> | A-23 |
| <i>QLGIN</i> | Industrial consumption of liquid petroleum gas for Census division <i>d</i> in year <i>y</i> | A-23 |
| <i>QLGRF</i> | Liquid petroleum gas consumed by the petroleum refining industry for Census division <i>d</i> in year <i>y</i> | A-18, B-85 |
| <i>QLPIN</i> | Industrial consumption of lease and plant fuel for Census division <i>d</i> in year <i>y</i> | 116, A-23, B-96 |
| <i>QMCIN</i> | Industrial consumption of metallurgical coal for Census division <i>d</i> in year <i>y</i> | A-23 |
| <i>QMGIN</i> | Industrial consumption of motor gasoline for Census division <i>d</i> in year <i>y</i> | A-23 |
| <i>QMSIN</i> | Industrial consumption of municipal solid waste for Census division <i>d</i> in year <i>y</i> | 113, A-23, B-90 |
| <i>QNGIN</i> | Industrial consumption of natural gas for Census division <i>d</i> in year <i>y</i> | A-23 |
| <i>QNGRF</i> | Natural gas consumed by the petroleum refining industry for Census division <i>d</i> in year <i>y</i> | 108, A-18, B-83 |

| Model Variable | Definition and Dimensions | Page Reference |
|----------------|---|---------------------------|
| <i>QOTIN</i> | Industrial consumption of other petroleum for Census division <i>d</i> in year <i>y</i> | A-23 |
| <i>QOTRF</i> | Other petroleum consumed by the petroleum refining industry for Census division <i>d</i> in year <i>y</i> | A-18, B-86 |
| <i>QPCIN</i> | Industrial consumption of petroleum coke for Census division <i>d</i> in year <i>y</i> | A-23 |
| <i>QPCRF</i> | Petroleum coke consumed by the petroleum refining industry for Census division <i>d</i> in year <i>y</i> | A-18, B-85 |
| <i>QPFIN</i> | Industrial consumption of petrochemical feedstocks for Census division <i>d</i> in year <i>y</i> | A-23 |
| <i>QPVIN</i> | Industrial consumption of photovoltaic for Census division <i>d</i> in year <i>y</i> | 113, A-23, B-90 |
| <i>QRLIN</i> | Industrial consumption of low sulfur residual fuel for Census division <i>d</i> in year <i>y</i> | A-23 |
| <i>QRLRF</i> | Residual fuel consumed by the petroleum refining industry in Census division <i>d</i> in year <i>y</i> | A-18, B-84 |
| <i>QRSIN</i> | Industrial consumption of residual fuel for Census division <i>d</i> in year <i>y</i> | A-23 |
| <i>QSASIN</i> | SEDS consumption of asphalt and road oil in Census division <i>d</i> in SEDS year <i>y</i> | A-18 |
| <i>QSCIIN</i> | SEDS net coke imports in Census division <i>d</i> in SEDS year <i>y</i> | A-18 |
| <i>QSCLIN</i> | SEDS consumption of steam coal in Census division <i>d</i> in SEDS year <i>y</i> | A-18 |
| <i>QSDSIN</i> | SEDS consumption of distillate in Census division <i>d</i> in SEDS year <i>y</i> | A-18 |
| <i>QSELIN</i> | SEDS consumption of electricity in Census division <i>d</i> in year <i>y</i> | 70, 106, A-18, B-59, B-81 |
| <i>QSGIN</i> | Industrial consumption of still gas for Census division <i>d</i> in year <i>y</i> | A-23 |
| <i>QSGRF</i> | Still gas consumed by the petroleum refining industry for Census division <i>d</i> in year <i>y</i> | A-18, B-85 |
| <i>QSKSIN</i> | SEDS consumption of kerosene in Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>QSLGIN</i> | SEDS consumption of liquid petroleum gas in Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>QSLPIN</i> | SEDS consumption of lease and plant fuel in Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>QSMCIN</i> | SEDS consumption of metallurgical coal in Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>QSMGIN</i> | SEDS consumption of motor gasoline in Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>QSNGIN</i> | SEDS consumption of natural gas in Census division <i>d</i> in year <i>y</i> | A-18 |

| Model Variable | Definition and Dimensions | Page Reference |
|-----------------------------|--|---|
| <i>QSOTIN</i> | SEDS consumption of other petroleum in Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>QSPCIN</i> | SEDS consumption of petroleum coke in Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>QSPFIN</i> | SEDS consumption of petrochemical feedstocks in Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>QSRLIN</i> | SEDS consumption of residual fuel in Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>QSSGIN</i> | SEDS consumption of still gas in Census division <i>d</i> in year <i>y</i> | A-18 |
| <i>QSTIN</i> | Industrial consumption of solar thermal in Census division <i>d</i> in year <i>y</i> | 112, A-23, B-90 |
| <i>QTPIN</i> | Industrial consumption of total petroleum in Census division <i>d</i> in year <i>y</i> | 111, A-23, B-88 |
| <i>QTRIN</i> | Industrial consumption of total renewables in Census division <i>d</i> in year <i>y</i> | 112, A-24, B-89 |
| <i>QTSIN</i> | Total industrial energy consumption in Census division <i>d</i> in year <i>y</i> | A-24 |
| <i>QTYINTR</i> | Consumption of intermediate fuel <i>f</i> in Census region <i>r</i> | A-21, B-67 to B-70 |
| <i>QTYMAIN</i> | Consumption of main fuel <i>f</i> in Census region <i>r</i> | 95 to 97, 100, A-22, B-65 to B-70, B-73 to B-80 |
| <i>QTYRENW</i> | Consumption of renewable fuel <i>f</i> in Census region <i>r</i> | 97, A-22, B-67 to B-71, B-74, B-76 to B-80 |
| <i>QWIIN</i> | Industrial consumption of wind in Census division <i>d</i> in year <i>y</i> | 113, A-24, B-90 |
| <i>REFCON</i> | Consumption of fuel <i>f</i> by the petroleum refining industry in year <i>y</i> | A-24, B-94 |
| <i>SEDSIND</i> | SEDS consumption of fuel <i>f</i> in Census division <i>d</i> | 120, A-22, B-100 |
| <i>STBYP</i> | Consumption of byproduct fuel <i>f</i> in steam turbines | A-22, B-40, B-46 |
| <i>STEELCON</i> | Consumption of fuel <i>f</i> by the blast furnace and basic steel products industry in year <i>y</i> | A-24, B-95 |
| <i>STEMCUR₉₀</i> | Total steam demand in 1990 | 86, A-19, A-68, B-32, B-33 |
| <i>STEMCUR</i> | Total steam demand | 85, 86, 90, 93, A-22, B-37, B-39, B-44 |
| <i>STEMCURF</i> | Amount of steam to be generated from purchased fuels | 93, 94, A-22, B-43, B-44 |
| <i>STFUEL</i> | Consumption of fuel <i>f</i> in steam turbines | 91, 95, A-22, B-39, B-40, B-45 |
| <i>SULFURCONT</i> | Sulfur content of fuel <i>f</i> | 98, 118, A-19, A-69, B-71, B-98 |
| <i>SUMPINT</i> | Cumulative unit energy consumption of fuel <i>f</i> at process step <i>s</i> | 131, 132, A-22, B-18, B-29 |
| <i>TALUMCON</i> | Total consumption of fuel <i>f</i> from the primary aluminum industry | A-22, B-80, B-95 |

| Model Variable | Definition and Dimensions | Page Reference |
|------------------------|---|--|
| <i>TCEMENTCON</i> | Total consumption of fuel <i>f</i> from the hydraulic cement industry | A-22, B-78, B-79, B-94 |
| <i>TCHEMCON</i> | Total consumption of fuel <i>f</i> from the bulk chemicals industry | A-22, B-77, B-93 |
| <i>TEMISM</i> | Total emissions of pollutant <i>p</i> from main fuel <i>f</i> in Census region <i>r</i> | A-22 |
| <i>TEMISR</i> | Total emissions of pollutant <i>p</i> for renewable fuel <i>f</i> in Census region <i>r</i> | 99, 118, A-22, B-73, B-98 |
| <i>TFOODCON</i> | Total consumption of fuel <i>f</i> from the food and kindred products industry | 100, A-22, B-75, B-76, B-93 |
| <i>TGLASSCON</i> | Total consumption of fuel <i>f</i> from the glass and glass products industry | A-22, B-77, B-78, B-94 |
| <i>TMANHP</i> | Total manufacturing consumption of fuel <i>f</i> for heat and power | 99, 114, A-22, B-73, B-74, B-92 |
| <i>TMISCFD</i> | Total consumption of miscellaneous fuels and feedstocks fuel <i>f</i> | A-22, B-75, B-92 |
| <i>TNONHP</i> | Total non-manufacturing consumption of fuel <i>f</i> for heat and power | 115, A-22, B-74, B-92 |
| <i>TOTEMIS</i> | Total emissions of pollutant <i>p</i> from fuel <i>f</i> in Census region <i>r</i> | 98, A-22, B-72 |
| <i>TPAPERCON</i> | Total consumption of fuel <i>f</i> from the paper and allied products industry | A-22, B-76, B-93 |
| <i>TQINTR</i> | Total consumption of intermediate fuel <i>f</i> in Census region <i>r</i> | A-22, B-70 |
| <i>TQMAIN</i> | Total consumption of main fuel <i>f</i> in Census region <i>r</i> | 97, 108, A-22, B-70, B-81 |
| <i>TQRENW</i> | Total consumption of renewable fuel <i>f</i> in Census region <i>r</i> | A-22, B-70, B-82 |
| <i>TREFCON</i> | Total consumption of fuel <i>f</i> from the petroleum refining industry | A-22, B-74, B-94 |
| <i>TSTEELCON</i> | Total consumption of fuel <i>f</i> from the blast furnace and basic steel products industry | A-22, B-79, B-95 |
| <i>UNCONTEMISSFACT</i> | Uncontrolled emission factor for pollutant <i>p</i> using fuel <i>f</i> | 98, 116, 117, A-19, A-70, B-71, B-95 to B-97 |
| <i>WPRC</i> | Price for fuel <i>t</i> in 1987 dollars | 84, 133, A-22, B-30, B-31 |

Table A-3. NEMS Industrial Module Inputs and Outputs

| Model Variable | Equation | Units |
|------------------------|---|--|
| MODULE INPUTS | (including inputs received from other NEMS modules) | |
| <i>BSSHR</i> | B-88, B-91, B-98, B-99 | NA |
| <i>BYPINT</i> | B-131, B-132 | IDVAL = 1: MMBtu/ton except for elec. Kwh/ton; IDVAL = 2: Trillion Btu/ Billion 1987 \$ |
| <i>BYSINT</i> | B-89 | NA |
| <i>CAPREG</i> | B-104 to B-106 | Megawatts |
| <i>CGOGCAP</i> | B-201 | Megawatts |
| <i>CGOGGEN</i> | B-202 | Gigawatt hours |
| <i>CGOGQ</i> | B-184, B-185, B-187, B-199, B-203, B-205 | Trillion Btu |
| <i>CGRECAP</i> | B-201 | Megawatts |
| <i>CGREGEN</i> | B-202 | Gigawatt hours |
| <i>CGREQ</i> | B-203 | Trillion Btu |
| <i>COPRCLG</i> | B-185 | Trillion Btu |
| <i>COPRCLQ</i> | B-185 | Trillion Btu |
| <i>CUMOUT88</i> | B-61 | IDVAL = 1: Tons; IDVAL = 2: Billion 1987 \$ |
| <i>DIVSHARE</i> | B-105, B-106, B-109, B-113 to B-116 | NA |
| <i>EINTER</i> | B-35, B-38 to B-57, B-61 | IDVAL = 1: MMBtu/ton except for elec. Kwh/ton; IDVAL = 2: Trillion Btu/ Billion 1987 \$ |
| <i>EMISSCONTROLFAC</i> | B-154, B-215 to B-217 | Metric tons/Trillion Btu |
| <i>EMPIND</i> | B-127 | Millions |
| <i>ENBINT</i> | B-1 | Trillion Btu/Thousand |
| <i>ENPINT</i> | B-3 to B-6, B-33, B-35, B-36, B-38 to B-58, B-60, B-61 | IDVAL = 1: MMBtu/ton except for elec. Kwh/ton; IDVAL = 2: Trillion Btu/ Billion 1987 \$ |
| <i>ENSINT</i> | B-88 | NA |
| <i>GEN90</i> | B-64 | Trillion Btu |
| <i>GENEQPHTRT</i> | B-74, B-75, B-94, B-95 | Trillion Btu/kWh |
| <i>GENEQPSHR</i> | B-70 | NA |
| <i>GENEQPSTEFF</i> | B-76, B-77 | NA |
| <i>GENUTIL</i> | B-66 | NA |
| <i>IDVAL</i> | Used in If statements | NA |

| Model Variable | Equation | Units |
|--------------------|---|---------------------|
| <i>IFBYP</i> | B-135 | NA |
| <i>IFMAX</i> | B-10 | NA |
| <i>IFSBYP</i> | B-94, B-95 | NA |
| <i>IFSMAX</i> | B-88, B-94, B-95, B-99 | NA |
| <i>INDDIR</i> | Used in If statements | NA |
| <i>INDMAX</i> | B-71 to B-73, B-87, B-151 to B-153, B-159 to B-161, B-164 | NA |
| <i>INDNAME</i> | | NA |
| <i>INDNUM</i> | Used in If statements | NA |
| <i>INDREG</i> | Used in If statements | NA |
| <i>INDSTEPNAME</i> | | NA |
| <i>IPASTP</i> | Used in If statements | NA |
| <i>ISTP</i> | Used in If statements | NA |
| <i>ITYPE</i> | Used in If statements | NA |
| <i>MC_MFGO</i> | B-123 | Millions |
| <i>MC_NMFGO</i> | B-122 | Millions |
| <i>MPASTP</i> | B-11 to B-13, B-136 to B-138 | NA |
| <i>MSEDYR</i> | B-193 | NA |
| <i>NSTEP</i> | Used in If statements | NA |
| <i>NTMAX</i> | B-234 | NA |
| <i>OWN90</i> | B-67 | Trillion Btu |
| <i>PCLIN</i> | B-124, B-125 | 1987 \$/Million Btu |
| <i>PDSIN</i> | B-124, B-125 | 1987 \$/Million Btu |
| <i>PELIN</i> | B-124, B-125 | 1987 \$/Million Btu |
| <i>PGFIN</i> | B-124, B-125 | 1987 \$/Million Btu |
| <i>PGIIN</i> | B-124, B-125 | 1987 \$/Million Btu |
| <i>PHDRAT</i> | B-19, B-229, B-230 | NA |
| <i>PKSIN</i> | B-124, B-125 | 1987 \$/Million Btu |
| <i>PLGIN</i> | B-124, B-125 | 1987 \$/Million Btu |
| <i>PLPIN</i> | B-124, B-125 | 1987 \$/Million Btu |
| <i>PMCIN</i> | B-124, B-125 | 1987 \$/Million Btu |
| <i>PMGIN</i> | B-124, B-125 | 1987 \$/Million Btu |
| <i>PNGIN</i> | B-124, B-125 | 1987 \$/Million Btu |
| <i>POTIN</i> | B-124, B-125 | 1987 \$/Million Btu |
| <i>PRLIN</i> | B-124, B-125 | 1987 \$/Million Btu |

| Model Variable | Equation | Units |
|-----------------------------|-----------------------------------|----------------------|
| <i>PRODFLOW</i> | B-21, B-26, B-30, B-232, B-233 | NA |
| <i>PRODRETR</i> | B-15, B-16 | NA |
| <i>PRODVX</i> | B-19, B-20, B-126, B-229 to B-231 | Billion 1987 \$ |
| <i>PRSIN</i> | B-124, B-125 | 1987 \$/Trillion Btu |
| <i>PTPIN</i> | B-124, B-125 | 1987 \$/Trillion Btu |
| <i>QBMRF</i> | B-199 | Trillion Btu |
| <i>QCLRF</i> | B-185 | Trillion Btu |
| <i>QDSRF</i> | B-188 | Trillion Btu |
| <i>QELRF</i> | B-162, B-183, B-204 | Trillion Btu |
| <i>QGFRF</i> | B-162 | Trillion Btu |
| <i>QGIRF</i> | B-162 | Trillion Btu |
| <i>QLGRF</i> | B-189 | Trillion Btu |
| <i>QNGRF</i> | B-184 | Trillion Btu |
| <i>QOTRF</i> | B-192 | Trillion Btu |
| <i>QPCRF</i> | B-191 | Trillion Btu |
| <i>QQLRF</i> | B-187 | Trillion Btu |
| <i>QSASIN</i> | B-124 | Trillion Btu |
| <i>QSCIIN</i> | B-124 | Trillion Btu |
| <i>QSCLIN</i> | B-124 | Trillion Btu |
| <i>QSDSIN</i> | B-124 | Trillion Btu |
| <i>QSELIN</i> | B-124, B-179 | Trillion Btu |
| <i>QSGRF</i> | B-162, B-190 | Trillion Btu |
| <i>QSKSIN</i> | B-124 | Trillion Btu |
| <i>QSLGIN</i> | B-124 | Trillion Btu |
| <i>QSLPIN</i> | B-124 | Trillion Btu |
| <i>QSMCIN</i> | B-124 | Trillion Btu |
| <i>QSMGIN</i> | B-124 | Trillion Btu |
| <i>QSNGIN</i> | B-124 | Trillion Btu |
| <i>QSOTIN</i> | B-124 | Trillion Btu |
| <i>QSPCIN</i> | B-124 | Trillion Btu |
| <i>QSPFIN</i> | B-124 | Trillion Btu |
| <i>QSRLIN</i> | B-124 | Trillion Btu |
| <i>QSSGIN</i> | B-124 | Trillion Btu |
| <i>STEMCUR₉₀</i> | B-64 | Trillion Btu |

| Model Variable | Equation | Units |
|-----------------------------|--|--|
| <i>SULFURCONT</i> | B-155, B-218 | NA |
| <i>UNCONTEMISSFACT</i> | B-154, B-215 to B-217 | Metric tons/Trillion Btu |
| MODULE PARAMETERS | | |
| <i>BCSC</i> | B-34, B-37, B-61 | NA |
| <i>BELAS</i> | B-59, B-61 | NA |
| <i>BSSHRCL</i> | B-98 | NA |
| <i>BSSHRE</i> | B-98 | NA |
| <i>BSSHRNG</i> | B-98 | NA |
| <i>BSSHROIL</i> | B-98 | NA |
| <i>BYPCSC</i> | B-129 | NA |
| <i>GSTEAM</i> | B-64, B-65 | NA |
| <i>OGEN</i> | B-67, B-68 | NA |
| CALCULATED VARIABLES | | |
| <i>AVGINT</i> | B-88, B-91 | NA |
| <i>BENCHFAC</i> | B-193, B-216, B-217, B-225 to B-227 | NA |
| <i>BIOFUELS</i> | B-226 | Trillion Btu |
| <i>BMAIN</i> | B-183 to B-197, B-215 to B-217, B-225, B-227 | Trillion Btu |
| <i>BOILSTEAM</i> | B-78 | Trillion Btu |
| <i>BSSHRLAG</i> | B-98 | NA |
| <i>BYPBSCI</i> | B-89 | Trillion Btu |
| <i>BYPBSCM</i> | B-89, B-141 | Trillion Btu |
| <i>BYPBSCR</i> | B-89, B-144 | Trillion Btu |
| <i>BYPCSCCUR</i> | B-129 to B-131 | NA |
| <i>BYPCSCLAG</i> | B-130 | NA |
| <i>BYPINTLAG</i> | B-131 | IDVAL = 1: MMBtu/ton except for elec. kWh/ton; IDVAL = 2: Trillion Btu/ Billion 1987 \$ |
| <i>BYPQTY</i> | B-132 to B-138 | Trillion Btu |
| <i>BYPSTM</i> | B-89, B-90 | Trillion Btu |
| <i>BYSQTY</i> | B-94, B-95 | Trillion Btu |
| <i>CAPD</i> | B-105 to B-108, B-112, B-117 to B-119 | Megawatts |
| <i>CAPDIV</i> | B-107, B-108 | Megawatts |
| <i>CAPGW</i> | B-115 to B-119, B-121, B-201 | Megawatts |

| Model Variable | Equation | Units |
|------------------|--|---|
| <i>CAPGWL</i> AG | B-118 | Megawatts |
| <i>CGFUEL</i> | B-79 to B-87 | Trillion Btu |
| <i>CSCCUR</i> | B-34, B-35, B-37 to B-57 | NA |
| <i>CUMOUT</i> | B-34 | IDVAL = 1: Tons; IDVAL = 2: Billion 1987 \$ |
| <i>CUMPROD</i> | B-36, B-58 | IDVAL = 1: Tons; IDVAL = 2: Billion 1987 \$ |
| <i>DEMIMAIN</i> | B-215 to B-218, B-220 | Metric tons |
| <i>DEMIRENW</i> | B-219, B-221 | Metric tons |
| <i>DIVFUEL</i> | B-109 to B-111, B-113 to B-116, B-203 | Trillion Btu |
| <i>DQMAIN</i> | B-181, B-183 to B-192, B-195, B-216, B-217 | Trillion Btu |
| <i>DQRENW</i> | B-182, B-198, B-199, B-226 | Trillion Btu |
| <i>DSRENW</i> | B-180, B-182, B-219 | Trillion Btu |
| <i>ELCAP</i> | B-66, B-73 | Megawatts |
| <i>ELCTOT</i> | B-73, B-100, B-115, B-116 | Megawatts |
| <i>ELDEM</i> | B-62 | Trillion Btu |
| <i>ELGEN</i> | B-65 to B-70, B-74 to B-77, B-83, B-94, B-95 | Trillion Btu |
| <i>ELOTOT</i> | B-71, B-101, B-105, B-107, B-113, B-115, B-116 | Trillion Btu |
| <i>ELOWN</i> | B-68, B-69, B-71, B-83, B-139 | Trillion Btu |
| <i>ELSALE</i> | B-69, B-72 | Trillion Btu |
| <i>ELSTOT</i> | B-72, B-102, B-105, B-107, B-114 to B-116 | Trillion Btu |
| <i>EMINCC</i> | B-224 | Metric tons |
| <i>EMINCX</i> | B-220 to B-224 | Million metric tons |
| <i>EMIRENW</i> | B-154 to B-159 | Metric tons |
| <i>EMPLX</i> | B-1, B-127, B-128 | Thousands |
| <i>ENBQTY</i> | B-1, B-2, B-62, B-63, B-139, B-140, B-142 | Trillion Btu |
| <i>ENBYPI</i> | B-137 | Trillion Btu |
| <i>ENBYPM</i> | B-136 | Trillion Btu |
| <i>ENBYPR</i> | B-138 | Trillion Btu |
| <i>ENPINTLAG</i> | B-33 | IDVAL = 1: MMBtu/ton except for elec. kWh/ton IDVAL = 2: Trillion Btu/ Billion 1987 \$ |
| <i>ENPIQTY</i> | B-12, B-14, B-63, B-142, B-143 | Trillion Btu |
| <i>ENPMQTY</i> | B-11, B-14, B-62, B-139 to B-141 | Trillion Btu |
| <i>ENPQTY</i> | B-3 to B-13 | Trillion Btu |

| Model Variable | Equation | Units |
|------------------|--|---|
| <i>ENPRQTY</i> | B-13, B-144 | Trillion Btu |
| <i>ENSQTY</i> | B-91 to B-97, B-140 to B-144 | Trillion Btu |
| <i>FUELSHARE</i> | B-179, B-182 | NA |
| <i>GCTFUEL</i> | B-75, B-77, B-81, B-93, B-97 | Trillion Btu |
| <i>GCTSTEAM</i> | B-77, B-78 | Trillion Btu |
| <i>GENGWH</i> | B-113, B-114, B-120, B-202 | Gigawatthours |
| <i>GENTOT</i> | B-87, B-103, B-109 | Trillion Btu |
| <i>GINTER</i> | B-64, B-65 | NA |
| <i>ICEFUEL</i> | B-74, B-76, B-80, B-92, B-96 | Trillion Btu |
| <i>ICESTEAM</i> | B-76, B-78 | Trillion Btu |
| <i>IDLCAP</i> | B-15, B-17, B-23, B-24 | IDVAL = 1: MMBtu/ton except for elec. kWh/ton IDVAL = 2: Trillion Btu/ Billion 1987 \$ |
| <i>IFSBYPI</i> | B-89 | NA |
| <i>IFSBYPM.</i> | B-89 | NA |
| <i>IFSBYPR</i> | B-89 | NA |
| <i>OINTER</i> | B-67, B-68 | Trillion Btu |
| <i>OTHIND</i> | B-193 to B-197, B-215 to B-217, B-227, B-228 | Trillion Btu |
| <i>OUTIND</i> | B-122, B-123, B-126, B-180 | Billion 1987 \$ |
| <i>PRCCUR</i> | B-59, B-60 | 1987 \$/Million Btu |
| <i>PRCX</i> | B-98, B-124, B-125 | 1987 \$/Million Btu |
| <i>PRCXLG</i> | B-98 | 1987 \$/Million Btu |
| <i>PRODCUR</i> | B-3 to B-6, B-14 to B-18, B-21 to B-32, B-129, B-130, B-132, B-232 to B-234 | IDVAL = 1: Tons IDVAL = 2: Billion 1987 \$ |
| <i>PRODLG</i> | B-129 | IDVAL = 1: Tons IDVAL = 2: Billion 1987 \$ |
| <i>PRODSUM</i> | B-26, B-27, B-30, B-31, B-233, B-234 | IDVAL = 1: MMBtu/ton except for elec. kWh/ton IDVAL = 2: Trillion Btu/ Billion 1987 \$ |
| <i>PRODX</i> | B-19 to B-21, B-230 to B-232 | IDVAL = 1: Tons IDVAL = 2: Billion 1987 \$ |
| <i>PRODZERO</i> | B-3 to B-5 | IDVAL = 1: Tons IDVAL = 2: Billion 1987 \$ |
| <i>QTYINTR</i> | B-142, B-143, B-146, B-149, B-152 | Trillion Btu |
| <i>QTYMAIN</i> | B-139 to B-141, B-145, B-148, B-151, B-160, B-163 to B-165, B-167, B-169, B-171, B-173, B-175, B-177 | Trillion Btu |

| Model Variable | Equation | Units |
|-------------------|---|------------------|
| <i>QTYRENW</i> | B-144, B-147, B-150, B-153, B-154, B-161, B-166, B-168, B-170, B-172, B-174, B-176, B-178 | Trillion Btu |
| <i>SEDSIND</i> | B-225 | Trillion Btu |
| <i>STBYP</i> | B-82, B-95 | Trillion Btu |
| <i>STEMCUR</i> | B-63, B-65, B-78, B-90 | Trillion Btu |
| <i>STEMCURF</i> | B-90, B-91 | Trillion Btu |
| <i>STFUEL</i> | B-79 to B-82, B-94 | Trillion Btu |
| <i>SUMPINT</i> | B-36, B-58 | Trillion Btu/ton |
| <i>TALUMCON</i> | B-177, B-178, B-214 | Trillion Btu |
| <i>TCEMENTCON</i> | B-173, B-174, B-211 | Trillion Btu |
| <i>TCHEMCON</i> | B-169, B-170, B-209 | Trillion Btu |
| <i>TEMISR</i> | B-159, B-219 | Metric tons |
| <i>TFOODCON</i> | B-165, B-166, B-207 | Trillion Btu |
| <i>TGLASSCON</i> | B-171, B-172, B-210 | Trillion Btu |
| <i>TMANHP</i> | B-160, B-161, B-204 | Trillion Btu |
| <i>TMISCFD</i> | B-164, B-206 | Trillion Btu |
| <i>TNONHP</i> | B-163, B-205 | Trillion Btu |
| <i>TOTEMIS</i> | B-158 | Metric tons |
| <i>TPAPERCON</i> | B-167, B-168, B-208 | Trillion Btu |
| <i>TQINTR</i> | B-152 | Trillion Btu |
| <i>TQMAIN</i> | B-151, B-181 | Trillion Btu |
| <i>TQRENW</i> | B-153, B-182 | Trillion Btu |
| <i>TREFCON</i> | B-162, B-212 | Trillion Btu |
| <i>TSTEELCON</i> | B-175, B-176, B-213 | Trillion Btu |
| <i>WPRC</i> | B-59, B-61 | 1987 dollars |

MODULE OUTPUTS

| | | |
|------------------|-------|----------------|
| <i>ALUMCON</i> | B-214 | Trillion Btu |
| <i>CEMENTCON</i> | B-211 | Trillion Btu |
| <i>CGINDCAP</i> | B-201 | Megawatts |
| <i>CGINDGEN</i> | B-202 | Gigawatt hours |
| <i>CGINDQ</i> | B-203 | Trillion Btu |
| <i>CHEMCON</i> | B-209 | Trillion Btu |
| <i>EMINC</i> | B-223 | Metric tons |
| <i>FOODCON</i> | B-207 | Trillion Btu |

| Model Variable | Equation | Units |
|-----------------------|-----------------|--------------|
| <i>GLASSCON</i> | B-210 | Trillion Btu |
| <i>MANHP</i> | B-204 | Trillion Btu |
| <i>MISCFD</i> | B-206 | Trillion Btu |
| <i>NONHP</i> | B-205 | Trillion Btu |
| <i>PAPERCON</i> | B-208 | Trillion Btu |
| <i>QASIN</i> | B-125, B-194 | Trillion Btu |
| <i>QBMIN</i> | B-199, B-200 | Trillion Btu |
| <i>QCIIN</i> | B-125, B-194 | Trillion Btu |
| <i>QCLIN</i> | B-125, B-194 | Trillion Btu |
| <i>QDSIN</i> | B-125, B-194 | Trillion Btu |
| <i>QELIN</i> | B-125, B-194 | Trillion Btu |
| <i>QGEIN</i> | B-200 | Trillion Btu |
| <i>QGFIN</i> | B-195, B-196 | Trillion Btu |
| <i>QGIIN</i> | B-196 | Trillion Btu |
| <i>QHOIN</i> | B-198, B-200 | Trillion Btu |
| <i>QKSIN</i> | B-125, B-194 | Trillion Btu |
| <i>QLGIN</i> | B-125, B-194 | Trillion Btu |
| <i>QLPIN</i> | B-194, B-216 | Trillion Btu |
| <i>QMCIN</i> | B-125, B-194 | Trillion Btu |
| <i>QMGIN</i> | B-125, B-194 | Trillion Btu |
| <i>QMSIN</i> | B-200 | Trillion Btu |
| <i>QNGIN</i> | B-125, B-194 | Trillion Btu |
| <i>QOTIN</i> | B-125, B-194 | Trillion Btu |
| <i>QPCIN</i> | B-125, B-194 | Trillion Btu |
| <i>QPFIN</i> | B-125, B-194 | Trillion Btu |
| <i>QPVIN</i> | B-200 | Trillion Btu |
| <i>QRLIN</i> | B-125, B-194 | Trillion Btu |
| <i>QRSIN</i> | B-125, B-194 | Trillion Btu |
| <i>QSGIN</i> | B-125, B-194 | Trillion Btu |
| <i>QSTIN</i> | B-200 | Trillion Btu |
| <i>QTPIN</i> | B-197 | Trillion Btu |
| <i>QTRIN</i> | B-200 | Trillion Btu |
| <i>QTSIN</i> | B-125 | Trillion Btu |
| <i>QWIIN</i> | B-200 | Trillion Btu |

| Model Variable | Equation | Units |
|-----------------------|-----------------|--------------|
| <i>REFCON</i> B-212 | | Trillion Btu |
| <i>STEELCON</i> B-213 | | Trillion Btu |

MODEL INPUT: BCSC

MODEL COMPONENT: Process/Assembly

DEFINITION: Energy savings coefficient at process step s for fuel f and vintage v

DISCUSSION:

The energy savings coefficients for the energy-intensive industries are assumed to be constant over the four Census regions. The coefficients for the food and kindred products, paper and allied products, glass and glass products, hydraulic cement, bulk chemicals, blast furnace and basic steel products, and primary aluminum industries were obtained from Arthur D. Little. These coefficients are determined through Relative Energy Intensity (REI) for both old and new plants. Relative Energy Intensity is defined as the ratio of energy use in a new or advanced process compared to the 1988 old plant average energy use which has been normalized to one. Regression analyses were performed to create a log-linear plot of REI versus time. The following equation is estimated by ADL in natural logarithms.

$$\ln(REI) = \beta \ln(t) \quad (A-1)$$

The intercept is assumed to be zero. The slope of the resulting linear plot of REI against time, or the coefficient β , is the energy savings coefficient. There is a separate coefficient for each process step, however the coefficients are the same for all fuels used at a particular process step. The coefficients for the TPCs are listed in Table E-13, Appendix E.

For the non-energy-intensive and non-manufacturing industries, the coefficients are based on regressions on NEA data and output from the 1990 Macroeconomic model.

SOURCES:

Decision Analysis Corporation and Arthur D. Little, "Industrial Model: Selected Process Flows Revised Final Report," prepared for EIA under Contract No. DE-AC01-92EI21946, Subtask 2B, Vienna, VA, April 26, 1993.

U. S. Department of Commerce, Office of Business Analysis, *National Energy Accounts*, PB89-187918, February 1989.

MODEL PARAMETER: *BELAS*

MODEL COMPONENT: Process/Assembly

DEFINITION: Own price elasticity at process step s for fuel f for old vintage and the cross price elasticity at process step s for fuel f and fuel t for old vintage

DISCUSSION:

The cross price elasticities for the energy intensive industries are zero for all process steps and fuels. The cross price elasticities for the non-manufacturing and non-energy-intensive industries were obtained through a series of regressions. The regressions were based on data from NEA and outputs from the 1990 Macroeconomic model. The resulting parameter estimates are the cross price elasticities. The price elasticity for steam was obtained using the elasticity from the fuel that had the largest boiler share in the BSC component by the four Census regions.

SOURCE:

U. S. Department of Commerce, Office of Business Analysis, *National Energy Accounts*, PB89-187918, February 1989.

MODEL INPUT: *BSSHR*

MODEL COMPONENT: Boiler/Steam/Cogeneration

DEFINITION: Share of total fuel consumption in the BSC component for fuel *f*

DISCUSSION:

The boiler shares for all industries are derived from the ADL Industrial Model Baseline Database energy consumption. The quantity of each fuel consumed by industry and region in the BSC component is divided by total energy consumption in the BSC component to determine the boiler share of each fuel. There is no BSC component for the following industries: coal mining, oil and gas mining, construction, glass and glass products, hydraulic cement, and primary aluminum. Therefore, this variable does not exist for these industries.

SOURCES:

Decision Analysis Corporation of Virginia and Arthur D. Little, "Industrial Model: Baseline Database Final Report," prepared for EIA under Contract No. DE-AC01-92EI21946, Subtask 1, Vienna VA, January 15, 1993, Appendix G.

Energy Information Administration, Manufacturing Energy Consumption Survey: Consumption of Energy 1988, DOE/EIA-0512(88), May 1991.

MODEL INPUT: BSSHRCL

MODEL COMPONENT: Boiler/Steam/Cogeneration

DEFINITION: Cross price elasticity for steam coal with fuel f

DISCUSSION:

Price elasticities for boiler use were obtained from an article in Energy Economics by Considine. The price elasticities were obtained from a linear logit form of a stationary fuel combustion model. This model is given in the following equation.

$$w_i = \frac{e^{f_i}}{\sum_{j=1}^n e^{f_j}} \quad (\text{A-2})$$

where:

$$f_i = \eta_i + \sum_{j=1}^n \phi_{ij} \ln P_j \quad (\text{A-3})$$

The price elasticities are found by differentiating the estimated linear logit model. Cross price elasticities are given by the following equation.

$$E_{ik} = w_j + \phi_{ik} - \sum_{j=1}^n w_j \phi_{jk} \quad (\text{A-4})$$

There is no BSC component in the coal mining, oil and gas mining, construction, glass and glass products, hydraulic cement, and primary aluminum industries, therefore this variable does not exist for those industries. In the industrial model, the cross elasticity of steam coal with natural gas is assumed to be zero.

SOURCE:

Considine, Timothy J., "Separability, functional form and regulatory policy in models of interfuel substitution," Energy Economics, April 1989, p. 82-94.

MODEL INPUT: *BSSHRE*
MODEL COMPONENT: Boiler/Steam/Cogeneration
DEFINITION: Own price elasticity for fuel *f*
DISCUSSION:

Price elasticities for boiler use were obtained from an article in Energy Economics by Considine. The price elasticities were obtained from a linear logit form of a stationary fuel combustion model. This model is given in the following equation.

$$w_i = \frac{e^{f_i}}{\sum_{j=1}^n e^{f_j}} \quad (\text{A-5})$$

where:

$$f_i = \eta_i + \sum_{j=1}^n \varphi_{ij} \ln P_j \quad (\text{A-6})$$

The price elasticities are found by differentiating the estimated linear logit model. Own price elasticities are given by the following equation.

$$E_{ii} = w_i - 1 + \varphi_{ii} - \sum_{j=1}^n w_j \varphi_{ji} \quad (\text{A-7})$$

There is no BSC component in the coal mining, oil and gas mining, construction, glass and glass products, hydraulic cement, and primary aluminum industries, therefore this variable does not exist for those industries.

SOURCE:

Considine, Timothy J., "Separability, functional form and regulatory policy in models of interfuel substitution," Energy Economics, April 1989, p. 82-94.

MODEL INPUT: BSSHRNG

MODEL COMPONENT: Boiler/Steam/Cogeneration

DEFINITION: Cross price elasticity for natural gas with fuel f

DISCUSSION:

Price elasticities for boiler use were obtained from an article in Energy Economics by Considine. The price elasticities were obtained from a linear logit form of a stationary fuel combustion model. This model is given in the following equation.

$$w_i = \frac{e^{f_i}}{\sum_{j=1}^n e^{f_j}} \quad (\text{A-8})$$

where:

$$f_i = \eta_i + \sum_{j=1}^n \varphi_{ij} \ln P_j \quad (\text{A-9})$$

The price elasticities are found by differentiating the estimated linear logit model. Cross price elasticities are given by the following equation.

$$E_{ik} = w_j + \varphi_{ik} - \sum_{j=1}^n w_j \varphi_{jk} \quad (\text{A-10})$$

There is no BSC component in the coal mining, oil and gas mining, construction, glass and glass products, hydraulic cement, and primary aluminum industries, therefore this variable does not exist for those industries. In the industrial model, the cross elasticity of natural gas with steam coal is assumed to be zero.

SOURCE:

Considine, Timothy J., "Separability, functional form and regulatory policy in models of interfuel substitution," Energy Economics, April 1989, p. 82-94.

MODEL INPUT: *BSSHROIL*
MODEL COMPONENT: Boiler/Steam/Cogeneration
DEFINITION: Price elasticity for oil crossed with fuel *f*
DISCUSSION:

Price elasticities for boiler use were obtained from an article in Energy Economics by Considine. The price elasticities were obtained from a linear logit form of a stationary fuel combustion model. This model is given in the following equation.

$$w_i = \frac{e^{f_i}}{\sum_{j=1}^n e^{f_j}} \quad (\text{A-11})$$

where:

$$f_i = \eta_i + \sum_{j=1}^n \varphi_{ij} \ln P_j \quad (\text{A-12})$$

The price elasticities are found by differentiating the estimated linear logit model. Cross price elasticities are given by the following equation.

$$E_{ik} = w_j + \varphi_{ik} - \sum_{j=1}^n w_j \varphi_{jk} \quad (\text{A-13})$$

There is no BSC component in the coal mining, oil and gas mining, construction, glass and glass products, hydraulic cement, and primary aluminum industries, therefore this variable does not exist for those industries.

SOURCE:

Considine, Timothy J., "Separability, functional form and regulatory policy in models of interfuel substitution," Energy Economics, April 1989, p. 82-94.

MODEL INPUT: *BYPCSC*

MODEL COMPONENT: Process/Assembly

DEFINITION: Byproduct technology possibility curve (TPC) coefficient for byproduct *b* at process step *s* and vintage *v*

DISCUSSION:

The byproduct TPC coefficients are zero for all byproducts currently considered. It only applies to the paper and allied products industry.

SOURCE:

Decision Analysis Corporation and Arthur D. Little, "Industrial Model: Selected Process Flows Revised Final Report," prepared for EIA under Contract No. DE-AC01-92EI21946, Subtask 2B, Vienna, VA, April 26, 1993.

MODEL INPUT: *BYPINT*

MODEL COMPONENT: Process/Assembly

DEFINITION: Byproduct rate of production for byproduct *b* at process step *s* and
vintage *v*

DISCUSSION:

The rate of production for each byproduct is calculated similarly to the calculation of unit energy consumption (UEC) for fuels used in the PA component. The total 1988 byproduct energy consumed in the BSC component is determined from the ADL Industrial Model Baseline Database. The total byproduct energy consumed is then divided by the 1988 value of output to obtain the UEC or rate of production for byproducts. Byproduct production in the paper and allied products industry includes pulping liquor produced in the kraft pulping process step and wood from the wood prep process step. Estimates of these two byproducts are obtained from *1988 Manufacturing Energy Consumption Survey (MECS)*. The production obtained from MECS is then divided by the total physical throughput to the particular process step to determine the rate of production. The total byproduct production from blast furnaces and coke ovens must be shared out to the two process steps based on the physical throughput obtained from ADL.

SOURCES:

Decision Analysis Corporation of Virginia and Arthur D. Little, "Industrial Model: Baseline Database Final Report," prepared for EIA under Contract No. DE-AC01-92EI21946, Subtask 1, Vienna VA, January 15, 1993.

Energy Information Administration, Manufacturing Energy Consumption Survey: Consumption of Energy, 1988, DOE/EIA-0512(88), Washington, D.C., May 1991.

Decision Analysis Corporation and Arthur D. Little, "Industrial Model: Selected Process Flows Revised Final Report," prepared for EIA under Contract No. DE-AC01-92EI21946, Subtask 2B, Vienna, VA, April 26, 1993.

MODEL INPUT: *BYSINT*

MODEL COMPONENT: Boiler/Steam/Cogeneration

DEFINITION: Intensity for byproduct *b* consumed in the BSC component

DISCUSSION:

The intensity for byproducts consumed in the BSC component was obtained from the Department of Energy.

SOURCE:

Department of Energy, "Industrial Energy Productivity Project - Final Report," Generic Energy Services, DOE/CS/40151-1, Vol. 7 of 9, February 1983.

MODEL INPUT: *CAPREG*

MODEL COMPONENT: Boiler/Steam/Cogeneration

DEFINITION: Existing or planned capacity for cogeneration for use u in Census region r using fuel f in year y

DISCUSSION:

The existing or planned capacity for cogeneration was obtained from EIA-867 data.

SOURCE:

Energy Information Administration, EIA-867, Survey of Independent Power Producers Database.

MODEL INPUT: *CUMOUT88*

MODEL COMPONENT:

DEFINITION: Cumulative output through the year 1988

DISCUSSION:

Cumulative output was from NEA data (1958 - 1985) and output DRI (1986 - 1988).

SOURCES:

U. S. Department of Commerce, Office of Business Analysis, *National Energy Accounts*,
PB89-187918, February 1989.

DRI, Inc., Data Series I/O-US/0293/Series.

MODEL INPUT: *EINTER*

MODEL COMPONENT: Process/Assembly

DEFINITION: Intercept at process step *s* for fuel *f* and vintage *v*

DISCUSSION:

Initial estimates of the intercept term are calculated based on initial UEC estimates and TPC coefficients. A series of regressions run by ADL determined the TPC coefficients (see the discussion of the variable *BCSC*). The resulting line of Relative Energy Intensity (REI) versus time has the TPC coefficient as the slope. The intercept of the regression line is used to calculate the variable *EINTER*. The regression equation solved by ADL is the following.

$$REI = \alpha + \beta t \quad (A-14)$$

Since the REI is defined as the ratio of the current year's UEC to the UEC for 1988, the above equation may be written as follows.

$$\log \left[\frac{UEC_t}{UEC_{88}} \right] = \alpha + \beta t \quad (A-15)$$

Upon solving the above equation for *UEC_t*, the following equation emerges.

$$UEC_t = UEC_{88} \times e^{\alpha} \times e^{\beta t} \quad (A-16)$$

The initial intercept estimate is the following part of the equation above.

$$EINTER = UEC_{88} \times e^{\alpha}$$

(A-17)

SOURCE:

Decision Analysis Corporation and Arthur D. Little, "Industrial Model: Selected Process Flows Revised Final Report," prepared for EIA under Contract No. DE-AC01-92EI21946, Subtask 2B, Vienna, VA, April 26, 1993.

MODEL INPUT: *EMISSCONTROLFAC*

MODEL COMPONENT:

DEFINITION: Emission control factor for pollutant *p* using fuel *f*

DISCUSSION:

Emission factors for all pollutants except CO₂ and total carbon were derived from EPA emissions factors. Carbon emission factors were obtained from (EIA).

SOURCE:

Energy Information Administration, "Emissions Greenhouse Gases: 1985 - 1990", DOE/EIA-0573 (Washington, D.C., September 1993).

MODEL INPUT: ENBINT

MODEL COMPONENT: Buildings

DEFINITION: Unit energy consumption (UEC) for fuel f used in building end use
 e

DISCUSSION:

There is no building energy use in the non-manufacturing industries due to lack of information, therefore, there is no unit energy consumption for these industries. For the manufacturing industries, the unit energy consumption for buildings is determined in the following manner. Total electricity consumption for buildings for lighting and air conditioning is provided by ADL. Percents of total electricity consumption for each end use are based on a study by Halger, Bailey & Company. Several assumptions were made to estimate energy use from this study. In particular, information was not available for the tobacco industry, so it was assumed to be similar to the food industry. Building energy use for the furniture industry was assumed to be similar to energy use in the lumber industry. Consumption of natural gas in buildings was determined from the 1985 energy consumption data from an ISTUM-2 run made by Energy and Environmental Analysis, Inc. Consumption of steam in buildings was determined through the following procedure:

1. Total fuel consumption for space heating is obtained using the percent shares from the Halger, Bailey study and total fuel consumption from MECS.
2. The ADL Industrial Model Baseline Database natural gas consumption estimate is subtracted from the total fuel consumption calculated above, resulting in the fuel consumption necessary to generate steam.
3. Using boiler efficiencies provided by ADL, the steam consumption is estimated.

The unit energy consumption is then calculated by dividing the consumption of each fuel for lighting and HVAC by an EIA estimate of 1988 employment for the industry. The UECs are calculated on a national basis and assumed to be constant for each region.

SOURCES:

Decision Analysis Corporation of Virginia and Arthur D. Little, "Industrial Model: Baseline Database Final Report," prepared for EIA under Contract No. DE-AC01-92EI21946, Subtask 1, Vienna VA, January 15, 1993, Appendix E.

Halger, Bailey & Company, "Industrial Buildings Energy Use," prepared for Department of Energy, Office of Buildings and Community Systems, March 1987.

Energy Information Administration, Manufacturing Energy Consumption Survey: Consumption of Energy 1988, DOE/EIA-0512(88), May 1991.

Energy and Environmental Analysis, Inc., "Industrial Energy Productivity Project - Final Report", prepared for the Department of Energy, DOE/CS/40151 (nine volumes), February 1983.

MODEL INPUT: *ENPINT*

MODEL COMPONENT: Process/Assembly

DEFINITION: Unit energy consumption (UEC) at process step *s* for fuel *f* and vintage *v*

DISCUSSION:

The UECs for the non-energy-intensive and non-manufacturing industries are obtained from ADL estimates. For the energy intensive industries, UECs are derived for each process step as well as for each fuel. The total unit energy consumption for each process step for each of the energy intensive industries is determined from ADL estimates and 1988 value of output. ADL provides estimates of UEC for electricity, steam, and direct fuels fired. The total consumption in the PA component is obtained for each industry and fuel from the ADL Industrial Model Baseline Database. The UEC for direct fuels fired is then shared out between the fuels consumed at each process step based on the ADL Industrial Model Baseline Database.

$$ENPINT_{v,f,s} = ENPINTLAG_{v,f,s} \quad (A-18)$$

where:

*ENPINT*_{*v,f,s*} = Unit energy consumption of fuel *f* at process step *s* for vintage *v*, and

*ENPINTLAG*_{*v,f,s*} = Lagged unit energy consumption of fuel *f* at process step *s* for vintage *v*.

$$ENPINT_{v,f,s} = EINTER_{v,f,s} \times CSCCUR_{v,f,s} \quad (A-19)$$

where:

*ENPINT*_{*v,f,s*} = Unit energy consumption of fuel *f* at process step *s* for vintage *v*,

| | | |
|------------------|---|--|
| $EINTER_{v,f,s}$ | = | Intercept at process step s for fuel f for vintage v , and |
| $CSCCUR_{v,f,s}$ | = | Current energy savings at process step s for fuel f for vintage v . |

The unit energy consumption is calculated at the national level, and is assumed to be constant for all Census regions. The initial UEC estimates are assumed equal for both old and new vintage. UEC estimates are measured in kWh/ton for electricity and in MMBtu/ton for all other fuels.

SOURCES:

Decision Analysis Corporation and Arthur D. Little, "Industrial Model: Selected Process Flows Revised Final Report," prepared for EIA under Contract No. DE-AC01-92EI21946, Subtask 2B, Vienna, VA, April 26, 1993.

Decision Analysis Corporation of Virginia and Arthur D. Little, "Industrial Model: Baseline Database Final Report," prepared for EIA under Contract No. DE-AC01-92EI21946, Subtask 1, Vienna VA, January 15, 1993.

MODEL INPUT: *ENSINT*

MODEL COMPONENT: Boiler/Steam/Cogeneration

DEFINITION: Intensity for fuel *f* consumed in the BSC component

DISCUSSION:

Intensity for fuels consumed in the BSC component were obtained from the Department of Energy.

SOURCE:

Department of Energy, "Industrial Energy Productivity Project - Final Report," Generic Energy Services, DOE/CS/40151-1, Vol. 7 of 9, February 1983.

MODEL INPUT: *GEN90*

MODEL COMPONENT: Boiler/Steam/Cogeneration

DEFINITION: 1990 generation of electricity

DISCUSSION:

Generation of electricity in 1990 was obtained from EIA-867 data.

SOURCE:

Energy Information Administration, EIA-867, Survey of Independent Power Producers Database.

MODEL INPUT: *GENEQPHTRT*

MODEL COMPONENT: Boiler/Steam/Cogeneration

DEFINITION: Heat rate for cogeneration of electricity by prime mover *m*

DISCUSSION:

Heat rates are assumed to be constant for all industries and all regions. Heat rates change based on the prime mover. For combustion turbines, including gas turbines and combined cycles, the heat rate is assumed to be 14,000 Btu/kWh. Internal combustion engines have a heat rate of 11,000 Btu/kWh. Steam turbines have a heat rate of 25,000 Btu/Kwh. Renewables, including wind turbines, solar and hydropower, are assumed to have a heat rate of 0 Btu/kWh.

SOURCE:

Decision Analysis Corporation of Virginia and Arthur D. Little, "Industrial Model: Baseline Database Final Report," prepared for EIA under contract No. DE-AC01-92EI21946, Task 92-016, Subtask 1, Vienna VA, January 15, 1993, p. 32.

MODEL INPUT: *GENEQPSHR*

MODEL COMPONENT: Boiler/Steam/Cogeneration

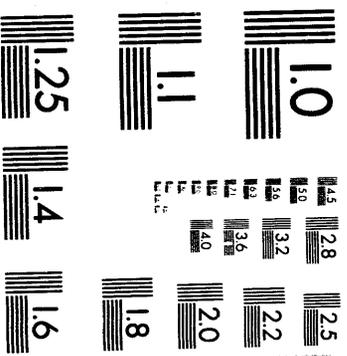
DEFINITION: Share of cogeneration for prime mover *m*

DISCUSSION:

The share of cogeneration by prime mover was obtained from EIA-867 data.

SOURCE:

Energy Information Administration, EIA-867, Survey of Independent Power Producers Database.



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MODEL INPUT: *GENEQPSTEFF*

MODEL COMPONENT: Boiler/Steam/Cogeneration

DEFINITION: Efficiency of cogeneration for prime mover *m*

DISCUSSION:

The efficiency for internal combustion engines and combustion turbines is 74 percent for all industries. The efficiencies for steam turbines and renewables are 0.

SOURCE:

ADL, Facsimile, February 8, 1993.

MODEL INPUT: *GENUTIL*

MODEL COMPONENT: Boiler/Steam/Cogeneration

DEFINITION: Capacity utilization for cogeneration

DISCUSSION:

Capacity utilization data was obtained from EIA-867 data.

SOURCE:

Energy Information Administration, EIA-867, Survey of Independent Power Producers Database.

MODEL INPUT: *GSTEAM*

MODEL COMPONENT: Boiler/Steam/Cogeneration

DEFINITION: Steam demand coefficient for cogeneration regressions

DISCUSSION:

The steam demand coefficient was estimated through a system of simultaneous linear regressions. The following equation was estimated from pooled EIA-867 data over the years 1989, 1990, and 1991.

$$LN(GEN) = \alpha + \beta x LN(STEAM) \quad (A-20)$$

The resulting coefficient, β , is the steam demand coefficient. Data for generation was obtained from the EIA-867 database. Data for steam demand was determined from 1988 MECS. The same coefficient is used for each industry and region.

SOURCES:

Energy Information Administration, EIA-867, Survey of Independent Power Producers Database.

Energy Information Administration, Manufacturing Energy Consumption Survey: Consumption of Energy 1988, DOE/EIA-0512(88), May 1991.

MODEL INPUT: *IDVAL*

MODEL COMPONENT: Process/Assembly

DEFINITION: Units of value of production

DISCUSSION:

A value of one for *IDVAL* indicates that the input data for value of production is in physical units. A value of two indicates that the value of production is in dollar units. The following industries have *IDVAL* equal to 1: paper and allied products, glass and glass products, hydraulic cement, blast furnaces and basic steel products, and primary aluminum.

MODEL INPUT: *INDDIR*
DEFINITION: Industry code
DISCUSSION:

The following table shows the industry codes used by the Industrial model.

| Industry Code | Industry Name | SIC Code |
|--------------------------|---|--------------------|
| Non-Manufacturing | | |
| 01 | Agricultural Production - Crops | 01 |
| 02 | Other Agriculture including livestock | 02 - 09 |
| 03 | Coal Mining | 12 |
| 04 | Oil and Gas Mining | 13 |
| 05 | Metal and Other Non-Metallic Mining | 10, 14 |
| 06 | Construction | 15, 16, 17 |
| Manufacturing | | |
| 07 | Food and Kindred Products | 20 |
| 08 | Tobacco Products | 21 |
| 09 | Textile Mill Products | 22 |
| 10 | Apparel and Other Textile Products | 23 |
| 11 | Lumber and Wood Products | 24 |
| 12 | Furniture and Fixtures | 25 |
| 13 | Paper and Allied Products | 26 |
| 14 | Printing and Publishing | 27 |
| 15 | Bulk Chemicals | 281, 282, 286, 287 |
| 19 | Other Chemicals and Allied Products | 283, 284, 285, 289 |
| 20 | Petroleum Refining | 291 |
| 21 | Asphalt and Miscellaneous Coal Products | 2911 |

| | | |
|----|--|---|
| 22 | Rubber and Miscellaneous Plastics Products | 30 |
| 23 | Leather and Leather Products | 31 |
| 24 | Glass and Glass Products | 321, 322, 323 |
| 25 | Cement, Hydraulic | 324 |
| 26 | Other Stone, Clay, and Glass Products | 325, 326, 327, 328, 329 |
| 27 | Blast Furnace and Basic Steel Products | 331, 332 |
| 28 | Primary Aluminum | 3334, 3341, 3353, 3354, 3355 |
| 29 | Other Primary Metals | 333 - 336, 339, with the above exceptions |
| 30 | Fabricated Metals Products | 34 |
| 31 | Industrial Machinery | 35 |
| 32 | Electronic and Other Electric Equipment | 36 |
| 33 | Transportation Equipment | 37 |
| 34 | Instruments and Related Products | 38 |
| 35 | Miscellaneous Manufacturing | 39 |

MODEL INPUT: *INDSTEPNAME*

MODEL COMPONENT: Process/Assembly

DEFINITION: Step name for process steps

DISCUSSION:

The following process steps are modeled in the Industrial model.

| Industry | Process Step |
|---------------------------|----------------------------|
| Food and Kindred Products | |
| | Direct Heating |
| | Hot Water and Steam |
| | Refrigeration and Freezing |
| | Other Electric Use |
| Paper and Allied Products | |
| | Papermaking |
| | Bleaching |
| | Waste Fibers Pulping |
| | Mechanical Pulping |
| | Semi-Chemical Pulping |
| | Kraft Pulping |
| | Wood Preparation |
| Bulk Chemicals | |

| | |
|---|---------------------|
| | Electrolytic |
| | Other Electric |
| | Direct Fuels |
| | Steam |
| | Feedstocks |
| Glass and Glass Products | |
| | Post-Forming |
| | Forming |
| | Melting/Recycled |
| | Melting/Virgin |
| | Batch Prep/Recycled |
| | Batch Prep/Virgin |
| Hydraulic Cement | |
| | Finish Grinding |
| | Dry Process |
| | Wet Process |
| Blast Furnace and Basic Steel Products | |
| | Cold Rolling |
| | Hot Rolling |
| | Ingot Casting |

| | |
|------------------|------------------------------------|
| | Continuous Casting |
| | Blast Furnace/Open Hearth |
| | Blast Furnace/Basic Oxygen Furnace |
| | Electric Arc Furnace |
| | Coke Ovens |
| Primary Aluminum | |
| | Aluminum Smelting |

SOURCE:

Decision Analysis Corporation and Arthur D. Little, "Industrial Model: Selected Process Flows Revised Final Report," prepared for EIA under Contract No. DE-AC01-92EI21946, Subtask 2B, Vienna, VA, April 26, 1993.

MODEL INPUT: *ITYPE*

MODEL COMPONENT: Process/Assembly

DEFINITION: Equation type for fuel *f* at process step *s*

DISCUSSION:

The equation type determines what method to use to calculate updated UECs. Equation type one assumes the UECs are constant. Equation type two is an econometrically estimated equation. Equation type three corresponds to the technology possibility curves. The non-energy-intensive industries, with a few exceptions, utilize an econometric equation, or equation type two, to estimate UECs. The energy intensive industries, with the exception of the feedstock process step in the bulk chemicals industry, use equation type 3 developed by ADL. The feedstock process step uses equation type one to estimate UEC.

MODEL INPUT: *OGEN*

MODEL COMPONENT: Boiler/Steam/Cogeneration

DEFINITION: Electricity generation for own use coefficient

DISCUSSION:

The electricity generation for own use coefficient was obtained from simultaneous regressions on EIA-867 data for the years 1989 through 1991. A regression relating total generation to steam demand was estimated, then the following equation was estimated for own use generation.

$$LN(OWN) = \alpha + \beta \times LN(GEN) \qquad (A-21)$$

The resulting slope coefficient, β , is the own use coefficient.

SOURCE:

Energy Information Administration, EIA-867, Survey of Independent Power Producers Database.

MODEL INPUT: *OWN90*

MODEL COMPONENT: Boiler/Steam/Cogeneration

DEFINITION: 1990 Electricity generation for own use

DISCUSSION:

1990 generation for own use was obtained from EIA-867 data.

SOURCE:

Energy Information Administration, EIA-867, Survey of Independent Power Producers Database.

MODEL INPUT: *PHDRAT*

MODEL COMPONENT: Process/Assembly

DEFINITION: 1990 production either in physical units or dollar value

DISCUSSION:

PHDRAT is in dollar units for the non-energy-intensive industries, and in physical units for the energy intensive industries except for the food and chemical industries, which are expressed in dollar value of output. Data for the non-energy-intensive industries are expressed in 1987 dollars inflated from 1982 million dollars using PCIO price deflators.

For the industries expressing value of output in physical units, data was obtained from various trade journals. Data for the paper, aluminum, and iron and steel industries were obtained from Business Statistics 1963-1991. Data for the cement industry was obtained from the Minerals Yearbook.

SOURCES:

Business Statistics 1963-1991, p. 110, 113, and 126.

Minerals Yearbook, U.S. Department of the Interior, Bureau of Mines, Volume II.

MODEL INPUT: *PRODFLOW*

MODEL COMPONENT: Process/Assembly

DEFINITION: Fraction of throughput to process step *s* linked through link *l* for
vintage *v*

DISCUSSION:

For the non-energy-intensive industries, the fraction of throughput is one since each non-energy-intensive industry is assumed to consist of only one process step linked to the consumer. For the energy intensive industries, the fraction of throughput to each process step is determined by examining detailed process flows of each industry. All process steps linked to final consumption have a throughput fraction of one since the total amount emerging from the process step is passed directly to the final consumption. In the food and kindred products industry, each step is linked only to the final consumption, therefore the fraction of throughput to each process step through its only link is one. For all other energy intensive industries, if the current step has only one link, then the total amount of throughput at the current process step is divided by the total amount of throughput at the previous step to get fraction of throughput. If the current step is linked to several steps, then the fraction of throughput is determined by dividing the amount of throughput at the current step by the sum of throughput to all steps linked to the current step. Data on physical throughput to each process step is obtained from ADL estimates.

SOURCE:

Decision Analysis Corporation and Arthur D. Little, "Industrial Model: Selected Process Flows Revised Final Report," prepared for EIA under Contract No. DE-AC01-92EI21946, Task 92-016, Subtask 2B, Vienna, VA, April 1993.

MODEL INPUT: *PRODRETR*

MODEL COMPONENT: *Process/Assembly*

DEFINITION: Retirement rate at process step *s*

DISCUSSION:

Retirement rates were obtained from the Bureau of the Census. Unpublished data from the Survey of Plant Capacity from 1977 to 1988 was used to develop retirement rates.

SOURCE:

Bureau of the Census, Survey of Plant Capacity unpublished data.

MODEL INPUT: *STEMCUR₉₀*

MODEL COMPONENT: Boiler/Steam/Cogeneration

DEFINITION: Initial steam demand

DISCUSSION:

Initial steam demand for 1990 is obtained from *1988 Manufacturing Energy Consumption Survey* (MECS) for each industry and region.

SOURCE:

Energy Information Administration, Manufacturing Energy Consumption Survey: Consumption of Energy 1988, DOE/EIA-0512(88), May 1991.

MODEL INPUT: *SULFURCONT*

MODEL COMPONENT:

DEFINITION: Sulfur content of fuel *f*

DISCUSSION:

Sulfur contents are not currently calculated in the model. Therefore, all values are set to one for all fuels.

MODEL INPUT: *UNCONTEMISSFACT*

MODEL COMPONENT:

DEFINITION: Uncontrolled emission factor for pollutant *p* using fuel *f*

DISCUSSION:

Uncontrolled emission factors for all pollutants except CO₂ and total carbon were derived from EPA emissions factors. Carbon emission factors were obtained EIA (1993).

SOURCE:

Energy Information Administration, "Emissions Greenhouse Gases: 1985 - 1990", DOE/EIA-0573 (Washington, D.C., September 1993).

Appendix B. Mathematical Representation of Model Algorithms

Introduction

This appendix presents the subroutine flow diagrams for the Industrial Sector Model and a detailed mathematical description of the industrial model. The diagrams depict the relation between the main modules and the various submodules of the model. The Industrial Sector Model has three main subroutines: IND, ISEAM, and MODCAL. All the other subroutines are called from these subroutines.

Equations are presented for each subroutine according to each of the three model components, as well as miscellaneous equations. Table B-1 provides the location of each equation by providing equations found in each subroutine.

Figure B-1. Main Industrial Subroutine - IND

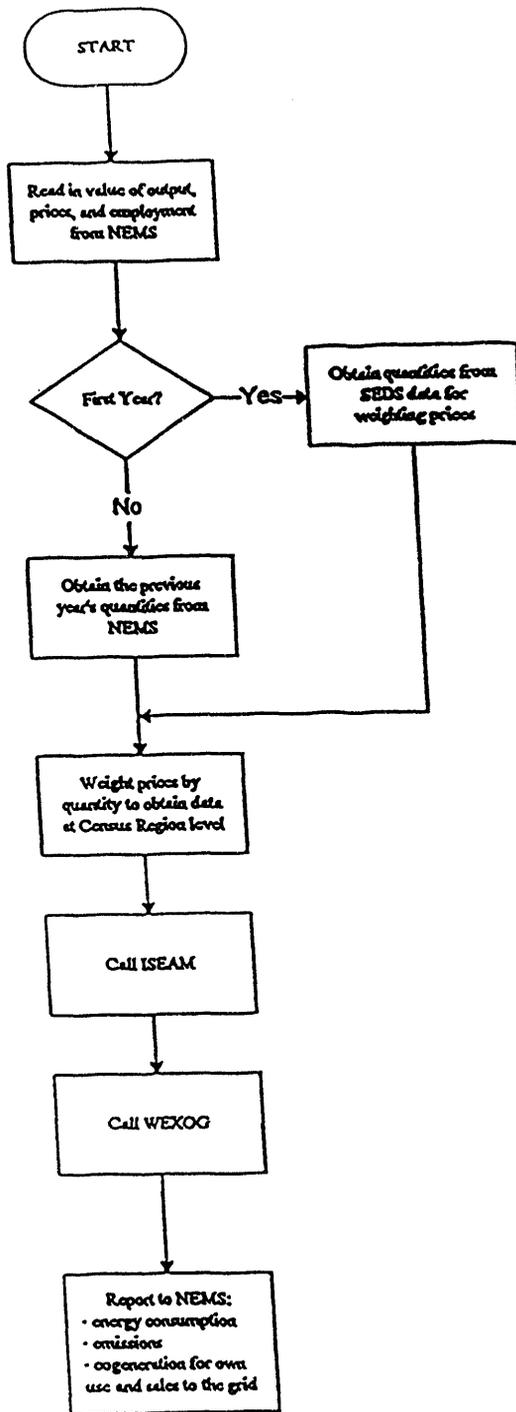


Figure B-2. Subroutine ISEAM

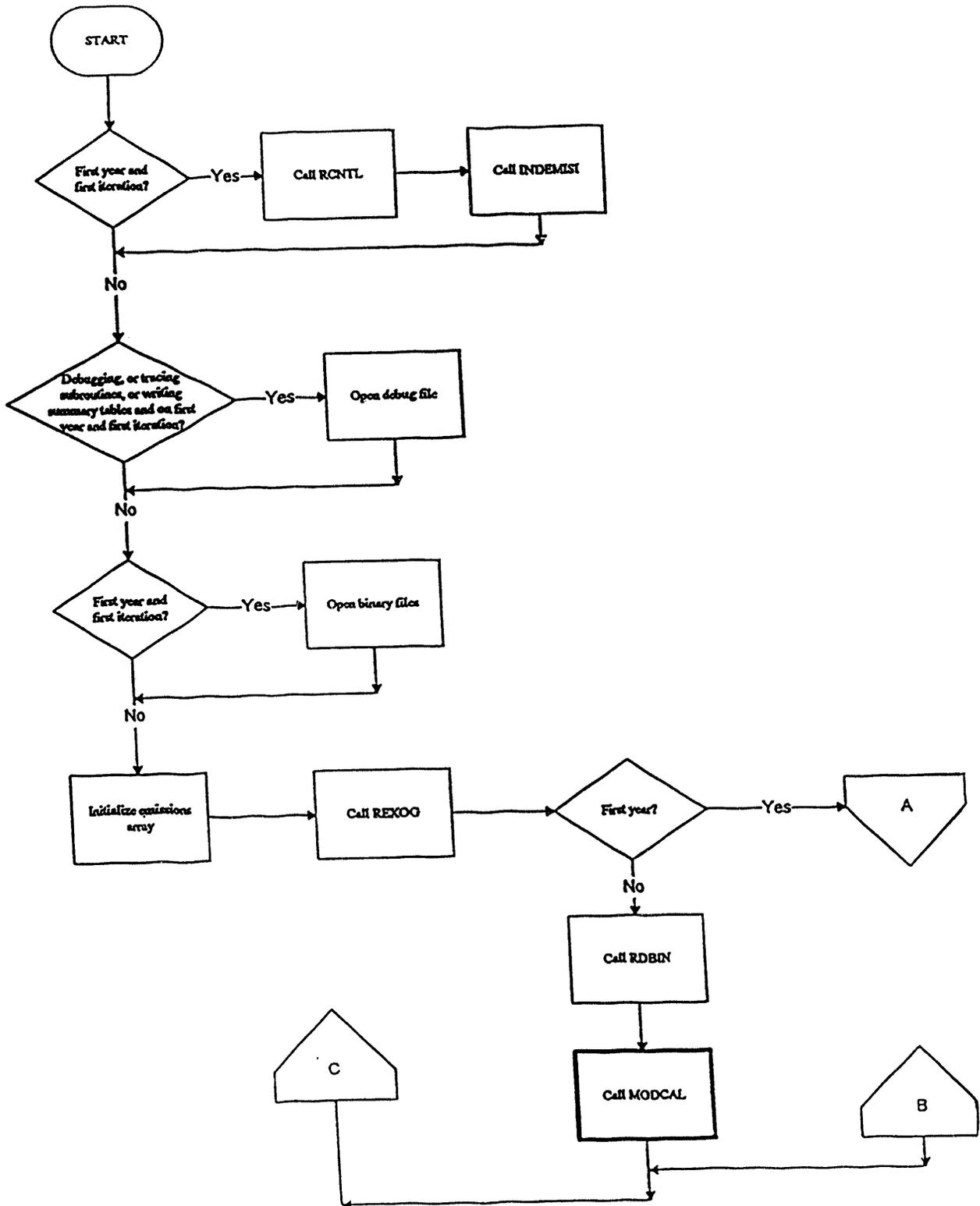


Figure B-2. Subroutine ISEAM, cont.

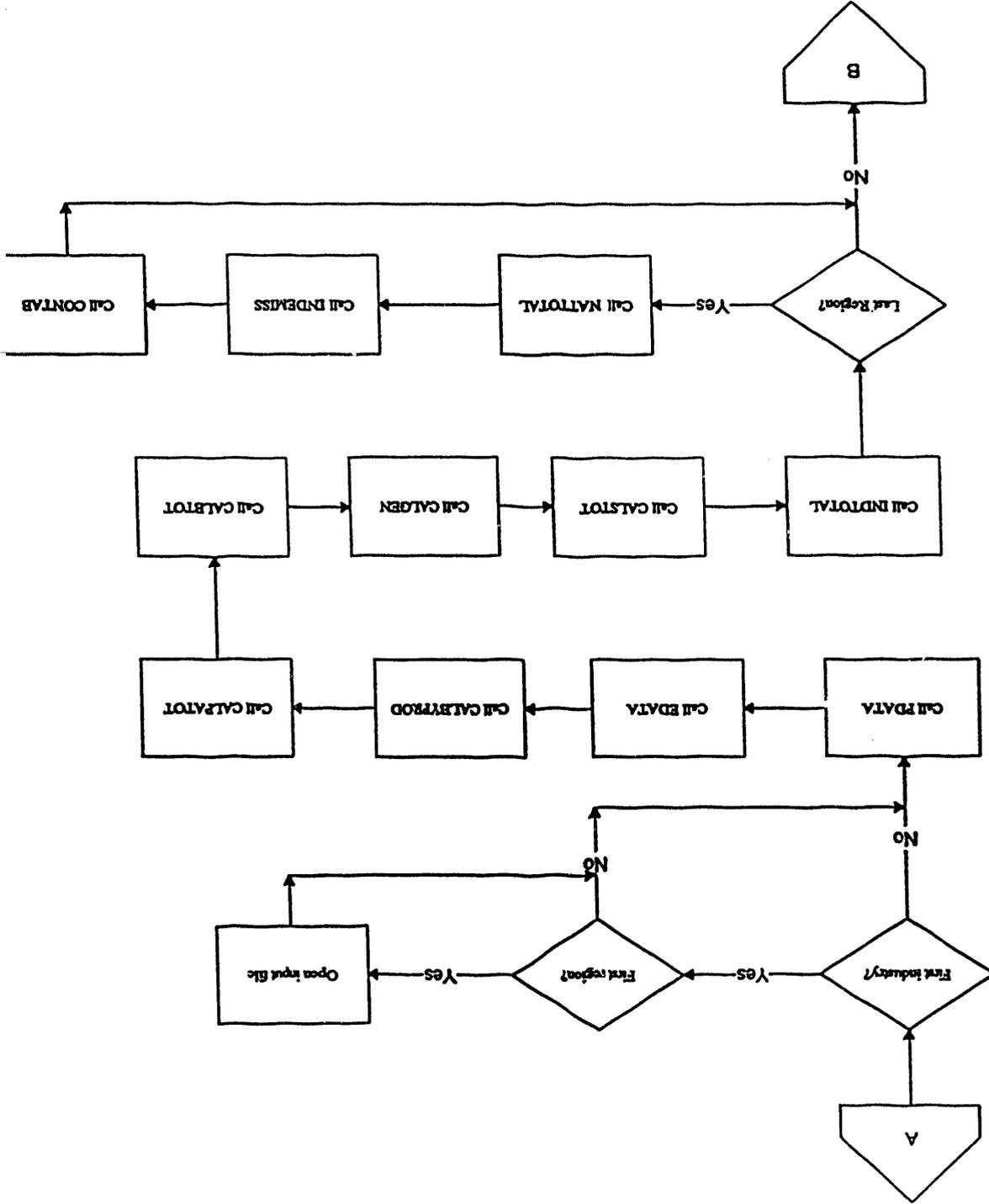


Figure B-2. Subroutine ISEAM, cont.

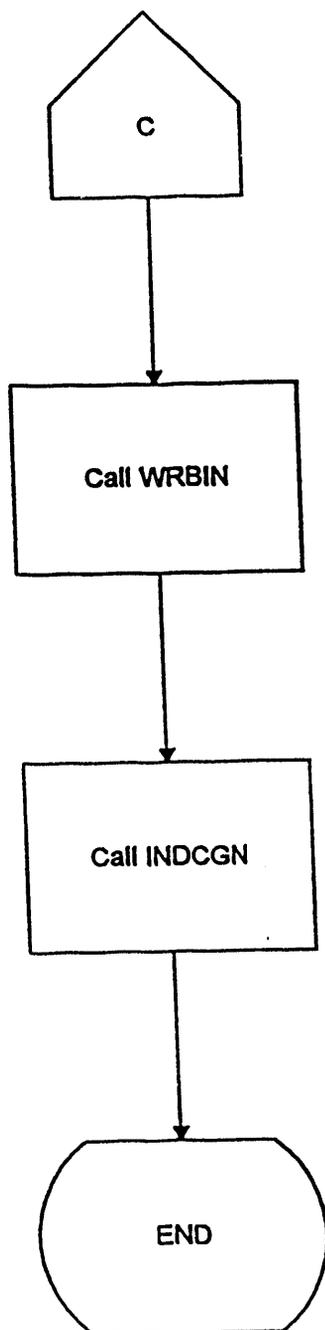


Figure B-3. Subroutine MODCAL

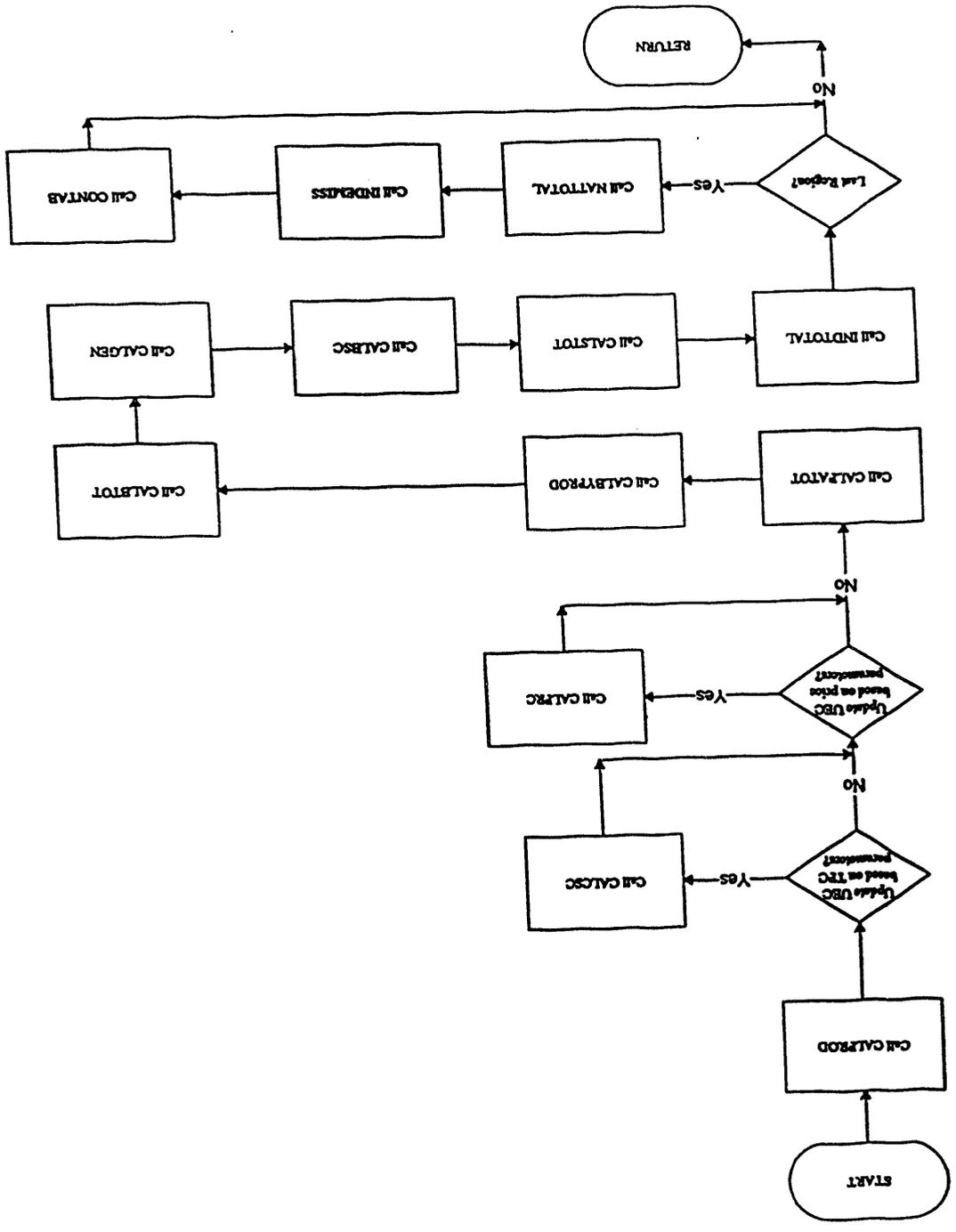


Table B-1. Equation locations

| Subroutine | Equation |
|------------------|----------------|
| <i>CALBSC</i> | B-98 to B-99 |
| <i>CALBTOT</i> | B-1 to B-2 |
| <i>CALBYPROD</i> | B-129 to B-138 |
| <i>CALCSC</i> | None |
| <i>CALCSC1</i> | B-33 |
| <i>CALCSC2</i> | B-34 to B-36 |
| <i>CALCSC3</i> | B-37 to B-58 |
| <i>CALGEN</i> | B-62 to B-73 |
| <i>CALINTER</i> | B-61 |
| <i>CALPATOT</i> | B-3 to B-14 |
| <i>CALPRC</i> | None |
| <i>CALPRC1</i> | None |
| <i>CALPRC2</i> | B-59 to B-60 |
| <i>CALPRC3</i> | None |
| <i>CALPROD</i> | B-15 to B-32 |
| <i>CALSTOT</i> | B-74 to B-87 |
| <i>CONTAB</i> | B-160 to B-178 |
| <i>EDATA</i> | None |
| <i>FUELBOIL</i> | B-88 to B-97 |
| <i>IBSEDS</i> | B-226 to B-229 |
| <i>IND</i> | B-122 to B-125 |
| <i>INDCGN</i> | B-100 to B-121 |

| | |
|-----------------|----------------|
| <i>INDEMISI</i> | None |
| <i>INDEMISS</i> | B-154 to B-159 |
| <i>INDTOTAL</i> | B-139 to B-147 |
| <i>ISEAM</i> | None |
| <i>MODCAL</i> | None |
| <i>NATTOTAL</i> | B-148 to B-153 |
| <i>PDATA</i> | B-230 to B-235 |
| <i>RCNTL</i> | None |
| <i>RDBIN</i> | None |
| <i>REXOG</i> | B-126 to B-128 |
| <i>SUMTAB</i> | B-179 |
| <i>WEXOG</i> | B-180 to B-225 |
| <i>WRBIN</i> | None |
| <i>WRQTY</i> | None |

BUILDINGS

CALBTOT

Calculate energy consumption in buildings

$$ENBQTY_{e,f} = EMPLX_{i,r} \times ENBINT_{e,f} \quad (\text{B-1})$$

where:

- $ENBQTY_{e,f}$ = Consumption of fuel f for building end use e ,
- $EMPLX_{i,r}$ = Employment for industry i in Census region r , and
- $ENBINT_{e,f}$ = Unit energy consumption of fuel f for building end use e .

$$ENBQTY_{total,f} = \sum_{e=1}^2 ENBQTY_{e,f} \quad (\text{B-2})$$

where:

- $ENBQTY_{total,f}$ = Consumption of fuel f for all building end uses, and
- $ENBQTY_{e,f}$ = Consumption of fuel f for building end use e .

PROCESS/ASSEMBLY

CALPATOT

For the construction industry, calculate consumption of asphalt and road oil for years after 1990.

$$ENPQTY_{v,asp,s} = ENPINT_{v,asp,s} \times PRODZERO_{v,s} + 0.4 \times (PRODCUR_{v,s} - PRODZERO_{v,s}) \quad (B-3)$$

where:

$ENPQTY_{v,asp,s}$ = Consumption of asphalt and road oil at process step s for vintage v ,

$ENPINT_{v,asp,s}$ = Unit energy consumption of asphalt and road oil at process step s for vintage v ,

$PRODZERO_{v,s}$ = 1990 production at process step s for vintage v , and

$PRODCUR_{v,s}$ = Production at process step s for vintage v .

For the bulk chemical industry and the natural gas feedstock process step, the following equations are used after 1990.

$$ENPQTY_{v,ngf,s} = ENPINT_{v,ngf,s} \times PRODZERO_{v,s} + 0.25 \times (PRODCUR_{v,s} - PRODZERO_{v,s}) \quad (B-4)$$

where:

$ENPQTY_{v,ngf,s}$ = Consumption of natural gas feedstock at process step s for vintage v ,

$ENPINT_{v,ngf,s}$ = Unit energy consumption of natural gas feedstock at process s step for vintage v ,

$PRODZERO_{v,s}$ = 1990 production at process step s for vintage v , and

$PRODCUR_{v,s}$ = Production at process step s for vintage v .

For liquid petroleum gas and petrochemical feedstocks the following is used.

$$ENPQTY_{v,fd} = ENPINT_{v,fd} \times PRODZERO_{v,fd} + 0.8 \times (PRODCUR_{v,fd} - PRODZERO_{v,fd}) \quad (B-5)$$

where:

$ENPQTY_{v,fd}$ = Consumption of fuel f at the feedstock process step for vintage v ,

$ENPINT_{v,fd}$ = Unit energy consumption of fuel f at the feedstock process step for vintage v ,

$PRODZERO_{v,fd}$ = 1990 production at the feedstock process step for vintage v , and

$PRODCUR_{v,fd}$ = Production at the feedstock process step for vintage v .

For all other fuels and process steps, calculate energy consumption

$$ENPQTY_{v,f,s} = PRODCUR_{v,s} \times ENPINT_{v,f,s} \quad (B-6)$$

where:

$ENPQTY_{v,f,s}$ = Consumption of fuel f at process step s for vintage v ,

$PRODCUR_{v,s}$ = Production at process step s for vintage v , and

$ENPINT_{v,f,s}$ = Unit energy consumption of fuel f at process step s for vintage v .

$$ENPQTY_{total,f,s} = \sum_{v=1}^3 ENPQTY_{v,f,s} \quad (B-7)$$

where:

$$\begin{aligned} ENPQTY_{total,f,s} &= \text{Consumption of fuel } f \text{ at process step } s \text{ for all vintages, and} \\ ENPQTY_{v,f,s} &= \text{Consumption of fuel } f \text{ at process step } s \text{ for vintage } v. \end{aligned}$$

Convert to trillion Btu. For electricity use the following equation.

$$ENPQTY_{v,elec,s} = \frac{ENPQTY_{v,elec,s} \times 3412.0}{10^6} \quad (\text{B-8})$$

where:

$$\begin{aligned} ENPQTY_{v,elec,s} &= \text{Consumption of electricity at process step } s \text{ for vintage } v, \\ 3412.0 &= \text{Conversion factor, 3412.0 Btu per kilowatthour, and} \\ 10^6 &= \text{Conversion factor to convert from MMBtu to trillion Btu.} \end{aligned}$$

For all other fuels use the following

$$ENPQTY_{v,f,s} = \frac{ENPQTY_{v,f,s}}{10^6} \quad (\text{B-9})$$

where:

$$\begin{aligned} ENPQTY_{v,f,s} &= \text{Consumption of fuel } f \text{ at process step } s \text{ for vintage } v, \text{ and} \\ 10^6 &= \text{Conversion factor to convert from MMBtu to trillion Btu.} \end{aligned}$$

$$ENPQTY_{v,total,s} = \sum_{f=1}^{IFMAX_s} ENPQTY_{v,f,s} \quad (\text{B-10})$$

where:

- $ENPQTY_{v,total,s}$ = Consumption of all fuels at process step s for vintage v ,
- $IFMAX_s$ = Number of fuels consumed at process step s , and
- $ENPQTY_{v,f,s}$ = Consumption of fuel f at process step s for vintage v .

Sum energy consumption for main fuels, intermediate fuels, and renewable fuels.

$$ENPMQTY_f = \sum_{s=1}^{MPASTP} ENPQTY_{total,f,s} \quad (\text{B-11})$$

where:

- $ENPMQTY_f$ = Consumption of main fuel f in the PA component,
- $MPASTP$ = Number of process steps, and
- $ENPQTY_{total,f,s}$ = Consumption of fuel f at process step s for all vintages.

$$ENPIQTY_f = \sum_{s=1}^{MPASTP} ENPQTY_{total,f,s} \quad (\text{B-12})$$

where:

- $ENPIQTY_f$ = Consumption of intermediate fuel f in the PA component,
 $MPASTP$ = Number of process steps, and
 $ENPQTY_{total,f,s}$ = Consumption of fuel f at process step s for all vintages.

$$ENPRQTY_f = \sum_{s=1}^{MPASTP} ENPQTY_{total,f,s} \quad (\text{B-13})$$

where:

- $ENPRQTY_f$ = Consumption of renewable fuel f in the PA component,
 $MPASTP$ = Number of process steps, and
 $ENPQTY_{total,f,s}$ = Consumption of fuel f at process step s for all vintages.

For the blast furnace and basic steel products industry at process step 8 (coke ovens), use the following equation:

$$ENPMQTY_{coke} = ENPIQTY_{coke} - \left[PRODCUR_{total,co} \times \frac{24.8}{10^6} \right] \quad (\text{B-14})$$

where:

- $ENPMQTY_{coke}$ = Consumption of coke imports in the PA component,
 $ENPIQTY_{coke}$ = Consumption of coke in the PA component,

- $PRODCUR_{total,co}$ = Production at the coke oven process step for all vintages, and
- $24.8/10^6$ = Conversion factor, where there are 24.8 MMBtu per short ton of coke converted to trillion Btu.

CALPROD

For the manufacturing industries, the following equations are used to retire old and mid vintage production.

$$PRODCUR_{old,s} = [PRODCUR_{old,s} + IDLCAP_{old,s}] \times (1 - PRODRETR_s) \quad (B-15)$$

where:

- $PRODCUR_{old,s}$ = Existing production at process step s for old vintage,
- $IDLCAP_{old,s}$ = Idle production for process step s for old vintage, and
- $PRODRETR_s$ = Retirement rate at process step s .

$$PRODCUR_{mid,s} = (PRODCUR_{mid,s} + PRODCUR_{new,s}) \times (1 - PRODRETR_s) \quad (B-16)$$

where:

- $PRODCUR_{mid,s}$ = Existing production at process step s for mid vintage,
- $PRODCUR_{new,s}$ = Production at process step s for new vintage, and
- $PRODRETR_s$ = Retirement rate at process step s .

For the non-manufacturing industries, there is no retirement data.

$$PRODCUR_{old,s} = PRODCUR_{old,s} + IDLCAP_{old,s} \quad (\text{B-17})$$

where:

$PRODCUR_{old,s}$ = Existing production at process step s for old vintage, and
 $IDLCAP_{old,s}$ = Idle production for process step s for old vintage.

$$PRODCUR_{mid,s} = PRODCUR_{mid,s} + PRODCUR_{new,s} \quad (\text{B-18})$$

where:

$PRODCUR_{mid,s}$ = Existing production at process step s for mid vintage, and
 $PRODCUR_{new,s}$ = Production at process step s for new vintage.

If IDVAL = 1, then

$$PRODX_{i,r} = PHDRAT \times PRODVX_{i,r} \quad (\text{B-19})$$

where:

$PRODX_{i,r}$ = Output in physical units for industry i in Census region r ,
 $PHDRAT$ = Ratio of physical units to value of output, and
 $PRODVX_{i,r}$ = Value of output for industry i in Census region r .

If IDVAL = 2, then

$$PRODX_{i,r} = PRODVX_{i,r} \quad (B-20)$$

where:

$$\begin{aligned} PRODX_{i,r} &= \text{Output in dollar units for industry } i \text{ in Census region } r, \text{ and} \\ PRODVX_{i,r} &= \text{Value of output for industry } i \text{ in Census region } r. \end{aligned}$$

If process step is linked to final consumption then,

$$PRODCUR_{total,s} = PRODFLOW_{old,s,l} \times PRODX_{i,r} \quad (B-21)$$

where:

$$\begin{aligned} PRODCUR_{total,s} &= \text{Production at process step } s \text{ for all vintages,} \\ PRODFLOW_{old,s,l} &= \text{Down-step throughput to process step } s \text{ linked by link } l \text{ for} \\ &\text{old vintage, and} \\ PRODX_{i,r} &= \text{Value of output for industry } i \text{ in Census region } r. \end{aligned}$$

If total current production is greater than production from old and middle vintage, then

$$PRODCUR_{new,s} = PRODCUR_{total,s} - PRODCUR_{old,s} - PRODCUR_{mid,s} \quad (B-22)$$

where:

$$\begin{aligned} PRODCUR_{new,s} &= \text{Production at process step } s \text{ for new vintage,} \\ PRODCUR_{total,s} &= \text{Total production at process step } s \text{ for all vintages,} \end{aligned}$$

$PRODCUR_{old,s}$ = Existing production at process step s for old vintage, and
 $PRODCUR_{mid,s}$ = Existing production at process step s for mid vintage.

If current production is equal to production from old and middle vintage, then $PRODCUR_{new,s} = 0.0$, and $PRODCUR_{mid,s}$ is unaltered.

If current production is less than production from old and middle vintage, then $PRODCUR_{new,s} = 0.0$ and

$$PRODCUR_{old,s} = PRODCUR_{old,s} - IDLCAP_{old,s} \quad (B-23)$$

where:

$PRODCUR_{old,s}$ = Existing production at process step s for old vintage, and
 $IDLCAP_{old,s}$ = Idle production for process step s for old vintage.

$$IDLCAP_{old,s} = PRODCUR_{old,s} + PRODCUR_{mid,s} - PRODCUR_{total,s} \quad (B-24)$$

where:

$IDLCAP_{old,s}$ = Idle production for process step s for old vintage,
 $PRODCUR_{old,s}$ = Existing production at process step s for old vintage,
 $PRODCUR_{mid,s}$ = Existing production at process step s for mid vintage, and
 $PRODCUR_{total,s}$ = Production at process step s for all vintages.

If $PRODCUR_{old,s}$ is less than 0, then

$$PRODCUR_{mid,s} = PRODCUR_{mid,s} + PRODCUR_{old,s} \quad (B-25)$$

where:

- $PRODCUR_{mid,s}$ = Existing production at process step s for mid vintage, and
 $PRODCUR_{old,s}$ = Existing production at process step s for old vintage.

If $PRODCUR_{mid,s}$ is less than 0, then $PRODCUR_{mid,s} = 0.0$.

If step is not linked to final consumption and there is no new production, then

$$PRODSUM_{new,s,l} = PRODCUR_{total,IP} \times PRODFLOW_{old,s,l} \quad (B-26)$$

where:

- $PRODSUM_{new,s,l}$ = Amount of throughput used at process step s through link l for new vintage,
 $PRODCUR_{total,IP}$ = Production at process step IP linked to process step s through link l for all vintages, and
 $PRODFLOW_{old,s,l}$ = Down-step throughput to process step s linked by link l for old vintage.

$$PRODCUR_{total,s} = PRODCUR_{total,s} + PRODSUM_{new,s,l} \quad (B-27)$$

where:

- $PRODCUR_{total,s}$ = Production at process step s for all vintages, and

$PRODSUM_{new,s,l}$ = Amount of throughput used at process step s through link l for new vintage.

If link l is the last link for process step s , then $PRODCUR_{new,s} = 0.0$. And,

$$PRODCUR_{old,s} = PRODCUR_{total,s} - PRODCUR_{mid,s} \quad (\text{B-28})$$

where:

$PRODCUR_{old,s}$ = Existing production at process step s for old vintage,
 $PRODCUR_{total,s}$ = Production at process step s for all vintages, and
 $PRODCUR_{mid,s}$ = Existing production at process step s for mid vintage.

If $PRODCUR_{old,s}$ is less than 0, then

$$PRODCUR_{mid,s} = PRODCUR_{mid,s} + PRODCUR_{old,s} \quad (\text{B-29})$$

where:

$PRODCUR_{mid,s}$ = Existing production at process step s for mid vintage, and
 $PRODCUR_{old,s}$ = Existing production at process step s for old vintage.

If $PRODCUR_{mid,s}$ is less than 0, then $PRODCUR_{mid,s} = 0.0$.

If there is new production, then

$$PRODSUM_{new,s,l} = PRODCUR_{new,IP} \times PRODFLOW_{new,s,l} \quad (B-30)$$

where:

$PRODSUM_{new,s,l}$ = Amount of throughput used at process step s through link l for new vintage,

$PRODCUR_{new,IP}$ = Production at process step IP linked to process step s through link l for new vintage, and

$PRODFLOW_{new,s,l}$ = Down-step throughput to process step s linked by link l for new vintage.

$$PRODCUR_{new,s} = PRODCUR_{new,s} + PRODSUM_{new,s,l} \quad (B-31)$$

where:

$PRODCUR_{new,s}$ = Production at process step s for new vintage, and

$PRODSUM_{new,s,l}$ = Amount of throughput used at process step s through link l for new vintage.

If new production at the first process step is not zero, then

$$PRODCUR_{total,s} = PRODCUR_{old,s} + PRODCUR_{mid,s} + PRODCUR_{new,s} \quad (B-32)$$

where:

$PRODCUR_{total,s}$ = Production at process step s for all vintages,

$PRODCUR_{old,s}$ = Existing production at process step s for old vintage,

$PRODCUR_{mid,s}$ = Existing production at process step s for mid vintage, and

$PRODCUR_{new,s}$ = Production at process step s for new vintage.

CALCSC1

Calculate UEC's

$$ENPINT_{v,f,s} = ENPINTLAG_{v,f,s} \quad (B-33)$$

where:

$ENPINT_{v,f,s}$ = Unit energy consumption of fuel f at process step s for vintage v , and

$ENPINTLAG_{v,f,s}$ = Lagged unit energy consumption of fuel f at process step s for vintage v .

CALCSC2

Calculate CSC's for old and new vintage. If $CUMOUT_{total,s}$ is less than or equal to zero, then $CSCCUR_{v,f,s} = 1.0$, otherwise use the following equation.

$$CSCCUR_{v,f,s} = [CUMOUT_{total,s}]^{BCSC_{v,f,s}} \quad (B-34)$$

where:

$CSCCUR_{v,f,s}$ = Current energy savings at process step s for fuel f for vintage v ,

- $CUMOUT_{total,s}$ = Cumulative output, from 1958 through the lag of the current year, at process step s for all vintages, and
- $BCSC_{v,f,s}$ = Energy savings coefficient at process step s for fuel f and vintage v .

Calculate the UEC's for old and new vintage.

$$ENPINT_{v,f,s} = EINTER_{v,f,s} \times CSCCUR_{v,f,s} \quad (\text{B-35})$$

where:

- $ENPINT_{v,f,s}$ = Unit energy consumption of fuel f at process step s for vintage v ,
- $EINTER_{v,f,s}$ = Intercept at process step s for fuel f for vintage v , and
- $CSCCUR_{v,f,s}$ = Current energy savings at process step s for fuel f for vintage v .

For mid vintage use the following equation for UEC.

$$ENPINT_{mid,f,s} = \frac{SUMPINT_{f,s}}{CUMPROD_{new,s}} \quad (\text{B-36})$$

where:

- $ENPINT_{mid,f,s}$ = Unit energy consumption of fuel f at process step s for mid vintage,
- $SUMPINT_{f,s}$ = Cumulative unit energy consumption of fuel f at process step s , and
- $CUMPROD_{new,s}$ = Cumulative production at process step s for new vintage.

CALCSC3

Calculate CSC's for old and new vintage.

$$CSCCUR_{v,f,s} = e^{BCSC_{v,f,s} \times (CURIYR - 1)} \quad (B-37)$$

where:

- $CSCCUR_{v,f,s}$ = Current energy savings at process step s for fuel f for vintage v ,
- $BCSC_{v,f,s}$ = Energy savings coefficient at process step s for fuel f and vintage v , and
- $CURIYR$ = Current year index.

Calculate UEC's.

$$ENPINT_{v,f,s} = EINTER_{v,f,s} \times CSCCUR_{v,f,s} \quad (B-38)$$

where:

- $ENPINT_{v,f,s}$ = Unit energy consumption of fuel f at process step s for vintage v ,
- $EINTER_{v,f,s}$ = Intercept at process step s for fuel f for vintage v , and
- $CSCCUR_{v,f,s}$ = Current energy savings at process step s for fuel f for vintage v .

For the cold rolling process step for the blast furnace and basic steel products industry, use the following equations for new vintage UEC's.

Electric

$$ENPINT_{new,elec,s} = EINTER_{new,elec,s} \times CSCCUR_{new,elec,s} \times \frac{1}{0.20} \times \left[0.20 + \frac{(0.21 - 0.20) \times (CURIYR - 1)}{25} \right] \quad (B-39)$$

where:

$ENPINT_{new,elec,s}$ = Unit energy consumption of electricity at process step s for new vintage,

$EINTER_{new,elec,s}$ = Intercept at process step s for electricity for new vintage,

$CSCCUR_{new,elec,s}$ = Current energy savings at process step s for electricity for new vintage, and

$CURIYR$ = Current year index.

Natural Gas

$$ENPINT_{new,ng,s} = EINTER_{new,ng,s} \times CSCCUR_{new,ng,s} \times \frac{1}{0.38} \times \left[0.38 + \frac{(0.31 - 0.38) \times (CURIYR - 1)}{25} \right] \quad (B-40)$$

where:

$ENPINT_{new,ng,s}$ = Unit energy consumption of natural gas at process step s for new vintage,

$EINTER_{new,ng,s}$ = Intercept at process step s for natural gas for new vintage,

$CSCCUR_{new,ng,s}$ = Current energy savings at process step s for natural gas for new vintage, and

$CURIYR$ = Current year index.

Residual fuel

$$ENPINT_{new,rfcs,s} = EINTER_{new,rfcs,s} \times CSCCUR_{new,rfcs,s} \times \frac{1}{0.007} \times \left[0.007 + \frac{(0.006 - 0.007) \times (CURIYR - 1)}{25} \right] \quad (B-41)$$

where:

- $ENPINT_{new, res, s}$ = Unit energy consumption of residual fuel at process step s for new vintage,
- $EINTER_{new, res, s}$ = Intercept at process step s for residual fuel for new vintage,
- $CSCCUR_{new, res, s}$ = Current energy savings at process step s for residual fuel for new vintage, and
- $CURIYR$ = Current year index.

Distillate

$$ENPINT_{new, dis, s} = EINTER_{new, dis, s} \times CSCCUR_{new, dis, s} \times \frac{1}{0.001} \times \left[0.001 + \frac{(0.0008 - 0.001) \times (CURIYR - 1)}{25} \right] \quad (\text{B-42})$$

where:

- $ENPINT_{new, dis, s}$ = Unit energy consumption of distillate at process step s for new vintage,
- $EINTER_{new, dis, s}$ = Intercept at process step s for distillate for new vintage,
- $CSCCUR_{new, dis, s}$ = Current energy savings at process step s for distillate for new vintage, and
- $CURIYR$ = Current year index.

Liquid petroleum gas

$$ENPINT_{new, lpg, s} = EINTER_{new, lpg, s} \times CSCCUR_{new, lpg, s} \times \frac{1}{0.001} \times \left[0.001 + \frac{(0.0008 - 0.001) \times (CURIYR - 1)}{25} \right] \quad (\text{B-43})$$

where:

- $ENPINT_{new,lp,g,s}$ = Unit energy consumption of liquid petroleum gas at process step s for new vintage,
- $EINTER_{new,lp,g,s}$ = Intercept at process step s for liquid petroleum gas for new vintage,
- $CSCCUR_{new,lp,g,s}$ = Current energy savings at process step s for liquid petroleum gas for new vintage, and
- $CURIYR$ = Current year index.

Petroleum coke

$$ENPINT_{new,pc,s} = EINTER_{new,pc,s} \times CSCCUR_{new,pc,s} \times \frac{1}{0.0002} \times \left[0.0002 + \frac{(0.00016 - 0.0002) \times (CURIYR - 1)}{25} \right] \quad (\text{B-44})$$

where:

- $ENPINT_{new,pc,s}$ = Unit energy consumption of petroleum coke at process step s for new vintage,
- $EINTER_{new,pc,s}$ = Intercept at process step s for petroleum coke for new vintage,
- $CSCCUR_{new,pc,s}$ = Current energy savings at process step s for petroleum coke for new vintage, and
- $CURIYR$ = Current year index.

Other petroleum

$$ENPINT_{new,pet,s} = EINTER_{new,pet,s} \times CSCCUR_{new,pet,s} \times \frac{1}{0.002} \times \left[0.002 + \frac{(0.0016 - 0.002) \times (CURIYR - 1)}{25} \right] \quad (\text{B-45})$$

where:

- $ENPINT_{new,pet,s}$ = Unit energy consumption of other petroleum at process step s for new vintage,
- $EINTER_{new,pet,s}$ = Intercept at process step s for other petroleum for new vintage,
- $CSCCUR_{new,pet,s}$ = Current energy savings at process step s for other petroleum for new vintage, and
- $CURIYR$ = Current year index.

Steam

$$ENPINT_{new,st,s} = EINTER_{new,st,s} \times CSCCUR_{new,st,s} \times \frac{1}{0.41} \times \left[0.41 + \frac{(0.47 - 0.41) \times (CURIYR - 1)}{25} \right] \quad (\text{B-46})$$

where:

- $ENPINT_{new,st,s}$ = Unit energy consumption of steam at process step s for new vintage,
- $EINTER_{new,st,s}$ = Intercept at process step s for steam for new vintage,
- $CSCCUR_{new,st,s}$ = Current energy savings at process step s for steam for new vintage, and
- $CURIYR$ = Current year index.

For the blast furnace process step in the blast furnace and basic steel products industry, use the following equations to calculate UEC's.

Natural Gas

$$ENPINT_{old,ng,s} = EINTER_{old,ng,s} \times CSCCUR_{old,ng,s} \times \frac{1}{0.06} \times \left[0.06 + \frac{(0.26 - 0.06) \times (CURIYR - 1)}{25} \right] \quad (B-47)$$

where:

- $ENPINT_{old,ng,s}$ = Unit energy consumption of natural gas at process step s for old vintage,
- $EINTER_{old,ng,s}$ = Intercept at process step s for natural gas for old vintage,
- $CSCCUR_{old,ng,s}$ = Current energy savings at process step s for natural gas for old vintage, and
- $CURIYR$ = Current year index.

$$ENPINT_{new,ng,s} = EINTER_{new,ng,s} \times CSCCUR_{new,ng,s} \times \frac{1}{0.07} \times \left[0.07 + \frac{(0.36 - 0.07) \times (CURIYR - 1)}{25} \right] \quad (B-48)$$

where:

- $ENPINT_{new,ng,s}$ = Unit energy consumption of natural gas at process step s for new vintage,
- $EINTER_{new,ng,s}$ = Intercept at process step s for natural gas for new vintage,
- $CSCCUR_{new,ng,s}$ = Current energy savings at process step s for natural gas for new vintage, and
- $CURIYR$ = Current year index.

Coke

$$ENPINT_{old, coke, s} = EINTER_{old, coke, s} \times CSCCUR_{old, coke, s} \times \frac{1}{0.77} \times \left[0.77 + \frac{(0.57 - 0.77) \times (CURIYR - 1)}{25} \right] \quad (B-49)$$

where:

- $ENPINT_{old, coke, s}$ = Unit energy consumption of coke at process step s for old vintage,
- $EINTER_{old, coke, s}$ = Intercept at process step s for coke for old vintage,
- $CSCCUR_{old, coke, s}$ = Current energy savings at process step s for coke for old vintage, and
- $CURIYR$ = Current year index.

$$ENPINT_{new, coke, s} = EINTER_{new, coke, s} \times CSCCUR_{new, coke, s} \times \frac{1}{0.82} \times \left[\frac{(0.00 - 0.82) \times (CURIYR - 1)}{25} \right] \quad (B-50)$$

where:

- $ENPINT_{new, coke, s}$ = Unit energy consumption of coke at process step s for new vintage,
- $EINTER_{new, coke, s}$ = Intercept at process step s for coke for new vintage,
- $CSCCUR_{new, coke, s}$ = Current energy savings at process step s for coke for new vintage, and
- $CURIYR$ = Current year index.

Steam Coal

$$ENPINT_{new,coal,s} = EINTER_{new,coal,s} \times CSCCUR_{new,coal,s} \times \frac{1}{0.01} \times \left[0.01 + \frac{(0.53 - 0.01) \times (CURIYR - 1)}{25} \right] \quad \text{(B-51)}$$

where:

- $ENPINT_{new,coal,s}$ = Unit energy consumption of steam coal at process step s for new vintage,
- $EINTER_{new,coal,s}$ = Intercept at process step s for steam coal for new vintage,
- $CSCCUR_{new,coal,s}$ = Current energy savings at process step s for steam coal for new vintage, and
- $CURIYR$ = Current year index.

For the dry process step in the hydraulic cement industry use the following equations to calculate UEC's.

Electricity

$$ENPINT_{new,elec,s} = EINTER_{new,elec,s} \times CSCCUR_{new,elec,s} \times \frac{1}{0.17} \left[0.17 + \frac{(0.21 - 0.17) \times (CURIYR - 1)}{25} \right] \quad \text{(B-52)}$$

where:

- $ENPINT_{new,elec,s}$ = Unit energy consumption of electricity at process step s for new vintage,
- $EINTER_{new,elec,s}$ = Intercept at process step s for electricity for new vintage,
- $CSCCUR_{new,elec,s}$ = Current energy savings at process step s for electricity for new vintage, and
- $CURIYR$ = Current year index.

Natural Gas

$$ENPINT_{new,ng,s} = EINTER_{new,ng,s} \times CSCCUR_{new,ng,s} \times \frac{1}{0.154} \left[0.154 + \frac{(0.147 - 0.154) \times (CURIYR - 1)}{25} \right] \quad (B-53)$$

where:

- $ENPINT_{new,ng,s}$ = Unit energy consumption of natural gas at process step s for new vintage,
- $EINTER_{new,ng,s}$ = Intercept at process step s for natural gas for new vintage,
- $CSCCUR_{new,ng,s}$ = Current energy savings at process step s for natural gas for new vintage, and
- $CURIYR$ = Current year index.

Steam Coal

$$ENPINT_{new,coal,s} = EINTER_{new,coal,s} \times CSCCUR_{new,coal,s} \times \frac{1}{0.53} \left[0.53 + \frac{(0.505 - 0.53) \times (CURIYR - 1)}{25} \right] \quad (B-54)$$

where:

- $ENPINT_{new,coal,s}$ = Unit energy consumption of steam coal at process step s for new vintage,
- $EINTER_{new,coal,s}$ = Intercept at process step s for steam coal for new vintage,
- $CSCCUR_{new,coal,s}$ = Current energy savings at process step s for steam coal for new vintage, and
- $CURIYR$ = Current year index.

Residual Fuel

$$ENPINT_{new,res,s} = EINTER_{new,res,s} \times CSCCUR_{new,res,s} \times \frac{1}{0.004} \left[0.004 + \frac{(0.0038 - 0.004) \times (CURIYR - 1)}{25} \right] \quad (B-55)$$

where:

- $ENPINT_{new,res,s}$ = Unit energy consumption of residual fuel at process step s for new vintage,
- $EINTER_{new,res,s}$ = Intercept at process step s for residual fuel for new vintage,
- $CSCCUR_{new,res,s}$ = Current energy savings at process step s for residual fuel for new vintage, and
- $CURIYR$ = Current year index.

Distillate Fuel

$$ENPINT_{new,dist,s} = EINTER_{new,dist,s} \times CSCCUR_{new,dist,s} \times \frac{1}{0.023} \left[0.023 + \frac{(0.022 - 0.023) \times (CURIYR - 1)}{25} \right] \quad (B-56)$$

where:

- $ENPINT_{new,dist,s}$ = Unit energy consumption of distillate fuel at process step s for new vintage,
- $EINTER_{new,dist,s}$ = Intercept at process step s for distillate fuel for new vintage,
- $CSCCUR_{new,dist,s}$ = Current energy savings at process step s for distillate fuel for new vintage, and
- $CURIYR$ = Current year index.

Other Petroleum

$$ENPINT_{new,pet,s} = EINTER_{new,pet,s} \times CSCCUR_{new,pet,s} \times \frac{1}{0.118} \left[0.118 + \frac{(0.112 - 0.118) \times (CURIYR - 1)}{25} \right] \quad (B-57)$$

where:

- $ENPINT_{new,pet,s}$ = Unit energy consumption of other petroleum at process step s for new vintage,
- $EINTER_{new,pet,s}$ = Intercept at process step s for other petroleum for new vintage,
- $CSCCUR_{new,pet,s}$ = Current energy savings at process step s for other petroleum for new vintage, and
- $CURIYR$ = Current year index.

Calculate UECs for middle vintage.

$$ENPINT_{mid,f,s} = \frac{SUMPINT_{f,s}}{CUMPROD_{new,s}} \quad (B-58)$$

where:

- $ENPINT_{mid,f,s}$ = Unit energy consumption of fuel f at process step s for middle vintage,
- $SUMPINT_{f,s}$ = Cumulative unit energy consumption of fuel f at process step s , and
- $CUMPROD_{new,s}$ = Cumulative production at process step s for new vintage.

CALPRC2

Calculate energy savings for old and new vintage.

$$PRCCUR_{v,f,s} = \prod_{t=1}^{11} [WPRC_t]^{BELAS_{v,f,s,t}} \quad (\text{B-59})$$

where:

- $PRCCUR_{v,f,s}$ = Current energy savings based on price for fuel f at process step s for vintage v ,
- $WPRC_t$ = Price for fuel t in 1987 dollars, and
- $BELAS_{v,f,s,t}$ = Own price elasticity at process step s for fuel f and cross price elasticity with fuel f and fuel t for vintage v .

Calculate UECs for old and new vintage.

$$ENPINT_{v,f,s} = ENPINT_{v,f,s} \times PRCCUR_{v,f,s} \quad (\text{B-60})$$

where:

- $ENPINT_{v,f,s}$ = Unit energy consumption of fuel f at process step s for vintage v , and
- $PRCCUR_{v,f,s}$ = Current energy savings based on price for fuel f at process step s for vintage v .

CALINTER

Calculate the intercept for old and new vintage.

$$EINTER_{old,f,s} = \frac{ENPINT_{old,f,s}}{[CUMOUT88]^{BCSC_{old,f,s}} \times \prod_{t=1}^{11} [WPRC_t]^{BELAS_{old,f,s,t}}} \quad (\text{B-61})$$

where:

- $EINTER_{old,f,s}$ = Intercept at process step s for fuel f for old vintage,
- $ENPINT_{old,f,s}$ = Unit energy consumption of fuel f at process step s for old vintage,
- $CUMOUT88$ = Cumulative output through the year 1988,
- $BCSC_{old,f,s}$ = Energy savings coefficient at process step s for fuel f and old vintage,
- $WPRC_t$ = Price for fuel t in 1987 dollars, and
- $BELAS_{old,f,s,t}$ = Own price elasticity at process step s for fuel f for old vintage, and cross price elasticity at process step s for fuel f and fuel t for old vintage.

The intercept for new vintage equals the intercept for old vintage calculated above.

BOILER/STEAM/COGENERATION

CALGEN

Calculate total electricity demand

$$ELDEM = ENPMQTY_{elec} + ENBQTY_{total,elec} \quad (B-62)$$

where:

| | | |
|-----------------------|---|---|
| $ELDEM$ | = | Total electricity demand from process/assembly and buildings, |
| $ENPMQTY_{elec}$ | = | Consumption of electricity in the PA component, and |
| $ENBQTY_{total,elec}$ | = | Consumption of electricity for all building end uses. |

Calculate total steam demand

$$STEMCUR = ENBQTY_{hvac,steam} + ENPIQTY_{steam} \quad (B-63)$$

- where:

| | | |
|-----------------------|---|---|
| $STEMCUR$ | = | Total steam demand, |
| $ENBQTY_{hvac,steam}$ | = | Consumption of steam for HVAC, and |
| $ENPIQTY_{steam}$ | = | Consumption of steam in the PA component. |

Calculate the intercept if year is 1990.

$$GINTER = \ln \left[\frac{GEN90}{(STEMCUR)_{90}^{GSTEAM}} \right] \quad (B-64)$$

where:

| | | |
|------------------------------|---|---------------------------------------|
| <i>GINTER</i> | = | Intercept for electricity generation, |
| <i>GEN90</i> | = | 1990 generation of electricity, |
| <i>STEMCUR</i> ₉₀ | = | Total steam demand for 1990, and |
| <i>GSTEAM</i> | = | Steam demand coefficient. |

Calculate total US electricity generation for the industry.

$$ELGEN_{total} = e^{GINTER} \times STEMCUR^{GSTEAM} \quad (B-65)$$

where:

| | | |
|-------------------------------|---|---|
| <i>ELGEN</i> _{total} | = | Electricity generation from all prime movers, |
| <i>GINTER</i> | = | Intercept term for electricity generation, |
| <i>STEMCUR</i> | = | Total steam demand, and |
| <i>GSTEAM</i> | = | Steam demand coefficient. |

Calculate capacity.

$$ELCAP = \frac{ELGEN_{total} \times 10^9}{GENUTIL \times 3412.0 \times 365.25 \times 24.0} \quad (B-66)$$

where:

| | | |
|------------------------------|---|---|
| <i>ELCAP</i> | = | Capacity for electricity generation, |
| <i>ELGEN_{total}</i> | = | Electricity generation from all prime movers, |
| <i>GENUTIL</i> | = | Capacity utilization for cogeneration, |
| 3412.0 | = | Conversion factor, 3412.0 Btu per kilowatthour, |
| 365.25 | = | Number of days per year, |
| 24.0 | = | Number of hours per day, and |
| 10 ⁹ | = | Conversion factor to convert to megawatts. |

Calculate intercept for own use generation.

$$OINTER = \ln \left[\frac{OWN90}{(ELGEN_{total})^{OGEN}} \right] \quad (B-67)$$

where:

| | | |
|------------------------------|---|---|
| <i>OINTER</i> | = | Intercept for own use generation, |
| <i>OWN90</i> | = | 1990 electricity generation for own use, |
| <i>ELGEN_{total}</i> | = | Electricity generation from all prime movers, and |
| <i>OGEN</i> | = | Own use generation coefficient. |

Calculate electricity generated for own use.

$$ELOWN = e^{OINTER} \times ELGEN_{total}^{OGEN} \quad (B-68)$$

where:

| | | |
|------------------------------|---|---|
| <i>ELOWN</i> | = | Electricity generation for own use, |
| <i>OINTER</i> | = | Intercept for own use generation, |
| <i>ELGEN_{total}</i> | = | Electricity generation from all prime movers, and |
| <i>OGEN</i> | = | Own use generation coefficient. |

Calculate electricity generated for sales.

$$ELSALE = ELGEN_{total} - ELOWN \quad (B-69)$$

where:

| | | |
|------------------------------|---|---|
| <i>ELSALE</i> | = | Electricity generation for sales to the grid, |
| <i>ELGEN_{total}</i> | = | Electricity generation from all prime movers, and |
| <i>ELOWN</i> | = | Electricity generation for own use. |

Calculate electricity generation by prime mover.

$$ELGEN_m = ELGEN_{total} \times GENEQPSHR_m \quad (B-70)$$

where:

| | | |
|------------------------------|---|--|
| <i>ELGEN_m</i> | = | Electricity generation from prime mover <i>m</i> , |
| <i>ELGEN_{total}</i> | = | Electricity generation from all prime movers, and |

$GENEQPSHR_m$ = Share of generation for prime mover m .

Electricity generation for own use (ELOWN), electricity generation for sales to the grid (ELSALE), and capacity for electricity generation (ELCAP) are totaled across industries for each region.⁹

$$ELOTOT_r = \sum_{i=1}^{INDMAX} ELOWN_{r,i} \text{ for } r=1,\dots,4. \quad (\text{B-71})$$

where:

$ELOTOT_r$ = Total industrial electricity generation for own use in Census region r ,

$INDMAX$ = Number of industries, and

$ELOWN$ = Electricity generation for own use.

$$ELSTOT_r = \sum_{i=1}^{INDMAX} ELSALE_{r,i} \text{ for } r=1,\dots,4. \quad (\text{B-72})$$

where:

$ELSTOT_r$ = Total industrial electricity generation for sales to the grid in Census region r ,

$INDMAX$ = Number of industries, and

$ELSALE$ = Electricity generation for sales to the grid.

⁹Notice that the variables are shown as indexed. Although the variables for the totals are subscripted, the non-total variables are not (they are shown that way as a convenience for this documentation). In the computer code, the individual values are computed for each industry and region combination and summed into the totals.

$$ELCTOT_r = \sum_{i=1}^{INDMAX} ELCAP_{r,i} \text{ for } r=1,\dots,4. \quad (\text{B-73})$$

where:

- ELCTOT_r* = Capacity for industrial electricity generation in Census region *r*,
- INDMAX* = Number of industries, and
- ELCAP* = Capacity for electricity generation.

CALSTOT

Calculate fuel consumption from internal combustion engine and combustion turbine.

$$ICEFUEL = ELGEN_{ice} \times \frac{GENEQPHTRT_{ice}}{3412.0} \quad (\text{B-74})$$

where:

- ICEFUEL* = Fuel consumption for electricity generation from internal combustion engines,
- ELGEN_{ice}* = Electricity generation from internal combustion engines,
- GENEQPHTRT_{ice}* = Heat rate for internal combustion engines, and
- 3412.0 = Conversion factor to convert from kWh to Btu.

$$GCTFUEL = ELGEN_{ct} \times \frac{GENEQPHTRT_{ct}}{3412.0} \quad (\text{B-75})$$

where:

- GCTFUEL* = Fuel consumption for electricity generation from combustion turbines,

| | | |
|-------------------|---|--|
| $ELGEN_{ct}$ | = | Electricity generation from combustion turbines, |
| $GENEQPHTRT_{ct}$ | = | Heat rate for combustion turbines, and |
| 3412.0 | = | Conversion factor to convert from kWh to Btu. |

Calculate steam generated for internal combustion engines and combustion turbines.

$$ICESTEAM = (ICEFUEL - ELGEN_{ice}) \times GENEQPSTEFF_{ice} \quad (B-76)$$

where:

| | | |
|---------------------|---|---|
| $ICESTEAM$ | = | Cogeneration of steam from internal combustion engines, |
| $ICEFUEL$ | = | Fuel consumption for electricity generation from internal combustion engines, |
| $ELGEN_{ice}$ | = | Electricity generation from internal combustion engines, and |
| $GENEQPSTEFF_{ice}$ | = | Efficiency for internal combustion engines. |

$$GCTSTEAM = (GCTFUEL - ELGEN_{ct}) \times GENEQPSTEFF_{ct} \quad (B-77)$$

where:

| | | |
|--------------------|---|---|
| $GCTSTEAM$ | = | Cogeneration of steam from combustion turbines, |
| $GCTFUEL$ | = | Fuel consumption for electricity generation from combustion turbines, |
| $ELGEN_{ct}$ | = | Electricity generation from combustion turbines, and |
| $GENEQPSTEFF_{ct}$ | = | Efficiency for combustion turbines. |

Calculate the steam generated from boilers.

$$BOILSTEAM = STEMCUR - (ICESTEAM + GCTSTEAM) \quad (B-78)$$

where:

| | | |
|------------------|---|--|
| <i>BOILSTEAM</i> | = | Steam generated from boilers, |
| <i>STEMCUR</i> | = | Total steam demand, |
| <i>ICESTEAM</i> | = | Cogeneration of steam from internal combustion engines, and |
| <i>GCTSTEAM</i> | = | Cogeneration of steam from combustion turbines. |

Calculate the total fuel consumed for cogeneration by internal combustion engines, combustion turbines, and steam turbines.

$$CGFUEL_{coal,total,r} = STFUEL_{coal} \quad (B-79)$$

where:

| | | |
|---------------------------------------|---|---|
| <i>CGFUEL</i> _{coal,total,r} | = | Consumption of coal for cogeneration of electricity for all uses in Census region <i>r</i> , and |
| <i>STFUEL</i> _{coal} | = | Consumption of coal in steam turbines. |

$$CGFUEL_{oil,total,r} = STFUEL_{oil} + ICEFUEL \quad (B-80)$$

where:

| | | |
|--------------------------------------|---|---|
| <i>CGFUEL</i> _{oil,total,r} | = | Consumption of distillate oil for cogeneration of electricity for all uses in Census region <i>r</i> , |
| <i>STFUEL</i> _{oil} | = | Consumption of distillate oil in steam turbines, and |

ICEFUEL = Fuel consumption for electricity generation from internal combustion engines.

$$CGFUEL_{ng,total,r} = STFUEL_{ng} + GCTFUEL \quad (B-81)$$

where:

*CGFUEL*_{ng,total,r} = Consumption of natural gas for cogeneration of electricity for all uses in Census region *r*,

*STFUEL*_{ng} = Consumption of natural gas in steam turbines, and

GCTFUEL = Fuel consumption for electricity generation from combustion turbines.

$$CGFUEL_{renew,total,r} = STFUEL_{bm} + STBYP_{bm} \quad (B-82)$$

where:

*CGFUEL*_{renew,total,r} = Consumption of renewables for cogeneration of electricity for all uses in Census region *r*,

*STFUEL*_{bm} = Consumption of biomass in steam turbines, and

*STBYP*_{bm} = Consumption of byproduct biomass in steam turbines.

Calculate the amount of fuel consumed for cogeneration for own use and sales to the grid.

$$CGFUEL_{f,own,r} = CGFUEL_{f,total,r} \times \left[\frac{ELOWN}{ELGEN_{total}} \right] \quad (B-83)$$

where:

*CGFUEL*_{f,own,r} = Consumption of fuel *f* for cogeneration of electricity for own use in Census region *r*,

- $CGFUEL_{f,total,r}$ = Consumption of fuel f for cogeneration of electricity for all uses in Census region r ,
- $ELOWN$ = Electricity generation for own use, and
- $ELGEN_{total}$ = Electricity generation from all prime movers.

$$CGFUEL_{f,sales,r} = CGFUEL_{f,total,r} - CGFUEL_{f,own,r} \quad (B-84)$$

where:

- $CGFUEL_{f,sales,r}$ = Consumption of fuel f for cogeneration of electricity for sales to the grid in Census region r ,
- $CGFUEL_{f,total,r}$ = Consumption of fuel f for cogeneration of electricity for all uses in Census region r , and
- $CGFUEL_{f,own,r}$ = Consumption of fuel f for cogeneration of electricity for own use in Census region r .

Calculate the total amount of fuel consumed for cogeneration for own use and sales to the grid.

$$CGFUEL_{total,u,r} = \sum_{f=1}^4 CGFUEL_{f,u,r} \text{ for } u=1,2 \text{ and } r=1,\dots,4. \quad (B-85)$$

where:

- $CGFUEL_{total,u,r}$ = Consumption of all fuels for cogeneration of electricity for use u in Census region r , and
- $CGFUEL_{f,u,r}$ = Consumption of fuel f for cogeneration of electricity for use u in Census region r .

Calculate the US total amount of fuel f consumed for cogeneration for own use and sales to the grid.

$$CGFUEL_{f,\mu,total} = \sum_{r=1}^4 CGFUEL_{f,\mu,r} \text{ for } f=1,\dots,4 \text{ and } u=1,2. \quad (\text{B-86})$$

where:

$CGFUEL_{f,u,total}$ = Consumption of fuel f for cogeneration of electricity for use u in all Census regions, and

$CGFUEL_{f,u,r}$ = Consumption of fuel f for cogeneration of electricity for use u in Census region r .

Calculate the total industrial fuel consumption for cogeneration.

$$GENTOT_{f,\mu,r} = \sum_{i=1}^{INDMAX} CGFUEL_{f,\mu,r} \quad (\text{B-87})$$

where:

$GENTOT_{f,\mu,r}$ = Total consumption of fuel f for cogeneration of electricity for use u in Census region r ,

$INDMAX$ = Number of industries, and

$CGFUEL_{f,\mu,r}$ = Consumption of fuel f for cogeneration of electricity for use u in Census region r .

FUELBOIL

$$AVGINT = \sum_{f=1}^{IFSMAX} BSSHR_f \times ENSINT_f \quad (B-88)$$

where:

| | | |
|---------------------------|---|--|
| <i>AVGINT</i> | = | Average intensity, |
| <i>IFSMAX</i> | = | Number of fuels consumed in the BSC component, |
| <i>BSSHR_f</i> | = | Share of total fuel consumption in the BSC component for fuel <i>f</i> , and |
| <i>ENSINT_f</i> | = | Intensity of fuel <i>f</i> in the BSC component. |

Calculate steam generated by byproduct fuels for main, intermediate, and renewable fuels.

$$BYPSTM = \sum_{f=1}^{IFSBYPM} \frac{BYPBSCM_f}{BYSINT_f} + \sum_{f=1}^{IFSBYPI} \frac{BYPBSCI_f}{BYSINT_f} + \sum_{f=1}^{IFSBYPR} \frac{BYPBSCR_f}{BYSINT_f} \quad (B-89)$$

where:

| | | |
|----------------------------|---|---|
| <i>BYPSTM</i> | = | Amount of steam generated from all byproduct fuels, |
| <i>IFSBYPM</i> | = | Number of byproduct main fuels, |
| <i>BYPBSCM_f</i> | = | Byproduct consumption of main fuel <i>f</i> in the BSC component, |
| <i>BYSINT_f</i> | = | Intensity for byproduct fuel <i>f</i> consumed in the BSC component, |
| <i>IFSBYPI</i> | = | Number of byproduct intermediate fuels, |
| <i>BYPBSCI_f</i> | = | Byproduct consumption of intermediate fuel <i>f</i> in the BSC component, |

IFSBYPR = Number of byproduct renewable fuels, and

BYPBSCR_f = Byproduct consumption of renewable fuel *f* in the BSC component.

Calculate the amount of steam to be generated from purchased fuels.

$$STEMCURF = STEMCUR - BYPSTM \quad (\text{B-90})$$

where:

STEMCURF = Amount of steam to be generated from purchased fuels,

STEMCUR = Total steam demand, and

BYPSTM = Amount of steam generated from all byproduct fuels.

Calculate the total amount of fuel consumed to generate steam.

$$ENSQTY_f = STEMCURF \times AVGINT \times BSSHR_f \quad (\text{B-91})$$

where:

ENSQTY_f = Consumption of fuel *f* to generate steam,

STEMCURF = Amount of steam to be generated from purchased fuels,

AVGINT = Average intensity, and

BSSHR_f = Share of total fuel consumption in the BSC component for fuel *f*.

$$ENSQTY_f = ENSQTY_f - ICEFUEL \quad (\text{B-92})$$

where:

- $ENSQTY_f$ = Consumption of fuel f to generate steam, and
 $ICEFUEL$ = Fuel consumption for electricity generation from internal combustion engines.

$$ENSQTY_f = ENSQTY_f - GCTFUEL \quad (B-93)$$

where:

- $ENSQTY_f$ = Consumption of fuel f to generate steam, and
 $GCTFUEL$ = Fuel consumption for electricity generation from combustion turbines.

Calculate the amount of fuel consumed in steam turbines.

$$STFUEL_f = \left[\frac{ENSQTY_f}{\sum_{f=1}^{IFSMAX} ENSQTY_f + \sum_{f=1}^{IFSBYP} BYSQTY_f} \right] \times ELGEN_{st} \times \frac{GENEQPHTRT_{st}}{3412.0} \quad (B-94)$$

where:

- $STFUEL_f$ = Consumption of fuel f in steam turbines,
 $ENSQTY_f$ = Consumption of fuel f to generate steam,
 $IFSMAX$ = Number of fuels consumed in the BSC component,
 $IFSBYP$ = Number of byproduct fuels consumed in the BSC component,
 $BYSQTY_f$ = Consumption of byproduct fuel f in the BSC component,

- $ELGEN_{st}$ = Electricity generation from steam turbines,
 $GENEQPHTRT_{st}$ = Heat rate for steam turbines, and
 3412.0 = Conversion factor to convert from kilowatt hours to Btu.

$$STBYP_f = \left[\frac{BYSQTY_f}{\sum_{f=1}^{IFSMAX} ENSQTY_f + \sum_{f=1}^{IFSBYP} BYSQTY_f} \right] \times ELGEN_{st} \times \frac{GENEQPHTRT_{st}}{3412.0} \quad (B-95)$$

where:

- $STBYP_f$ = Consumption of byproduct fuel f in steam turbines,
 $BYSQTY_f$ = Consumption of byproduct fuel f in the BSC component,
 $IFSBYP$ = Number of byproduct fuels consumed in the BSC component,
 $IFSMAX$ = Number of fuels consumed in the BSC component,
 $ENSQTY_f$ = Consumption of fuel f to generate steam,
 $ELGEN_{st}$ = Electricity generation from steam turbines,
 $GENEQPHTRT_{st}$ = Heat rate for steam turbines, and
 3412.0 = Conversion factor to convert from kilowatt hours to Btu.

$$ENSQTY_f = ENSQTY_f + ICEFUEL \quad (B-96)$$

where:

- $ENSQTY_f$ = Consumption of fuel f to generate steam, and

ICEFUEL = Fuel consumption for electricity generation from internal combustion engines.

$$ENSQTY_f = ENSQTY_f + GCTFUEL \quad (B-97)$$

where:

ENSQTY_f = Consumption of fuel *f* to generate steam, and

GCTFUEL = Fuel consumption for electricity generation from combustion turbines.

CALBSC

Calculate boiler fuel shares.

$$BSSHR_f = BSSHRLAG_f \times \left[\frac{PRCX_{f,r}}{PRCXLAG_f} \right]^{BSSHRE_f} \times \left[\frac{PRCX_{ng,r}}{PRCXLAG_{ng}} \right]^{BSSHRNG_f} \times \left[\frac{PRCX_{oil,r}}{PRCXLAG_{oil}} \right]^{BSSHROIL_f} \times \left[\frac{PRCX_{coal,r}}{PRCXLAG_{coal}} \right]^{BSSHRCL_f} \quad (B-98)$$

where:

BSSHR_f = Share of total fuel consumption in the BSC component for fuel *f*,

BSSHRLAG_f = Lagged boiler share for fuel *f*,

PRCX_{f,r} = Price for fuel *f* in Census region *r*,

PRCXLAG_f = Lagged price for fuel *f*,

BSSHRE_f = Own price elasticity for fuel *f*,

- $BSSHRNG_f$ = Cross price elasticity for natural gas with fuel f ,
 $BSSHROIL_f$ = Cross price elasticity for oil with fuel f , and
 $BSSHRCL_f$ = Cross price elasticity for coal with fuel f .

$$BSSHR_f = \frac{BSSHR_f}{\sum_{f=1}^{IFSMAX} BSSHR_f} \quad (\text{B-99})$$

where:

- $BSSHR_f$ = Share of total fuel consumption in the BSC component for fuel f , and
 $IFSMAX$ = Number of fuels consumed in the BSC component.

INDCGN

$$ELCTOT_{total} = \sum_{r=1}^4 ELCTOT_r \quad (\text{B-100})$$

where:

- $ELCTOT_{total}$ = Capacity for industrial electricity generation in all Census regions, and
 $ELCTOT_r$ = Capacity for industrial electricity generation in Census region r .

$$ELOTOT_{total} = \sum_{r=1}^4 ELOTOT_r \quad (B-101)$$

where:

$ELOTOT_{total}$ = Total industrial electricity generation for own use in all Census regions, and

$ELOTOT_r$ = Total industrial electricity generation for own use in Census region r .

$$ELSTOT_{total} = \sum_{r=1}^4 ELSTOT_r \quad (B-102)$$

where:

$ELSTOT_{total}$ = Total industrial electricity generation for sales to the grid in all Census regions, and

$ELSTOT_r$ = Total industrial electricity generation for sales to the grid in Census region r .

$$GENTOT_{f,u,total} = \sum_{r=1}^4 GENTOT_{f,u,r} \quad (B-103)$$

where:

$GENTOT_{f,u,total}$ = Total consumption of fuel f for cogeneration of electricity for use u in all Census regions, and

$GENTOT_{f,u,r}$ = Total consumption of fuel f for cogeneration of electricity for use u in Census region r .

For 1990 and 1991,

$$CAPREG_{r,y,t-fuel,total} = \sum_{f=1}^4 CAPREG_{r,y,f,total} \quad (B-104)$$

where:

- $CAPREG_{r,y,t-fuel,total}$ = Existing or planned capacity for cogeneration of electricity for all uses in Census region r using all fuels in year y , and
- $CAPREG_{r,y,f,total}$ = Existing or planned capacity for cogeneration of electricity for all uses in Census region r using fuel f in year y .

$$CAPD_{d,y,f,own,pl} = \left[\frac{ELOTOT_r}{ELOTOT_r + ELSTOT_r} \right] \times CAPREG_{r,y,f,total} \times DIVSHARE_d \quad (B-105)$$

where:

- $CAPD_{d,y,f,own,pl}$ = Existing or planned capacity for cogeneration of electricity for own use in Census division d using fuel f in year y ,
- $ELOTOT_r$ = Total industrial electricity generation for own use in Census region r ,
- $ELSTOT_r$ = Total industrial electricity generation for sales to the grid in Census region r ,
- $CAPREG_{r,y,f,total}$ = Existing or planned capacity for cogeneration of electricity for all uses in Census region r using fuel f in year y , and
- $DIVSHARE_d$ = Electricity share for Census division d .

$$CAPD_{d,y,f,sales,pl} = [CAPREG_{r,y,f,total} - CAPREG_{r,y,f,own}] \times DIVSHARE_d \quad (B-106)$$

where:

- $CAPD_{d,y,f,sales,pl}$ = Existing or planned capacity for cogeneration of electricity for sales to the grid in Census division d using fuel f in year y ,
- $CAPREG_{r,y,f,total}$ = Existing or planned capacity for cogeneration of electricity for all uses in Census region r using fuel f in year y ,
- $CAPREG_{r,y,f,own}$ = Existing or planned capacity for cogeneration of electricity for own use in Census region r using fuel f in year y , and
- $DIVSHARE_d$ = Electricity share for Census division d .

If 1992 through 1996,

$$CAPD_{d,y,own,pl} = CAPD_{d,y-1,f,own,pl} + \left[\frac{ELOTOT_r}{ELOTOT_r + ELSTOT_r} \right] \times CAPDIV_{d,y,f,total,pl} \quad (B-107)$$

where:

- $CAPD_{d,y,f,own,pl}$ = Existing or planned capacity for cogeneration of electricity for own use in Census division d using fuel f in year y ,
- $CAPD_{d,y-1,f,own,pl}$ = Existing or planned capacity for cogeneration of electricity for own use in Census division d using fuel f in year $y-1$,
- $ELOTOT_r$ = Total industrial electricity generation for own use in Census region r ,
- $ELSTOT_r$ = Total industrial electricity generation for sales to the grid in Census region r , and
- $CAPDIV_{d,y,f,total,pl}$ = Planned capacity for electricity generation for all uses in Census division d using fuel f in year y .

$$CAPD_{d,y,sales,pl} = CAPD_{d,y-1,sales,pl} + CAPDIV_{d,y,f,total,pl} - CAPDIV_{d,y,f,own,pl} \quad (B-108)$$

where:

$CAPD_{d,y,f,sales,pl}$ = Existing or planned capacity for cogeneration of electricity for sales to the grid in Census division d using fuel f in year y ,

$CAPD_{d,y-1,f,sales,pl}$ = Existing or planned capacity for cogeneration of electricity for sales to the grid in Census division d using fuel f in year $y-1$,

$CAPDIV_{d,y,f,total,pl}$ = Planned capacity for electricity generation for all uses in Census division d using fuel f in year y , and

$CAPDIV_{d,y,f,own,pl}$ = Planned capacity for electricity generation for own use in Census division d using fuel f in year y .

Calculate fuel consumption for each census division.

$$DIVFUEL_{d,f,u} = GENTOT_{f,u,r} \times DIVSHARE_d \quad (B-109)$$

where:

$DIVFUEL_{d,f,u}$ = Consumption of fuel f for cogeneration of electricity for use u in Census division d ,

$GENTOT_{f,u,r}$ = Total consumption of fuel f for cogeneration of electricity for use u in Census region r , and

$DIVSHARE_d$ = Electricity share for Census division d .

$$DIVFUEL_{d,total,u} = \sum_{f=1}^4 DIVFUEL_{d,f,u} \quad (B-110)$$

where:

$DIVFUEL_{d,total,u}$ = Consumption of all fuels for cogeneration of electricity for use u in Census division d , and

$DIVFUEL_{d,f,u}$ = Consumption of fuel f for cogeneration of electricity for use u in Census division d .

$$DIVFUEL_{total,f,u} = \sum_{d=1}^9 DIVFUEL_{d,f,u} \quad (\text{B-111})$$

where:

$DIVFUEL_{total,f,u}$ = Consumption of fuel f for cogeneration of electricity for use u in all Census divisions, and

$DIVFUEL_{d,f,u}$ = Consumption of fuel f for cogeneration of electricity for use u in Census division d .

$$CAPD_{total,y,total,u,pl} = \sum_{d=1}^9 CAPD_{d,y,total,u,pl} \quad (\text{B-112})$$

where:

$CAPD_{total,y,total,u,pl}$ = Existing or planned capacity for cogeneration of electricity for use u in all Census divisions using all fuels in year y , and

$CAPD_{d,y,total,u,pl}$ = Existing or planned capacity for cogeneration of electricity for use u in Census division d using all fuels in year y .

Convert total generation to gigawatt hours and capacity to megawatts.
The following equation calculates electric generation for own use.

$$GENGWH_{d,f,own} = ELOTOT_r \times DIVSHARE_d \times \left[\frac{DIVFUEL_{d,f,own}}{DIVFUEL_{d,total,own}} \right] \times \frac{10^6}{3412.0} \quad (\text{B-113})$$

where:

- $GENGWH_{d,f,own}$ = Cogeneration of electricity for own use using fuel f in Census division d ,
- $ELOTOT_r$ = Total industrial electricity generation for own use in Census region r ,
- $DIVSHARE_d$ = Electricity share for Census division d ,
- $DIVFUEL_{d,f,own}$ = Consumption of fuel f for cogeneration of electricity for own use in Census division d ,
- $DIVFUEL_{d,total,own}$ = Consumption of all fuels for cogeneration of electricity for own use in Census division d , and
- $10^6/3412.0$ = Conversion factor to convert trillion Btu to megawatts.

$$GENGWH_{d,f,sales} = ELSTOT_r \times DIVSHARE_d \times \left[\frac{DIVFUEL_{d,f,sales}}{DIVFUEL_{d,total,sales}} \right] \times \frac{10^6}{3412.0} \quad (\text{B-114})$$

where:

- $GENGWH_{d,f,sales}$ = Cogeneration of electricity for sales to the grid using fuel f in Census division d ,
- $ELSTOT_r$ = Total industrial electricity generation for sales to the grid in Census region r ,

- $DIVSHARE_d$ = Electricity share for Census division d ,
- $DIVFUEL_{d,f,sales}$ = Consumption of fuel f for cogeneration of electricity for sales to the grid in Census division d ,
- $DIVFUEL_{d,total,sales}$ = Consumption of all fuels for cogeneration of electricity for sales to the grid in Census division d , and
- $10^6/3412.0$ = Conversion factor to convert trillion Btu to megawatts.

$$CAPGW_{d,f,own,pl} = ELCTOT_r \times \left[\frac{ELOTOT_r}{ELOTOT_r + ELSTOT_r} \right] \times DIVSHARE_d \times \left[\frac{DIVFUEL_{d,f,own}}{DIVFUEL_{d,total,own}} \right] \quad (B-115)$$

where:

- $CAPGW_{d,f,own,pl}$ = Existing or planned capacity for cogeneration of electricity for own use using fuel f in Census division d ,
- $ELCTOT_r$ = Capacity for industrial electricity generation in Census region r ,
- $ELOTOT_r$ = Total industrial electricity generation for own use in Census region r ,
- $ELSTOT_r$ = Total industrial electricity generation for sales to the grid in Census region r ,
- $DIVSHARE_d$ = Electricity share for Census division d ,
- $DIVFUEL_{d,f,own}$ = Consumption of fuel f for cogeneration of electricity for own use in Census division d , and
- $DIVFUEL_{d,total,own}$ = Consumption of all fuels for cogeneration of electricity for own use in Census division d .

$$CAPGW_{d,f,sales,pl} = \left\{ ELCTOT_r \times \left[\frac{ELSTOT_r}{ELOTOT_r + ELSTOT_r} \right] \right\} \times DIVSHARE_d \times \left[\frac{DIVFUEL_{d,f,sales}}{DIVFUEL_{d,total,sales}} \right] \quad (B-116)$$

where:

| | | |
|---------------------------|---|--|
| $CAPGW_{d,f,sales,pl}$ | = | Existing or planned capacity for cogeneration of electricity for sales to the grid using fuel f in Census division d , |
| $ELCTOT_r$ | = | Capacity for industrial electricity generation in Census region r , |
| $ELOTOT_r$ | = | Total industrial electricity generation for own use in Census region r , |
| $ELSTOT_r$ | = | Total industrial electricity generation for sales to the grid in Census region r , |
| $DIVSHARE_d$ | = | Electricity share for Census division d , |
| $DIVFUEL_{d,f,sales}$ | = | Consumption of fuel f for cogeneration of electricity for sales to the grid in Census division d , and |
| $DIVFUEL_{d,total,sales}$ | = | Consumption of all fuels for cogeneration of electricity for sales to the grid in Census division d . |

For 1990 through 1996,

$$CAPGW_{d,f,\mu,pl} = CAPD_{d,y,f,\mu,pl} \quad (\text{B-117})$$

where:

| | | |
|-----------------------|---|--|
| $CAPGW_{d,f,\mu,pl}$ | = | Existing or planned capacity for cogeneration of electricity for use μ using fuel f in Census division d , and |
| $CAPD_{d,y,f,\mu,pl}$ | = | Existing or planned capacity for cogeneration of electricity for use μ in Census division d using fuel f in year y . |

After 1996, if $CAPGW_{d,f,\mu,pl} > CAPGWLAG_{d,f,\mu,pl}$, then

$$CAPGW_{d,f,u,pl} = CAPD_{d,y-1,f,u,pl} + [CAPGW_{d,f,u,pl} - CAPGWLAG_{d,f,u,pl}] \quad (\text{B-118})$$

where:

- $CAPGW_{d,f,u,pl}$ = Planned capacity for cogeneration of electricity for use u using fuel f in Census division d ,
- $CAPD_{d,y-1,f,u,pl}$ = Existing or planned capacity for cogeneration of electricity for use u in Census division d using fuel f in year $y-1$,
- $CAPGW_{d,f,u,pl}$ = Planned capacity for cogeneration of electricity for use u using fuel f in Census division d , and
- $CAPGWLAG_{d,f,u,pl}$ = Lagged planned capacity for cogeneration of electricity for use u using fuel f in Census division d .

Otherwise,

$$CAPGW_{d,f,u,pl} = CAPD_{d,y-1,f,u,pl} \quad (\text{B-119})$$

where:

- $CAPGW_{d,f,u,pl}$ = Planned capacity for cogeneration of electricity for use u using fuel f in Census division d , and
- $CAPD_{d,y-1,f,u,pl}$ = Existing or planned capacity for cogeneration of electricity for use u in Census division d using fuel f in year $y-1$.

$$GENGWH_{total,f,u} = \sum_{d=1}^9 GENGWH_{d,f,u} \quad (\text{B-120})$$

where:

- $GENGWH_{total,f,u}$ = Cogeneration of electricity for use u using fuel f in all Census divisions, and

$GENGWH_{d,f,u}$ = Cogeneration of electricity for use u using fuel f in Census division d .

$$CAPGW_{total,f,u,status} = \sum_{d=1}^9 CAPGW_{d,f,u,status} \quad (B-121)$$

where:

$CAPGW_{total,f,u,status}$ = Planned or unplanned capacity for cogeneration of electricity for use u using fuel f in all Census divisions, and

$CAPGW_{d,f,u,status}$ = Planned or unplanned capacity for cogeneration of electricity for use u using fuel f in Census division d .

OTHER INDUSTRIAL MODEL EQUATIONS

IND

For the non-manufacturing industries, calculate value of output.

$$OUTIND_{i,d} = \frac{MC_NMFGO_{d,i,y}}{10^3} \quad (B-122)$$

where:

| | | |
|---------------------|---|---|
| $OUTIND_{i,d}$ | = | Gross value of output for industry i in Census division d , |
| $MC_NMFGO_{d,i,y}$ | = | Gross value of output for non-manufacturing industry i in Census division d in year y , and |
| 10^3 | = | Conversion factor to convert million \$1987 to billion \$1987. |

For the manufacturing industries, calculate value of output.

$$OUTIND_{i,d} = \frac{MC_MFGO_{d,i,y}}{10^3} \quad (B-123)$$

where:

| | | |
|--------------------|---|---|
| $OUTIND_{i,d}$ | = | Gross value of output for industry i in Census division d , |
| $MC_MFGO_{d,i,y}$ | = | Gross value of output for manufacturing industry i in Census division d in year y , and |
| 10^3 | = | Conversion factor to convert million \$1987 to billion \$1987. |

If the year is 1990, regional prices are calculated by the following for electricity, similarly for the other fuels.

$$PRCX_{elec,r} = \frac{\sum_{d=1}^{NUM_r} DPRCX_{elec,d} \times QSELIN_{d,1990}}{\sum_{d=1}^{NUM_r} QSELIN_{d,1990}} \quad (\text{B-124})$$

where:

- $PRCX_{elec,r}$ = Price of electricity in Census region r ,
- NUM_r = Number of Census divisions in Census region r ,
- $DPRCX_{elec,d}$ = Price of electricity in Census division d , and
- $QSELIN_{d,1990}$ = SEDS consumption of electricity in Census division d in 1990.

If the year is after 1990, regional prices are calculated by the following for electricity, similarly for other fuels.

$$PRCX_{elec,r} = \frac{\sum_{d=1}^{NUM_r} DPRCX_{elec,d} \times QELIN_{d,y-1}}{\sum_{d=1}^{NUM_r} QELIN_{d,y-1}} \quad (\text{B-125})$$

where:

- $PRCX_{elec,r}$ = Price of electricity in Census region r ,
- NUM_r = Number of Census divisions in Census region r ,
- $DPRCX_{elec,d}$ = Price of electricity in Census division d , and

$QELIN_{d,y-1}$ = Industrial consumption of electricity in Census division d in year $y-1$.

REXOG

Aggregate value of output to the regional level:

$$PRODVX_{i,r} = \sum_{d=1}^{NUM_r} OUTIND_{i,d} \quad (\text{B-126})$$

where:

$PRODVX_{i,r}$ = Value of output in dollar units for industry i in Census region r ,

NUM_r = Number of Census divisions in Census region r , and

$OUTIND_{i,d}$ = Gross value of output for industry i in Census division d .

Aggregate employment values to the regional level:

$$EMPLX_{i,r} = \sum_{d=1}^{NUM_r} EMPIND_{i,d} \quad (\text{B-127})$$

where:

$EMPLX_{i,r}$ = Employment for industry i in Census region r ,

NUM_r = Number of Census divisions in Census region r , and

$EMPIND_{i,d}$ = Employment for industry i in Census division d .

$$EMPLX_{i,r} = EMPLX_{i,r} \times 10^3 \quad (B-128)$$

where:

- $EMPLX_{i,r}$ = Employment for industry i in Census region r , and
 10^3 = Conversion factor to convert from millions to thousands.

CALBYPROD

Calculate the current TPC for byproducts for old and new vintage. Currently, only the paper and allied products industry has a TPC for byproducts. For all other industries, the UEC remains unchanged.

$$BYPCSCCUR_{v,f,s} = \left[\frac{PRODCUR_{total,s}}{PRODLAG_{total,s}} \right]^{BYPCSC_{v,f,s}} \quad (B-129)$$

where:

- $BYPCSCCUR_{v,f,s}$ = Current energy savings for byproduct fuel f at process step s for vintage v ,
 $PRODCUR_{total,s}$ = Production at process step s for all vintages,
 $PRODLAG_{total,s}$ = Lagged production at process step s for all vintages, and
 $BYPCSC_{v,f,s}$ = Byproduct technology possibility curve coefficient for byproduct fuel f at process step s for vintage v .

Calculate the TPC for middle vintage.

$$BYPCSCCUR_{mid,f,s} = \frac{(PRODCUR_{new,s} \times BYPCSCCUR_{new,f,s}) + (PRODCUR_{mid,s} \times BYPCSCLAG_{mid,f,s})}{PRODCUR_{new,s} + PRODCUR_{mid,s}} \quad (\text{B-130})$$

where:

- $BYPCSCCUR_{mid,f,s}$ = Current energy savings for byproduct fuel f at process step s for mid vintage,
- $PRODCUR_{new,s}$ = New production at process step s for new vintage,
- $BYPCSCCUR_{new,f,s}$ = Current energy savings for byproduct fuel f at process step s for new vintage,
- $PRODCUR_{mid,s}$ = Existing production at process step s for mid vintage, and
- $BYPCSCLAG_{mid,f,s}$ = Lagged energy savings for byproduct fuel f at process step s for middle vintage.

Calculate the rate of byproduct energy produced.

$$BYPINT_{v,f,s} = BYPINTLAG_{v,f,s} \times BYPCSCCUR_{v,f,s} \quad (\text{B-131})$$

where:

- $BYPINT_{v,f,s}$ = Rate of byproduct energy production for byproduct fuel f at process step s for vintage v ,
- $BYPINTLAG_{v,f,s}$ = Lagged rate of byproduct energy production for byproduct fuel f at process step s for vintage v , and
- $BYPCSCCUR_{v,f,s}$ = Current energy savings for byproduct fuel f at process step s for vintage v .

Calculate byproduct energy production.

$$BYPQTY_{v,f,s} = PRODCUR_{v,s} \times BYPINT_{v,f,s} \quad (B-132)$$

where:

- $BYPQTY_{v,f,s}$ = Byproduct energy production for byproduct fuel f at process step s for vintage v ,
- $PRODCUR_{v,s}$ = Production at process step s for vintage v , and
- $BYPINT_{v,f,s}$ = Rate of byproduct energy production for byproduct fuel f at process step s for vintage v .

$$BYPQTY_{total,f,s} = \sum_{v=1}^2 BYPQTY_{v,f,s} \quad (B-133)$$

where:

- $BYPQTY_{total,f,s}$ = Byproduct energy production for byproduct fuel f at process step s for all vintages, and
- $BYPQTY_{v,f,s}$ = Byproduct energy production for byproduct fuel f at process step s for vintage v .

$$BYPQTY_{v,f,s} = \frac{BYPQTY_{v,f,s}}{10^6} \quad (B-134)$$

where:

- $BYPQTY_{v,f,s}$ = Byproduct energy production for byproduct fuel f at process step s for vintage v , and
- 10^6 = Conversion factor to convert to trillion Btu.

$$BYPQTY_{v,total,s} = \sum_{f=1}^{IFBYP_s} BYPQTY_{v,f,s} \quad (B-135)$$

where:

- $BYPQTY_{v,total,s}$ = Byproduct energy production for all byproduct fuels at process step s for vintage v ,
- $IFBYP_s$ = Number of byproducts consumed at process step s , and
- $BYPQTY_{v,f,s}$ = Byproduct energy production for byproduct fuel f at process step s for vintage v .

Calculate byproduct energy production for main, intermediate, and renewable fuels.

$$ENBYPM_{f,v} = \sum_{s=1}^{MPASTP} BYPQTY_{v,f,s} \quad (B-136)$$

where:

- $ENBYPM_{f,v}$ = Byproduct energy production for main byproduct fuel f for vintage v ,
- $MPASTP$ = Number of process steps, and
- $BYPQTY_{v,f,s}$ = Byproduct energy production for byproduct fuel f at process step s for vintage v .

$$ENBYPI_{f,v} = \sum_{s=1}^{MPASTP} BYPQTY_{v,f,s} \quad (B-137)$$

where:

- $ENBYPI_{f,v}$ = Byproduct energy production for intermediate byproduct fuel f for vintage v ,

$MPASTP$ = Number of process steps, and
 $BYPQTY_{v,f,s}$ = Byproduct energy production for byproduct fuel f at process step s for vintage v .

$$ENBYPR_{f,v} = \sum_{s=1}^{MPASTP} BYPQTY_{v,f,s} \quad (\text{B-138})$$

where:

$ENBYPR_{f,v}$ = Byproduct energy production for renewable byproduct fuel f for vintage v ,
 $MPASTP$ = Number of process steps, and
 $BYPQTY_{v,f,s}$ = Byproduct energy production for byproduct fuel f at process step s for vintage v .

INDTOTAL

Calculate total consumption of electricity.

$$QTYMAIN_{elec,r} = ENPMQTY_{elec} + ENBQTY_{total,elec} - ELOWN \quad (\text{E-139})$$

where:

$QTYMAIN_{elec,r}$ = Consumption of purchased electricity in Census region r ,
 $ENPMQTY_{elec}$ = Consumption of electricity in the PA component,
 $ENBQTY_{elec}$ = Consumption of electricity for all building end uses, and
 $ELOWN$ = Electricity generated for own use.

$$QTYMAIN_{ng,r} = ENPMQTY_{ng} + ENBQTY_{total,ng} + ENSQTY_{ng} \quad (\text{B-140})$$

where:

- $QTYMAIN_{ng,r}$ = Consumption of natural gas in Census region r ,
- $ENPMQTY_{ng}$ = Consumption of natural gas in the PA component,
- $ENBQTY_{total,ng}$ = Consumption of natural gas for all building end uses, and
- $ENSQTY_{ng}$ = Consumption of natural gas to generate steam.

For all other main fuels,

$$QTYMAIN_{f,r} = ENPMQTY_f + ENSQTY_f + BYPBSCM_f \quad (\text{B-141})$$

where:

- $QTYMAIN_{f,r}$ = Consumption of all other main fuels f in Census region r ,
- $ENPMQTY_f$ = Consumption of all other main fuels f in the PA component,
- $ENSQTY_f$ = Consumption of all other main fuels f to generate steam, and
- $BYPBSCM_f$ = Byproduct consumption of main fuel f from the BSC component.

$$QTYINTR_{steam,r} = ENPIQTY_{steam} + ENBQTY_{total,steam} \quad (\text{B-142})$$

where:

| | | |
|---------------------|---|---|
| $QTYINTR_{steam,r}$ | = | Consumption of steam in Census region r , |
| $ENPIQTY_{steam}$ | = | Consumption of steam in the PA component, |
| $ENBQTY_{total,ng}$ | = | Consumption of steam for all building end uses, |

For all other intermediate fuels,

$$QTYINTR_{f,r} = ENPIQTY_f + ENSQTY_f \quad (\text{B-143})$$

where:

| | | |
|-----------------|---|--|
| $QTYINTR_{f,r}$ | = | Consumption of all other intermediate fuels f in Census region r , |
| $ENPIQTY_f$ | = | Consumption of all other intermediate fuels f in the PA component, and |
| $ENSQTY_f$ | = | Consumption of all other intermediate fuels f to generate steam. |

$$QTYRENW_{f,r} = ENPRQTY_f + ENSQTY_f + BYPBSCR_f \quad (\text{B-144})$$

where:

| | | |
|-----------------|---|---|
| $QTYRENW_{f,r}$ | = | Consumption of renewable fuel f in Census region r , |
| $ENPRQTY_f$ | = | Consumption of renewable fuel f in the PA component, |
| $ENSQTY_f$ | = | Consumption of renewable fuel f to generate steam, and |
| $BYPBSCR_f$ | = | Byproduct consumption of renewable fuel f in the BSC component. |

$$QTYMAIN_{total,r} = \sum_{f=1}^{22} QTYMAIN_{f,r} \quad (\text{B-145})$$

where:

$QTYMAIN_{total,r}$ = Consumption of all main fuels in Census region r , and
 $QTYMAIN_{f,r}$ = Consumption of main fuel f in Census region r .

$$QTYINTR_{total,r} = \sum_{f=1}^6 QTYINTR_{f,r} \quad (\text{B-146})$$

where:

$QTYINTR_{total,r}$ = Consumption of all intermediate fuels in Census region r ,
and
 $QTYINTR_{f,r}$ = Consumption of intermediate fuel f in Census region r .

$$QTYRENEW_{total,r} = \sum_{f=1}^9 QTYRENEW_{f,r} \quad (\text{B-147})$$

where:

$QTYRENEW_{total,r}$ = Consumption of all renewable fuels in Census region r , and
 $QTYRENEW_{f,r}$ = Consumption of renewable fuel f in Census region r .

NATTOTAL

$$QTYMAIN_{f,total} = \sum_{r=1}^4 QTYMAIN_{f,r} \quad (\text{B-148})$$

where:

$QTYMAIN_{f,total}$ = Consumption of main fuel f in all Census regions, and
 $QTYMAIN_{f,r}$ = Consumption of main fuel f in Census region r .

$$QTYINTR_{f,total} = \sum_{r=1}^4 QTYINTR_{f,r} \quad (\text{B-149})$$

where:

$QTYINTR_{f,total}$ = Consumption of intermediate fuel f in all Census regions, and
 $QTYINTR_{f,r}$ = Consumption of intermediate fuel f in Census region r .

$$QTYRENW_{f,total} = \sum_{r=1}^4 QTYRENW_{f,r} \quad (\text{B-150})$$

where:

$QTYRENW_{f,total}$ = Consumption of renewable fuel f in all Census regions, and
 $QTYRENW_{f,r}$ = Consumption of renewable fuel f in Census region r .

Calculate total industrial consumption.

$$TQMAIN_{f,r} = \sum_{i=1}^{INDMAX} QTYMAIN_{i,f,r} \text{ for } f=1,\dots,4 \text{ and } r=1,\dots,4. \quad (\text{B-151})$$

where:

- $TQMAIN_{f,r}$ = Total consumption of main fuel f in Census region r ,
- $INDMAX$ = Number of industries, and
- $QTYMAIN_{i,f,r}$ = Total consumption of main fuel f in Census region r in industry i .

$$TQINTR_{f,r} = \sum_{i=1}^{INDMAX} QTYINTR_{i,f,r} \text{ for } f=1,\dots,4 \text{ and } r=1,\dots,4. \quad (\text{B-152})$$

where:

- $TQINTR_{f,r}$ = Total consumption of intermediate fuel f in Census region r ,
- $INDMAX$ = Number of industries, and
- $QTYINTR_{i,f,r}$ = Total consumption of intermediate fuel f in Census region r in industry i .

$$TQRENW_{f,r} = \sum_{i=1}^{INDMAX} QTYRENW_{i,f,r} \text{ for } f=1,\dots,4 \text{ and } r=1,\dots,4. \quad (\text{B-153})$$

where:

- $TQRENW_{f,r}$ = Total consumption of renewable fuel f in Census region r ,
- $INDMAX$ = Number of industries, and

$QTYRENW_{i,f,r}$ = Total consumption of renewable fuel f in Census region r in industry i .

INDEMISS

Calculate emissions.

$$EMIRENW_{f,p,r} = QTYRENW_{f,r} \times UNCONTEMISSFACT_{f,p} \times EMISSCONTROLFAC_{f,p} \quad (\text{B-154})$$

where:

$EMIRENW_{f,p,r}$ = Emissions of pollutant p from renewable fuel f in Census region r ,

$QTYRENW_{f,r}$ = Consumption of renewable fuel f in Census region r ,

$UNCONTEMISSFACT_{f,p}$ = Uncontrolled emission factor for pollutant p using fuel f , and

$EMISSCONTROLFAC_{f,p}$ = Emissions control factor for pollutant p using fuel f .

For emissions of SO_x use the following equation.

$$EMIRENW_{f,sox,r} = EMIRENW_{f,sox,r} \times SULFURCONT_f \quad (\text{B-155})$$

where:

$EMIRENW_{f,sox,r}$ = Emissions of SO_x from renewable fuel f in Census region r , and

$SULFURCONT_f$ = Sulfur content of fuel f .



1.0



1.1



1.25



1.4



1.6



2.8



2.5



3.2



2.2



3.6



2.0



4.0



1.8



4.5



5.0



5.6



6.3



7.1



8.0



9.0



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$$EMIRENW_{f,p,total} = \sum_{r=1}^4 EMIRENW_{f,p,r} \quad (B-156)$$

where:

$EMIRENW_{f,p,total}$ = Emissions of pollutant p from renewable fuel f in all Census regions, and

$EMIRENW_{f,p,r}$ = Emissions of pollutant p from renewable fuel f in Census region r .

$$EMIRENW_{total,p,r} = \sum_{f=1}^8 EMIRENW_{f,p,r} \quad (B-157)$$

where:

$EMIRENW_{total,p,r}$ = Emissions of pollutant p from all renewable fuels in Census region r , and

$EMIRENW_{f,p,r}$ = Emissions of pollutant p from renewable fuel f in Census region r .

$$TOTEMIS_{renw,p,r} = \sum_{f=1}^8 EMIRENW_{f,p,r} \quad (B-158)$$

where:

$TOTEMIS_{renw,p,r}$ = Total emissions of pollutant p from renewables in Census region r , and

$EMIRENW_{f,p,r}$ = Emissions of pollutant p from renewable fuel f in Census region r .

Calculate emissions for total industrial sector.

$$TEMISR_{f,p,r} = \sum_{i=1}^{INDMAX} EMIRENW_{i,f,p,r} \text{ for } f=1,\dots,4, \text{ } p=1,\dots,8, \text{ and } r=1,\dots,4. \quad (\text{B-159})$$

where:

$TEMISR_{f,p,r}$ = Total emissions of pollutant p for renewable fuel f in Census region r ,

$INDMAX$ = Number of industries, and

$EMIRENW_{i,f,p,r}$ = Emissions of pollutant p from renewable fuel f in Census region r in industry i .

CONTAB

Calculate consumption for heat and power.

$$TMANHP_f = \sum_{i=7}^{INDMAX} QTYMAIN_{f,i} \text{ for } f=1,\dots,NUM_{fg} \quad (\text{B-160})$$

where:

$TMANHP_f$ = Total manufacturing consumption of fuel f for heat and power,

$INDMAX$ = Number of industries,

NUM_{fg} = Number of fuels in fuel group fg , and

$QTYMAIN_{f,i}$ = Total consumption of main fuel f in all Census regions for industry i .

$$TMANHP_{renw} = \sum_{i=7}^{INDMAX} \sum_{f=1}^8 QTYRENW_{f,total} \quad (B-161)$$

where:

$TMANHP_{renw}$ = Total manufacturing consumption of renewables for heat and power,

$INDMAX$ = Number of industries, and

$QTYRENW_{f,i}$ = Consumption of renewable fuel f in all Census regions for industry i .

$$TREFCON_{elec} = \sum_{d=1}^9 QELRF_{d,y} \quad (B-162)$$

where:

$TREFCON_{elec}$ = Total consumption of electricity from the petroleum refining industry, and

$QELRF_{d,y}$ = Electricity consumed by petroleum refining industry for Census division d in year y .

Similarly for the other fuels.

$$TNONHP_f = \sum_{i=1}^6 QTYMAIN_{f,i}, \text{ for } F=1, \dots, NUM_{Fg} \quad (B-163)$$

where:

$TNONHP_f$ = Total non-manufacturing consumption of main fuel f for heat and power,

NUM_{fg} = Number of fuels in fuel group fg , and

$QTYMAIN_{f,i}$ = Consumption of main fuel f in all Census regions for non-manufacturing industry i .

Calculate consumption for miscellaneous feedstocks.

$$TMISCFD_f = \sum_{i=1}^{INDMAX} QTYMAIN_{f,i} \text{ for } f=1,\dots,NUM_{fg} \quad (\text{B-164})$$

where:

$TMISCFD_f$ = Total consumption of miscellaneous and feedstock fuel f ,
 $INDMAX$ = Number of industries,
 NUM_{fg} = Number of fuels in fuel group fg , and
 $QTYMAIN_{f,i}$ = Total consumption of main fuel f for all Census regions for industry i .

Calculate consumption for the food and kindred products industry.

$$TFOODCON_f = \sum_{f=1}^{NUM_{fg}} QTYMAIN_{f,total} \quad (\text{B-165})$$

where:

$TFOODCON_f$ = Total consumption of fuel f by the food and kindred products industry,
 NUM_{fg} = Number of fuels in fuel group fg , and
 $QTYMAIN_{f,total}$ = Consumption of main fuel f for all Census regions.

$$TFOODCON_{renw} = \sum_{f=1}^8 QTYRENW_{f,total} \quad (B-166)$$

where:

$TFOODCON_{renw}$ = Total consumption of renewables by the food and kindred products industry, and

$QTYRENW_{f,total}$ = Consumption of renewable fuel f for all Census regions.

Calculate consumption for the paper and allied products industry:

$$TPAPERCON_f = \sum_{f=1}^{NUM_{fg}} QTYMAIN_{f,total} \quad (B-167)$$

where:

$TPAPERCON_f$ = Total consumption of fuel f by the paper and allied products industry,

NUM_{fg} = Number of fuels in fuel group fg , and

$QTYMAIN_{f,total}$ = Consumption of main fuel f for all Census regions.

$$TPAPERCON_{renw} = \sum_{f=1}^8 QTYRENW_{f,total} \quad (B-168)$$

where:

$TPAPERCON_{renw}$ = Total consumption of renewables by the paper and allied products industry, and

$QTYRENW_{f,total}$ = Consumption of renewable fuel f for all Census regions.

Calculate consumption for the bulk chemical industry:

$$TCHEMCON_f = \sum_{f=1}^{NUM_{fg}} QTYMAIN_{f,total} \quad (\text{B-169})$$

where:

$TCHEMCON_f$ = Total consumption of fuel f by the bulk chemical industry,
 NUM_{fg} = Number of fuels in fuel group fg , and
 $QTYMAIN_{f,total}$ = Consumption of main fuel f for all Census regions.

$$TCHEMCON_{renw} = \sum_{f=1}^8 QTYRENW_{f,total} \quad (\text{B-170})$$

where:

$TCHEMCON_{renw}$ = Total consumption of renewables by the bulk chemical industry, and
 $QTYRENW_{f,total}$ = Consumption of renewable fuel f for all Census regions.

Calculate consumption for the glass and glass products industry:

$$TGLASSCON_f = \sum_{f=1}^{NUM_{fg}} QTYMAIN_{f,total} \quad (\text{B-171})$$

where:

$TGLASSCON_f$ = Total consumption of fuel f by the glass and glass products industry,

NUM_{fg} = Number of fuels in fuel group fg , and
 $QTYMAIN_{f,total}$ = Consumption of main fuel f for all Census regions.

$$TGLASSCON_{renw} = \sum_{f=1}^8 QTYRENW_{f,total} \quad (\text{B-172})$$

where:

$TGLASSCON_{renw}$ = Total consumption of renewables by the glass and glass products industry, and
 $QTYRENW_{f,total}$ = Consumption of renewable fuel f for all Census regions.

Calculate consumption for the hydraulic cement industry:

$$TCEMENTCON_f = \sum_{f=1}^{NUM_{fg}} QTYMAIN_{f,total} \quad (\text{B-173})$$

where:

$TCEMENTCON_f$ = Total consumption of fuel f by the hydraulic cement industry,
 NUM_{fg} = Number of fuels in fuel group fg , and
 $QTYMAIN_{f,total}$ = Consumption of main fuel f for all Census regions.

$$TCEMENTCON_{renw} = \sum_{f=1}^8 QTYRENW_{f,total} \quad (\text{B-174})$$

where:

$TCEMENTCON_{renw}$ = Total consumption of renewables by the hydraulic cement industry, and

$QTYRENEW_{f,total}$ = Consumption of renewable fuel f for all Census regions.

Calculate consumption for the blast furnace and basic steel products industry:

$$TSTEELCON_f = \sum_{f=1}^{NUM_{fg}} QTYMAIN_{f,total} \quad (\text{B-175})$$

where:

$TSTEELCON_f$ = Total consumption of fuel f by the blast furnace and basic steel products industry,

NUM_{fg} = Number of fuels in fuel group fg , and

$QTYMAIN_{f,total}$ = Consumption of main fuel f for all Census regions.

$$TSTEELCON_{renw} = \sum_{f=1}^8 QTYRENEW_{f,total} \quad (\text{B-176})$$

where:

$TSTEELCON_{renw}$ = Total consumption of renewables by the blast furnace and basic steel products industry, and

$QTYRENEW_{f,total}$ = Consumption of renewable fuel f for all Census regions.

Calculate consumption for the primary aluminum industry:

$$TALUMCON_f = \sum_{f=1}^{NUM_{fg}} QTYMAIN_{f,total} \quad (B-177)$$

where:

$TALUMCON_f$ = Total consumption of fuel f by the primary aluminum industry,

NUM_{fg} = Number of fuels in fuel group fg , and

$QTYMAIN_{f,total}$ = Consumption of main fuel f for all Census regions.

$$TALUMCON_{renw} = \sum_{f=1}^8 QTYRENW_{f,total} \quad (B-178)$$

where:

$TALUMCON_{renw}$ = Total consumption of renewables by the primary aluminum industry, and

$QTYRENW_{f,total}$ = Consumption of renewable fuel f for all Census regions.

WEXOG

Calculate shares to share from Census regions to divisions:

$$FUELSHARE_{elec,d} = \frac{QSELIN_{d,1990}}{\sum_{d=1}^{NUM_r} QSELIN_{d,1990}} \quad (B-179)$$

where:

- $FUELSHARE_{elec,d}$ = Share of consumption for electricity in Census division d ,
- $QSELIN_{d,1990}$ = SEDS consumption of electricity in Census division d in 1990, and
- NUM_r = Number of Census divisions in Census region r .

Similarly for the other fuels.

$$DSRENEW_{f,d} = \frac{OUTIND_{13,d} + OUTIND_{11,d}}{NUM_r} \quad (B-180)$$
$$\sum_{d=1} (OUTIND_{13,d} + OUTIND_{11,d})$$

where:

- $DSRENEW_{f,d}$ = Share of output for renewable fuel f in Census division d ,
- $OUTIND_{13,d}$ = Gross value of output for the paper and allied products industry in Census division d ,
- $OUTIND_{11,d}$ = Gross value of output for the lumber and wood products industry in Census division d , and
- NUM_r = Number of Census divisions in Census region r .

$$DQMAIN_{f,d} = TQMAIN_{f,r} \times FUELSHARE_{f,d} \quad (B-181)$$

where:

- $DQMAIN_{f,d}$ = Consumption of main fuel f in Census division d ,
- $TQMAIN_{f,r}$ = Total consumption of main fuel f in Census region r , and

$FUELSHARE_{f,d}$ = Share of consumption of fuel f in Census division d .

$$DQRENW_{f,d} = TQRENW_{f,r} \times DSRENW_{f,d} \quad (\text{B-182})$$

where:

$DQRENW_{f,d}$ = Consumption of renewable fuel f in Census division d ,

$TQRENW_{f,r}$ = Total consumption of renewable fuel f in Census region r ,
and

$DSRENW_{f,d}$ = Share of output for renewable fuel f in Census division d .

Calculate consumption values to benchmark:

$$BMAIN_{elec,d} = DQMAIN_{elec,d} + QELRF_{d,y} \quad (\text{B-183})$$

where:

$BMAIN_{elec,d}$ = Consumption of electricity in Census division d ,

$DQMAIN_{elec,d}$ = Consumption of electricity in Census division d , and

$QELRF_{d,y}$ = Electricity consumed by petroleum refining industry in
Census division d in year y .

$$BMAIN_{ng,d} = \left[\sum_{f=3}^5 DQMAIN_{f,d} \right] + QNGRF_{d,y} + \sum_{u=1}^2 CGOGQ_{d,y,ng,u} \quad (\text{B-184})$$

where:

$BMAIN_{ng,d}$ = Consumption of natural gas in Census division d ,

$DQMAIN_{f,d}$ = Consumption of natural gas fuel f in Census division d ,

$QNGRF_{d,y}$ = Natural gas consumed by petroleum refining industry in Census division d in year y , and

$CGOGQ_{d,y,ng,u}$ = Consumption of natural gas from cogeneration of electricity for use u in enhanced oil recovery in Census division d in year y .

$$BMAIN_{coal,d} = DQMAIN_{coal,d} + QCLRF_{d,y} + COPRCLQ_{d,y} + COPRCLG_{d,y} + \sum_{u=1}^2 CGOGQ_{d,y,coal,u} \quad (B-185)$$

where:

$BMAIN_{coal,d}$ = Consumption of coal in Census division d ,

$DQMAIN_{coal,d}$ = Consumption of coal in Census division d ,

$QCLRF_{d,y}$ = Coal consumed by petroleum refining industry in Census division d in year y ,

$COPRCLQ_{d,y}$ = Supply of coal liquids in Census division d in year y ,

$COPRCLG_{d,y}$ = Supply of coal gases in Census division d in year y , and

$CGOGQ_{d,y,coal,u}$ = Consumption of coal from cogeneration of electricity for use u in enhanced oil recovery in Census division d in year y .

For metallurgical coal, net coke imports, motor gasoline, asphalt and road oil, petrochemical feedstocks, and kerosene use the following equation.

$$BMAIN_{f,d} = DQMAIN_{f,d} \quad (B-186)$$

where:

$BMAIN_{f,d}$ = Consumption of fuel f in Census division d , and

$DQMAIN_{f,d}$ = Consumption of fuel f in Census division d ,

$$BMAIN_{res,d} = DQMAIN_{res,d} + QRLRF_{d,y} + \sum_{u=1}^2 CGOGQ_{d,y,res,u} \quad (B-187)$$

where:

- $BMAIN_{res,d}$ = Consumption of residual fuel in Census division d ,
- $DQMAIN_{res,d}$ = Consumption of residual fuel in Census division d ,
- $QRLRF_{d,y}$ = Residual fuel consumed by petroleum refining industry in Census division d in year y , and
- $CGOGQ_{d,y,res,u}$ = Consumption of residual fuel from cogeneration of electricity for use u in enhanced oil recovery in Census division d in year y .

$$BMAIN_{dis,d} = DQMAIN_{dis,d} + QDSRF_{d,y} \quad (B-188)$$

where:

- $BMAIN_{dis,d}$ = Consumption of distillate in Census division d ,
- $DQMAIN_{dis,d}$ = Consumption of distillate in Census division d , and
- $QDSRF_{d,y}$ = Distillate fuel consumed by petroleum refining industry in Census division d in year y .

$$BMAIN_{lpg,d} = \left[\sum_{f=12}^{13} DQMAIN_{f,d} \right] + QLGRF_{d,y} \quad (B-189)$$

where:

- $BMAIN_{lpg,d}$ = Consumption of liquid petroleum gas in Census division d ,

$DQMAIN_{f,d}$ = Consumption of liquid petroleum gas fuel f in Census division d , and

$QLGRF_{d,y}$ = Liquid petroleum gas consumed by petroleum refining industry in Census division d in year y .

$$BMAIN_{sg,d} = DQMAIN_{sg,d} + QSGRF_{d,y} \quad (\text{B-190})$$

where:

$BMAIN_{sg,d}$ = Consumption of still gas in Census division d ,

$DQMAIN_{sg,d}$ = Consumption of still gas in Census division d , and

$QSGRF_{d,y}$ = Still gas consumed by petroleum refining industry in Census division d in year y .

$$BMAIN_{pc,d} = DQMAIN_{pc,d} + QPCRF_{d,y} \quad (\text{B-191})$$

where:

$BMAIN_{pc,d}$ = Consumption of petroleum coke in Census division d ,

$DQMAIN_{pc,d}$ = Consumption of petroleum coke in Census division d , and

$QPCRF_{d,y}$ = Petroleum coke consumed by petroleum refining industry in Census division d in year y .

$$BMAIN_{pet,d} = DQMAIN_{lube,d} + \left[\sum_{f=21}^{22} DQMAIN_{f,d} \right] + QOTRF_{d,y} \quad (\text{B-192})$$

where:

- $BMAIN_{pet,d}$ = Consumption of other petroleum in Census division d ,
- $DQMAIN_{lube,d}$ = Consumption of lubes and waxes in Census division d ,
- $DQMAIN_{f,d}$ = Consumption of other petroleum fuel f in Census division d , and
- $QOTRF_{d,y}$ = Other petroleum consumed by petroleum refining industry in Census division d in year y .

Calculate consumption for other industrial:

$$OTHIND_{f,d} = \left[BMAIN_{f,d} \times \frac{\sum_{y=1}^{MSEDYR} BENCHFAC_{f,d}}{2.0} \right] - BMAIN_{f,d} \quad (B-193)$$

where:

- $OTHIND_{f,d}$ = Consumption of fuel f for "other industry" in Census division d ,
- $BMAIN_{f,d}$ = Consumption of fuel f in Census division d ,
- $MSEDYR$ = Index of SEDS years, and
- $BENCHFAC_{f,d}$ = Benchmark factor for fuel f in Census division d .

Calculate benchmarked consumption values:

$$QELIN_{d,y} = BMAIN_{elec,d} + OTHIND_{elec,d} \quad (B-194)$$

where:

- $QELIN_{d,y}$ = Industrial consumption of electricity in Census division d in year y ,
- $BMAIN_{elec,d}$ = Consumption of electricity in Census division d , and
- $OTHIND_{elec,d}$ = Consumption of electricity for "other industry" in Census division d .

Similarly for the other fuels:

$$QGFIN_{d,y} = [BMAIN_{ng,d} + OTHIND_{ng,d}] \times \left[\frac{DQMAIN_{cng,d} + DQMAIN_{fds,d}}{BMAIN_{ng,d}} \right] \quad (B-195)$$

where:

- $QGFIN_{d,y}$ = Industrial consumption of core natural gas in Census division d in year y ,
- $BMAIN_{ng,d}$ = Consumption of natural gas in Census division d ,
- $OTHIND_{ng,d}$ = Consumption of natural gas for "other industry" in Census division d ,
- $DQMAIN_{ncng,d}$ = Consumption of core natural gas in Census division d , and
- $DQMAIN_{fds,d}$ = Consumption of feedstock natural gas in Census division d .

$$QGIIN_{d,y} = (BMAIN_{ng,d} + OTHIND_{ng,d}) - QGFIN_{d,y} \quad (B-196)$$

where:

$QGIIN_{d,y}$ = Industrial consumption of non-core natural gas in Census division d in year y ,

$BMAIN_{ng,d}$ = Consumption of natural gas in Census division d ,

$OTHIND_{ng,d}$ = Consumption of natural gas for "other industry" in Census division d , and

$QGFIN_{d,y}$ = Industrial consumption of core natural gas in Census division d in year y .

$$QTPIN_{d,y} = \sum_{f=6}^{15} BMAIN_{f,d} + OTHIND_{f,d} \quad (B-197)$$

where:

$QTPIN_{d,y}$ = Consumption of total petroleum in Census division d in year y ,

$BMAIN_{f,d}$ = Consumption of fuel f in Census division d , and

$OTHIND_{f,d}$ = Consumption of fuel f for "other industry" in Census division d .

$$QHOIN_{d,y} = DQRENW_{hydro,d} \quad (B-198)$$

where:

$QHOIN_{d,y}$ = Industrial consumption of hydropower in Census division d in year y , and

$DQRENW_{hydro,d}$ = Consumption of hydropower in Census division d .

Similarly for other renewables.

For biomass use the following equation:

$$QBMIN_{d,y} = \left[\sum_{f=2}^3 DQRENW_{f,d} \right] + \left[\sum_{u=1}^2 CGOGQ_{d,y,bm,u} \right] + QBMRF_{d,y} \quad (\text{B-199})$$

where:

- $QBMIN_{d,y}$ = Industrial consumption of biomass in Census division d in year y ,
- $DQRENW_{f,d}$ = Consumption of renewable fuel f in Census division d ,
- $CGOGQ_{d,y,bm,u}$ = Consumption of biomass from cogeneration of electricity for use u in enhanced oil recovery in Census division d in year y , and
- $QBMRF_{d,y}$ = Biomass consumed by petroleum refining industry in Census division d in year y .

$$QTRIN_{d,y} = QHOIN_{d,y} + QBMIN_{d,y} + QGEIN_{d,y} + QSTIN_{d,y} + QPVIN_{d,y} + QWIIN_{d,y} + QMSIN_{d,y} \quad (\text{B-200})$$

where:

- $QTRIN_{d,y}$ = Consumption of total renewables in Census division d in year y ,
- $QHOIN_{d,y}$ = Consumption of hydropower in Census division d in year y ,
- $QBMIN_{d,y}$ = Consumption of biomass in Census division d in year y ,
- $QGEIN_{d,y}$ = Consumption of geothermal in Census division d in year y ,
- $QSTIN_{d,y}$ = Consumption of solar thermal in Census division d in year y ,

- $QPVIN_{d,y}$ = Consumption of photovoltaic in Census division d in year y ,
- $QWIIN_{d,y}$ = Consumption of wind in Census division d in year y , and
- $QMSIN_{d,y}$ = Consumption of municipal solid waste in Census division d in year y .

Calculate NEMS cogeneration variables:

$$CGINDCAP_{d,y,f,u,pl} = CAPGW_{d,f,u,pl} + CGRECAP_{d,y,f,u,pl} + CGOGCAP_{d,y,f,u,pl} \quad (\text{B-201})$$

where:

- $CGINDCAP_{d,y,f,u,pl}$ = Industrial planned capacity for cogeneration for use u using fuel f in Census division d in year y ,
- $CAPGW_{d,f,u,pl}$ = Planned capacity for cogeneration of electricity for use u using fuel f in Census division d ,
- $CGRECAP_{d,y,f,u,pl}$ = Refinery planned capacity for cogeneration for use u using fuel f in Census division d in year y .
- $COGOCAP_{d,y,f,u,pl}$ = Oil and gas planned capacity for cogeneration for use u using fuel f in Census division d in year y .

$$CGINDGEN_{d,y,f,u} = GENGWH_{d,f,u} + CGREGEN_{d,y,f,u} + CGOGGEN_{d,y,f,u} \quad (\text{B-202})$$

where:

- $CGINDGEN_{d,y,f,u}$ = Industrial cogeneration of electricity for use u using fuel f in Census division d in year y ,
- $GENGWH_{d,f,u}$ = Cogeneration of electricity for use u using fuel f in Census division d ,

$CGREGEN_{d,y,f,u}$ = Refinery cogeneration of electricity for use u using fuel f in Census division d in year y , and

$CGOGGEN_{d,y,f,u}$ = Oil and gas cogeneration of electricity for use u using fuel f in Census division d in year y .

$$CGINDQ_{d,y,f,u} = DIVFUEL_{d,f,u} + CGREQ_{d,y,f,u} + CGOGQ_{d,y,f,u} \quad (\text{B-203})$$

where:

$CGINDQ_{d,y,f,u}$ = Industrial consumption of fuel f for cogeneration of electricity for use u in Census division d in year y ,

$DIVFUEL_{d,f,u}$ = Consumption of fuel f for cogeneration of electricity for use u in Census division d ,

$CREGQ_{d,y,f,u}$ = Consumption of fuel f from cogeneration of electricity for use u in refineries in Census division d in year y , and

$CGOGQ_{d,y,f,u}$ = Consumption of fuel f from cogeneration of electricity for use u in enhanced oil recovery in Census division d in year y .

$$MANHP_{elec,y} = TMANHP_{elec} + QELRF_{total,y} \quad (\text{B-204})$$

where:

$MANHP_{elec,y}$ = Consumption of electricity for manufacturing heat and power in year y ,

$TMANHP_{elec}$ = Total manufacturing consumption of electricity for manufacturing heat and power, and

$QELRF_{total,y}$ = Electricity consumed by petroleum refining industry in year y .

$$NONHP_{fy} = TNONHP_f + \sum_{u=1}^2 CGOGQ_{total,y,f,u} \quad (B-205)$$

where:

- $NONHP_{fy}$ = Consumption of fuel f for non-manufacturing heat and power in year y ,
- $TNONHP_f$ = Total non-manufacturing consumption of fuel f for heat and power, and
- $CGOGQ_{total,y,f,u}$ = Consumption of fuel f from cogeneration of electricity for use u in enhanced oil recovery in all Census divisions in year y .

$$MISCFD_{fy} = TMISCFD_f \quad (B-206)$$

where:

- $MISCFD_{fy}$ = Consumption of miscellaneous fuels and feedstocks f in year y , and
- $TMISCFD_f$ = Total consumption of miscellaneous fuels and feedstocks f .

$$FOODCON_{fy} = TFOODCON_f \quad (B-207)$$

where:

- $FOODCON_{fy}$ = Consumption of fuel f by the food and kindred products industry in year y , and
- $TFOODCON_f$ = Total consumption of fuel f by the food and kindred products industry.

$$PAPERCON_{f,y} = TPAPERCON_f \quad (\text{B-208})$$

where:

$PAPERCON_{f,y}$ = Consumption of fuel f by the paper and allied products industry in year y , and

$TPAPERCON_f$ = Total consumption of fuel f by the paper and allied products industry in year y .

$$CHEMCON_{f,y} = TCHEMCON_f \quad (\text{B-209})$$

where:

$CHEMCON_{f,y}$ = Consumption of fuel f by the bulk chemical industry in year y , and

$TCHEMCON_f$ = Total consumption of fuel f by the bulk chemical industry.

$$GLASSCON_{f,y} = TGLASSCON_f \quad (\text{B-210})$$

where:

$GLASSCON_{f,y}$ = Consumption of fuel f by the glass and glass products industry in year y , and

$TGLASSCON_f$ = Total consumption of fuel f by the glass and glass products industry.

$$CEMENTCON_{f,y} = TCEMENTCON_f \quad (B-211)$$

where:

$CEMENTCON_{f,y}$ = Consumption of fuel f by the hydraulic cement industry in year y , and

$TCEMENTCON_f$ = Total consumption of fuel f by the hydraulic cement industry.

$$REFCON_{f,y} = TREFCON_f \quad (B-212)$$

where:

$REFCON_{f,y}$ = Consumption of fuel f by the petroleum refining industry in year y , and

$TREFCON_f$ = Total consumption of fuel f by the petroleum refining industry.

$$STEELCON_{f,y} = TSTEELCON_f \quad (B-213)$$

where:

$STEELCON_{f,y}$ = Consumption of fuel f by the blast furnace and basic steel products industry in year y , and

$TSTEELCON_f$ = Total consumption of fuel f by the blast furnace and basic steel products industry.

$$ALUMCON_{f,y} = TALUMCON_f \quad (B-214)$$

where:

$ALUMCON_{f,y}$ = Consumption of fuel f by the primary aluminum industry in year y , and

$TALUMCON_f$ = Total consumption of fuel f by the primary aluminum industry.

$$DEMIMAIN_{f,p,d} = [BMAIN_{f,d} + OTHIND_{f,d}] \times UNCONTEMISSFACT_{f,p} \times EMISSCONTROLFAC_{f,p} \quad (B-215)$$

where:

$DEMIMAIN_{f,p,d}$ = Emissions of pollutant p from main fuel f in Census division d ,

$BMAIN_{f,d}$ = Consumption of main fuel f in Census division d ,

$OTHIND_{f,d}$ = Consumption of fuel f from "other industry" in Census division d ,

$UNCONTEMISSFACT_{f,p}$ = Uncontrolled emission factor for pollutant p using fuel f , and

$EMISSCONTROLFAC_{f,p}$ = Emissions control factor for pollutant p using fuel f .

$$DEMIMAIN_{ng,p,d} = (BMAIN_{ng,d} + OTHIND_{ng,d}) - (BENCHFAC_{ng,d} \times DQMAIN_{ng,d}) + (BENCHFAC_{ng,d} \times QLPIN_{d,y} \times UNCONTEMISSFACT_{cng,p} \times EMISSCONTROLFAC_{cng,p}) + (BENCHFAC_{ng,d} \times DQMAIN_{ng,d} \times UNCONTEMISSFACT_{fng,p} \times EMISSCONTROLFAC_{fng,p}) \quad (B-216)$$

where:

| | | |
|---------------------------|---|--|
| $DEMIMAIN_{ng,p,d}$ | = | Emissions of pollutant p from natural gas in Census division d , |
| $BMAIN_{ng,d}$ | = | Consumption of natural gas feedstocks in Census division d , |
| $OTHIND_{ng,d}$ | = | Consumption of natural gas feedstocks from other industry in Census division d , |
| $BENCHFAC_{ng,d}$ | = | Benchmark factor for natural gas feedstocks in Census division d , |
| $DQMAIN_{ng,d}$ | = | Consumption of natural gas feedstocks in Census division d , |
| $QLPIN_{d,y}$ | = | Industrial consumption of lease and plant natural gas in Census division d in year y , |
| $UNCONTEMISSFACT_{cng,p}$ | = | Uncontrolled emission factor for pollutant p using core natural gas, |
| $EMISSCONTROLFAC_{cng,p}$ | = | Emissions control factor for pollutant p using core natural gas, |
| $UNCONTEMISSFACT_{fng,p}$ | = | Uncontrolled emission factor for pollutant p using feedstock natural gas, and |
| $EMISSCONTROLFAC_{fng,p}$ | = | Emissions control factor for pollutant p using feedstock natural gas. |

$$DEMIMAIN_{lpg,p,d} = ((BMAIN_{lpg,d} + OTHIND_{lpg,d}) - (BENCHFAC_{lpg,d} \times DQMAIN_{lpg,d})) \times (UNCONTEMISSFACT_{lpg,p} \times EMISSCONTROLFAC_{lpg,p}) + (BENCHFAC_{lpg,d} \times DQMAIN_{lpg,d} \times UNCONTEMISSFACT_{lpg,p} \times EMISSCONTROLFAC_{lpg,p}) \quad (\text{B-217})$$

where:

| | | |
|-----------------------------|---|---|
| $DEMIMAIN_{lp,p,d}$ | = | Emissions of pollutant p from liquid petroleum gas in Census division d , |
| $BMAIN_{lp,d}$ | = | Consumption of liquid petroleum gas in Census division d , |
| $OTHIND_{lp,d}$ | = | Consumption of liquid petroleum gas from "other industry" in Census division d , |
| $BENCHFAC_{lp,d}$ | = | Benchmark factor for liquid petroleum gas in Census division d , |
| $DQMAIN_{lp,d}$ | = | Consumption of liquid petroleum gas in Census division d , |
| $UNCONTEMISSFACT_{lp,hp,p}$ | = | Uncontrolled emission factor for pollutant p using liquid petroleum gas for heat and power, |
| $EMISSCONTROLFAC_{lp,hp,p}$ | = | Emissions factor for pollutant p using liquid petroleum gas for heat and power, |
| $UNCONTEMISSFACT_{lp,fp,p}$ | = | Uncontrolled emission factor for pollutant p using liquid petroleum gas for feedstocks, and |
| $EMISSCONTROLFAC_{lp,fp,p}$ | = | Emissions factor for pollutant p using liquid petroleum gas for feedstocks. |

For emissions of SO_x the following equation is used.

$$DEMIMAIN_{f,p,d} = DEMIMAIN_{f,p,d} \times SULFURCONT_f \quad (B-218)$$

where:

| | | |
|--------------------|---|--|
| $DEMIMAIN_{f,p,d}$ | = | Emissions of pollutant p from main fuel f in Census division d , and |
| $SULFURCONT_f$ | = | Sulfur content of fuel f . |

$$DEMIRENW_{f,p,d} = TEMISR_{f,p,r} \times DSRENEW_{f,d} \quad (B-219)$$

where:

$DEMIRENW_{f,p,d}$ = Emissions of pollutant p from renewable fuel f in Census division d ,

$TEMISR_{f,p,r}$ = Total emissions of pollutant p from renewable fuel f in Census region r , and

$DSRENEW_{f,d}$ = Share of output of renewable fuel f in Census division d .

$$EMINCX_{f,p,d,y} = \sum_{f=1}^{NUM_{fg}} DEMIMAIN_{f,p,d} \quad (B-220)$$

where:

$EMINCX_{f,p,d,y}$ = Emissions of pollutant p from fuel f in Census division d in year y ,

NUM_{fg} = Number of fuels in fuel group fg , and

$DEMIMAIN_{f,p,d}$ = Emissions of pollutant p from main fuel f in Census division d .

$$EMINCX_{renw,p,d,y} = \sum_{f=1}^8 DEMIRENW_{f,p,d} \quad (B-221)$$

where:

$EMINCX_{renw,p,d,y}$ = Emissions of pollutant p from renewables in Census division d in year y , and

$DEMIRENW_{f,p,d}$ = Emissions of pollutant p from renewable fuel f in Census division d .

$$EMINCX_{f,p,total,y} = \sum_{d=1}^9 EMINCX_{f,p,d,y} \quad (\text{B-222})$$

where:

$EMINCX_{f,p,total,y}$ = Emissions of pollutant p from fuel f all Census divisions in year y ,

$EMINCX_{f,p,d,y}$ = Emissions of pollutant p from fuel f in Census division d in year y ,

$$EMINC_{f,p,y} = \frac{EMINCX_{f,p,total,y}}{10^6} \quad (\text{B-223})$$

where:

$EMINC_{f,p,y}$ = Industrial emissions of pollutant p from fuel f in year y ,

$EMINCX_{f,p,total,y}$ = Emissions of pollutant p from fuel f in all Census divisions in year y , and

10^6 = Conversion factor to convert to million metric tons.

$$EMINCC_{d,p,y} = \frac{\sum_{f=1}^4 EMINCX_{f,p,d,y}}{10^6} \quad (\text{B-224})$$

where:

- $EMINCC_{d,p,y}$ = Industrial emissions of pollutant p in Census division d in year y ,
- $EMINCX_{f,p,d,y}$ = Emissions of pollutant p from fuel f in Census division d in year y , and
- 10^6 = Conversion factor to convert to million metric tons.

IBSEDS

Calculate benchmark factors.

$$BENCHFAC_{f,d} = \frac{SEDSIND_{f,d}}{BMAIN_{f,d}} \quad (\text{B-225})$$

where:

- $BENCHFAC_{f,d}$ = Benchmark factor for fuel f in Census division d ,
- $SEDSIND_{f,d}$ = SEDS consumption of fuel f in Census division d , and
- $BMAIN_{f,d}$ = Consumption of main fuel f in Census division d .

$$BENCHFAC_{bm,d} = \frac{BIOFUELS_d}{\sum_{f=2}^3 DQRENW_{f,d}} \quad (\text{B-226})$$

where:

- $BENCHFAC_{bm,d}$ = Benchmark factor for biomass in Census division d ,
- $BIOFUELS_d$ = Consumption of biofuels in Census division d , and

$DQRENW_{f,d}$ = Consumption of renewable fuel f in Census division d .

$$OTHIND_{f,d} = [BENCHFAC_{f,d} \times BMAIN_{f,d}] - BMAIN_{f,d} \quad (\text{B-227})$$

where:

$OTHIND_{f,d}$ = Consumption of fuel f for "other industry" in Census division d ,

$BMAIN_{f,d}$ = Consumption of main fuel f in Census division d , and

$BENCHFAC_{f,d}$ = Benchmark factor for fuel f in Census division d .

$$OTHIND_{f,total} = \sum_{d=1}^9 OTHIND_{f,d} \quad (\text{B-228})$$

where:

$OTHIND_{f,total}$ = Consumption of fuel f for "other industry" all Census divisions, and

$OTHIND_{f,d}$ = Consumption of fuel f for "other industry" in Census division d .

PDATA

$$PHDRAT = \frac{PHDRAT}{PRODVX_{i,r}} \quad (\text{B-229})$$

where:

$PHDRAT$ = Ratio of physical units to value of output, and

$PRODVX_{i,r}$ = Value of output for industry i in Census region r .

If $IDVAL = 1$, then

$$PRODX_{i,r} = PHDRAT \times PRODVX_{i,r} \quad (B-230)$$

where:

$PRODX_{i,r}$ = Output in physical units for industry i in Census region r ,

$PHDRAT$ = Ratio of physical units to value of output, and

$PRODVX_{i,r}$ = Value of output for industry i in Census region r .

If $IDVAL = 2$, then

$$PRODX_{i,r} = PRODVX_{i,r} \quad (B-231)$$

where:

$PRODX_{i,r}$ = Output in dollar units for industry i in Census region r , and

$PRODVX_{i,r}$ = Value of output for industry i in Census region r .

If process step s is linked to final consumption, then use the following equation:

$$PRODCUR_{total,s} = PRODFLOW_{old,s,l} \times PRODX_{i,r} \quad (B-232)$$

where:

- $PRODCUR_{total,s}$ = Production at process step s for all vintages,
- $PRODFLOW_{old,s,l}$ = Down-step throughput to process step s linked by link l for old vintage, and
- $PRODX_{i,r}$ = Output for industry i in Census region r .

If process step is linked to some other step, then use the following equation:

$$PRODSUM_{s,l} = PRODFLOW_{old,s,l} \times PRODCUR_{total,s} \quad (B-233)$$

where:

- $PRODSUM_{s,l}$ = Amount of throughput used at process step s through link l ,
- $PRODFLOW_{old,s,l}$ = Down-step throughput to process step s linked by link l for old vintage, and
- $PRODCUR_{total,s}$ = Production at process step s through link l for all vintages.

$$PRODCUR_{total,s} = \sum_{l=1}^{NTMAX_s} PRODSUM_{s,l} \quad (B-234)$$

where:

- $PRODCUR_{total,s}$ = Production at process step s for all vintages,
- $NTMAX_s$ = Number of links at process step s , and

*PRODSUM*_{s,l} = Amount of throughput used at process step *s* through link *l*.

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Appendix D. Model Abstract

Model Name:

Industrial Demand Model

Model Acronym:

None

Description:

The Industrial Demand Model is based upon economic and engineering relationships that model industrial sector energy consumption at the nine Census division level of detail. The seven most energy intensive industries are modeled at the detailed process step level and 25 other industries are modeled at a less detailed level. The industrial model incorporates three components: buildings, process and assembly, and boiler, steam, and cogeneration. The model estimates consumption of 22 main fuels, 6 intermediate fuels, and 8 renewable fuels.

Purpose of the Model:

As a component of the National Energy Modeling System integrated forecasting tool, the industrial model generates mid-term forecasts of industrial sector energy consumption. The industrial model facilitates policy analysis of energy markets, technological development, environmental issues, and regulatory development as they impact industrial sector energy consumption.

Most Recent Model Update:

November 1993.

Part of another Model?

National Energy Modeling System (NEMS)

Model Interfaces:

Receives inputs from the Electricity Market Module, Oil and Gas Market Module, Renewable Fuels Module, Macroeconomic Activity Module, and Petroleum Market Module.

Official Model Representative:

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Documentation:

Model Documentation Report: Industrial Sector Model of the National Energy Modeling System, December 1993.

Archive Media and Installation Manual(s):

As of this writing, the model has not been officially archived. The model will be archived on IBM 3090 mainframe magnetic tape storage as part of the National Energy Modeling System production runs used to generate the Annual Energy Outlook 1994.

Energy System Described:

Domestic industrial sector energy consumption

Coverage:

- Geographic: Nine Census divisions: New England, Mid Atlantic, East North Central, West North Central, South Atlantic, East South Central, West South Central, Mountain, and Pacific.
- Time Unit/Frequency: Annual, 1990 through 2010

Modeling Features:

- Structure: 26 manufacturing and 6 nonmanufacturing industries. The manufacturing industries are further subdivided into the energy intensive and non-energy-intensive industries.
- Each industry is modelled as three separate but interrelated components consisting of the process/assembly component (PA), the buildings component (BLD), and the boiler/steam/cogeneration component (BSC).
- Modeling Technique: Ordinary least-squares with log transformations is used for the nonmanufacturing and non-energy-intensive manufacturing industries. The energy intensive industries are modeled through the use of a detailed process flow accounting procedure.

Non-DOE Input Sources:

National Energy Accounts

Major Industrial Power Plant Database

Historical Dollar Value of Output in the Industrial Sector

DOE Input Sources:

Form EI-867: Survey of Independent Power Producers

- Electricity generation, total and by prime mover
- Electricity generation for own use and sales
- Capacity utilization

Manufacturing Energy Consumption Survey 1988, May 1991

State Energy Data System 1991, May 1993

Computing Environment:

- Hardware Used: IBM 3090
- Operating System: MVS
- Language/Software Used: VS FORTRAN, Ver 2.05

- Memory Requirement: 437K
- Storage Requirement: Model has not yet been archived. It will require an as-yet undetermined number of tracks of an IBM 3380 disk pack.
- Estimated Run Time: 1.1 minutes for a 1990-2010 run in non-iterating NEMS mode on an IBM 3090.
- Special Features: None.

Independent Expert Reviews Conducted:

None.

Status of Evaluation Efforts by Sponsor:

None.

Appendix E. Data Quality and Estimation

Introduction

The NEMS Industrial Demand Model develops forecasts of industrial sector energy consumption based on the data elements as detailed in Appendix A of this report. This Appendix provides the initial values and sources for the input data, and the estimation methods, results, and quality of the parameter estimates. References are also provided at the end of the Appendix for the quality of the Manufacturing Energy Consumption Survey (MECS 1988) and the Non-Utility Power Producer Report (EIA-867).

Table E-1. Building Component UEC (Trillion Btu/Thousand People Employed)

| SIC | Industry | Building Use and Energy Source | | | |
|-------------------------|------------------------------|--------------------------------|----------|--------------|-----------|
| | | Lighting | HVAC | | |
| | | Elec. UEC | Elec UEC | Nat. Gas UEC | Steam UEC |
| 20 | Food & Kindred Products | 0.009 | 0.006 | 0.013 | 0.062 |
| 21 | Tobacco | 0.007 | 0.005 | 0.000 | 0.071 |
| 22 | Textiles | 0.017 | 0.014 | 0.005 | 0.033 |
| 23 | Apparel | 0.001 | 0.002 | 0.005 | 0.009 |
| 24 | Lumber | 0.002 | 0.006 | 0.000 | 0.031 |
| 25 | Furniture | 0.001 | 0.002 | 0.002 | 0.030 |
| 26 | Pulp & Paper | 0.054 | 0.008 | 0.002 | 0.096 |
| 27 | Printing | 0.001 | 0.008 | 0.002 | 0.016 |
| 281, 282, 286, 287 | Bulk Chemicals | 0.037 | 0.018 | 0.002 | 0.118 |
| 283, 284, 285, 289 | Other Chemicals | 0.002 | 0.001 | 0.002 | 0.002 |
| 2911 | Petroleum Refining | 0.156 | 0.074 | 0.036 | 0.123 |
| 295, 299 | Other Petroleum | 0.002 | 0.001 | 0.001 | 0.001 |
| 30 | Rubber | 0.005 | 0.015 | 0.002 | 0.013 |
| 31 | Leather | 0.003 | 0.003 | 0.000 | 0.035 |
| 321, 322, 323 | Glass and Glass Products | 0.148 | 0.084 | 0.030 | 0.000 |
| 324 | Hydraulic Cement | 0.010 | 0.006 | 0.000 | 0.000 |
| 325, 326, 327, 328, 329 | Other | 0.005 | 0.003 | 0.002 | 0.000 |
| 331,332, etc. | Blast Furnaces & Basic Steel | 0.788 | 0.374 | 0.957 | 1.231 |
| 3334, 3341, etc. | Primary Aluminum | 0.053 | 0.025 | 0.000 | 0.007 |
| 333-336, 339 | Other Primary Metals | 0.003 | 0.001 | 0.000 | 0.004 |
| 34 | Fabricated Metals | 0.006 | 0.005 | 0.012 | 0.030 |
| 35 | Industrial Machinery | 0.006 | 0.012 | 0.000 | 0.014 |
| 36 | Electronic Equipment | 0.006 | 0.017 | 0.001 | 0.011 |
| 37 | Transportation Equipment | 0.010 | 0.007 | 0.003 | 0.037 |

Table E-1. Building Component UEC (Trillion Btu/Thousand People Employed)

| SIC | Industry | Building Use and Energy Source | | | |
|-----|-----------------------------|--------------------------------|----------|--------------|-----------|
| | | Lighting | HVAC | | |
| | | Elec. UEC | Elec UEC | Nat. Gas UEC | Steam UEC |
| 38 | Instruments | 0.004 | 0.014 | 0.001 | 0.027 |
| 39 | Miscellaneous Manufacturing | 0.003 | 0.003 | 0.007 | 0.011 |

Source: [30].

**Table E-2.A. Non-Manufacturing Sector PA Component UEC
(Trillion Btu/Billion 1987\$ Output)**

| SIC | Census Region | Elec | Ngas | Resid | Dist | Liq Gas | Motor Gas | Coal | Coke&Br | Other | Total | Steam |
|-----------------------|---------------|-------|--------|-------|-------|---------|-----------|-------|---------|-------|--------|-------|
| 1 Agri-Crops | 1 | 1.116 | 0.369 | 0.000 | 4.656 | 0.643 | 0.764 | 0.002 | 0.000 | 0.133 | 6.434 | 0.162 |
| | 2 | 1.116 | 0.369 | 0.000 | 4.656 | 0.643 | 0.764 | 0.002 | 0.000 | 0.133 | 6.434 | 0.162 |
| | 3 | 1.116 | 0.369 | 0.000 | 4.656 | 0.643 | 0.764 | 0.002 | 0.000 | 0.133 | 6.434 | 0.162 |
| | 4 | 1.116 | 0.369 | 0.000 | 4.656 | 0.643 | 0.764 | 0.002 | 0.000 | 0.133 | 6.434 | 0.162 |
| 2-9 Agri-Other | 1 | 0.320 | 0.119 | 0.000 | 1.335 | 0.185 | 0.219 | 0.000 | 0.000 | 0.041 | 1.860 | 0.042 |
| | 2 | 0.320 | 0.119 | 0.000 | 1.335 | 0.185 | 0.219 | 0.000 | 0.000 | 0.041 | 1.860 | 0.042 |
| | 3 | 0.320 | 0.119 | 0.000 | 1.335 | 0.185 | 0.219 | 0.000 | 0.000 | 0.041 | 1.860 | 0.042 |
| | 4 | 0.320 | 0.119 | 0.000 | 1.335 | 0.185 | 0.219 | 0.000 | 0.000 | 0.041 | 1.860 | 0.042 |
| 12 Coal Mining | 1 | 1.973 | 3.596 | 0.117 | 0.376 | 0.051 | 0.055 | 0.277 | 0.000 | 0.000 | 4.472 | 0.000 |
| | 2 | 1.973 | 3.596 | 0.117 | 0.376 | 0.051 | 0.055 | 0.277 | 0.000 | 0.000 | 4.472 | 0.000 |
| | 3 | 1.973 | 3.596 | 0.117 | 0.376 | 0.051 | 0.055 | 0.277 | 0.000 | 0.000 | 4.472 | 0.000 |
| | 4 | 1.973 | 3.596 | 0.117 | 0.376 | 0.051 | 0.055 | 0.277 | 0.000 | 0.000 | 4.472 | 0.000 |
| 13 Oil&Gas Mining | 1 | 1.754 | 10.739 | 0.377 | 1.235 | 0.172 | 0.175 | 0.909 | 0.000 | 0.014 | 13.607 | 0.698 |
| | 2 | 1.754 | 10.739 | 0.377 | 1.235 | 0.172 | 0.175 | 0.909 | 0.000 | 0.014 | 13.607 | 0.698 |
| | 3 | 1.754 | 10.739 | 0.377 | 1.235 | 0.172 | 0.175 | 0.909 | 0.000 | 0.014 | 13.607 | 0.698 |
| | 4 | 1.754 | 10.739 | 0.377 | 1.235 | 0.172 | 0.175 | 0.909 | 0.000 | 0.014 | 13.607 | 0.698 |
| 10,14 Metal Mining | 1 | 5.572 | 13.033 | 0.425 | 1.384 | 0.193 | 0.198 | 0.826 | 0.000 | 0.000 | 16.054 | 0.272 |
| | 2 | 5.572 | 13.033 | 0.425 | 1.384 | 0.193 | 0.198 | 0.826 | 0.000 | 0.000 | 16.054 | 0.272 |
| | 3 | 5.572 | 13.033 | 0.425 | 1.384 | 0.193 | 0.198 | 0.826 | 0.000 | 0.000 | 16.054 | 0.272 |
| | 4 | 5.572 | 13.033 | 0.425 | 1.384 | 0.193 | 0.198 | 0.826 | 0.000 | 0.000 | 16.054 | 0.272 |
| 15,16,17 Construction | 1 | 0.174 | 0.164 | 0.047 | 0.485 | 0.013 | 0.112 | 0.000 | 0.000 | 1.069 | 1.890 | 0.000 |
| | 2 | 0.174 | 0.164 | 0.047 | 0.485 | 0.013 | 0.112 | 0.000 | 0.000 | 1.069 | 1.890 | 0.000 |
| | 3 | 0.174 | 0.164 | 0.047 | 0.485 | 0.013 | 0.112 | 0.000 | 0.000 | 1.069 | 1.890 | 0.000 |
| | 4 | 0.174 | 0.164 | 0.047 | 0.485 | 0.013 | 0.112 | 0.000 | 0.000 | 1.069 | 1.890 | 0.000 |

Source: [30].

**Table E-2.B. Non-Energy-Intensive Manufacturing Sector PA Component UEC
(Trillion Btu/Billion 1987\$ Output)**

| SIC | Census Region | Elec | Ngas | Reald | Dist | Liq Gas | Coal | Coke&Br | Total Other | Steam | Total Consump. | Bfg/Coq | Waste Gas | Pst Csts | Pulp Liq. | Wood | Byprod. | Total Byprod. | |
|----------------------------------|---------------|-------|-------|-------|-------|---------|-------|---------|-------------|-------|----------------|---------|-----------|----------|-----------|-------|---------|---------------|-------|
| 21 Tobacco | 1 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 2 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 3 | 0.150 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 22 Textiles | 1 | 0.633 | 0.296 | 0.189 | 0.077 | 0.045 | 0.000 | 0.912 | 0.108 | 1.395 | 2.764 | 0.911 | 0.000 | 0.000 | 0.000 | 0.011 | 0.000 | 0.000 | 0.022 |
| | 2 | 0.477 | 0.282 | 0.001 | 0.002 | 0.009 | 0.000 | 0.005 | 0.000 | 1.597 | 3.807 | 0.602 | 0.000 | 0.000 | 0.000 | 0.009 | 0.000 | 0.000 | 0.019 |
| | 3 | 1.625 | 0.379 | 0.653 | 0.042 | 0.016 | 0.000 | 0.000 | 0.090 | 0.776 | 1.935 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 4 | 0.781 | 0.364 | 0.000 | 0.009 | 0.005 | 0.000 | 0.000 | 0.000 | 0.000 | 0.041 | 0.318 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 23 Apparel | 1 | 0.152 | 0.087 | 0.018 | 0.019 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.480 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 2 | 0.259 | 0.152 | 0.000 | 0.007 | 0.000 | 0.011 | 0.000 | 0.001 | 0.000 | 0.480 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 3 | 0.396 | 0.097 | 0.003 | 0.004 | 0.000 | 0.026 | 0.000 | 0.000 | 0.009 | 0.384 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 4 | 0.100 | 0.026 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.007 | 0.132 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 24 Lumber | 1 | 0.572 | 0.235 | 0.064 | 0.293 | 0.000 | 0.000 | 0.000 | 0.000 | 1.410 | 2.788 | 0.000 | 0.000 | 0.000 | 0.000 | 0.192 | 0.000 | 0.192 | 0.155 |
| | 2 | 0.718 | 0.213 | 0.061 | 0.123 | 0.000 | 0.025 | 0.000 | 0.173 | 1.204 | 2.516 | 0.000 | 0.000 | 0.000 | 0.000 | 0.155 | 0.000 | 0.155 | 0.000 |
| | 3 | 1.496 | 0.194 | 0.024 | 0.151 | 0.000 | 0.010 | 0.000 | 0.674 | 3.109 | 5.660 | 0.000 | 0.000 | 0.000 | 0.000 | 0.606 | 0.000 | 0.606 | 0.606 |
| | 4 | 0.700 | 0.111 | 0.019 | 0.137 | 0.000 | 0.000 | 0.000 | 0.669 | 2.940 | 4.576 | 0.000 | 0.000 | 0.000 | 0.000 | 0.601 | 0.000 | 0.601 | 0.601 |
| 25 Furniture | 1 | 0.321 | 0.449 | 0.021 | 0.033 | 0.001 | 0.000 | 0.000 | 0.005 | 0.655 | 0.886 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 | 0.001 | 0.001 |
| | 2 | 0.455 | 0.744 | 0.002 | 0.014 | 0.000 | 0.000 | 0.000 | 0.004 | 0.660 | 1.281 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 | 0.001 | 0.001 |
| | 3 | 0.670 | 0.376 | 0.000 | 0.042 | 0.000 | 0.000 | 0.000 | 0.029 | 0.135 | 1.265 | 0.000 | 0.000 | 0.000 | 0.000 | 0.004 | 0.000 | 0.004 | 0.004 |
| | 4 | 0.192 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.009 | 0.200 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 27 Printing | 1 | 0.273 | 0.088 | 0.001 | 0.011 | 0.016 | 0.000 | 0.000 | 0.011 | 0.000 | 1.177 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 2 | 0.686 | 0.463 | 0.001 | 0.001 | 0.015 | 0.000 | 0.000 | 0.014 | 0.000 | 1.035 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 3 | 0.782 | 0.219 | 0.004 | 0.002 | 0.014 | 0.000 | 0.000 | 0.000 | 0.000 | 0.526 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 4 | 0.363 | 0.128 | 0.000 | 0.001 | 0.033 | 0.000 | 0.000 | 0.000 | 0.000 | 0.268 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Chem., Other 28,3,284,285,289 | 1 | 0.010 | 0.034 | 0.042 | 0.045 | -0.000 | 0.000 | 0.000 | 0.004 | 0.083 | 0.268 | 0.000 | 0.032 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 2 | 0.022 | 0.112 | 0.023 | 0.010 | -0.000 | 0.000 | 0.000 | 0.028 | 0.028 | 0.470 | 0.000 | 0.016 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 3 | 0.059 | 0.956 | 0.053 | 0.046 | -0.000 | 0.000 | 0.000 | 0.761 | 1.373 | 3.247 | 0.000 | 0.445 | 0.000 | 0.000 | 0.000 | 0.000 | 0.445 | 0.493 |
| | 4 | 0.029 | 0.118 | 0.004 | 0.016 | -0.000 | 0.000 | 0.000 | 0.027 | 0.128 | 0.322 | 0.000 | 0.016 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Misc Refining | 1 | 0.068 | 0.029 | 0.011 | 0.294 | 0.000 | 0.051 | 0.000 | 0.526 | 0.207 | 1.021 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 2 | 0.069 | 0.029 | 0.005 | 0.148 | 0.000 | 0.037 | 0.000 | 0.526 | 0.207 | 1.021 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 3 | 0.261 | 0.441 | 0.002 | 0.172 | 0.000 | 0.047 | 0.000 | 2.948 | 1.026 | 4.897 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 4 | 0.243 | 0.140 | 0.014 | 0.308 | 0.000 | 0.000 | 0.000 | 2.608 | 0.728 | 4.041 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 30 Rubber | 1 | 0.885 | 0.222 | 0.019 | 0.067 | 0.018 | 0.000 | 0.000 | 0.023 | 0.667 | 1.900 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 2 | 1.068 | 0.515 | 0.010 | 0.006 | 0.063 | 0.000 | 0.000 | 0.012 | 0.845 | 2.519 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 3 | 1.227 | 0.460 | 0.029 | 0.018 | 0.012 | 0.000 | 0.000 | 0.027 | 0.930 | 2.703 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 4 | 0.639 | 0.353 | 0.003 | 0.007 | 0.011 | 0.000 | 0.000 | 0.000 | 0.375 | 1.287 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

**Table E-2.B. Non-Energy-Intensive Manufacturing Sector PA Component UEC
(Trillion Btu/Billion 1987\$ Output)**

| | Census Region | Elec | Ngas | Reid | Dist | Liq Gas | Coal | Coke&Br | Total Other | Steam | Total Consump. | Waste Gas | Pet Coke | Pulp Lq. | Wood | Byprod. | Byprod. | Total |
|---------------------|------------------|-------|-------|-------|-------|---------|-------|---------|----------------|-------|-------------------|-----------|----------|----------|-------|---------|---------|-------|
| SIC | | | | | | | | | | | | | | | | | | |
| 31 Leather | 1 | 0.185 | 0.339 | 0.139 | 0.071 | 0.000 | 0.131 | 0.000 | 0.000 | 0.004 | 0.869 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 2 | 0.477 | 0.493 | 0.058 | 0.010 | 0.000 | 0.053 | 0.000 | 0.003 | 0.003 | 1.157 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 3 | 0.704 | 0.000 | 0.012 | 0.000 | 0.000 | 0.000 | 0.000 | 0.007 | 0.000 | 0.730 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 4 | 0.307 | 0.868 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 1.177 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| SC&G, Other | 1 | 0.405 | 3.381 | 0.355 | 0.159 | 0.074 | 0.310 | 0.029 | 0.096 | 0.577 | 5.465 | 0.000 | 0.000 | 0.000 | 0.044 | 0.011 | 0.056 | 0.056 |
| 325-336,327,328,329 | 2 | 0.513 | 3.264 | 0.014 | 0.151 | 0.060 | 0.758 | 0.000 | 0.233 | 0.553 | 5.486 | 0.000 | 0.000 | 0.000 | 0.108 | 0.028 | 0.076 | 0.136 |
| | 3 | 0.635 | 4.199 | 0.232 | 0.208 | 0.110 | 0.573 | 0.000 | 0.130 | 0.711 | 6.798 | 0.000 | 0.000 | 0.000 | 0.060 | 0.016 | 0.076 | 0.076 |
| | 4 | 0.474 | 2.439 | 0.044 | 0.109 | 0.144 | 0.566 | 0.073 | 0.114 | 0.419 | 4.381 | 0.000 | 0.000 | 0.000 | 0.000 | 0.026 | 0.014 | 0.067 |
| Prim. Metals, Other | 1 | 0.211 | 0.794 | 0.009 | 0.052 | 0.000 | 0.000 | 0.244 | 0.037 | 0.592 | 1.640 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 335-336,339 | 2 | 0.372 | 1.742 | 0.009 | 0.017 | 0.000 | 0.000 | 1.014 | 0.083 | 0.589 | 3.846 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 3 | 0.354 | 0.840 | 0.009 | 0.026 | 0.000 | 0.000 | 0.296 | 0.029 | 0.194 | 1.845 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 4 | 0.614 | 0.688 | 0.001 | 0.047 | 0.000 | 0.000 | 0.100 | 0.014 | 0.194 | 1.658 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.010 |
| 34 Fab Metals | 1 | 0.505 | 0.855 | 0.027 | 0.066 | 0.035 | 0.005 | 0.008 | 0.021 | 0.183 | 1.703 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 2 | 0.670 | 0.947 | 0.011 | 0.008 | 0.029 | 0.023 | 0.006 | 0.074 | 0.188 | 1.906 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 3 | 0.654 | 0.754 | 0.000 | 0.007 | 0.022 | 0.003 | 0.010 | 0.014 | 0.126 | 1.600 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 4 | 0.533 | 0.574 | 0.000 | 0.032 | 0.007 | 0.000 | 0.000 | 0.067 | 0.113 | 1.316 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 35 Ind Machinery | 1 | 0.348 | 0.230 | 0.020 | 0.032 | 0.007 | 0.000 | 0.000 | 0.000 | 0.103 | 0.740 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 2 | 0.388 | 0.535 | 0.000 | 0.010 | 0.016 | 0.000 | 0.003 | 0.005 | 0.193 | 1.149 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 3 | 0.321 | 0.238 | 0.000 | 0.013 | 0.004 | 0.000 | 0.000 | 0.008 | 0.073 | 0.715 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 4 | 0.268 | 0.355 | 0.000 | 0.001 | 0.013 | 0.000 | 0.000 | 0.011 | 0.100 | 0.720 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 36 Electronics | 1 | 0.333 | 0.218 | 0.020 | 0.019 | 0.018 | 0.000 | 0.004 | 0.009 | 0.116 | 0.742 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 2 | 0.276 | 0.328 | 0.005 | 0.001 | 0.010 | 0.000 | 0.000 | 0.007 | 0.075 | 0.636 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 3 | 0.310 | 0.233 | 0.002 | 0.004 | 0.012 | 0.000 | 0.000 | 0.000 | 0.075 | 0.626 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 4 | 0.282 | 0.108 | 0.000 | 0.001 | 0.009 | 0.000 | 0.000 | 0.014 | 0.080 | 0.828 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 37 Transportation | 1 | 0.130 | 0.242 | 0.008 | 0.005 | 0.006 | 0.003 | 0.023 | 0.014 | 0.047 | 0.583 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 2 | 0.245 | 0.233 | 0.000 | 0.000 | 0.007 | 0.000 | 0.000 | 0.013 | 0.028 | 0.539 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 3 | 0.276 | 0.190 | 0.016 | 0.008 | 0.003 | 0.000 | 0.000 | 0.007 | 0.015 | 0.412 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 4 | 0.244 | 0.138 | 0.001 | 0.003 | 0.003 | 0.000 | 0.000 | 0.007 | 0.015 | 0.876 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 38 Instruments | 1 | 0.445 | 0.174 | 0.022 | 0.024 | 0.001 | 0.000 | 0.000 | 0.007 | 0.174 | 0.876 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 2 | 0.631 | 0.428 | 0.004 | 0.004 | 0.003 | 0.000 | 0.000 | 0.000 | 0.062 | 1.132 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 3 | 0.732 | 0.304 | 0.001 | 0.001 | 0.000 | 0.000 | 0.000 | 0.003 | 0.043 | 0.967 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 4 | 0.634 | 0.247 | 0.000 | 0.001 | 0.000 | 0.000 | 0.000 | 0.001 | 0.068 | 0.913 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 39 Misc. Mfg | 1 | 0.252 | 0.508 | 0.018 | 0.034 | 0.013 | 0.000 | 0.000 | 0.001 | 0.060 | 0.926 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 2 | 0.386 | 0.460 | 0.000 | 0.070 | 0.000 | 0.000 | 0.000 | 0.000 | 0.060 | 0.926 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 3 | 0.753 | 0.000 | 0.007 | 0.003 | 0.032 | 0.000 | 0.000 | 0.073 | 0.017 | 0.907 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| | 4 | 0.185 | 0.112 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.011 | 0.308 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

Table E-3. Food and Kindred Product Industry End-Use Flow (Trillion Btu/Billion 1987\$ Output)

| End-Use Flows | Elec | Nat Gas | Resid | Dist | Other Petro. | LPG | Coal+Coke | Steam | Byproduct |
|-------------------|-------|---------|-------|-------|--------------|-------|-----------|-------|-----------|
| Direct Heating | 0.0 | 0.373 | 0.017 | 0.018 | 0.022 | 0.005 | 0.023 | 0.0 | 0.030 |
| Hot Water & Steam | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.236 | 0.0 |
| Refrig & Freezing | 0.081 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Other Electric | 0.392 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Source: [31].

Table E-4. Pulp and Paper Industry UEC (Energy Use/Ton of Pulp)

| Process Step | Flow MMTons | Elec Kwh/ton | Nat Gas MMBtu/ton | Distillate MMBtu/ton | Resid MMBtu/ton | Other Petro. MMBtu/ton | LPG MMBtu/ton | Coal MMBtu/ton | Steam MMBtu/ton | Wood MMBtu/ton | Pulping Liquor MMBtu/ton |
|---------------------------------------|-------------|-----------------|----------------------|-------------------------|--------------------|------------------------------|------------------|-------------------|--------------------|-------------------|--------------------------------|
| Wood Preparation | 58.0 | 117.23 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.92 | 0.0 |
| Pulping | | | | | | | | | | | |
| Waste Fibers | 17.95 | 351.70 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.6 | 0.0 | 0.0 |
| Mechanical | 7.5 | 1494.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 |
| Semi-Mechanical | 4.1 | 410.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 6.0 | 0.0 | 0.0 |
| Kraft | 46.5 | 410.0 | 1.194 | 0.02 | 0.174 | 0.029 | 0.041 | 0.005 | 12.8 | 0.039 | 17.98 |
| Bleaching | 33.64 | 87.92 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 6.4 | 0.0 | 0.0 |
| Papermaking, Converting, and Misc. | 76.0 | 468.93 | 0.318 | 0.005 | 0.46 | 0.008 | 0.011 | 0.001 | 7.5 | 0.010 | 0.0 |

Source: [31].

Table E-5. Bulk Chemical Industry End-Use Flow (Trillion Btu/Billion 1987\$ Output)

| End-Use Flows | Elec | Nat Gas | Resid | Dist | Other Petro. | LPG | Coal | Steam |
|---------------------------------|-------|---------|-------|-------|--------------|-------|-------|-------|
| Electrolytic/Electrothermal Use | 1.166 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Other Electricity Use | 3.616 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Direct Fuel Use | 0.0 | 4.281 | 0.301 | 0.039 | 0.105 | 0.009 | 0.026 | 0.0 |
| Steam Use | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 6.391 |

Source: [31].

Table E-6. Glass and Glass Product Industry UEC (Energy Use/Ton of Product)

| Process Step | Elec Kwh/ton | Nat Gas MMBtu/ton | Resid MMBtu/ton | Dist MMBtu/ton | Other Petro. MMBtu/ton | Coal MMBtu/ton |
|-------------------|-----------------|----------------------|--------------------|-------------------|---------------------------|-------------------|
| Batch Preparation | 61.547 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Melting/Refining | 52.755 | 8.371 | 0.192 | 0.624 | 0.086 | 0.326 |
| Forming | 342.907 | 0.480 | 0.011 | 0.036 | 0.005 | 0.019 |
| Post-Forming | 26.377 | 2.040 | 0.047 | 0.152 | 0.021 | 0.080 |

Source: [31].

Table E-7. Hydraulic Cement Industry UEC (Energy Use/Ton of Product)

| Process Step | Elec Kwh/ton | Nat Gas MMBtu/ton | Resid MMBtu/ton | Dist MMBtu/ton | Other Petro. MMBtu/ton | Coal MMBtu/ton |
|------------------------|-------------------------|------------------------------|----------------------------|---------------------------|---------------------------------------|---------------------------|
| Portland Cement | | | | | | |
| Wet Process | 216.882 | 1.376 | 0.037 | 0.207 | 1.051 | 4.729 |
| Dry Process | 190.504 | 0.949 | 0.026 | 0.143 | 0.724 | 3.259 |
| Finish Grinding | 67.409 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Source: [31].

Table E-8. Blast Furnace and Basic Steel Products Industry UEC (Energy Use/Ton of Product)

| Unit Process | Flow MMtons | Electricity | Steam | Coal | Coke | Natural Gas(1) | Fuel Oil(1) | Waste Gases (2) | Misc.(3) |
|------------------------------------|-------------|-------------|-------|------|-------|----------------|-------------|-----------------|----------|
| Coke Ovens | 28.9 | 0.10 | 0.80 | 38.6 | | 0.26 | 0.01 | -2.76 | -3.78 |
| Iron and Steel Making (4) | | | | | | | | | |
| Open Hearth/Blast Furnace | 5.1 | 0.11 | 0.77 | 0.06 | 11.90 | 4.50 | 1.79 | -1.34 | 0.10 |
| Blast Furnace/BOF | 57.9 | 0.20 | 1.28 | 0.91 | | 0.85 | 0.31 | -2.25 | -0.05 |
| Electric Arc Furnace | 36.9 | 2.13 | 0.00 | 0.00 | | 0.00 | 0.00 | 0.00 | 0.00 |
| Casting/Primary Breakdown | | | | | | | | | |
| Continuous Casting | 57.6 | 0.09 | 0.01 | 0.00 | | 0.30 | 0.00 | 0.00 | 0.00 |
| Ingot Casting/Primary Rolling | 37.3 | 0.11 | 0.03 | 0.00 | | 1.66 | 0.00 | 0.09 | 0.00 |
| Hot Rolling | 83.8 | 0.35 | 0.02 | 0.00 | | 2.50 | 0.02 | 0.09 | 0.00 |
| Cold Rolling and Finishing | 29.2 | 0.79 | 1.61 | 0.00 | | 1.75 | 0.05 | 0.44 | 0.00 |

Note: Natural gas makes up 93% of purchased gas and liquid fuels.

- (1) Purchased natural gas and liquid fuels.
- (2) Net waste gas use: input-output.
- (3) Includes tar and pitch, light oils, and coke breeze.
- (4) Energy values for coke accounted for by coal used in coke ovens.

Source: [31].

Table E-9. Primary Aluminum Industry UEC (Energy Use/Ton of Product)

| Process Step | Elec Kwh/ton | Nat Gas MMBtu/ton | Other Petro. MMBtu/ton | Coal MMBtu/ton |
|-------------------|-----------------|----------------------|------------------------------|-------------------|
| Aluminum Smelting | 15,457.209 | 3.546 | 2.054 | 0.370 |

Source: [31].

Table E-10. BSC Fuel Component Shares

| SIC | Industry | Census Region | Resid | Dist | Liq Gas | Coal | Coke&Br | Total Other | Total Consump. |
|-----|-----------|---------------|-------|-------|---------|-------|---------|-------------|----------------|
| 20 | Food | 1 | 0.151 | 0.133 | 0.010 | 0.102 | 0.000 | 0.047 | 1.000 |
| | | 2 | 0.556 | 0.011 | 0.006 | 0.381 | 0.000 | 0.033 | 1.000 |
| | | 3 | 0.531 | 0.068 | 0.000 | 0.110 | 0.000 | 0.160 | 1.000 |
| | | 4 | 0.583 | 0.029 | 0.029 | 0.135 | 0.000 | 0.247 | 1.000 |
| 21 | Tobacco | 1 | 0.474 | 0.025 | 0.000 | 0.846 | 0.000 | 0.000 | 1.000 |
| | | 2 | 0.075 | 0.000 | 0.000 | 0.846 | 0.000 | 0.000 | 1.000 |
| | | 3 | 0.000 | 0.075 | 0.000 | 0.000 | 0.000 | 0.000 | 1.000 |
| | | 4 | 0.075 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 1.000 |
| 22 | Textile | 1 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 1.000 |
| | | 2 | 0.461 | 0.060 | 0.031 | 0.038 | 0.000 | 0.048 | 1.000 |
| | | 3 | 0.979 | 0.004 | 0.014 | 0.000 | 0.000 | 0.000 | 1.000 |
| | | 4 | 0.508 | 0.028 | 0.010 | 0.333 | 0.000 | 0.035 | 1.000 |
| 23 | Apparel | 1 | 0.982 | 0.013 | 0.006 | 0.000 | 0.000 | 0.000 | 1.000 |
| | | 2 | 0.551 | 0.216 | 0.005 | 0.000 | 0.000 | 0.003 | 1.000 |
| | | 3 | 0.782 | 0.061 | 0.051 | 0.097 | 0.000 | 0.009 | 1.000 |
| | | 4 | 0.515 | 0.042 | 0.085 | 0.237 | 0.000 | 0.092 | 1.000 |
| 24 | Lumber | 1 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 1.000 |
| | | 2 | 1.000 | 0.335 | 0.000 | 0.000 | 0.000 | 0.000 | 1.000 |
| | | 3 | 0.502 | 0.154 | 0.149 | 0.101 | 0.000 | 0.079 | 1.000 |
| | | 4 | 0.498 | 0.181 | 0.044 | 0.038 | 0.000 | 0.295 | 1.000 |
| 25 | Furniture | 1 | 0.336 | 0.222 | 0.040 | 0.000 | 0.000 | 0.296 | 1.000 |
| | | 2 | 0.341 | 0.200 | 0.054 | 0.000 | 0.000 | 0.013 | 1.000 |
| | | 3 | 0.517 | 0.079 | 0.043 | 0.178 | 0.000 | 0.009 | 1.000 |
| | | 4 | 0.114 | 0.099 | 0.045 | 0.119 | 0.000 | 0.030 | 1.000 |
| 26 | Paper | 1 | 0.000 | 0.000 | 0.089 | 0.000 | 0.000 | 0.046 | 1.000 |
| | | 2 | 0.187 | 0.027 | 0.000 | 0.127 | 0.000 | 0.025 | 1.000 |
| | | 3 | 0.333 | 0.010 | 0.000 | 0.606 | 0.000 | 0.013 | 1.000 |
| | | 4 | 0.388 | 0.011 | 0.000 | 0.408 | 0.000 | 0.055 | 1.000 |
| 27 | Printing | 1 | 0.138 | 0.009 | 0.000 | 0.214 | 0.000 | 0.058 | 1.000 |
| | | 2 | 0.538 | 0.217 | 0.000 | 0.000 | 0.000 | 0.226 | 1.000 |
| | | 3 | 0.527 | 0.030 | 0.000 | 0.000 | 0.000 | 0.047 | 1.000 |
| | | 4 | 0.940 | 0.004 | 0.000 | 0.000 | 0.000 | 0.106 | 1.000 |
| | | | 0.820 | 0.027 | 0.000 | 0.000 | 0.000 | 1.000 | |
| | | | 0.967 | 0.033 | 0.000 | 0.000 | 0.000 | 1.000 | |

Table E-10. BSC Fuel Component Shares, cont.

| SIC | Industry | Census Region | Ngas | Resid | Diat | Liq Gas | Coal | Coke&Br | Other | Total Consump. |
|---------|-----------------------|---------------|-------|-------|-------|---------|-------|---------|-------|----------------|
| 281,282 | Industry Bulk Chem | 1 | 0.401 | 0.305 | 0.041 | 0.002 | 0.053 | 0.000 | 0.187 | 0.012 |
| 286,287 | | 2 | 0.501 | 0.064 | 0.003 | 0.000 | 0.392 | 0.000 | 0.037 | 0.002 |
| | | 3 | 0.659 | 0.023 | 0.002 | 0.002 | 0.148 | 0.002 | 0.153 | 0.010 |
| | | 4 | 0.823 | 0.016 | 0.009 | 0.002 | 0.093 | 0.000 | 0.054 | 0.003 |
| 283,284 | OtherChem | 1 | 0.332 | 0.306 | 0.125 | 0.000 | 0.108 | 0.000 | 0.087 | 0.042 |
| 285,289 | | 2 | 0.315 | 0.049 | 0.008 | 0.000 | 0.609 | 0.000 | 0.013 | 0.006 |
| | | 3 | 0.553 | 0.023 | 0.007 | 0.000 | 0.309 | 0.000 | 0.072 | 0.035 |
| | | 4 | 0.716 | 0.017 | 0.027 | 0.000 | 0.201 | 0.000 | 0.026 | 0.013 |
| 295,299 | Asph, Coal & Misc | 1 | 0.068 | 0.126 | 0.000 | 0.000 | 0.283 | 0.000 | 0.523 | 0.000 |
| | | 2 | 0.085 | 0.065 | 0.000 | 0.000 | 0.259 | 0.000 | 0.590 | 0.000 |
| | | 3 | 0.263 | 0.006 | 0.000 | 0.000 | 0.067 | 0.000 | 0.664 | 0.000 |
| | | 4 | 0.118 | 0.055 | 0.000 | 0.000 | 0.000 | 0.000 | 0.827 | 0.000 |
| 30 | Rubber | 1 | 0.468 | 0.177 | 0.099 | 0.001 | 0.218 | 0.000 | 0.022 | 0.016 |
| | | 2 | 0.849 | 0.068 | 0.007 | 0.002 | 0.058 | 0.000 | 0.010 | 0.006 |
| | | 3 | 0.691 | 0.193 | 0.019 | 0.000 | 0.064 | 0.000 | 0.019 | 0.013 |
| | | 4 | 0.938 | 0.044 | 0.017 | 0.001 | 0.000 | 0.000 | 0.000 | 0.000 |
| 31 | Leather | 1 | 0.209 | 0.537 | 0.108 | 0.000 | 0.146 | 0.000 | 0.000 | 0.000 |
| | | 2 | 0.463 | 0.340 | 0.088 | 0.000 | 0.091 | 0.000 | 0.017 | 0.000 |
| | | 3 | 0.000 | 0.509 | 0.166 | 0.000 | 0.000 | 0.000 | 0.325 | 0.000 |
| | | 4 | 1.000 | 0.000 | 0.000 | 0.000 | 0.145 | 0.000 | 0.004 | 0.000 |
| 321,322 | Glass&Glass Prods. | 1 | 0.692 | 0.112 | 0.047 | 0.000 | 0.333 | 0.000 | 0.009 | 0.000 |
| 323 | | 2 | 0.612 | 0.004 | 0.042 | 0.000 | 0.212 | 0.000 | 0.004 | 0.000 |
| | | 3 | 0.678 | 0.058 | 0.048 | 0.000 | 0.212 | 0.000 | 0.006 | 0.000 |
| | | 4 | 0.612 | 0.017 | 0.039 | 0.000 | 0.326 | 0.000 | 0.000 | 0.000 |
| 324 | Hydraulic Cement | 1 | 0.150 | 0.049 | 0.063 | 0.000 | 0.738 | 0.000 | 0.000 | 0.000 |
| | | 2 | 0.070 | 0.001 | 0.030 | 0.000 | 0.899 | 0.000 | 0.000 | 0.000 |
| | | 3 | 0.112 | 0.019 | 0.050 | 0.000 | 0.820 | 0.000 | 0.000 | 0.000 |
| | | 4 | 0.072 | 0.004 | 0.029 | 0.000 | 0.896 | 0.000 | 0.000 | 0.000 |

Table E-10. BSC Fuel Component Shares, cont.

| SIC | Industry | Census Region | Ngas | Resid | Diat | Liq Gas | Coal | Coke&Br | Total Other | Total Consump. |
|-----------|------------------------|---------------|-------|-------|-------|---------|-------|---------|-------------|----------------|
| 325,326 | Industry | 1 | 0.744 | 0.079 | 0.039 | 0.000 | 0.131 | 0.000 | 0.007 | 1.000 |
| 327,328 | Other SCG | 2 | 0.651 | 0.003 | 0.034 | 0.000 | 0.297 | 0.000 | 0.015 | 1.000 |
| 329 | | 3 | 0.722 | 0.041 | 0.040 | 0.000 | 0.190 | 0.000 | 0.007 | 1.000 |
| | | 4 | 0.653 | 0.012 | 0.032 | 0.000 | 0.293 | 0.000 | 0.010 | 1.000 |
| 331,332 | Blast Furn&Basic Steel | 1 | 0.405 | 0.101 | 0.074 | 0.000 | 0.331 | 0.057 | 0.032 | 1.000 |
| | | 2 | 0.391 | 0.045 | 0.023 | 0.000 | 0.406 | 0.104 | 0.032 | 1.000 |
| | | 3 | 0.422 | 0.100 | 0.037 | 0.000 | 0.347 | 0.068 | 0.025 | 1.000 |
| | | 4 | 0.754 | 0.027 | 0.143 | 0.000 | 0.000 | 0.050 | 0.026 | 1.000 |
| 3334,3341 | Primary Aluminum | 1 | 0.897 | 0.008 | 0.022 | 0.000 | 0.065 | 0.000 | 0.009 | 1.000 |
| 3353,3354 | | 2 | 0.898 | 0.003 | 0.007 | 0.000 | 0.082 | 0.000 | 0.009 | 1.000 |
| | | 3 | 0.909 | 0.007 | 0.011 | 0.000 | 0.066 | 0.000 | 0.006 | 1.000 |
| | | 4 | 0.970 | 0.001 | 0.025 | 0.000 | 0.000 | 0.000 | 0.004 | 1.000 |
| 333-336 | Other Primary Metals | 1 | 0.744 | 0.062 | 0.060 | 0.000 | 0.105 | 0.000 | 0.028 | 1.000 |
| 339 | | 2 | 0.780 | 0.030 | 0.020 | 0.000 | 0.140 | 0.000 | 0.030 | 1.000 |
| | | 3 | 0.776 | 0.062 | 0.030 | 0.000 | 0.110 | 0.000 | 0.021 | 1.000 |
| | | 4 | 0.899 | 0.011 | 0.075 | 0.000 | 0.000 | 0.000 | 0.015 | 1.000 |
| 34 | Fab Metals | 1 | 0.701 | 0.087 | 0.136 | 0.000 | 0.033 | 0.000 | 0.042 | 1.000 |
| | | 2 | 0.747 | 0.034 | 0.017 | 0.000 | 0.155 | 0.000 | 0.047 | 1.000 |
| | | 3 | 0.891 | 0.004 | 0.034 | 0.001 | 0.029 | 0.000 | 0.042 | 1.000 |
| | | 4 | 0.755 | 0.000 | 0.025 | 0.001 | 0.000 | 0.000 | 0.219 | 1.000 |
| 35 | Ind Machinery | 1 | 0.461 | 0.202 | 0.228 | 0.003 | 0.107 | 0.000 | 0.000 | 1.000 |
| | | 2 | 0.565 | 0.002 | 0.037 | 0.003 | 0.387 | 0.000 | 0.006 | 1.000 |
| | | 3 | 0.779 | 0.012 | 0.152 | 0.008 | 0.023 | 0.000 | 0.027 | 1.000 |
| | | 4 | 0.955 | 0.000 | 0.013 | 0.002 | 0.000 | 0.000 | 0.030 | 1.000 |
| 36 | Electronic | 1 | 0.525 | 0.169 | 0.225 | 0.000 | 0.039 | 0.000 | 0.043 | 1.000 |
| | | 2 | 0.670 | 0.033 | 0.010 | 0.000 | 0.256 | 0.000 | 0.032 | 1.000 |
| | | 3 | 0.742 | 0.026 | 0.063 | 0.000 | 0.169 | 0.000 | 0.000 | 1.000 |
| | | 4 | 0.962 | 0.000 | 0.038 | 0.001 | 0.000 | 0.000 | 0.000 | 1.000 |

Table E-10. BSC Fuel Component Shares, cont.

| SIC | Industry | Census Region | Ngas | Resid | Dist | Liq Gas | Coal | Coke&Br | Total Other | Total Consump. | | |
|-----|----------------|------------------|-------|-------|-------|---------|-------|---------|----------------|-------------------|-------|-------|
| | | | | | | | | | | | 1 | 2 |
| 37 | Transportation | 1 | 0.290 | 0.304 | 0.149 | 0.000 | 0.235 | 0.000 | 0.022 | 0.000 | 1.000 | |
| | | 2 | 0.469 | 0.042 | 0.026 | 0.000 | 0.427 | 0.000 | 0.037 | 0.000 | 1.000 | |
| | | 3 | 0.653 | 0.137 | 0.065 | 0.000 | 0.085 | 0.000 | 0.060 | 0.000 | 1.000 | |
| | | 4 | 0.868 | 0.014 | 0.046 | 0.000 | 0.011 | 0.000 | 0.061 | 0.000 | 1.000 | |
| 38 | Instruments | 1 | 0.125 | 0.151 | 0.040 | 0.003 | 0.676 | 0.000 | 0.005 | 0.000 | 1.000 | |
| | | 2 | 0.863 | 0.071 | 0.024 | 0.043 | 0.000 | 0.000 | 0.000 | 0.000 | 1.000 | |
| | | 3 | 0.871 | 0.021 | 0.027 | 0.081 | 0.000 | 0.000 | 0.000 | 0.036 | 0.000 | 1.000 |
| | | 4 | 0.958 | 0.000 | 0.006 | 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.000 | 1.000 |
| 39 | Misc Mfg | 1 | 0.585 | 0.110 | 0.103 | 0.000 | 0.201 | 0.000 | 0.000 | 0.000 | 1.000 | |
| | | 2 | 0.773 | 0.000 | 0.088 | 0.000 | 0.139 | 0.000 | 0.000 | 0.000 | 1.000 | |
| | | 3 | 0.000 | 0.238 | 0.043 | 0.000 | 0.000 | 0.000 | 0.000 | 0.719 | 0.000 | 1.000 |
| | | 4 | 1.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 1.000 |

Source: [30].

Table E-11. Boiler Fuel Share Elasticities

| | Petroleum | Natural Gas | Steam Coal |
|--------------------|------------------|--------------------|-------------------|
| Petroleum | -0.33 | 0.05 | 0.17 |
| Natural Gas | 0.04 | -0.47 | 0.00 |
| Steam Coal | 0.63 | 0.00 | -1.01 |

Source: [95].

Table E-12. Advanced and State-of-The-Art Technologies

Pulp and Paper

Wood preparation: savings over current technology - 16%

- Whole Tree Debarking/Chipping*
- Chip Screening Equipment*

State-Of-The-Art Technologies (Energy Savings by Process Step)

Chemical

Technologies (Kraft, Sulfite):

- Continuous Digesters
- Batch Digesters
- Radar Displacement Heating
- Sunds Defibrator Cold Blow and Extended Delignification
- EKONO's White Liquor Impregnation
- Anthraquinone Pulping
- Alkaline Sulfite Anthraquinone (ASOQ) and Neutral Sulfite Anthraquinone (NSAQ) Pulping
- Tampella Recovery System
- Advanced Black Liquor Evaporator
- Process Controls System

Mechanical and Semi-Mechanical Technologies:

- Pressurized Groundwood (PGW)
- PGW-Plus
- Thermo-Refiner Mechanical Pulping
- Heat Recovery in TMP*
- Cyclotherm System for Heat Recovery*
- Chemimechanical Pulping
- Chemi-Thermomechanical Pulping (CTMP)
- Process Control System

Semi-Chemical Technologies:

- See Chemical and Mechanical S-O-A technologies above

Waste Paper Pulping Technologies:

- Advanced pulping
- Advanced De-inking

Bleaching Oxygen Predelignification Technologies:

- Oxygen Bleaching
- Displacement Bleaching
- Bio-bleaching

Papermaking Technologies:

- Extended Nip Press*
- Hot Pressing
- IR Moisture Profiling*
- Reduced Air Requirement*
- Waste Heat Recovery*
- Process Control System*

* Potential for retrofit

Advanced Technologies

Wood Preparation:

Total Savings Over Average
S-O-A technologies are foreseen to be modest. Most of the energy savings that can be achieved in the future are in the use of computer control, more efficient electric motors/drives, etc. Assume REI's to decrease by 0.5% per year.

Chemical (Kraft/Sulfite) Technologies:

- Technology Introduction: 2005-2015**
- Non-Sulfur Chemimechanical (NSCM) Pulping
 - Advanced Alcohol Pulping
 - Biological Pulping
 - Ontario Paper Co (OPCO) Process
 - Black Liquor Concentration*
 - Black Liquor Heat Recovery*
 - Black Liquor Gasification*

Mechanical Technologies:

- Technology Introduction: 2005-2015**
- Advanced Chemical/Thermal Treatment
 - Non-sulfur Chemimechanical (NSCM)
 - OPCO Process

Semi-Chemical Technologies:

Technology Introduction: 2005-2015

- OPCO Process
- NSCM Process
- Waste Pulping - Improvements in steam use, computer control, etc., assumed to decrease REI by 0.2% per year

Bleaching Technologies:

Technology Introduction: 2005-2015

- Ozone Bleaching
- NO₂/O₂ Bleaching
- Biobleaching

Papermaking Technologies:

Technology Introduction: 2005-2015

- High-Consistency Forming*
- Advances in Wet Pressing
- Press Drying*
- Impulse Drying*
- Air Radio-Frequency-Assisted (ARFA) Drying*

* Potential for retrofit

Glass and Glass Product Industry

State-Of-The-Art Technologies (Energy Savings by Process Step)

Batch Preparation Technologies:

- Computerized Weighing, Mixing, and Charging

Melting/Refining Technologies:

Total savings over average current technologies: 21-27%

- Chemical Boosting
- Oxygen Enriched Combustion Air*
- Automatic Tap Charging Transformers for Electric Melters
- Sealed-in Burner Systems*
- Dual-Depth Melter
- Chimney Block Regenerator

- Refractories
- Reduction of Regenerator Air Leakage*
- Recuperative Burners*

Forming
Post Forming
Technologies:

- Emhart Type 540 Forehearth
- EH-F 400 Series Forehearth
- Forehearth High-Pressure Gas Firing System
- Lightweighting*

* Potential for retrofit

Advanced Technologies

Batch Preparation
Technologies:

No advanced technologies identified

Melting/Refining
Technologies:

Technology Introduction: 1995-2010

- Direct Coal Firing
- Submerged Burner Combustion
- Coal-Fired Hot Gas Generation*
- Advanced Glass Melter
- Batch Liquefaction
- Molybdenum-Lined Electric Melter
- Ultrasonic Bath Agitation/Refining*
- Excess Heat Extraction from Regenerators
- Thermochemical Recuperator
- Sol-Gel Process
- Furnace Insulation Materials*
- Pressure Swing Adsorption Oxygen Generator*
- Hollow Fiber Membrane Air Separation Process*

* Potential for retrofit

Forming
Post-Forming

Technology Introduction: 1995-2010

- **Mold Design***
- **Mold Cooling Systems**
- **Automatic Gob Control**
- **Improved Glass Strengthening Techniques***
- **Improved Protective Coatings***

*** Potential for retrofit**

Hydraulic Cement Industry

State-Of-The-Art Technologies

(Energy Savings by Process Step)

**Dry Process
Technologies:**

- **Roller Mills***
- **High-Efficiency Classifiers***
- **Grinding Media and Mill Linings***
- **Waste Heat Drying***
- **Kiln Feed Slurry Dewatering***
- **Dry-Preheater/Precalciner Kilns**
- **Kiln Radiation and Infiltration Losses***
- **Kiln Internal Efficiency Enhancement***
- **Waste Fuels***
- **Controlled Particle Size Distribution
Cement**
- **High-Pressure Roller Press**
- **Finish Mill Internals, Configuration,
and Operation**
- **Grinding Aids***

**Imports - Finish Grinding
Technologies:**

- **High-Efficiency Classifiers***
- **Controlled Particle Size Distribution
Cement***
- **High Pressure Roller Press**
- **Roller Mills***
- **Finish Mill Internals, Configuration,
and Operation**
- **Grinding Aids***

* Potential for retrofit

Advanced Technologies

Dry Process
Technologies:

Technology Introduction: 1997-2013

- Autogenous Mills
- Differential Grinding
- Sensors and Controls*
- Fluidized-Bed Drying
- Stationary Clinkering Systems
- All-Electric Kilns
- Sensors for On-Line Analysis*
- Advanced Kiln Control*
- Catalyzed, Low-Temperature Calcination
- Alkali Specification Modification*
- Cone Crushers*
- Advanced (Non-Mechanical) Comminution
- Modifying Fineness Specifications*
- Blended Cements*
- Advanced Waste Combustion

Imports - Finish Grinding

Technology Introduction: 1997-2013

- Sensors and Controls*
- Cone Crushers*
- Advanced (Non-Mechanical) Comminution
- Modifying Fineness Specifications*
- Blended Cements*

* Potential for retrofit

Iron and Steel Industry

State-Of-The-Art Technologies

(Energy Savings by Process Step)

Cokemaking
Technologies:

- Dry Quenching of Coke*
- Carbonization Control

- Programmed Heating
- Wet Quenching of Coke with Energy Recovery*
- Sensible Heat Recovery of Off-Gases*

**Ironmaking
Technologies:**

Blast Furnace

- Coal Injection*
- Water-Cooling
- Movable Throat Armor*
- Top Gas Pressure Recovery*
- Hot Stove Waste Heat Recovery*
- Insulation of Cold Blast Main*
- Recovery of BF Gas Released During Charging
- Slag Waste Heat Recovery*
- Paul Wurth Top*
- External Desulfurization - injection of calcium carbide or mag-coke as a desulfurizing reagent*
- Midrex/HBI

**Steelmaking
Technologies:**

Basic Oxygen Furnace

- Gas Recovery in Combination with Sensible Heat Recovery*
- Two working vessels concept*
- Combined Top and Bottom Oxygen Blowing*
- In-Process Control (Dynamic) of Temp and Carbon Content*

Electric Arc Furnace

- DC Arc Furnaces*
- Ultra-High Power (UHP)*
- Computerization*
- Bottom Tap Vessels*
- Water-Cooled Furnace Panels and Top*
- Water-Cooled Electrode Sections*
- Oxy-Fuel Burners*
- Long Arc Foamy Slag Practice*
- Material Handling Practices*

Induction Furnaces*

Energy Optimizing Furnaces*

Scrap-Preheating*

Ladle Drying and Preheating*

Injection Steelmaking (ladle metallurgy)

- Vacuum Arc Decarburization*
- Argon Stirring*

Specialty Steelmaking Processes

- Electroslag Remelting (ESR)*
- Argon-Oxygen Decarburization (AOD)*
- Vacuum Induction Melting (VIM)*
- Electron Beam Melting (EBM)*
- Vacuum Arc Remelting (VAR)*

Steelcasting
Technologies:

- Modern Casters*
- Thin Slab Casting
- Slab Heat Recovery*
- Soaking Pit Utilization and Pit Vacant Time*

Steelforming (rolling)
Technologies:

Hot charging

Preheating Furnaces

- Improved Insulation*
- Waste Heat Recovery and Air Preheating*
- Waste Heat Recovery and Fuel Gas Preheating*
- Increased Length of the Preheating Furnace
- Waste Heat Boilers
- Evaporative Cooling of Furnace Skids

Direct Rolling

- Leveling Furnace*

- The Coil Box*
- Covered Delay Table*

Pickling - Insulated Floats*

Annealing

- Air Preheating*
- Fuel Gas Preheating*
- Combustion Control*

Continuous Annealing

Continuous Cold Rolling

* Potential for retrofit

Advanced Technologies

Ironmaking
Technologies:

- PLASMARED
- COREX
- Direct Iron Ore Smelting (AISI)
- HiSmelt
- Fastmet
- Iron Carbide Route
- KR Process
- Iron ore reduction/steelmaking (AISI)

Direct Steelmaking
Technologies:

PLASMAMELT

INRED

ELRED

Foster Wheeler - Tetronics Expand
Processive Plasma Process

Steelmaking
Technologies:

- Scrap Preheating*
- Energy Optimizing Furnace (EOF)

- Modern Electric Arc Furnace with Continuous Charging/Scrap Preheating
- Modern Basic Oxygen Furnace
 - Injection of Carbonaceous Fuels
 - Increased Scrap Use
- Ladle Drying and Preheating*
- Injection Steelmaking

Steelcasting Technologies:

- Horizontal Continuous Caster*
- Near Net Shapecasting*
- Direct Strip Casting*
- Ultra Thin Strip Casting*
- Spray Casting

Hot/Cold Rolling:

- Direct Rolling
- Continuous Cold Rolling and Finishing
- In Line Melting/Rolling
- Advanced Coating

*Potential for retrofit

NOTE: Many advanced technologies in the Blast Furnace and Basic Steel Products Industry are more energy intensive than their predecessors. Thus it is expected that these new technologies will not fully replace the old ones, but rather provide enhancement particularly for high quality steels. Other advantages include accelerated reaction rates, reduced reactor volume and residence time, lower capital investment, and higher scrap use.

Primary Aluminum Industry

State-Of-The-Art Technologies (Energy Savings by Process Step)

Alumina Refining Technologies:

- Advanced Digesters
- Heat Recovery*

Primary Aluminum Technologies

- Advanced Cells
- New Cathodes*

Semi-Fabrication Technologies

- Continuous-Strip Casting
- Electromagnetic Casting

Secondary Aluminum
Technologies:

- Induction Melting
- Advanced Melting

* Potential for retrofit

Advanced Technologies

Alumina Refining
Technologies:

- Retrofit of S-O-A technologies*

Primary Aluminum
Technologies:

- Technology Introduction: 2003-2023
- Carbothermic Reduction
 - Inert Anodes (potential for retrofit)*
 - Bipolar Cell Technology
 - Wettable Cathodes*

Semi-Fabrication
Technologies:

- Technology Introduction: 1995-2010
- New Melting Technology*
 - Preheaters*

Secondary Aluminum
Technologies:

- Technology Introduction: 1995-2010
- New Melting Technology (submerged radiant burners)
 - Preheaters*
 - Heat Recovery Technology

* Potential for retrofit

Table E-13. Coefficients for Technology Possibility Curves

| SIC | Industry | Process Unit | REI Old Plant | | | REI New Plant | | |
|--------------------------------------|----------------------------|--------------|------------------|------|-------------|------------------|---------|-------------|
| | | | InREIo | REIo | a = (slope) | InREIo | REIo | a = (slope) |
| --- GENERIC END USES OF ENERGY ----- | | | | | | | | |
| 20 | Food* | Direct Fuel | 0 | 1 | -0.00401 | -0.10432 | 0.90094 | -0.00436 |
| | | Steam | 0 | 1 | -0.00301 | -0.10432 | 0.90094 | -0.00436 |
| | | Electric | 0 | 1 | -0.00201 | -0.10432 | 0.90094 | -0.00436 |
| 281 | Inorganic Chemicals* | Direct Fuel | 0 | 1 | -0.00401 | -0.10432 | 0.90094 | -0.00436 |
| | | Steam | 0 | 1 | -0.00301 | -0.10432 | 0.90094 | -0.00436 |
| | | Electric | 0 | 1 | -0.00201 | -0.10432 | 0.90094 | -0.00436 |
| | | Electrolytic | 0 | 1 | -0.00075 | -0.0503 | 0.95094 | -0.00412 |
| 282 | Plastics* | Direct Fuel | 0 | 1 | -0.00401 | -0.10432 | 0.90094 | -0.00436 |
| | | Steam | 0 | 1 | -0.00301 | -0.10432 | 0.90094 | -0.00436 |
| | | Electric | 0 | 1 | -0.00201 | -0.10432 | 0.90094 | -0.00436 |
| 286 | Organic Chemicals* | Direct Fuel | 0 | 1 | -0.00401 | -0.10432 | 0.90094 | -0.00436 |
| | | Steam | 0 | 1 | -0.00301 | -0.10432 | 0.90094 | -0.00436 |
| | | Electric | 0 | 1 | -0.00201 | -0.10432 | 0.90094 | -0.00436 |
| 287 | Agricultural Chemicals* | Direct Fuel | 0 | 1 | -0.00401 | -0.10432 | 0.90094 | -0.00436 |
| | | Steam | 0 | 1 | -0.00301 | -0.10432 | 0.90094 | -0.00436 |
| | | Electric | 0 | 1 | -0.00201 | -0.10432 | 0.90094 | -0.00436 |

Table E-13. Coefficients for Technology Possibility Curves, cont.

| SIC | Industry | Process Unit | REI | | REI | | REI | |
|-----|------------|-------------------------|---------------------|-------------------|--------------------------|---------------------|-------------------|--------------------------|
| | | | Old Plant lnREIo | Old Plant REIo | Old Plant a = (slope) | New Plant lnREIo | New Plant REIo | New Plant a = (slope) |
| 26 | Pulp/Paper | Wood Preparation | 0 | 1 | -0.00305 | -0.17271 | 0.84138 | -0.0052 |
| | | Waste Pulping | 0 | 1 | -0.00131 | -0.07243 | 0.93013 | -0.00204 |
| | | Mechanical Pulping | 0 | 1 | -0.00305 | -0.16882 | 0.84466 | -0.00076 |
| | | Semi Chemical Pulping | 0 | 1 | -0.0059 | -0.32906 | 0.7196 | -0.00378 |
| | | Kraft Sulfite | 0 | 1 | -0.00611 | -0.32597 | 0.72183 | -0.00616 |
| | | Bleaching | 0 | 1 | -0.00486 | -0.26365 | 0.76824 | -0.00329 |
| | | Paper Making | 0 | 1 | -0.00654 | -0.36191 | 0.69835 | 0.00527 |
| | | | | | | | | |
| 32 | Glass | Batch Preparation | 0 | 1 | -0.00102 | -0.12556 | 0.882 | -0.02535 |
| | | Melting/Refining | 0 | 1 | -0.00528 | -0.16481 | 0.84805 | -0.00404 |
| | | Forming | 0 | 1 | -0.00255 | -0.20849 | 0.81343 | -0.00112 |
| | | Post-Forming | 0 | 1 | -0.00259 | -0.24747 | 0.78077 | -0.00834 |
| 32 | Cement | Dry Process | 0 | 1 | -0.00528 | -0.4716 | 0.624 | NA |
| | | Wet Process | 0 | 1 | -0.00244 | NA | NA | NA |
| | | Finish Grinding | 0 | 1 | -0.00528 | -0.1764 | 0.83828 | -0.01097 |
| 33 | Iron/Steel | Coke Oven | 0 | 1 | 0 | -0.17429 | 0.84005 | -0.00116 |
| | | BF/OH | 0 | 1 | 0 | NA | NA | NA |
| | | BF/BOF(1) | 0 | 1 | 0 | 0 | 1.0 | 0 |
| | | EDF | 0 | 1 | 0 | 0 | 1.0 | 0 |
| | | Ingot Cast/Primary Roll | 0 | 1 | 0 | 0 | 1 | 0 |
| | | Cont Casting | 0 | 1 | 0 | 0 | 1 | 0 |
| | | Hot Rolling | 0 | 1 | -0.01774 | -0.61941 | 0.53826 | -0.03863 |
| | | Cold Rolling | 0 | 1 | -0.00675 | -0.164 | 0.84 | -0.00837 |
| 33 | Aluminum | Alumina Refinery | 0 | 1 | -0.00472 | -0.10514 | 0.9002 | -0.00163 |
| | | Primary Aluminum | 0 | 1 | -0.00688 | -0.05417 | 0.89996 | -0.0094 |
| | | Semi-Fabrication | 0 | 1 | -0.01259 | -0.46282 | 0.62951 | -0.00794 |
| | | Secondary Aluminum | 0 | 1 | -0.01442 | -0.42486 | 0.65386 | -0.01589 |

Table E-14. Changes in Fractional Energy Shares

| | <u>Old Plant</u> | | <u>New Plant</u> | |
|---|------------------|------|------------------|------|
| | 1988 | 2015 | 1988 | 2015 |
| CEMENT | | | | |
| - wet process: electric | 0.11 | 0.11 | NA | NA |
| - wet process: direct fuels (1) | 0.89 | 0.89 | NA | NA |
| - dry process: electric | 0.09 | 0.09 | 0.17 | 0.21 |
| - dry process: direct fuels (1) | 0.91 | 0.91 | 0.83 | 0.79 |
| IRON AND STEEL | | | | |
| - EAF: electric | 1.0 | 0.72 | 0.96 | 0.44 |
| - EAF: direct fuels (2) | 0 | 0.28 | 0.04 | 0.56 |
| - Cold Rolling: electric | 0.17 | 0.17 | 0.20 | 0.21 |
| - Cold Rolling: steam | 0.35 | 0.35 | 0.41 | 0.47 |
| - Cold Rolling: direct | 0.48 | 0.48 | 0.39 | 0.32 |
| - Iron and Steel Making (BF/BOF): electric | 0.01 | 0.01 | 0.02 | 0.02 |
| - Iron and Steel Making (BF/BOF): steam | 0.08 | 0.08 | (3) | (3) |
| - Iron and Steel Making (BF/BOF): natural gas | 0.06 | 0.26 | 0.09 | 0.09 |
| - Iron and Steel Making (BF/BOF): steam coal | 0.06 | 0.06 | 0.07 | 0.36 |
| - Iron and Steel Making (BF/BOF): coke | 0.77 | 0.57 | 0 | 0.53 |
| - Iron and Steel Making (BF/BOF): fuel oil | 0.02 | 0.02 | 0.82 | 0 |
| OTHER SECTORS | (4) | | (5) | (5) |

(1) Predominantly coal

(2) Predominantly natural gas

(3) Blast Furnace/Basic Oxygen Furnace (BF/BOF)

and future new iron/steelmaking technologies; see Table M-2

(4) See UEC's in Section 5 to develop fractional energy shares

(5) Fractional energy shares, as a first approximation, remain unchanged (b=0)

Source: [31].

Table E-15. Non-energy-Intensive Industry UEC Regressions

(Data is located in Table E-22)

Agriculture - Crops (Natural Gas)

$$\begin{aligned}
 UECNATGS &= 1.113 - 0.727 \times RPGAS58 \\
 \text{Std.Err.} &\quad (0.043) \quad (0.059) \\
 \text{T-Statistic} &\quad 25.764 \quad -12.230 \\
 \text{Adj. } R^2 &= 0.846
 \end{aligned}
 \tag{E-1}$$

Agriculture - Other (Natural Gas)

$$\begin{aligned}
 UECNATGS &= -3.247 - 2.774 \times RPOIL58 + 0.948 \times RPGAS58 \\
 \text{Std.Err.} &\quad (0.075) \quad (0.427) \quad (0.110) \\
 \text{T-Statistic} &\quad -43.464 \quad -6.499 \quad 8.606 \\
 \text{Adj. } R^2 &= 0.739
 \end{aligned}
 \tag{E-2}$$

Coal Mining (Natural Gas)

$$\begin{aligned}
 UECNATGS &= -2.600 - 0.657 \times RPGAS58 + 0.832 \times CURTAIL \\
 \text{Std.Err.} &\quad (0.058) \quad (0.107) \quad (0.301) \\
 \text{T-Statistic} &\quad -45.075 \quad -6.167 \quad 2.765 \\
 \text{Adj. } R^2 &= 0.587
 \end{aligned}
 \tag{E-3}$$

Tobacco (Oil)

$$\begin{aligned}
 UECOIL &= -2.498 - 1.229 \times RPELEC58 + 2.276 \times CURTAIL \\
 \text{Std.Err.} &\quad (0.066) \quad (0.239) \quad (0.306) \\
 \text{T-Statistic} &\quad -37.993 \quad -5.155 \quad 7.428 \\
 \text{Adj. } R^2 &= 0.720
 \end{aligned}
 \tag{E-4}$$

Textiles (Oil)

$$\begin{array}{l}
 \text{UECOIL} = 0.630 - 0.741 \times \text{RPOIL58} + 1.881 \times \text{CURTAIL} \\
 \text{Std.Err.} \quad (0.065) \quad (0.104) \quad (0.380) \\
 \text{T-Statistic} \quad 9.714 \quad -7.138 \quad 4.946 \\
 \text{Adj. } R^2 = 0.658
 \end{array}
 \tag{E-5}$$

Textiles (Natural Gas)

$$\begin{array}{l}
 \text{UECNATGS} = 0.286 + 0.757 \times \text{RPOIL58} - 1.024 \times \text{RPGAS58} + 0.233 \times \text{RCUMOUT} - 0.840 \times \text{CURTAIL} \\
 \text{Std.Err.} \quad (0.057) \quad (0.133) \quad (0.131) \quad (0.026) \quad (0.162) \\
 \text{T-Statistic} \quad 4.993 \quad 5.711 \quad -7.800 \quad 9.063 \quad -5.174 \\
 \text{Adj. } R^2 = 0.823
 \end{array}
 \tag{E-6}$$

Textiles (Electricity)

$$\begin{array}{l}
 \text{UECELEC} = 0.261 + 0.157 \times \text{RPOIL58} - 0.504 \times \text{RPELEC58} + 0.073 \times \text{RCUMOUT} + 0.225 \times \text{CURTAIL} \\
 \text{Std.Err.} \quad (0.036) \quad (0.051) \quad (0.091) \quad (0.018) \quad (0.079) \\
 \text{T-Statistic} \quad 7.340 \quad 3.076 \quad -5.545 \quad 4.108 \quad 2.832 \\
 \text{Adj. } R^2 = 0.843
 \end{array}
 \tag{E-7}$$

Apparel (Oil)

$$\begin{array}{l}
 \text{UECOIL} = -1.578 - 0.593 \times \text{RPOIL58} - 0.518 \times \text{RPELEC58} \\
 \text{Std.Err.} \quad (0.082) \quad (0.101) \quad (0.213) \\
 \text{T-Statistic} \quad -19.141 \quad -5.868 \quad -2.439 \\
 \text{Adj. } R^2 = 0.642
 \end{array}
 \tag{E-8}$$

Apparel (Electricity)

Printing (Oil)

$$\begin{aligned} \text{UECOIL} &= -1.397 - 0.766 \times \text{RPOIL58} \\ \text{Std.Err.} & \quad (0.062) \quad (0.105) \\ \text{T-Statistic} & \quad -22.502 \quad -7.273 \\ & \quad \text{Adj. } R^2 = 0.650 \end{aligned} \tag{E-14}$$

Printing (Electricity)

$$\begin{aligned} \text{UECELEC} &= -1.130 + 0.491 \times \text{RPGAS58} - 1.320 \times \text{RPELEC58} + 0.347 \times \text{RPCOALS58} \\ \text{Std.Err.} & \quad (0.024) \quad (0.050) \quad (0.066) \quad (0.068) \\ \text{T-Statistic} & \quad -46.622 \quad 9.911 \quad -20.002 \quad 5.108 \\ & \quad \text{Adj. } R^2 = 0.965 \end{aligned} \tag{E-15}$$

Rubber (Electricity)

$$\begin{aligned} \text{UECELEC} &= -0.034 + 0.387 \times \text{RPGAS58} - 0.525 \times \text{RPELEC58} \\ \text{Std.Err.} & \quad (0.025) \quad (0.034) \quad (0.092) \\ \text{T-Statistic} & \quad -1.371 \quad 11.400 \quad -5.700 \\ & \quad \text{Adj. } R^2 = 0.826 \end{aligned} \tag{E-16}$$

Leather (Oil)

$$\begin{aligned} \text{UECOIL} &= -0.515 - 0.215 \times \text{RPOIL58} - 0.441 \times \text{RPELEC58} \\ \text{Std.Err.} & \quad (0.031) \quad (0.032) \quad (0.087) \\ \text{T-Statistic} & \quad -16.472 \quad -6.777 \quad -5.086 \\ & \quad \text{Adj. } R^2 = 0.760 \end{aligned} \tag{E-17}$$

Industrial Machinery (Oil)

$$\begin{aligned} \text{UECOIL} &= -1.010 - 0.944 \times \text{RPOIL58} \\ \text{Std.Err.} & \quad (0.084) \quad (0.139) \\ \text{T-Statistic} & \quad -12.022 \quad -6.811 \\ \text{Adj. R}^2 &= 0.619 \end{aligned} \tag{E-22}$$

Electronics (Oil)

$$\begin{aligned} \text{UECOIL} &= -0.924 - 1.274 \times \text{RPOIL58} + 1.624 \times \text{CURTAIL} \\ \text{Std.Err.} & \quad (0.080) \quad (0.137) \quad (0.479) \\ \text{T-Statistic} & \quad -11.578 \quad -9.306 \quad 3.387 \\ \text{Adj. R}^2 &= 0.752 \end{aligned} \tag{E-23}$$

Electronics (Coal)

$$\begin{aligned} \text{UECCOAL} &= 0.717 - 0.800 \quad \text{OUT} \\ \text{Std.Err.} & \quad (0.188) \quad (0.060) \\ \text{T-Statistic} & \quad 3.804 \quad -13.314 \\ \text{Adj. R}^2 &= 0.867 \end{aligned} \tag{E-24}$$

Transportation Equipment (Coal)

$$\begin{aligned} \text{UECCOAL} &= -0.987 - 1.338 \times \text{RPCOAL58} \\ \text{Std.Err.} & \quad (0.066) \quad (0.163) \\ \text{T-Statistic} & \quad -15.009 \quad -8.215 \\ \text{Adj. R}^2 &= 0.704 \end{aligned} \tag{E-25}$$

Instruments (Oil)

$$\begin{array}{l}
 \text{UECOIL} = -0.412 - 0.586 \times \text{RPOIL58} - 0.213 \times \text{RCUMOUT} + 1.667 \times \text{CURTAIL} \\
 \text{Std.Err.} \quad (0.176) \quad (0.149) \quad (0.065) \quad (0.363) \\
 \text{T-Statistic} \quad -2.334 \quad -3.945 \quad -3.286 \quad 4.590 \\
 \text{Adj. R}^2 = 0.746
 \end{array} \tag{E-26}$$

Instruments (Natural Gas)

$$\begin{array}{l}
 \text{UECNATGS} = -0.566 - 0.374 \times \text{RPGAS58} + 0.049 \times \text{RCUMOUT} \\
 \text{Std.Err.} \quad (0.062) \quad (0.067) \quad (0.023) \\
 \text{T-Statistic} \quad -9.191 \quad -5.580 \quad 2.141 \\
 \text{Adj. R}^2 = 0.550
 \end{array} \tag{E-27}$$

Miscellaneous Manufacturing (Oil)

$$\begin{array}{l}
 \text{UECOIL} = -0.526 - 0.948 \times \text{RPOIL58} \\
 \text{Std.Err.} \quad (0.079) \quad (0.131) \\
 \text{T-Statistic} \quad -6.620 \quad -7.219 \\
 \text{Adj. R}^2 = 0.646; \quad \text{D-W} = 0.282
 \end{array} \tag{E-28}$$

Table E-16. Cogeneration Regressions

Generation

$$\begin{aligned} \text{LNGENK} &= -2.799 + 0.960 \times \text{LNSTEAM} \\ \text{Std.Err.} &\quad (0.325) \quad (0.081) \\ \text{T-Statistic} &\quad -8.605 \quad 11.795 \\ \text{System Weighted } R^2 &= 0.691 \end{aligned} \tag{E-29}$$

Generation for own use

$$\begin{aligned} \text{LNOWNK} &= -1.153 + 1.307 \times \text{LNGENK} \\ \text{Std.Err.} &\quad (0.137) \quad (0.081) \\ \text{T-Statistic} &\quad -8.392 \quad 16.220 \\ \text{System Weighted } R^2 &= 0.691 \end{aligned} \tag{E-30}$$

Table E-17. Regional Technology Shares

| Industry | Technology | Census Region | | | | |
|--|-----------------------|---------------|-------|-------|-------|------|
| | | NE | MW | SO | WE | US |
| Paper and Allied Products | | | | | | |
| | Kraft (incl. Sulfite) | 6.0% | 5.0% | 72.0% | 17.0% | 100% |
| | Semi-Chemical | 11.0% | 30.0% | 48.0% | 11.0% | 100% |
| | Mechanical | 19.0% | 14.0% | 47.0% | 20.0% | 100% |
| | Waste Fiber | 18.0% | 31.0% | 34.0% | 17.0% | 100% |
| Hydraulic Cement | | | | | | |
| | Wet Process | 17.3% | 26.6% | 43.0% | 13.1% | 100% |
| | Dry Process | 9.2% | 28.9% | 35.0% | 26.8% | 100% |
| Blast Furnace and Basic Steel Products | | | | | | |
| | Electric Arc Furnace | 23.6% | 36.1% | 31.6% | 8.7% | 100% |
| | Basic Oxygen Furnace | 10.5% | 69.5% | 20.0% | 0.0% | 100% |
| | Open Hearth | 34.5% | 0.0% | 36.2% | 29.3% | 100% |
| | Coke Oven | 23.9% | 50.4% | 23.5% | 2.1% | 100% |
| Primary Aluminum | | | | | | |
| | Smelters | 7.0% | 15.7% | 43.3% | 34.1% | 100% |

Source: [31].

Table E-18. Retirements

| Industry | Retirement Rate (%) | Industry | Retirement Rate (%) |
|---|---------------------|---|---------------------|
| Food and Kindred Products | 1.7 | Blast Furnace and Basic Steel Products (Blast Furnace/Open Hearth) | 50.0 |
| Tobacco Products | 4.3 | Blast Furnace and Basic Steel Products (Blast Furnace/Basic Oxygen Furnace) | 0.0 |
| Textile Mill Products | 4.6 | Blast Furnace and Basic Steel Products (Electric Arc Furnace) | 1.5 |
| Apparel and Other Textile Products | 1.9 | Primary Aluminum | 2.1 |
| Lumber and Wood Products | 0.7 | Other Primary Metals | 1.2 |
| Furniture and Fixtures | 1.0 | Fabricated Metals | 2.1 |
| Paper and Allied Products | 2.3 | Industrial Machinery | 2.7 |
| Printing and Publishing | 5.4 | Electronic Equipment | 4.5 |
| Bulk Chemicals | 1.9 | Transportation Equipment | 1.6 |
| Other Chemicals | 3.6 | Instruments | 1.5 |
| Asphalt and Miscellaneous Coal Products | 2.2 | Miscellaneous Manufacturing | 2.3 |

Source: [94].

Table E-19. Recycling

| Sector | Estimate for 1988 | Projected for 2015 |
|--|-------------------|--------------------|
| Paper and Allied Products (waste pulping) | 24% | 37% |
| Blast Furnace and Basic Steel Products (scrap melting in electric arc furnace) | 37% | 50% |

Source: [31].

Table E-20. Emission Factors

| Fuel Type | Million Metric Tons Carbon per Quadrillion Btu | Proportion of Nonfuel Use (If Any) Sequestered |
|-----------------------------------|---|---|
| Petroleum | | |
| Motor Gasoline | 19.23 | - |
| LPG | 17.09 | 0.80 |
| Jet Fuel | 19.27 | - |
| Distillate Fuel | 19.77 | - |
| Residual Fuel | 21.44 | - |
| Asphalt and Road Oil | 20.83 | 1.00 |
| Oil | 21.00 | 0.50 |
| Lubricants | 19.25 | 0.80 |
| Petrochemical Feed | 19.23 | - |
| Aviation Gas | 19.27 | - |
| Kerosene | 27.04 | 1.00 |
| Petroleum Coke | 19.23 | 0.00 |
| Special Naphtha | | |
| Other: Waxes and Miscellaneous | 20.83 | 1.00 |
| Coal | | |
| Anthracite Coal | 27.85 | 0.75 |
| Bituminous Coal | 25.12 | 0.75 |
| Subbituminous Coal | 25.98 | 0.75 |
| Lignite | 26.35 | 0.75 |
| Natural Gas | | |
| Natural Gas | 14.39 | 0.33 |

Source: [41].

Table E-21. Data Quality References for MECS and EIA-867

A discussion of the data quality of the MECS data can be found in:
Manufacturing Energy Consumption Survey, Consumption of Energy: 1988, Energy Information Administration, Office of Energy Markets and End Use, U.S. Department of Energy, Washington, DC. pp. 151-155.

The data quality assessment on the EIA-867 data can be found in:
Quality Assessment (EIA-867 Annual Non-Utility Power Producer Report), Office of Statistical Standards, Energy Information Administration, U.S. Department of Energy. October, 1991.

Table E-22A. Non-Manufacturing Consumption and Output, 1958-1985

Sources: Consumption: [97]

Output: U.S. Department of Commerce and DRI, Inc.

Notes: All dollar values are expressed in constant 1987 dollars. The deflator is given in Table E-22D. Prices are per million Btu and quantities are trillion Btus. Output is billion dollars.

The mnemonics are as follows: NATGAS and NATGS--Natural Gas; COAL--Coal; MGAS--Motor Gasoline; LPG--Liquid Petroleum Gas; DIST--Distillate; ASPHAL and ASPH--Asphalt and Road Oil; RESID--Residual Fuel Oil; OIL--Other Oil Products; ELEC--Electricity; OUTPUT--Value of Output.

SIC-AGRI PRODUCTION

| YEAR | QOIL | QNATGAS | QCOAL | QELEC | QMGAS | QLPG | QDIST | QASPHAL | QRESID | OUTPUT |
|------|--------|---------|-------|---------|---------|---------|---------|---------|--------|---------|
| 58 | 7.3762 | 102.940 | 0 | 28.9716 | 323.195 | 7.0795 | 38.913 | 0 | 0 | 33.1422 |
| 59 | 7.0220 | 107.138 | 0 | 34.3114 | 316.264 | 10.9055 | 43.118 | 0 | 0 | 35.1345 |
| 60 | 7.1948 | 111.475 | 0 | 37.9725 | 317.889 | 17.1517 | 60.842 | 0 | 0 | 37.4119 |
| 61 | 6.9123 | 115.471 | 0 | 39.2486 | 294.175 | 23.8586 | 78.967 | 0 | 0 | 37.2503 |
| 62 | 6.9172 | 119.730 | 0 | 40.5588 | 288.592 | 31.2055 | 94.843 | 0 | 0 | 38.4282 |
| 63 | 6.6358 | 124.471 | 0 | 41.8007 | 272.451 | 39.1035 | 114.190 | 0 | 0 | 40.4324 |
| 64 | 6.3112 | 129.475 | 0 | 42.0976 | 259.165 | 46.9446 | 135.439 | 0 | 0 | 41.3848 |
| 65 | 6.1286 | 132.285 | 0 | 45.7348 | 256.769 | 51.3184 | 157.582 | 0 | 0 | 41.8353 |
| 66 | 5.4019 | 135.556 | 0 | 45.6017 | 226.408 | 54.1796 | 180.230 | 0 | 0 | 43.7362 |
| 67 | 4.9466 | 133.936 | 0 | 47.6933 | 207.215 | 57.5245 | 202.494 | 0 | 0 | 45.5314 |
| 68 | 4.6810 | 142.425 | 0 | 49.9145 | 201.274 | 60.7409 | 215.775 | 0 | 0 | 47.4888 |
| 69 | 4.2532 | 145.847 | 0 | 56.1346 | 184.952 | 63.5953 | 243.403 | 0 | 0 | 50.1269 |
| 70 | 3.7715 | 149.381 | 0 | 59.6285 | 169.632 | 64.7653 | 248.013 | 0 | 0 | 51.9809 |
| 71 | 3.5259 | 153.050 | 0 | 61.9214 | 158.168 | 65.5387 | 279.500 | 0 | 0 | 51.8856 |
| 72 | 3.1484 | 145.075 | 0 | 61.5577 | 134.524 | 74.8885 | 280.852 | 0 | 0 | 56.0432 |
| 73 | 3.7433 | 152.622 | 0 | 65.1086 | 155.756 | 81.0004 | 362.750 | 0 | 0 | 62.0630 |
| 74 | 2.7274 | 105.025 | 0 | 61.7525 | 104.507 | 55.3975 | 300.935 | 0 | 0 | 57.8237 |
| 75 | 3.1313 | 126.266 | 0 | 61.0749 | 134.889 | 58.4749 | 309.046 | 0 | 0 | 56.6367 |
| 76 | 3.1510 | 152.630 | 0 | 63.6322 | 117.027 | 69.6237 | 357.312 | 0 | 0 | 63.5892 |
| 77 | 3.1236 | 104.264 | 0 | 63.0804 | 119.113 | 63.2834 | 367.558 | 0 | 0 | 65.0305 |
| 78 | 3.5215 | 145.261 | 0 | 64.1388 | 108.567 | 67.2208 | 474.159 | 0 | 0 | 66.4719 |
| 79 | 3.4022 | 108.395 | 0 | 76.2524 | 109.567 | 69.8584 | 425.598 | 0 | 0 | 71.3046 |
| 80 | 3.0374 | 82.560 | 0 | 72.1000 | 92.010 | 59.4222 | 392.832 | 0 | 0 | 75.7135 |
| 81 | 2.9803 | 75.085 | 0 | 85.3624 | 91.562 | 59.7400 | 375.700 | 0 | 0 | 71.1351 |
| 82 | 2.7669 | 88.651 | 0 | 72.8230 | 74.519 | 62.1087 | 365.097 | 0 | 0 | 69.9481 |
| 83 | 2.7290 | 64.866 | 0 | 64.3551 | 68.297 | 45.1660 | 379.003 | 0 | 0 | 53.3301 |
| 84 | 2.7307 | 68.669 | 0 | 68.1875 | 65.776 | 53.4892 | 378.325 | 0 | 0 | 66.3871 |
| 85 | 2.6658 | 49.405 | 0 | 65.8861 | 59.946 | 50.0875 | 373.645 | 0 | 0 | 70.5416 |

Table E-22A. Non-Manufacturing Consumption and Output, 1958-1985

SIC=OTHER AGRICULTURE

| YEAR | QOIL | QNATGAS | QCOAL | QELEC | QMGAS | QLPG | QDIST | QASPHAL | QRESID | OUTPUT |
|------|--------|---------|--------|---------|---------|---------|---------|---------|--------|---------|
| 58 | 2.5390 | 2.4051 | 0.5593 | 17.9510 | 134.011 | 2.8475 | 5.7521 | 0 | 0.0011 | 61.522 |
| 59 | 2.5774 | 2.4991 | 0.5308 | 21.1159 | 139.976 | 4.5668 | 6.5582 | 0 | 0.0011 | 65.485 |
| 60 | 2.3905 | 2.6280 | 0.5199 | 22.8723 | 131.612 | 6.5775 | 8.4960 | 0 | 0.0011 | 66.463 |
| 61 | 2.3431 | 3.0815 | 0.5952 | 24.3574 | 129.767 | 9.5429 | 11.1103 | 0 | 0.0011 | 69.785 |
| 62 | 2.3114 | 3.1558 | 0.5711 | 25.1302 | 129.713 | 12.5553 | 13.6226 | 0 | 0.0011 | 71.060 |
| 63 | 2.1268 | 3.1223 | 0.5932 | 25.9175 | 121.645 | 15.4466 | 16.0172 | 0 | 0.0011 | 74.467 |
| 64 | 2.0695 | 3.2961 | 0.6027 | 26.8659 | 121.862 | 19.3468 | 19.3739 | 0 | 0.0010 | 76.547 |
| 65 | 1.8413 | 3.3628 | 0.6447 | 24.8460 | 111.322 | 19.4513 | 20.8024 | 0 | 0.0011 | 75.644 |
| 66 | 1.6836 | 3.7871 | 0.7063 | 28.1647 | 104.996 | 21.7993 | 24.3946 | 0 | 0.0012 | 76.732 |
| 67 | 1.4758 | 4.0688 | 0.7061 | 28.6060 | 94.830 | 22.6968 | 26.6664 | 0 | 0.0011 | 79.113 |
| 68 | 1.3388 | 3.7757 | 0.6780 | 30.5985 | 90.168 | 23.3708 | 28.5081 | 0 | 0.0011 | 79.785 |
| 69 | 1.1801 | 4.0313 | 0.7323 | 30.5875 | 83.272 | 24.4278 | 31.2381 | 0 | 0.0010 | 79.561 |
| 70 | 1.1148 | 4.3966 | 0.7729 | 32.3660 | 83.130 | 26.9107 | 34.1616 | 0 | 0.0011 | 81.885 |
| 71 | 0.9214 | 4.4839 | 0.8176 | 35.3076 | 71.221 | 24.8912 | 35.1845 | 0 | 0.0010 | 84.303 |
| 72 | 0.7864 | 4.1332 | 0.8423 | 30.6845 | 61.326 | 28.2334 | 35.3115 | 0 | 0.0011 | 86.588 |
| 73 | 0.8422 | 4.0157 | 0.8283 | 30.2093 | 65.908 | 28.3825 | 42.2191 | 0 | 0.0013 | 83.230 |
| 74 | 0.6484 | 3.0504 | 0.8598 | 31.5670 | 50.267 | 21.9930 | 39.7646 | 0 | 0.0012 | 83.089 |
| 75 | 0.7068 | 6.8090 | 0.8500 | 33.2835 | 55.420 | 22.2972 | 41.4848 | 0 | 0.0012 | 84.120 |
| 76 | 0.7261 | 14.2123 | 0.9037 | 43.7797 | 51.214 | 30.7960 | 56.8109 | 0 | 0.0014 | 87.922 |
| 77 | 0.7115 | 13.2863 | 0.9769 | 48.8151 | 48.966 | 29.7696 | 63.7933 | 0 | 0.0011 | 90.486 |
| 78 | 0.7949 | 25.8696 | 0.9217 | 59.4818 | 45.5072 | 36.0598 | 96.7911 | 0 | 0.0011 | 91.980 |
| 79 | 0.7107 | 15.1733 | 0.9394 | 60.7632 | 41.7407 | 34.5535 | 70.3390 | 0 | 0.0009 | 91.064 |
| 80 | 0.7007 | 9.6057 | 0.9434 | 61.9278 | 39.2793 | 33.6837 | 72.2651 | 0 | 0.0008 | 91.374 |
| 81 | 0.5566 | 6.9818 | 1.0741 | 56.8581 | 31.4403 | 27.3362 | 53.8553 | 0 | 0.0005 | 94.403 |
| 82 | 0.5066 | 8.1395 | 1.0324 | 48.9354 | 26.5730 | 28.0260 | 52.1715 | 0 | 0.0003 | 95.964 |
| 83 | 0.6432 | 8.1385 | 1.0651 | 58.0019 | 31.8740 | 27.9289 | 71.6385 | 0 | 0.0003 | 97.332 |
| 84 | 0.5236 | 6.7633 | 1.0373 | 49.3414 | 25.7073 | 26.2377 | 57.3603 | 0 | 0.0003 | 98.699 |
| 85 | 0.4866 | 4.5963 | 1.1461 | 45.6705 | 23.1177 | 23.3538 | 53.3602 | 0 | 0.0002 | 100.448 |

Table E-22A. Non-Manufacturing Consumption and Output, 1958-1985

SIC=COAL MINING

| YEAR | QOIL | QNTGAS | QCOAL | QELEC | QMGAS | QLPG | QDIST | QASPHAL | QRESID | OUTPUT |
|------|------|--------|--------|---------|--------|--------|---------|---------|---------|---------|
| 58 | 0 | 0.7228 | 5.6050 | 16.7736 | 4.6501 | 2.4690 | 14.4013 | 0 | 1.7783 | 13.2922 |
| 59 | 0 | 0.7765 | 4.9245 | 16.7486 | 4.4388 | 2.3326 | 14.1527 | 0 | 1.7489 | 13.2831 |
| 60 | 0 | 0.8376 | 4.4300 | 16.8461 | 4.2576 | 2.2080 | 14.0049 | 0 | 1.7309 | 13.3109 |
| 61 | 0 | 0.8603 | 3.6493 | 16.2630 | 3.9090 | 1.9982 | 13.2967 | 0 | 1.6444 | 12.8115 |
| 62 | 0 | 0.9560 | 3.1551 | 17.0262 | 3.8804 | 1.9554 | 13.6853 | 0 | 1.6935 | 13.3638 |
| 63 | 0 | 1.0957 | 2.6669 | 18.3908 | 3.9610 | 1.9628 | 14.5260 | 0 | 1.7991 | 14.5492 |
| 64 | 0 | 1.1443 | 2.6591 | 16.6692 | 3.3483 | 1.5649 | 13.7212 | 0 | 1.6944 | 13.5340 |
| 65 | 0 | 1.5066 | 3.4286 | 19.3653 | 3.5924 | 1.5543 | 16.6231 | 0 | 2.0472 | 15.9564 |
| 66 | 0 | 1.7262 | 3.6785 | 19.6788 | 3.3302 | 1.2982 | 17.6275 | 0 | 2.1661 | 16.4888 |
| 67 | 0 | 1.9446 | 3.9867 | 19.7877 | 3.0064 | 1.0035 | 18.5103 | 0 | 2.2691 | 17.0395 |
| 68 | 0 | 1.6654 | 3.7169 | 20.7763 | 3.1375 | 1.0891 | 19.9894 | 0 | 2.7055 | 16.7740 |
| 69 | 0 | 1.4515 | 3.6375 | 22.6512 | 3.4023 | 1.2231 | 22.3271 | 0 | 3.2661 | 17.1379 |
| 70 | 0 | 1.2838 | 3.6490 | 25.7678 | 3.8519 | 1.4245 | 25.9377 | 0 | 4.0390 | 18.4311 |
| 71 | 0 | 0.9224 | 3.2241 | 24.8862 | 3.7042 | 1.4047 | 25.5177 | 0 | 4.1881 | 16.8432 |
| 72 | 0 | 0.7223 | 3.2544 | 28.2362 | 4.1864 | 1.6244 | 29.4314 | 0 | 5.0465 | 18.0040 |
| 73 | 0 | 0.8825 | 3.4938 | 28.4981 | 4.7691 | 1.4714 | 32.8729 | 0 | 5.4948 | 17.9126 |
| 74 | 0 | 1.0802 | 3.9201 | 29.4992 | 5.4833 | 1.3557 | 37.2223 | 0 | 6.0986 | 18.2782 |
| 75 | 0 | 1.3486 | 4.5482 | 32.1406 | 6.5529 | 1.2956 | 43.9451 | 0 | 7.0734 | 19.5577 |
| 76 | 0 | 1.6134 | 5.0299 | 34.1822 | 7.5675 | 1.1925 | 50.2325 | 0 | 7.9313 | 20.4716 |
| 77 | 0 | 1.8415 | 5.6516 | 35.2646 | 8.4071 | 1.0419 | 55.3238 | 0 | 8.6293 | 20.8371 |
| 78 | 0 | 1.5530 | 4.7076 | 35.1441 | 7.8163 | 0.8045 | 53.7639 | 0 | 8.2834 | 20.0146 |
| 79 | 0 | 1.5657 | 5.2336 | 42.3468 | 8.7755 | 0.6960 | 63.2308 | 0 | 9.6116 | 23.3047 |
| 80 | 0 | 1.4005 | 5.1552 | 46.4745 | 8.9605 | 0.4962 | 67.7577 | 0 | 10.1686 | 24.7670 |
| 81 | 0 | 1.1107 | 4.7372 | 47.3010 | 8.4707 | 0.2459 | 67.3825 | 0 | 9.9983 | 24.4928 |
| 82 | 0 | 0.8612 | 4.4431 | 50.2083 | 8.3349 | 0.0000 | 69.9295 | 0 | 10.2342 | 25.2239 |
| 83 | 0 | 0.8071 | 3.8585 | 47.9439 | 7.3925 | 0.0000 | 65.3214 | 0 | 9.4616 | 23.6703 |
| 84 | 0 | 0.9079 | 3.9309 | 55.2181 | 7.8909 | 0.0000 | 73.6338 | 0 | 10.5529 | 26.3206 |
| 85 | 0 | 0.9002 | 3.4851 | 55.8938 | 7.3847 | 0.0000 | 72.9918 | 0 | 10.3495 | 25.4981 |

Table E-22A. Non-Manufacturing Consumption and Output, 1958-1985

SIC-OIL & GAS

| YEAR | QOIL | QNATGAS | QCOAL | QELEC | QMGAS | QLPG | QDIST | QASPHAL | QRESID | OUTPUT |
|------|------|---------|-------|---------|---------|---------|---------|---------|---------|---------|
| 58 | 0 | 176.749 | 0 | 15.783 | 24.6278 | 35.0137 | 27.160 | 0 | 9.0001 | 64.664 |
| 59 | 0 | 178.693 | 0 | 17.720 | 25.3936 | 37.1225 | 27.931 | 0 | 9.3667 | 68.443 |
| 60 | 0 | 171.060 | 0 | 18.885 | 24.2894 | 36.4408 | 26.531 | 0 | 9.0797 | 69.500 |
| 61 | 0 | 167.420 | 0 | 20.457 | 24.5437 | 37.7073 | 26.888 | 0 | 9.2749 | 70.604 |
| 62 | 0 | 165.791 | 0 | 22.223 | 25.3503 | 39.9332 | 27.930 | 0 | 9.6443 | 72.453 |
| 63 | 0 | 159.962 | 0 | 23.846 | 24.4432 | 39.4158 | 26.926 | 0 | 9.5115 | 75.086 |
| 64 | 0 | 160.693 | 0 | 25.579 | 23.2685 | 35.6347 | 30.691 | 0 | 9.3922 | 77.852 |
| 65 | 0 | 158.294 | 0 | 26.392 | 20.9358 | 29.9405 | 32.657 | 0 | 8.7667 | 80.370 |
| 66 | 0 | 157.812 | 0 | 27.836 | 18.2785 | 23.8438 | 33.847 | 0 | 8.2180 | 83.597 |
| 67 | 0 | 157.522 | 0 | 33.563 | 15.7579 | 17.9741 | 36.405 | 0 | 8.6965 | 87.769 |
| 68 | 0 | 163.235 | 0 | 37.113 | 16.4336 | 19.9420 | 37.937 | 0 | 11.8834 | 92.779 |
| 69 | 0 | 170.076 | 0 | 40.408 | 17.4963 | 22.4058 | 40.490 | 0 | 15.1793 | 96.085 |
| 70 | 0 | 173.760 | 0 | 44.188 | 17.3516 | 23.7998 | 39.907 | 0 | 18.5581 | 99.953 |
| 71 | 0 | 171.957 | 0 | 45.863 | 16.7217 | 24.4977 | 38.289 | 0 | 21.0957 | 98.685 |
| 72 | 0 | 174.390 | 0 | 48.536 | 18.0118 | 27.1778 | 41.549 | 0 | 24.5337 | 99.456 |
| 73 | 0 | 190.731 | 0 | 53.010 | 19.7770 | 25.8987 | 46.811 | 0 | 24.7026 | 100.577 |
| 74 | 0 | 204.774 | 0 | 56.326 | 22.7723 | 25.1856 | 54.972 | 0 | 25.0407 | 96.554 |
| 75 | 0 | 212.578 | 0 | 59.067 | 25.8792 | 24.0345 | 62.930 | 0 | 25.4303 | 92.782 |
| 76 | 0 | 225.757 | 0 | 62.983 | 27.8173 | 22.1525 | 67.812 | 0 | 25.7818 | 91.826 |
| 77 | 0 | 242.769 | 0 | 68.830 | 31.5591 | 20.8567 | 76.627 | 0 | 27.4290 | 94.304 |
| 78 | 0 | 248.550 | 0 | 81.329 | 34.7107 | 22.2914 | 82.497 | 0 | 29.9395 | 97.598 |
| 79 | 0 | 251.788 | 0 | 89.605 | 36.2072 | 22.1009 | 84.413 | 0 | 30.6634 | 99.589 |
| 80 | 0 | 256.093 | 0 | 100.531 | 43.4867 | 23.8364 | 97.765 | 0 | 33.5505 | 105.918 |
| 81 | 0 | 260.366 | 0 | 111.894 | 54.2788 | 25.8315 | 116.842 | 0 | 37.1027 | 108.380 |
| 82 | 0 | 248.977 | 0 | 118.924 | 51.7244 | 24.7546 | 109.731 | 0 | 36.6423 | 103.920 |
| 83 | 0 | 238.047 | 0 | 125.780 | 48.0817 | 23.9392 | 101.981 | 0 | 36.5229 | 96.726 |
| 84 | 0 | 239.778 | 0 | 134.152 | 55.8872 | 24.5590 | 114.198 | 0 | 38.5572 | 103.763 |
| 85 | 0 | 231.217 | 0 | 138.124 | 51.9046 | 21.4368 | 105.895 | 0 | 37.6967 | 98.932 |

Table E-22A. Non-Manufacturing Consumption and Output, 1958-1985

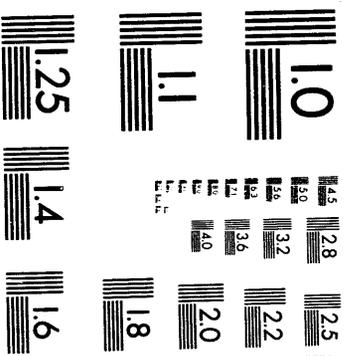
SIC=METAL & OTH MINING

| YEAR | QOIL | QNATGAS | QCOAL | QELEC | QMGAS | QLPG | QDIST | QASPHAL | QRESID | OUTPUT |
|------|------|---------|---------|---------|---------|--------|---------|---------|---------|---------|
| 58 | 0 | 116.615 | 44.1008 | 24.5736 | 13.6299 | 5.3927 | 32.3714 | 0 | 22.3927 | 13.2265 |
| 59 | 0 | 123.612 | 42.1888 | 25.8609 | 13.9017 | 5.2641 | 34.7114 | 0 | 24.0297 | 13.5397 |
| 60 | 0 | 130.043 | 51.1256 | 30.3684 | 13.4580 | 5.2421 | 37.5995 | 0 | 28.6198 | 15.3178 |
| 61 | 0 | 129.516 | 47.4838 | 31.6281 | 12.8165 | 4.7526 | 38.0217 | 0 | 28.5487 | 15.1465 |
| 62 | 0 | 128.758 | 45.8050 | 33.3639 | 12.3632 | 4.2331 | 39.2359 | 0 | 29.3424 | 15.4884 |
| 63 | 0 | 131.831 | 46.9318 | 35.5875 | 11.9904 | 3.7447 | 41.3676 | 0 | 32.0138 | 15.9089 |
| 64 | 0 | 151.920 | 50.1496 | 39.9900 | 12.3563 | 4.0795 | 45.7591 | 0 | 33.7168 | 16.9923 |
| 65 | 0 | 171.822 | 51.5614 | 44.6258 | 12.6721 | 4.4227 | 49.9076 | 0 | 34.4205 | 17.9401 |
| 66 | 0 | 194.597 | 51.6190 | 49.5983 | 12.8266 | 4.8140 | 54.0692 | 0 | 35.4724 | 18.8082 |
| 67 | 0 | 196.497 | 45.5382 | 46.7833 | 11.8706 | 4.4322 | 51.9272 | 0 | 32.4241 | 17.4248 |
| 68 | 0 | 205.231 | 44.1706 | 51.4192 | 11.9458 | 4.8628 | 55.9081 | 0 | 31.2269 | 18.4283 |
| 69 | 0 | 219.898 | 44.9488 | 57.8916 | 11.9111 | 5.4214 | 60.4715 | 0 | 30.7852 | 19.3651 |
| 70 | 0 | 231.627 | 42.0535 | 62.6507 | 11.7805 | 5.8867 | 64.0843 | 0 | 29.6651 | 19.8172 |
| 71 | 0 | 230.746 | 37.8001 | 61.2098 | 11.2031 | 5.6725 | 63.4545 | 0 | 27.3176 | 18.9698 |
| 72 | 0 | 248.240 | 36.2828 | 66.0090 | 11.1613 | 6.0614 | 67.3644 | 0 | 26.9581 | 19.3781 |
| 73 | 0 | 258.561 | 44.6366 | 74.6308 | 11.9706 | 5.7314 | 77.2435 | 0 | 30.2068 | 20.9710 |
| 74 | 0 | 247.408 | 47.4042 | 75.0009 | 11.1528 | 4.9567 | 77.3256 | 0 | 30.8862 | 20.4982 |
| 75 | 0 | 220.942 | 46.9977 | 70.7088 | 9.5254 | 3.9498 | 71.5036 | 0 | 29.3430 | 17.9076 |
| 76 | 0 | 224.864 | 51.9082 | 77.8028 | 9.8472 | 3.6633 | 79.1594 | 0 | 31.9266 | 18.9827 |
| 77 | 0 | 215.323 | 56.5266 | 76.6002 | 9.7966 | 3.1559 | 81.1090 | 0 | 33.1354 | 18.6467 |
| 78 | 0 | 225.728 | 67.8656 | 90.8074 | 10.2884 | 4.0424 | 86.3990 | 0 | 31.6042 | 20.7743 |
| 79 | 0 | 229.783 | 84.8346 | 99.0999 | 10.1262 | 4.7646 | 84.2820 | 0 | 29.4039 | 21.1424 |
| 80 | 0 | 204.909 | 88.7913 | 93.0849 | 8.6730 | 4.7809 | 70.6230 | 0 | 23.7418 | 18.9586 |
| 81 | 0 | 184.551 | 93.2357 | 96.9294 | 7.8864 | 5.0783 | 64.8400 | 0 | 19.6534 | 18.7025 |
| 82 | 0 | 133.157 | 72.9771 | 74.1086 | 6.2486 | 4.5292 | 49.6368 | 0 | 12.6722 | 14.4695 |
| 83 | 0 | 134.688 | 85.5905 | 80.6292 | 6.3887 | 4.8530 | 50.2846 | 0 | 12.7035 | 15.0877 |
| 84 | 0 | 131.494 | 99.8405 | 92.0866 | 5.9886 | 4.8186 | 47.8683 | 0 | 12.5297 | 17.6217 |
| 85 | 0 | 117.077 | 99.3416 | 94.2924 | 5.8327 | 4.5407 | 46.5370 | 0 | 11.4843 | 17.6511 |

Table E-22A. Non-Manufacturing Consumption and Output, 1958-1985

SIC=CONSTRUCTION

| YEAR | QOIL | QNATGAS | QCOAL | QELEC | QMGAS | QLPG | QDIST | QASPHAL | QRESID | OUTPUT |
|------|---------|---------|-------|---------|---------|--------|---------|---------|---------|---------|
| 58 | 33.1053 | 85.110 | 0 | 19.5442 | 64.1250 | 1.4583 | 158.131 | 461.041 | 21.8651 | 330.073 |
| 59 | 38.9082 | 97.489 | 0 | 21.2501 | 66.0021 | 1.7777 | 163.004 | 495.486 | 23.8596 | 364.278 |
| 60 | 36.4030 | 93.781 | 0 | 22.5808 | 71.2180 | 1.8391 | 169.987 | 449.523 | 23.3175 | 367.596 |
| 61 | 37.2572 | 95.660 | 0 | 23.5361 | 71.5402 | 1.8813 | 172.894 | 513.262 | 23.3990 | 377.236 |
| 62 | 39.7399 | 99.269 | 0 | 25.0750 | 67.7357 | 2.0933 | 177.277 | 548.533 | 24.5944 | 386.585 |
| 63 | 40.2742 | 101.819 | 0 | 26.7810 | 65.6320 | 2.1905 | 184.375 | 491.607 | 23.5992 | 409.802 |
| 64 | 41.2624 | 103.811 | 0 | 28.1117 | 66.2086 | 2.2325 | 183.160 | 495.990 | 23.2518 | 420.257 |
| 65 | 43.9960 | 108.363 | 0 | 29.6095 | 65.6320 | 2.3258 | 182.785 | 560.173 | 25.0926 | 438.988 |
| 66 | 45.0162 | 107.986 | 0 | 30.5649 | 66.2036 | 2.4430 | 195.054 | 594.119 | 25.1770 | 440.324 |
| 67 | 44.5625 | 105.524 | 0 | 30.9402 | 61.5769 | 2.6242 | 184.360 | 567.276 | 24.7495 | 438.049 |
| 68 | 47.3925 | 111.726 | 0 | 31.3156 | 53.7122 | 2.8688 | 175.000 | 614.896 | 25.6370 | 456.037 |
| 69 | 47.8176 | 112.344 | 0 | 31.7284 | 53.3886 | 3.3449 | 181.065 | 619.674 | 26.3037 | 456.928 |
| 70 | 45.7534 | 107.120 | 0 | 31.8956 | 56.0488 | 3.4065 | 172.207 | 694.620 | 27.8352 | 436.325 |
| 71 | 50.3184 | 115.121 | 0 | 33.0591 | 50.9349 | 3.6066 | 175.825 | 762.989 | 29.0410 | 468.140 |
| 72 | 53.5564 | 122.129 | 0 | 34.3489 | 44.3179 | 3.7432 | 186.181 | 745.087 | 29.3186 | 501.098 |
| 73 | 55.0741 | 122.777 | 0 | 36.6383 | 44.3392 | 3.7470 | 204.797 | 815.481 | 31.2601 | 497.099 |
| 74 | 46.9714 | 107.078 | 0 | 39.2997 | 41.2787 | 3.4614 | 180.811 | 814.658 | 28.5215 | 443.606 |
| 75 | 41.5825 | 99.148 | 0 | 40.0469 | 34.2575 | 3.1846 | 178.041 | 632.709 | 25.0262 | 422.744 |
| 76 | 45.5256 | 106.043 | 0 | 40.6304 | 29.1298 | 3.3799 | 199.917 | 573.384 | 29.7130 | 449.733 |
| 77 | 48.3658 | 114.063 | 0 | 41.5999 | 28.3353 | 3.4046 | 239.132 | 640.348 | 31.4448 | 478.554 |
| 78 | 51.1925 | 111.469 | 0 | 46.4243 | 27.8330 | 3.5496 | 249.432 | 706.003 | 31.1111 | 503.451 |
| 79 | 50.0009 | 100.002 | 0 | 47.8330 | 24.9286 | 2.5179 | 221.189 | 670.702 | 26.5769 | 513.900 |
| 80 | 45.0635 | 82.085 | 0 | 44.8307 | 60.5244 | 2.5462 | 194.986 | 550.297 | 27.0899 | 498.193 |
| 81 | 42.3773 | 70.239 | 0 | 44.5105 | 51.7583 | 2.7175 | 158.171 | 421.421 | 21.5890 | 489.151 |
| 82 | 38.8209 | 56.444 | 0 | 42.5206 | 41.5796 | 2.9219 | 160.656 | 376.569 | 19.9122 | 448.010 |
| 83 | 43.0419 | 63.542 | 0 | 49.0038 | 35.3024 | 2.9761 | 166.126 | 454.631 | 16.4563 | 471.470 |
| 84 | 49.0803 | 71.004 | 0 | 57.1652 | 32.6838 | 3.1656 | 196.666 | 491.276 | 22.5858 | 526.581 |
| 85 | 51.5245 | 75.234 | 0 | 62.2028 | 31.3848 | 3.2089 | 198.880 | 560.868 | 19.9723 | 552.301 |



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Table E-22B. Non-Manufacturing Prices, 1958-1985

Sources: Prices: [97]

Notes: All dollar values are expressed in constant 1987 dollars. The deflator is given in Table E-22D. Prices are per million Btu.

The mnemonics are as follows: NATGAS and NATGS--Natural Gas; COAL--Coal; MGAS--Motor Gasoline; LPG--Liquid Petroleum Gas; DIST--Distillate; ASPHAL and ASPH--Asphalt and Road Oil; ELEC--Electricity

SIC-AGRI PRODUCTION

| YEAR | POIL87 | PNATGS87 | PCOAL87 | PELEC87 | PMGAS87 | PDIST87 | PASPH87 | PLPG87 | PRESID87 |
|------|---------|----------|---------|---------|---------|---------|---------|---------|----------|
| 58 | 16.3644 | 1.16530 | . | 27.2473 | 8.6781 | 4.5807 | . | 4.14053 | . |
| 59 | 16.1358 | 1.18098 | . | 25.7590 | 8.7138 | 4.6612 | . | 4.28733 | . |
| 60 | 15.9585 | 1.23606 | . | 24.7991 | 8.7950 | 4.4773 | . | 4.42141 | . |
| 61 | 16.1871 | 1.34208 | . | 24.8506 | 8.6947 | 4.5437 | . | 4.50267 | . |
| 62 | 16.8007 | 1.20576 | . | 24.6231 | 8.4413 | 4.3912 | . | 4.55108 | . |
| 63 | 15.9916 | 1.39968 | . | 24.4594 | 8.3482 | 4.3176 | . | 4.99890 | . |
| 64 | 16.0147 | 1.34901 | . | 24.4410 | 8.1398 | 4.2644 | . | 4.78496 | . |
| 65 | 16.3695 | 1.33992 | . | 23.4258 | 7.9673 | 4.1896 | . | 4.53002 | . |
| 66 | 16.9355 | 1.27066 | . | 21.9312 | 7.8323 | 4.0938 | . | 4.63524 | . |
| 67 | 16.5959 | 1.28803 | . | 20.9896 | 7.7579 | 3.9949 | . | 5.09095 | . |
| 68 | 15.8132 | 1.25008 | . | 19.8152 | 7.4423 | 3.9417 | . | 4.81486 | . |
| 69 | 14.8406 | 1.11692 | . | 18.1225 | 7.2621 | 3.8153 | . | 4.43049 | . |
| 70 | 14.4428 | 1.15219 | . | 17.6515 | 7.1323 | 3.4444 | . | 4.38128 | . |
| 71 | 14.9832 | 1.19577 | . | 18.1511 | 7.2686 | 3.8933 | . | 4.63490 | . |
| 72 | 14.3891 | 1.17895 | . | 16.8446 | 6.6138 | 3.5320 | . | 3.98035 | . |
| 73 | 12.8959 | 1.08677 | . | 16.3927 | 6.7666 | 3.9465 | . | 3.66509 | . |
| 74 | 16.0869 | 1.38060 | . | 17.3629 | 8.5602 | 5.8631 | . | 7.05352 | . |
| 75 | 15.2195 | 1.70564 | . | 18.2878 | 8.3189 | 5.7293 | . | 6.49014 | . |
| 76 | 13.4838 | 2.11894 | . | 18.7729 | 8.3864 | 5.7338 | . | 6.64328 | . |
| 77 | 12.4777 | 2.55474 | . | 19.2941 | 8.2856 | 5.7915 | . | 7.31991 | . |
| 78 | 12.6228 | 2.82137 | . | 19.3766 | 8.1080 | 5.5323 | . | 7.09733 | . |
| 79 | 15.5547 | 3.61092 | . | 18.9432 | 9.9972 | 7.5069 | . | 7.23558 | . |
| 80 | 20.0308 | 4.09268 | . | 19.2936 | 13.0761 | 9.9360 | . | 9.30083 | . |
| 81 | 22.8176 | 4.50546 | . | 19.8361 | 13.3016 | 10.6006 | . | 9.53211 | . |
| 82 | 20.5802 | 4.40538 | . | 21.6490 | 12.1172 | 9.5505 | . | 9.23836 | . |
| 83 | 19.4970 | 5.36652 | . | 21.8046 | 11.0614 | 8.2783 | . | 9.64924 | . |
| 84 | 19.3761 | 4.83685 | . | 21.9973 | 10.3677 | 7.9237 | . | 9.10984 | . |
| 85 | 18.6511 | 4.60188 | . | 22.2607 | 9.9520 | 7.3860 | . | 9.17779 | . |

Table E-22B. Non-Manufacturing Prices, 1958-1985

SIC=OTHER AGRICULTURE

| YEAR | POIL87 | PNATGS87 | PCOAL87 | PELEC87 | PMGAS87 | PDIST87 | PASPH87 | PLPG87 | PRESID87 |
|------|---------|----------|---------|---------|---------|---------|---------|---------|----------|
| 58 | 16.3639 | 1.16663 | 2.89145 | 26.5914 | 8.6781 | 4.5805 | . | 4.14042 | 1.42045 |
| 59 | 16.1348 | 1.18230 | 2.96575 | 25.3469 | 8.7138 | 4.6609 | . | 4.28731 | 1.42045 |
| 60 | 15.9576 | 1.23727 | 2.85558 | 24.4610 | 8.7950 | 4.4771 | . | 4.42137 | 1.39860 |
| 61 | 16.1855 | 1.34311 | 2.86832 | 24.5278 | 8.6947 | 4.5436 | . | 4.50266 | 1.38265 |
| 62 | 16.7997 | 1.20684 | 2.81137 | 24.2822 | 8.4413 | 4.3912 | . | 4.55102 | 1.35181 |
| 63 | 15.9911 | 1.40062 | 2.85714 | 24.1547 | 8.3482 | 4.3175 | . | 4.99886 | 1.33690 |
| 64 | 16.0141 | 1.34981 | 2.73139 | 24.0777 | 8.1398 | 4.2644 | . | 4.78494 | 1.44404 |
| 65 | 16.3688 | 1.34068 | 2.62159 | 23.0829 | 7.9673 | 4.1895 | . | 4.52998 | 1.28041 |
| 66 | 16.9335 | 1.27141 | 2.66840 | 21.7415 | 7.8323 | 4.0938 | . | 4.63525 | 1.41723 |
| 67 | 16.5933 | 1.28873 | 2.61745 | 20.8463 | 7.7579 | 3.9949 | . | 5.09096 | 1.50015 |
| 68 | 15.8116 | 1.25080 | 2.51340 | 19.7028 | 7.4423 | 3.9416 | . | 4.81483 | 1.42939 |
| 69 | 14.3408 | 1.11766 | 2.52952 | 18.1751 | 7.2621 | 3.8153 | . | 4.43049 | 1.47929 |
| 70 | 14.4413 | 1.15288 | 2.83723 | 17.9309 | 7.1323 | 3.4443 | . | 4.38127 | 1.29132 |
| 71 | 14.9815 | 1.19664 | 3.02333 | 18.5433 | 7.2686 | 3.8933 | . | 4.63490 | 1.70455 |
| 72 | 14.3863 | 1.17985 | 2.89340 | 17.3443 | 6.6138 | 3.5320 | . | 3.98035 | 1.64011 |
| 73 | 12.8923 | 1.08792 | 2.93492 | 17.0202 | 6.7666 | 3.9465 | . | 3.66507 | 1.86254 |
| 74 | 16.0828 | 1.38205 | 4.05103 | 18.8932 | 8.5602 | 5.8630 | . | 7.05351 | 4.26875 |
| 75 | 15.2157 | 1.70634 | 4.28168 | 19.9319 | 8.3189 | 5.7292 | . | 6.49012 | 3.72629 |
| 76 | 13.4831 | 2.11927 | 4.32152 | 20.0761 | 8.3864 | 5.7337 | . | 6.64328 | 3.55094 |
| 77 | 12.4776 | 2.55504 | 4.37732 | 20.6688 | 8.2856 | 5.7915 | . | 7.31991 | 3.74045 |
| 78 | 12.6220 | 2.82150 | 3.78147 | 20.0384 | 8.1080 | 5.5323 | . | 7.09731 | 3.32226 |
| 79 | 15.5530 | 3.61100 | 3.30582 | 19.4232 | 9.9972 | 7.5069 | . | 7.23560 | 4.23442 |
| 80 | 20.0308 | 4.09289 | 3.38223 | 19.7951 | 13.0762 | 9.9360 | . | 9.30083 | 5.40446 |
| 81 | 22.8173 | 4.50561 | 3.79957 | 20.6723 | 13.3016 | 10.6005 | . | 9.53208 | 6.08365 |
| 82 | 20.5811 | 4.40568 | 3.64826 | 22.2427 | 12.1172 | 9.5505 | . | 9.23837 | 5.96659 |
| 83 | 19.4949 | 5.36672 | 3.13010 | 21.9401 | 11.0614 | 8.2783 | . | 9.64924 | 4.59242 |
| 84 | 19.3771 | 4.83713 | 3.21587 | 22.1903 | 10.3677 | 7.9237 | . | 9.10985 | 5.49451 |
| 85 | 18.6505 | 4.60217 | 2.99385 | 22.1904 | 9.9520 | 7.3860 | . | 9.17780 | 5.29661 |

Table E-22B. Non-Manufacturing Prices, 1958-1985

SIC=COAL MINING

| YEAR | POIL87 | PNATGS87 | PCOAL87 | PELEC87 | PMGAS87 | PDIST87 | PASPH87 | PLPG87 | PRESID87 |
|------|--------|----------|---------|---------|---------|---------|---------|---------|----------|
| 58 | . | 1.51862 | 0.69560 | 14.9046 | 7.8678 | 3.99411 | . | 2.87993 | 2.24385 |
| 59 | . | 1.58514 | 0.65909 | 14.6757 | 7.9498 | 3.83162 | . | 2.97783 | 2.26392 |
| 60 | . | 1.61818 | 0.59489 | 15.4195 | 7.9419 | 3.63109 | . | 3.20600 | 2.24294 |
| 61 | . | 1.65695 | 0.57149 | 12.6902 | 7.7886 | 3.62444 | . | 2.88149 | 2.16219 |
| 62 | . | 1.64914 | 0.53492 | 13.4352 | 7.5053 | 3.38224 | . | 2.38212 | 2.17275 |
| 63 | . | 1.60386 | 0.51696 | 12.4932 | 7.0653 | 3.42677 | . | 2.47658 | 1.92498 |
| 64 | . | 1.45092 | 0.59886 | 13.2969 | 7.0102 | 3.25381 | . | 2.35168 | 1.97422 |
| 65 | . | 1.36489 | 0.65008 | 13.8881 | 7.2894 | 3.16018 | . | 2.29577 | 1.92276 |
| 66 | . | 1.27290 | 0.74056 | 15.1504 | 7.1587 | 3.09224 | . | 2.51290 | 1.92405 |
| 67 | . | 1.18904 | 0.82543 | 11.4273 | 7.0916 | 3.11697 | . | 2.38078 | 1.83554 |
| 68 | . | 1.35329 | 0.76144 | 9.9430 | 6.8492 | 2.98627 | . | 2.00269 | 1.75882 |
| 69 | . | 1.49488 | 0.71779 | 9.3601 | 6.7081 | 2.88819 | . | 1.81661 | 1.57753 |
| 70 | . | 1.67272 | 0.80455 | 9.3484 | 6.5666 | 2.83309 | . | 1.83916 | 1.84824 |
| 71 | . | 1.98192 | 0.80784 | 9.9553 | 6.6160 | 2.92118 | . | 1.93365 | 2.33250 |
| 72 | . | 2.14093 | 0.71196 | 9.6697 | 6.0297 | 2.76416 | . | 1.90316 | 2.39648 |
| 73 | . | 2.03362 | 0.78458 | 9.5155 | 6.1212 | 2.99459 | . | 2.16871 | 2.82072 |
| 74 | . | 1.99893 | 1.36519 | 11.5588 | 8.4533 | 5.14121 | . | 5.18425 | 5.27705 |
| 75 | . | 2.11406 | 1.58157 | 11.9272 | 8.6982 | 5.40170 | . | 5.46863 | 5.36161 |
| 76 | . | 2.47675 | 1.58676 | 11.9897 | 8.2506 | 5.45518 | . | 7.26449 | 5.19258 |
| 77 | . | 2.91442 | 1.51897 | 13.5378 | 7.6608 | 5.59183 | . | 5.83683 | 4.84875 |
| 78 | . | 2.95046 | 1.82997 | 12.1154 | 7.3611 | 5.28999 | . | 4.70113 | 4.26761 |
| 79 | . | 3.56353 | 1.93001 | 11.8946 | 9.4603 | 6.90435 | . | 5.55986 | 4.93674 |
| 80 | . | 3.84342 | 1.97775 | 12.3991 | 12.6987 | 9.15377 | . | 8.07757 | 5.95349 |
| 81 | . | 4.01373 | 2.05787 | 13.0269 | 12.7860 | 9.61315 | . | 7.66744 | 7.17099 |
| 82 | . | 4.07199 | 2.17011 | 14.0631 | 10.9596 | 8.80770 | . | . | 6.24986 |
| 83 | . | 4.20038 | 2.08049 | 12.0087 | 9.2440 | 7.59189 | . | . | 6.30447 |
| 84 | . | 3.99570 | 2.09121 | 13.3973 | 7.8084 | 6.67288 | . | . | 5.36130 |
| 85 | . | 3.71316 | 2.09925 | 13.1412 | 7.1512 | 5.76728 | . | . | 4.39371 |

Table E-22B. Non-Manufacturing Prices, 1958-1985

SIC=OIL & GAS

| YEAR | POIL87 | PNATGS87 | PCOAL87 | PELEC87 | PMGAS87 | PDIST87 | PASPH87 | PLPG87 | PRESID87 |
|------|--------|----------|---------|---------|---------|---------|---------|---------|----------|
| 58 | . | 0.58131 | . | 14.5747 | 8.3061 | 3.76752 | . | 2.87992 | 2.14347 |
| 59 | . | 0.63167 | . | 14.7882 | 8.4788 | 3.59975 | . | 2.97784 | 2.13335 |
| 60 | . | 0.66999 | . | 16.0252 | 8.5819 | 3.38975 | . | 3.20600 | 2.07915 |
| 61 | . | 0.71137 | . | 13.6576 | 8.4916 | 3.36318 | . | 2.88171 | 1.97368 |
| 62 | . | 0.73133 | . | 15.0081 | 8.2400 | 3.11763 | . | 2.38213 | 1.95034 |
| 63 | . | 0.73209 | . | 14.5002 | 7.8520 | 3.13102 | . | 2.47653 | 1.69176 |
| 64 | . | 0.66832 | . | 15.1712 | 7.7760 | 3.00711 | . | 2.35193 | 1.78126 |
| 65 | . | 0.63592 | . | 14.4813 | 8.1167 | 2.94750 | . | 2.29580 | 1.73142 |
| 66 | . | 0.60300 | . | 14.5398 | 8.0069 | 2.91373 | . | 2.51288 | 1.69542 |
| 67 | . | 0.57483 | . | 12.3324 | 7.9224 | 2.99001 | . | 2.38071 | 1.66335 |
| 68 | . | 0.58299 | . | 10.3850 | 7.5426 | 2.91372 | . | 2.00293 | 1.46873 |
| 69 | . | 0.58144 | . | 9.4638 | 7.3161 | 2.86333 | . | 1.81651 | 1.20783 |
| 70 | . | 0.59656 | . | 9.1165 | 7.1325 | 2.85980 | . | 1.83913 | 1.25911 |
| 71 | . | 0.65099 | . | 9.3614 | 7.1792 | 3.00671 | . | 1.93358 | 1.40173 |
| 72 | . | 0.65625 | . | 8.7851 | 6.5491 | 2.89674 | . | 1.90308 | 1.28161 |
| 73 | . | 0.69468 | . | 8.8044 | 6.6333 | 3.04253 | . | 2.16876 | 1.59754 |
| 74 | . | 0.76992 | . | 10.9007 | 9.1232 | 5.08253 | . | 5.18445 | 3.21850 |
| 75 | . | 0.92459 | . | 11.4446 | 9.3417 | 5.20164 | . | 5.46860 | 3.49231 |
| 76 | . | 1.23199 | . | 11.6603 | 8.8083 | 5.10161 | . | 7.26457 | 3.52691 |
| 77 | . | 1.67143 | . | 13.3315 | 8.1100 | 5.08225 | . | 5.83711 | 3.43918 |
| 78 | . | 1.74727 | . | 12.1164 | 7.7272 | 4.93301 | . | 4.70088 | 3.16019 |
| 79 | . | 2.19403 | . | 12.0915 | 9.8362 | 6.58998 | . | 5.55952 | 3.84749 |
| 80 | . | 2.48137 | . | 12.8628 | 13.0603 | 8.94925 | . | 8.07743 | 4.95679 |
| 81 | . | 2.73455 | . | 13.8301 | 12.9964 | 9.60744 | . | 7.66603 | 6.38389 |
| 82 | . | 2.94013 | . | 15.3093 | 11.0017 | 8.98699 | . | 7.17828 | 5.81354 |
| 83 | . | 3.03073 | . | 12.9110 | 9.1540 | 7.90943 | . | 7.13399 | 6.15614 |
| 84 | . | 2.88237 | . | 14.1694 | 7.6099 | 7.09896 | . | 6.47279 | 5.55376 |
| 85 | . | 2.67583 | . | 13.7169 | 6.8552 | 6.27607 | . | 6.86259 | 4.80373 |

Table E-22B. Non-Manufacturing Prices, 1958-1985

SIC=METAL & OTH MINING

| YEAR | POIL87 | PNATGS87 | PCOAL87 | PELEC87 | PMGAS87 | PDIST87 | PASPH87 | PLPG87 | PRESID87 |
|------|--------|----------|---------|---------|---------|---------|---------|---------|----------|
| 58 | . | 0.88479 | 1.34008 | 13.3084 | 8.4183 | 3.51138 | . | 2.87998 | 1.97421 |
| 59 | . | 0.93406 | 1.33594 | 13.3904 | 8.4790 | 3.37763 | . | 2.97779 | 1.98881 |
| 60 | . | 0.97108 | 1.29885 | 14.0063 | 8.4369 | 3.22796 | . | 3.20592 | 1.98229 |
| 61 | . | 1.00905 | 1.25655 | 11.5451 | 8.2371 | 3.23035 | . | 2.88159 | 1.89447 |
| 62 | . | 1.01962 | 1.20776 | 12.3132 | 7.9013 | 3.02677 | . | 2.38218 | 1.87421 |
| 63 | . | 1.00790 | 1.18617 | 11.6355 | 7.3990 | 3.07168 | . | 2.47644 | 1.62712 |
| 64 | . | 0.96600 | 1.14203 | 11.8004 | 7.2451 | 2.93478 | . | 2.35199 | 1.61093 |
| 65 | . | 0.96237 | 1.06082 | 11.7656 | 7.4390 | 2.85526 | . | 2.29577 | 1.51698 |
| 66 | . | 0.95467 | 1.05115 | 12.3814 | 7.2122 | 2.80601 | . | 2.51280 | 1.47493 |
| 67 | . | 0.94767 | 1.00916 | 9.1318 | 7.0555 | 2.84292 | . | 2.38079 | 1.36244 |
| 68 | . | 0.93275 | 0.96037 | 8.1385 | 6.6716 | 2.70127 | . | 2.00282 | 1.30478 |
| 69 | . | 0.91396 | 0.94610 | 7.7951 | 6.4259 | 2.58872 | . | 1.81649 | 1.16685 |
| 70 | . | 0.91839 | 1.12984 | 7.9181 | 6.2181 | 2.51913 | . | 1.83918 | 1.35876 |
| 71 | . | 0.98350 | 1.20946 | 8.6636 | 6.2084 | 2.58259 | . | 1.93362 | 1.70181 |
| 72 | . | 0.97496 | 1.16430 | 8.5782 | 5.6316 | 2.42781 | . | 1.90308 | 1.73928 |
| 73 | . | 1.04164 | 1.18280 | 8.7994 | 5.7391 | 2.64125 | . | 2.16880 | 2.07389 |
| 74 | . | 1.14913 | 1.86459 | 11.0417 | 7.9848 | 4.55416 | . | 5.18454 | 3.93584 |
| 75 | . | 1.38019 | 1.91720 | 11.7209 | 8.2809 | 4.80136 | . | 5.46879 | 4.06431 |
| 76 | . | 1.86100 | 1.70193 | 12.1442 | 7.8946 | 4.87623 | . | 7.26455 | 4.00018 |
| 77 | . | 2.56881 | 1.38277 | 14.1267 | 7.3571 | 5.04254 | . | 5.83721 | 3.80477 |
| 78 | . | 2.66356 | 1.72005 | 13.0963 | 7.1860 | 4.84812 | . | 4.70084 | 3.45584 |
| 79 | . | 3.30460 | 1.78656 | 13.2878 | 9.3858 | 6.42342 | . | 5.55958 | 4.13029 |
| 80 | . | 3.66980 | 1.79151 | 14.3145 | 12.8073 | 8.66037 | . | 8.07756 | 5.16369 |
| 81 | . | 3.96808 | 1.86502 | 15.5942 | 13.1254 | 9.23427 | . | 7.66598 | 6.44783 |
| 82 | . | 4.21808 | 1.88244 | 17.3341 | 11.4677 | 8.59463 | . | 7.17829 | 5.85805 |
| 83 | . | 4.34961 | 1.80363 | 14.8086 | 9.8513 | 7.53126 | . | 7.13403 | 6.10398 |
| 84 | . | 4.12499 | 1.86140 | 16.6182 | 8.4652 | 6.74389 | . | 6.47277 | 5.34336 |
| 85 | . | 3.86147 | 1.87969 | 16.2361 | 7.9269 | 5.92719 | . | 6.86249 | 4.52399 |

Table E-22B. Non-Manufacturing Prices, 1958-1985

SIC=CONSTRUCTION

| YEAR | POIL87 | PNATGS87 | PCOAL87 | PELEC87 | PMGAS87 | PDIST87 | PASPH87 | PLPG87 | PRESID87 |
|------|---------|----------|---------|---------|---------|---------|---------|---------|----------|
| 58 | 15.1275 | 2.87427 | . | 27.8196 | 7.8080 | 3.7807 | 2.44549 | 3.48463 | 1.48049 |
| 59 | 15.0070 | 2.90421 | . | 27.2474 | 7.6073 | 3.5988 | 2.46477 | 3.52347 | 1.53060 |
| 60 | 14.7923 | 2.96067 | . | 27.7299 | 7.5854 | 3.2641 | 2.44564 | 3.57867 | 1.50760 |
| 61 | 15.0276 | 2.96519 | . | 26.1879 | 7.4193 | 3.2766 | 2.42777 | 3.26871 | 1.51753 |
| 62 | 15.6018 | 2.89760 | . | 25.8216 | 7.1901 | 3.2582 | 2.37637 | 2.87197 | 1.45695 |
| 63 | 14.9207 | 2.85685 | . | 24.5671 | 7.0478 | 3.2420 | 2.36349 | 3.03802 | 1.40874 |
| 64 | 14.9826 | 2.72499 | . | 23.1714 | 6.8587 | 3.0777 | 2.49726 | 3.02845 | 1.39346 |
| 65 | 15.2896 | 2.66555 | . | 21.9811 | 6.8975 | 3.0253 | 2.26157 | 3.07557 | 1.42930 |
| 66 | 15.8293 | 2.57453 | . | 20.5356 | 6.8571 | 2.9687 | 2.14706 | 3.24890 | 1.39431 |
| 67 | 15.5219 | 2.49731 | . | 19.7322 | 6.8733 | 3.0027 | 2.03302 | 3.39252 | 1.43256 |
| 68 | 14.8211 | 2.34800 | . | 18.4328 | 6.6629 | 2.9447 | 1.93378 | 2.58627 | 1.40881 |
| 69 | 13.9006 | 2.23900 | . | 17.2554 | 6.4883 | 2.8842 | 1.79529 | 2.28786 | 1.30977 |
| 70 | 13.4371 | 2.23261 | . | 16.7356 | 6.4179 | 2.8986 | 1.74087 | 3.33820 | 1.27070 |
| 71 | 13.9988 | 2.34216 | . | 17.6515 | 6.5610 | 3.0919 | 2.04557 | 3.51801 | 1.70294 |
| 72 | 13.4839 | 2.27297 | . | 16.7690 | 5.9265 | 2.8037 | 1.86347 | 3.20671 | 1.65659 |
| 73 | 12.0887 | 2.25421 | . | 16.3217 | 6.0246 | 3.2822 | 1.74780 | 3.23610 | 1.85477 |
| 74 | 15.1619 | 2.41333 | . | 18.6031 | 6.7819 | 5.1331 | 3.28236 | 5.24319 | 4.12217 |
| 75 | 14.3603 | 2.74014 | . | 19.2409 | 7.8630 | 5.0155 | 3.46347 | 4.90521 | 3.79912 |
| 76 | 12.7351 | 3.13640 | . | 19.3893 | 7.8341 | 5.0291 | 3.39086 | 5.04048 | 3.51976 |
| 77 | 11.8336 | 3.56720 | . | 20.1330 | 7.8631 | 5.3296 | 3.33284 | 5.49998 | 3.87335 |
| 78 | 12.0450 | 3.64311 | . | 19.9608 | 7.6282 | 5.1497 | 2.77690 | 5.40906 | 3.37649 |
| 79 | 15.0062 | 4.08191 | . | 20.1048 | 9.4635 | 7.1354 | 3.39797 | 5.73661 | 4.53067 |
| 80 | 19.3213 | 4.61704 | . | 21.3374 | 12.3756 | 9.4154 | 4.62889 | 6.77247 | 5.69951 |
| 81 | 22.1943 | 4.94833 | . | 22.2877 | 12.5059 | 10.2859 | 5.42673 | 7.06238 | 6.45583 |
| 82 | 20.1402 | 5.60753 | . | 23.1179 | 12.3720 | 9.2380 | 5.01359 | 7.06752 | 5.56361 |
| 83 | 19.1764 | 6.22763 | . | 22.8814 | 11.4845 | 7.5692 | 4.96052 | 7.35843 | 5.16675 |
| 84 | 19.0071 | 5.92251 | . | 22.9958 | 10.7704 | 7.1745 | 5.49839 | 6.96599 | 5.17548 |
| 85 | 18.3298 | 5.64773 | . | 22.5712 | 10.1543 | 6.6550 | 5.24512 | 7.10115 | 4.43873 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

Sources: Consumption, 1958-1985: [97]

Consumption, 1988: [99]

Output and Deflator: U.S. Department of Commerce and DRI, Inc.

Notes: All dollar values are expressed in constant 1987 dollars. Prices are per million Btu and quantities are trillion Btus. Output is billion dollars.

The mnemonics are as follows: NATGAS and NATGS--Natural Gas;

COAL--Coal; ELEC--Electricity; OIL--All Oil Products;

OUTPUT--Value of Output; DOL87 -Deflator for 1987 Dollars.

SIC=FOOD

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 171.828 | 151.902 | 295.667 | 250.559 | 53.391 |
| 59 | 178.297 | 145.648 | 311.604 | 243.253 | 57.762 |
| 60 | 183.761 | 149.388 | 316.156 | 240.428 | 60.956 |
| 61 | 187.761 | 134.336 | 316.291 | 226.954 | 63.317 |
| 62 | 192.475 | 134.048 | 338.979 | 217.326 | 65.016 |
| 63 | 197.419 | 131.767 | 345.946 | 208.311 | 68.247 |
| 64 | 205.617 | 147.716 | 387.690 | 220.185 | 77.695 |
| 65 | 205.665 | 140.824 | 390.580 | 215.394 | 75.696 |
| 66 | 209.827 | 140.354 | 418.515 | 209.965 | 80.435 |
| 67 | 224.283 | 138.899 | 452.915 | 211.206 | 83.257 |
| 68 | 227.615 | 160.203 | 542.923 | 219.182 | 91.777 |
| 69 | 231.617 | 156.925 | 508.301 | 176.249 | 99.324 |
| 70 | 233.717 | 154.932 | 558.146 | 149.321 | 115.108 |
| 71 | 240.021 | 155.129 | 586.322 | 135.308 | 115.279 |
| 72 | 254.265 | 194.276 | 543.972 | 130.916 | 117.299 |
| 73 | 250.845 | 198.139 | 520.249 | 125.641 | 121.628 |
| 74 | 260.037 | 154.459 | 527.554 | 88.887 | 125.818 |
| 75 | 257.792 | 179.413 | 501.474 | 93.101 | 130.677 |
| 76 | 274.466 | 198.236 | 484.744 | 94.199 | 133.280 |
| 77 | 277.138 | 216.734 | 466.095 | 99.834 | 136.638 |
| 78 | 284.726 | 230.512 | 464.735 | 111.369 | 138.262 |
| 79 | 283.657 | 161.002 | 506.265 | 112.540 | 134.895 |
| 80 | 287.826 | 125.077 | 527.164 | 122.602 | 140.296 |
| 81 | 291.994 | 102.466 | 512.771 | 116.723 | 141.352 |
| 82 | 302.254 | 104.311 | 526.540 | 118.381 | 156.771 |
| 83 | 303.857 | 100.408 | 554.659 | 121.138 | 149.786 |
| 84 | 306.316 | 88.009 | 553.173 | 128.893 | 154.723 |
| 85 | 316.148 | 76.961 | 480.964 | 121.100 | 154.884 |
| 86 | 318.500 | 0.0 | 0.0 | 0.0 | 0.0 |
| 87 | 333.677 | 0.0 | 0.0 | 0.0 | 0.0 |
| 88 | 341.586 | 89.1 | 488.1 | 149.6 | 171.3 |
| 89 | 340.410 | 0.0 | 0.0 | 0.0 | 0.0 |
| 90 | 347.143 | 0.0 | 0.0 | 0.0 | 0.0 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=TOBACCO

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|--------|---------|---------|--------|
| 58 | 28.5615 | 2.1466 | 1.2262 | 5.9576 | 1.1157 |
| 59 | 29.4756 | 2.2781 | 1.4311 | 6.5861 | 1.1908 |
| 60 | 32.4867 | 2.5203 | 1.5589 | 7.2039 | 1.2522 |
| 61 | 29.1509 | 2.2434 | 1.5418 | 6.9939 | 1.2863 |
| 62 | 32.3128 | 2.3850 | 1.7161 | 7.3750 | 1.3580 |
| 63 | 32.3548 | 2.7490 | 2.1321 | 8.5025 | 1.7435 |
| 64 | 33.0059 | 2.9286 | 2.3230 | 8.6889 | 1.9176 |
| 65 | 32.5611 | 3.1251 | 2.6851 | 9.6957 | 2.0916 |
| 66 | 31.9486 | 3.1076 | 2.9441 | 9.6608 | 2.3031 |
| 67 | 32.1733 | 3.0580 | 3.2615 | 9.9614 | 2.5147 |
| 68 | 31.5166 | 3.6445 | 3.6847 | 8.4880 | 2.5761 |
| 69 | 30.3692 | 4.5151 | 3.9434 | 7.0196 | 2.7057 |
| 70 | 30.8464 | 5.2169 | 4.8237 | 6.3329 | 2.9036 |
| 71 | 31.3664 | 5.0656 | 4.7199 | 5.0587 | 3.0981 |
| 72 | 32.4133 | 6.6132 | 4.1284 | 4.1031 | 3.2960 |
| 73 | 33.9001 | 7.3256 | 4.1582 | 3.7593 | 3.8692 |
| 74 | 34.3462 | 6.8959 | 5.6341 | 3.7573 | 3.5076 |
| 75 | 34.6435 | 7.8625 | 3.5827 | 3.7017 | 3.6543 |
| 76 | 35.6843 | 8.7214 | 3.1750 | 4.0473 | 3.8351 |
| 77 | 33.0080 | 9.7534 | 3.1714 | 6.2120 | 4.2650 |
| 78 | 32.8593 | 7.5200 | 2.3080 | 7.9621 | 4.3189 |
| 79 | 32.2646 | 5.0474 | 3.5352 | 7.6447 | 4.5083 |
| 80 | 33.3054 | 3.2772 | 4.2578 | 9.6439 | 4.7526 |
| 81 | 32.8593 | 3.1017 | 4.1601 | 9.4559 | 4.8519 |
| 82 | 34.7922 | 2.9974 | 3.8226 | 9.6429 | 4.9798 |
| 83 | 30.7777 | 3.1927 | 4.1406 | 11.7259 | 5.2033 |
| 84 | 30.6290 | 2.7580 | 3.8002 | 11.7268 | 4.8734 |
| 85 | 30.4804 | 2.9785 | 3.7022 | 12.7723 | 5.0713 |
| 86 | 28.9935 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 87 | 29.1422 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 88 | 30.7777 | 2.0000 | 2.1000 | 16.9000 | 2.9000 |
| 89 | 29.5883 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 90 | 30.4804 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=TEXTILE MILLS

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 27.9009 | 65.852 | 38.866 | 87.5482 | 39.387 |
| 59 | 30.8180 | 63.372 | 42.594 | 83.2451 | 43.359 |
| 60 | 30.0388 | 65.173 | 44.122 | 80.0699 | 43.744 |
| 61 | 30.8008 | 59.417 | 45.954 | 75.5246 | 44.257 |
| 62 | 32.9319 | 61.878 | 51.301 | 72.4159 | 46.756 |
| 63 | 33.8331 | 62.988 | 57.619 | 73.1662 | 48.917 |
| 64 | 35.8797 | 69.447 | 66.000 | 75.8023 | 53.513 |
| 65 | 37.7765 | 68.656 | 71.797 | 77.1532 | 56.558 |
| 66 | 40.4285 | 68.916 | 80.744 | 76.1743 | 61.268 |
| 67 | 40.5411 | 70.459 | 95.327 | 80.3793 | 67.304 |
| 68 | 42.2793 | 75.696 | 100.432 | 69.3696 | 73.448 |
| 69 | 42.4589 | 83.759 | 102.523 | 59.7630 | 77.607 |
| 70 | 41.8188 | 80.170 | 110.809 | 49.3247 | 79.248 |
| 71 | 43.0861 | 86.989 | 124.639 | 46.1105 | 82.432 |
| 72 | 45.2852 | 106.284 | 117.586 | 36.3150 | 91.791 |
| 73 | 43.7786 | 100.055 | 109.555 | 30.0336 | 96.121 |
| 74 | 41.3051 | 71.131 | 110.551 | 25.8341 | 88.686 |
| 75 | 40.3376 | 83.206 | 96.044 | 27.2393 | 87.929 |
| 76 | 46.0386 | 100.766 | 85.721 | 31.9033 | 92.971 |
| 77 | 50.3404 | 112.692 | 82.453 | 34.6803 | 91.873 |
| 78 | 50.4469 | 109.494 | 85.307 | 30.3244 | 91.791 |
| 79 | 51.3069 | 74.997 | 108.668 | 31.4901 | 90.491 |
| 80 | 49.4791 | 52.972 | 112.598 | 33.4150 | 87.794 |
| 81 | 49.1566 | 45.414 | 111.245 | 36.7008 | 87.277 |
| 82 | 44.7460 | 38.423 | 97.461 | 34.5946 | 81.502 |
| 83 | 50.2316 | 38.471 | 111.972 | 42.0542 | 89.159 |
| 84 | 50.9840 | 32.513 | 112.304 | 43.9094 | 90.760 |
| 85 | 48.1868 | 27.987 | 99.353 | 40.1512 | 87.092 |
| 86 | 50.0153 | 0.000 | 0.000 | 0.0000 | 0.000 |
| 87 | 55.8235 | 0.000 | 0.000 | 0.0000 | 0.000 |
| 88 | 55.5005 | 28.400 | 92.900 | 38.7000 | 101.500 |
| 89 | 55.8228 | 0.000 | 0.000 | 0.0000 | 0.000 |
| 90 | 54.6400 | 0.000 | 0.000 | 0.0000 | 0.000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=APPAREL & OTHER

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 35.6720 | 10.7751 | 7.6347 | 13.4148 | 7.2965 |
| 59 | 38.5674 | 9.9445 | 8.3153 | 12.2417 | 7.7567 |
| 60 | 38.9655 | 9.7842 | 8.6877 | 10.9323 | 7.9955 |
| 61 | 39.3384 | 7.8517 | 8.4152 | 8.5015 | 8.1312 |
| 62 | 41.8996 | 8.4399 | 10.5115 | 7.5417 | 9.1090 |
| 63 | 44.6091 | 8.3152 | 11.3307 | 7.1133 | 9.8174 |
| 64 | 46.1517 | 9.8676 | 14.0002 | 7.8972 | 11.3363 |
| 65 | 48.8970 | 10.1762 | 15.7052 | 8.3547 | 11.3449 |
| 66 | 51.2732 | 11.3307 | 19.0763 | 9.1083 | 12.5243 |
| 67 | 53.6111 | 13.9490 | 24.5518 | 10.8618 | 14.1482 |
| 68 | 55.7218 | 17.3486 | 32.1074 | 12.1956 | 17.7555 |
| 69 | 57.9511 | 15.5199 | 28.3947 | 9.1708 | 18.6192 |
| 70 | 55.4421 | 14.6783 | 28.6873 | 7.5714 | 20.6730 |
| 71 | 58.5742 | 14.6903 | 29.0120 | 6.7252 | 22.2797 |
| 72 | 64.8665 | 16.7597 | 27.4109 | 4.9195 | 24.2992 |
| 73 | 66.7991 | 15.6225 | 24.8448 | 3.2882 | 25.0772 |
| 74 | 62.1602 | 12.4526 | 25.7935 | 1.9645 | 24.8392 |
| 75 | 61.0561 | 12.0509 | 23.2079 | 2.1080 | 26.0354 |
| 76 | 64.6676 | 13.9670 | 20.2812 | 2.0623 | 25.7064 |
| 77 | 71.3467 | 15.8817 | 21.8967 | 2.5091 | 24.9200 |
| 78 | 73.9034 | 15.4107 | 25.5735 | 2.3149 | 23.0091 |
| 79 | 68.5582 | 10.2104 | 24.5615 | 2.0627 | 20.2720 |
| 80 | 69.6568 | 8.4767 | 24.4435 | 2.7885 | 20.6412 |
| 81 | 69.7535 | 10.2823 | 24.1603 | 3.3585 | 20.6655 |
| 82 | 69.3229 | 7.3766 | 19.5872 | 2.8575 | 21.6088 |
| 83 | 72.5839 | 7.6706 | 20.3757 | 2.9638 | 21.3209 |
| 84 | 74.1332 | 6.7524 | 20.3444 | 2.5927 | 24.0453 |
| 85 | 72.1786 | 5.8358 | 17.0990 | 2.2309 | 20.9077 |
| 86 | 73.0181 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 87 | 84.7468 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 88 | 79.6005 | 5.1000 | 21.7000 | 2.9000 | 22.7000 |
| 89 | 77.2262 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 90 | 74.9542 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=LUMBER & WOOD

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 30.7633 | 48.1945 | 17.777 | 17.9534 | 12.5147 |
| 59 | 33.2236 | 48.9260 | 22.895 | 18.6026 | 14.0989 |
| 60 | 32.4591 | 39.5498 | 21.976 | 14.6096 | 14.5108 |
| 61 | 32.5008 | 30.8894 | 23.038 | 11.5903 | 15.4888 |
| 62 | 33.7677 | 26.3917 | 26.965 | 8.7991 | 16.5301 |
| 63 | 36.4296 | 38.9492 | 46.663 | 11.9362 | 17.1470 |
| 64 | 38.2695 | 45.8226 | 58.770 | 12.6414 | 19.9337 |
| 65 | 39.2432 | 49.5655 | 69.374 | 13.3968 | 19.9938 |
| 66 | 39.1652 | 53.1392 | 80.065 | 13.3531 | 22.8024 |
| 67 | 41.2446 | 59.4374 | 96.487 | 14.4964 | 25.9018 |
| 68 | 41.7938 | 69.6936 | 122.006 | 14.7411 | 30.6646 |
| 69 | 40.7397 | 68.5783 | 121.556 | 12.3782 | 32.7557 |
| 70 | 42.6614 | 58.2375 | 114.959 | 9.3042 | 35.7653 |
| 71 | 42.0645 | 51.8058 | 109.416 | 7.7854 | 39.6885 |
| 72 | 49.9018 | 63.3435 | 100.709 | 7.6262 | 46.3369 |
| 73 | 49.5615 | 66.7308 | 97.546 | 7.9329 | 46.5930 |
| 74 | 47.5708 | 52.9662 | 93.003 | 7.4680 | 50.7672 |
| 75 | 45.1118 | 56.4044 | 88.991 | 3.8294 | 49.4449 |
| 76 | 49.2211 | 57.9518 | 81.382 | 4.1631 | 53.1662 |
| 77 | 55.3211 | 53.2785 | 67.252 | 4.1615 | 55.1220 |
| 78 | 56.1408 | 59.5536 | 72.101 | 3.6131 | 56.8729 |
| 79 | 54.5014 | 49.8665 | 79.912 | 3.1163 | 54.8158 |
| 80 | 54.1501 | 44.2338 | 62.625 | 2.7712 | 50.0445 |
| 81 | 51.8082 | 40.0833 | 49.692 | 2.3613 | 49.5689 |
| 82 | 49.7005 | 30.4752 | 37.068 | 1.7359 | 49.8739 |
| 83 | 53.6817 | 32.8984 | 38.849 | 2.0818 | 52.7045 |
| 84 | 56.8434 | 34.2220 | 36.256 | 2.1277 | 57.0902 |
| 85 | 57.0885 | 33.6109 | 29.572 | 1.9334 | 57.2043 |
| 86 | 61.1869 | 0.0 | 0.0 | 0.0 | 0.0 |
| 87 | 71.8317 | 0.0 | 0.0 | 0.0 | 0.0 |
| 88 | 71.1291 | 28.5 | 35.1 | 2.3 | 56.1 |
| 89 | 68.9043 | 0.0 | 0.0 | 0.0 | 0.0 |
| 90 | 67.4882 | 0.0 | 0.0 | 0.0 | 0.0 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=FURNITURE & FIXTURES

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 13.7162 | 4.6066 | 7.2165 | 15.3195 | 4.4220 |
| 59 | 14.9030 | 4.0702 | 6.7211 | 13.5100 | 4.9474 |
| 60 | 14.6784 | 4.3583 | 6.7631 | 12.6502 | 5.0122 |
| 61 | 14.3290 | 4.1060 | 6.6361 | 11.1605 | 4.9986 |
| 62 | 15.5705 | 5.0781 | 8.2242 | 11.5219 | 5.3160 |
| 63 | 16.3812 | 4.7813 | 7.1562 | 12.5314 | 5.5787 |
| 64 | 17.5395 | 5.3314 | 6.7829 | 14.9921 | 6.3805 |
| 65 | 19.0497 | 5.6072 | 6.7313 | 18.1537 | 6.7797 |
| 66 | 20.4152 | 6.1316 | 6.7467 | 20.9864 | 7.1413 |
| 67 | 20.4431 | 6.6675 | 6.8621 | 24.6387 | 7.8443 |
| 68 | 21.3465 | 6.2218 | 9.0617 | 18.9851 | 9.0316 |
| 69 | 22.4744 | 6.5854 | 11.8219 | 14.5948 | 10.8434 |
| 70 | 21.1279 | 7.4205 | 17.4280 | 11.6934 | 11.5668 |
| 71 | 21.9636 | 7.6583 | 23.9831 | 8.5590 | 11.4781 |
| 72 | 26.3340 | 12.1826 | 26.1966 | 7.5180 | 11.8261 |
| 73 | 27.8197 | 10.5125 | 23.7421 | 4.5776 | 12.9759 |
| 74 | 25.0724 | 9.1489 | 27.5332 | 3.4157 | 13.6959 |
| 75 | 21.7550 | 9.2679 | 20.7796 | 3.1158 | 13.2557 |
| 76 | 24.0431 | 9.3976 | 20.3811 | 2.4866 | 13.5423 |
| 77 | 27.2607 | 10.5042 | 21.6884 | 3.7825 | 14.2964 |
| 78 | 29.6677 | 10.7214 | 23.6545 | 3.3655 | 14.5174 |
| 79 | 29.2166 | 9.5529 | 23.0160 | 2.9297 | 13.7599 |
| 80 | 28.6575 | 7.5427 | 21.6080 | 2.9027 | 13.4828 |
| 81 | 28.7737 | 6.2924 | 19.9374 | 3.1919 | 14.1366 |
| 82 | 27.3097 | 5.3323 | 19.5669 | 2.6643 | 13.6467 |
| 83 | 29.0224 | 4.7866 | 21.1612 | 2.3780 | 14.5611 |
| 84 | 31.7889 | 4.4619 | 22.9489 | 2.5822 | 15.5140 |
| 85 | 31.9132 | 3.7566 | 22.0248 | 2.2669 | 15.2690 |
| 86 | 32.9370 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 87 | 36.6247 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 88 | 36.7463 | 5.8000 | 22.7000 | 2.9000 | 19.3000 |
| 89 | 37.3218 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 90 | 36.8680 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=PAPER

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 40.478 | 162.359 | 219.762 | 356.677 | 42.439 |
| 59 | 44.747 | 165.426 | 233.677 | 356.423 | 47.888 |
| 60 | 44.925 | 183.178 | 236.683 | 364.801 | 50.924 |
| 61 | 46.759 | 176.742 | 242.459 | 366.907 | 53.303 |
| 62 | 49.250 | 194.010 | 269.310 | 376.074 | 57.629 |
| 63 | 52.239 | 206.175 | 286.354 | 361.801 | 63.037 |
| 64 | 54.700 | 232.429 | 303.778 | 354.762 | 69.291 |
| 65 | 58.400 | 258.205 | 339.186 | 370.190 | 73.270 |
| 66 | 62.634 | 273.244 | 373.104 | 361.385 | 82.455 |
| 67 | 63.004 | 273.202 | 399.285 | 346.858 | 88.228 |
| 68 | 66.817 | 314.368 | 423.991 | 321.439 | 99.341 |
| 69 | 70.965 | 385.758 | 428.889 | 289.017 | 107.496 |
| 70 | 69.175 | 370.768 | 456.209 | 246.758 | 112.870 |
| 71 | 69.661 | 413.046 | 506.301 | 245.553 | 119.114 |
| 72 | 74.782 | 552.935 | 432.224 | 215.092 | 125.528 |
| 73 | 81.681 | 548.340 | 379.555 | 197.680 | 129.984 |
| 74 | 83.770 | 476.254 | 447.243 | 226.671 | 139.449 |
| 75 | 73.399 | 468.177 | 391.229 | 202.395 | 133.482 |
| 76 | 81.317 | 521.891 | 371.879 | 225.035 | 148.280 |
| 77 | 85.196 | 521.977 | 363.792 | 241.248 | 152.040 |
| 78 | 88.828 | 527.736 | 356.205 | 212.696 | 155.625 |
| 79 | 89.558 | 446.800 | 428.534 | 213.834 | 157.502 |
| 80 | 88.168 | 385.318 | 432.824 | 230.854 | 169.523 |
| 81 | 89.294 | 295.603 | 451.671 | 249.421 | 178.102 |
| 82 | 87.461 | 262.680 | 419.327 | 269.340 | 172.442 |
| 83 | 93.352 | 246.110 | 452.770 | 334.271 | 176.792 |
| 84 | 98.759 | 208.670 | 461.134 | 376.558 | 182.902 |
| 85 | 96.382 | 184.811 | 420.024 | 380.566 | 179.642 |
| 86 | 100.433 | 0.000 | 0.000 | 0.000 | 0.000 |
| 87 | 105.844 | 0.000 | 0.000 | 0.000 | 0.000 |
| 88 | 109.448 | 194.800 | 428.300 | 309.000 | 189.400 |
| 89 | 109.599 | 0.000 | 0.000 | 0.000 | 0.000 |
| 90 | 110.047 | 0.000 | 0.000 | 0.000 | 0.000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=PRINTING

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|--------|---------|
| 58 | 32.2723 | 9.3231 | 15.0242 | 4.1582 | 10.2498 |
| 59 | 34.4821 | 8.1611 | 14.2498 | 3.4740 | 11.2597 |
| 60 | 35.5699 | 8.8202 | 15.2730 | 3.4410 | 11.8705 |
| 61 | 36.3297 | 8.4010 | 15.8913 | 3.1745 | 12.7712 |
| 62 | 37.7051 | 9.2458 | 18.3266 | 3.1288 | 13.6959 |
| 63 | 37.8533 | 9.4378 | 18.8360 | 2.6941 | 13.9859 |
| 64 | 39.9517 | 10.4953 | 20.4057 | 2.4108 | 15.8147 |
| 65 | 41.9285 | 11.3040 | 22.6277 | 2.2176 | 16.3129 |
| 66 | 44.2969 | 12.0259 | 24.9670 | 1.8414 | 17.2512 |
| 67 | 46.4596 | 13.1985 | 28.8762 | 1.5636 | 19.8478 |
| 68 | 47.2847 | 13.5653 | 34.4047 | 1.3812 | 23.5566 |
| 69 | 49.2536 | 14.5217 | 40.1501 | 1.1868 | 25.7540 |
| 70 | 47.1820 | 13.2763 | 46.5750 | 0.9474 | 31.0460 |
| 71 | 47.4329 | 11.0250 | 46.4517 | 0.6898 | 30.9505 |
| 72 | 50.9241 | 12.6705 | 42.9888 | 1.2233 | 31.2541 |
| 73 | 52.9805 | 11.9831 | 39.1984 | 1.8668 | 33.3935 |
| 74 | 51.6499 | 8.2285 | 33.5995 | 2.1282 | 30.6843 |
| 75 | 48.9888 | 10.5016 | 34.9056 | 1.9973 | 33.8985 |
| 76 | 51.1661 | 8.5941 | 27.9601 | 1.8517 | 34.5399 |
| 77 | 56.9721 | 10.8352 | 33.8625 | 1.7946 | 36.0105 |
| 78 | 60.6009 | 10.9040 | 34.3426 | 1.5142 | 35.2999 |
| 79 | 61.3267 | 10.7101 | 39.1211 | 1.4392 | 32.3741 |
| 80 | 62.0525 | 9.0515 | 39.9787 | 0.9079 | 32.9439 |
| 81 | 63.6249 | 8.5820 | 40.7663 | 0.5732 | 35.1514 |
| 82 | 66.7699 | 8.9536 | 42.8204 | 0.7105 | 36.2972 |
| 83 | 69.5520 | 8.0254 | 46.1929 | 0.9289 | 36.4644 |
| 84 | 73.6646 | 6.8667 | 52.0422 | 1.3046 | 42.9001 |
| 85 | 76.2048 | 4.5614 | 45.2660 | 1.2797 | 42.2501 |
| 86 | 78.1401 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 87 | 85.7606 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 88 | 86.9702 | 4.4000 | 48.5000 | 0.0000 | 58.2000 |
| 89 | 86.4864 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 90 | 87.9379 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 78 | 52.0214 | 0 | 0 | 0 | 0 |
| 79 | 53.5913 | 0 | 0 | 0 | 0 |
| 80 | 48.6674 | 0 | 0 | 0 | 0 |
| 81 | 49.2383 | 0 | 0 | 0 | 0 |
| 82 | 44.2431 | 0 | 0 | 0 | 0 |
| 83 | 47.3830 | 0 | 0 | 0 | 0 |
| 84 | 48.6674 | 0 | 0 | 0 | 0 |
| 85 | 45.5990 | 0 | 0 | 0 | 0 |
| 86 | 46.6694 | 0 | 0 | 0 | 0 |
| 87 | 55.6607 | 0 | 0 | 0 | 0 |
| 88 | 59.0146 | 0 | . | 0 | 0 |
| 89 | 58.7292 | 0 | 0 | 0 | 0 |
| 90 | 60.4418 | 0 | 0 | 0 | 0 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=BULK CHEMICALS

| YEAR | OUTPUT | QOIL | QNGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 41.398 | 72.991 | 544.47 | 430.527 | 259.144 |
| 59 | 47.582 | 78.318 | 627.02 | 468.508 | 268.377 |
| 60 | 48.080 | 85.875 | 644.89 | 488.381 | 272.321 |
| 61 | 49.306 | 81.879 | 648.66 | 486.200 | 280.226 |
| 62 | 53.469 | 87.979 | 723.84 | 508.898 | 277.176 |
| 63 | 57.706 | 92.586 | 815.10 | 512.820 | 288.719 |
| 64 | 63.169 | 99.306 | 895.70 | 509.629 | 264.029 |
| 65 | 68.365 | 100.883 | 1006.82 | 534.089 | 287.044 |
| 66 | 73.107 | 100.812 | 1138.49 | 524.257 | 285.986 |
| 67 | 73.897 | 97.674 | 1229.36 | 500.565 | 298.208 |
| 68 | 78.554 | 113.069 | 1271.66 | 480.050 | 294.069 |
| 69 | 83.093 | 142.459 | 1293.89 | 464.231 | 302.558 |
| 70 | 80.604 | 148.631 | 1338.01 | 420.463 | 277.793 |
| 71 | 81.843 | 166.434 | 1357.02 | 431.807 | 307.884 |
| 72 | 98.617 | 231.928 | 1369.07 | 363.185 | 353.264 |
| 73 | 111.465 | 253.434 | 1432.54 | 330.763 | 378.393 |
| 74 | 115.046 | 247.335 | 1736.57 | 334.424 | 380.014 |
| 75 | 94.162 | 239.004 | 1515.07 | 295.949 | 384.129 |
| 76 | 107.061 | 291.767 | 1598.64 | 286.327 | 439.741 |
| 77 | 119.188 | 353.913 | 1444.02 | 312.010 | 451.922 |
| 78 | 124.531 | 350.729 | 1382.50 | 277.076 | 442.717 |
| 79 | 128.580 | 245.156 | 1483.67 | 298.699 | 440.068 |
| 80 | 118.984 | 160.434 | 1455.70 | 296.903 | 403.629 |
| 81 | 120.596 | 123.195 | 1399.60 | 329.349 | 399.010 |
| 82 | 107.331 | 112.071 | 1226.45 | 302.697 | 360.821 |
| 83 | 117.065 | 104.678 | 1245.26 | 342.118 | 384.733 |
| 84 | 122.405 | 91.675 | 1321.74 | 359.182 | 413.997 |
| 85 | 115.260 | 79.333 | 1101.01 | 317.709 | 388.113 |
| 86 | 117.058 | 0.000 | 0.00 | 0.000 | 0.000 |
| 87 | 135.943 | 0.000 | 0.00 | 0.000 | 0.000 |
| 88 | 142.411 | 112.600 | 1439.00 | 263.800 | 394.100 |
| 89 | 142.231 | 0.000 | 0.00 | 0.000 | 0.000 |
| 90 | 144.887 | 0.000 | 0.00 | 0.000 | 0.000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=OTHER CHEMICALS

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 27.576 | 37.8796 | 48.539 | 58.1655 | 9.3900 |
| 59 | 30.998 | 35.8647 | 50.165 | 52.8097 | 10.4989 |
| 60 | 31.067 | 37.8451 | 50.996 | 50.0066 | 10.8264 |
| 61 | 31.992 | 35.9967 | 53.362 | 47.0972 | 11.4098 |
| 62 | 34.295 | 36.7406 | 57.376 | 45.1935 | 12.1536 |
| 63 | 37.156 | 37.4775 | 59.203 | 43.9460 | 13.4400 |
| 64 | 39.421 | 41.0862 | 62.488 | 47.0354 | 14.2998 |
| 65 | 42.862 | 46.5062 | 72.244 | 57.0397 | 15.5827 |
| 66 | 46.141 | 44.9279 | 73.074 | 57.3847 | 16.7871 |
| 67 | 48.457 | 45.1735 | 78.724 | 63.8537 | 18.0905 |
| 68 | 51.986 | 46.8967 | 85.782 | 57.9596 | 20.4176 |
| 69 | 54.412 | 68.4887 | 119.444 | 67.8986 | 23.1575 |
| 70 | 56.361 | 51.5224 | 102.245 | 45.4272 | 25.1671 |
| 71 | 57.339 | 55.3534 | 115.444 | 44.6088 | 26.4944 |
| 72 | 63.552 | 69.1267 | 109.179 | 42.0245 | 29.9370 |
| 73 | 67.017 | 66.0635 | 100.029 | 38.5132 | 31.0358 |
| 74 | 67.570 | 59.4779 | 116.929 | 36.6531 | 30.1998 |
| 75 | 65.004 | 57.1824 | 103.079 | 36.4044 | 30.2953 |
| 76 | 71.233 | 60.9729 | 103.749 | 39.3619 | 31.9808 |
| 77 | 74.649 | 71.6689 | 98.314 | 42.4351 | 33.2262 |
| 78 | 79.036 | 73.8884 | 99.536 | 40.2356 | 35.5346 |
| 79 | 81.125 | 57.5152 | 124.130 | 31.0504 | 38.3110 |
| 80 | 78.075 | 43.8064 | 118.636 | 31.0846 | 35.3442 |
| 81 | 79.698 | 37.0713 | 123.241 | 32.3088 | 37.7715 |
| 82 | 80.731 | 32.9311 | 125.210 | 32.1186 | 37.5995 |
| 83 | 81.948 | 31.5049 | 141.402 | 34.5686 | 37.6092 |
| 84 | 85.531 | 26.3222 | 140.829 | 35.7468 | 40.2374 |
| 85 | 85.676 | 22.9310 | 128.080 | 33.5830 | 39.5747 |
| 86 | 90.574 | 0.0 | 0.0 | 0.0 | 0.0 |
| 87 | 97.650 | 0.0 | 0.0 | 0.0 | 0.0 |
| 88 | 101.210 | 10.8 | 72.9 | 25.6 | 21.6 |
| 89 | 101.797 | 0.0 | 0.0 | 0.0 | 0.0 |
| 90 | 104.697 | 0.0 | 0.0 | 0.0 | 0.0 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=SIC 29, COAL & MISC

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|--------|--------|
| 58 | 5.5963 | 13.4733 | 12.8236 | 4.1338 | 1.2965 |
| 59 | 5.9271 | 16.1308 | 16.9382 | 4.7286 | 1.6378 |
| 60 | 6.5518 | 18.6480 | 19.3915 | 4.9759 | 1.9449 |
| 61 | 6.0346 | 16.4220 | 18.6919 | 4.2658 | 2.1018 |
| 62 | 6.4247 | 15.4767 | 18.5216 | 3.6006 | 1.7230 |
| 63 | 7.2985 | 17.7127 | 21.4366 | 3.8805 | 1.9210 |
| 64 | 7.6821 | 18.8696 | 21.9381 | 3.6664 | 2.1940 |
| 65 | 7.7659 | 19.2329 | 22.5649 | 3.6101 | 2.3270 |
| 66 | 7.9568 | 19.7473 | 23.9221 | 3.3800 | 2.3543 |
| 67 | 8.4925 | 23.1251 | 29.5122 | 3.8080 | 2.4293 |
| 68 | 8.8124 | 19.1169 | 27.3581 | 2.2852 | 2.8695 |
| 69 | 9.0783 | 18.7534 | 27.9788 | 1.4393 | 3.0878 |
| 70 | 9.7808 | 18.5169 | 33.0874 | 0.8976 | 3.4598 |
| 71 | 9.9284 | 18.5605 | 37.5944 | 0.4088 | 3.6372 |
| 72 | 10.9101 | 23.1248 | 39.5528 | 0.2294 | 3.7600 |
| 73 | 11.5258 | 22.9016 | 39.7127 | 0.2813 | 3.9887 |
| 74 | 11.0370 | 17.3200 | 44.1506 | 0.2627 | 4.8314 |
| 75 | 10.5311 | 20.0935 | 43.7087 | 0.4261 | 4.9680 |
| 76 | 11.8894 | 20.6173 | 36.3583 | 0.1852 | 4.8996 |
| 77 | 13.3446 | 27.3642 | 39.0800 | 0.4417 | 5.7015 |
| 78 | 14.8881 | 33.4646 | 43.1471 | 0.5976 | 5.9154 |
| 79 | 15.0150 | 25.2291 | 47.7901 | 0.5111 | 5.7462 |
| 80 | 13.3617 | 20.4287 | 47.2774 | 0.5056 | 5.8103 |
| 81 | 13.3788 | 18.1480 | 41.3786 | 0.3045 | 5.3989 |
| 82 | 13.6695 | 25.0616 | 37.6527 | 0.2114 | 6.3941 |
| 83 | 13.7450 | 30.1836 | 33.6203 | 0.1834 | 6.2170 |
| 84 | 13.8548 | 29.2031 | 27.1544 | 0.1001 | 5.6297 |
| 85 | 14.6771 | 33.6229 | 21.0568 | 0.0399 | 5.9335 |
| 86 | 14.9893 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 87 | 16.6468 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 88 | 16.2335 | 3.8000 | 4.5000 | 1.8000 | 2.1000 |
| 89 | 16.0397 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 90 | 15.9257 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=RUBBER & MISC

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 16.9488 | 21.2678 | 20.623 | 65.0229 | 17.354 |
| 59 | 20.3130 | 21.5195 | 22.665 | 63.1111 | 19.643 |
| 60 | 20.6650 | 23.2547 | 24.100 | 62.4835 | 20.598 |
| 61 | 20.9052 | 21.9780 | 24.875 | 58.7289 | 21.404 |
| 62 | 23.2367 | 24.9176 | 29.427 | 60.1173 | 24.021 |
| 63 | 24.5082 | 24.6960 | 31.247 | 57.4166 | 25.259 |
| 64 | 26.6332 | 26.7227 | 34.401 | 57.0803 | 27.549 |
| 65 | 29.5901 | 29.2689 | 41.010 | 63.0737 | 31.247 |
| 66 | 32.1093 | 28.8975 | 44.597 | 60.1090 | 38.389 |
| 67 | 33.4824 | 29.5922 | 51.751 | 62.1640 | 36.475 |
| 68 | 38.7804 | 30.5804 | 56.935 | 55.3479 | 43.295 |
| 69 | 43.0644 | 35.4330 | 64.688 | 49.8445 | 47.608 |
| 70 | 42.1248 | 35.7081 | 76.943 | 41.1637 | 50.733 |
| 71 | 46.4666 | 39.3990 | 91.607 | 37.6084 | 55.056 |
| 72 | 48.6545 | 61.4843 | 98.788 | 42.3304 | 61.727 |
| 73 | 54.6428 | 63.3141 | 89.245 | 40.3289 | 68.227 |
| 74 | 52.9477 | 50.0817 | 91.848 | 35.3920 | 64.740 |
| 75 | 45.5273 | 55.7432 | 79.126 | 27.4032 | 64.122 |
| 76 | 49.6261 | 64.0211 | 76.506 | 25.6329 | 67.387 |
| 77 | 59.3543 | 77.2621 | 83.173 | 28.6858 | 76.965 |
| 78 | 62.4027 | 68.0194 | 86.974 | 22.2128 | 78.375 |
| 79 | 60.5247 | 49.7873 | 94.440 | 20.5321 | 77.925 |
| 80 | 54.7879 | 33.2143 | 89.903 | 20.5650 | 73.907 |
| 81 | 58.5519 | 24.1453 | 95.245 | 19.1741 | 78.180 |
| 82 | 59.4400 | 23.1073 | 93.784 | 14.8524 | 105.079 |
| 83 | 63.0725 | 22.7199 | 103.417 | 13.0115 | 109.320 |
| 84 | 71.9617 | 20.7347 | 109.363 | 10.6580 | 100.827 |
| 85 | 73.1435 | 18.1597 | 98.817 | 7.1929 | 102.710 |
| 86 | 74.5963 | 0.0000 | 0.000 | 0.0000 | 0.000 |
| 87 | 84.7828 | 0.0000 | 0.000 | 0.0000 | 0.000 |
| 88 | 87.1580 | 22.2000 | 110.400 | 8.3000 | 106.800 |
| 89 | 87.6952 | 0.0000 | 0.000 | 0.0000 | 0.000 |
| 90 | 89.2908 | 0.0000 | 0.000 | 0.0000 | 0.000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=LEATHER

| YEAR | OUTPUT | QOIL | QNGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|--------|
| 58 | 14.4596 | 9.5041 | 4.8844 | 15.5870 | 2.6341 |
| 59 | 14.8872 | 8.7862 | 5.0110 | 13.2687 | 2.6989 |
| 60 | 14.4472 | 9.7302 | 5.6301 | 12.7740 | 2.7057 |
| 61 | 14.2231 | 8.8463 | 5.8678 | 11.1109 | 2.8388 |
| 62 | 14.4139 | 9.1670 | 6.5399 | 9.9326 | 3.0231 |
| 63 | 14.3713 | 8.5749 | 6.3686 | 8.6508 | 3.1766 |
| 64 | 14.9945 | 9.3603 | 6.8057 | 8.3625 | 3.2892 |
| 65 | 15.3241 | 10.4295 | 7.8781 | 8.9737 | 3.5928 |
| 66 | 15.4872 | 10.8778 | 8.7675 | 8.7275 | 4.0603 |
| 67 | 15.8542 | 10.6962 | 9.3691 | 8.3978 | 4.5005 |
| 68 | 16.4358 | 12.6646 | 10.8343 | 8.9401 | 4.9304 |
| 69 | 15.6101 | 11.4455 | 9.0649 | 6.2622 | 5.1146 |
| 70 | 14.6560 | 12.9621 | 11.0830 | 5.2109 | 6.1178 |
| 71 | 14.1438 | 11.2058 | 9.4883 | 3.9856 | 5.0601 |
| 72 | 14.1274 | 11.5544 | 8.0587 | 3.3895 | 5.4217 |
| 73 | 13.8939 | 9.3901 | 6.4919 | 2.5573 | 5.4217 |
| 74 | 13.6604 | 7.4598 | 6.5888 | 1.6028 | 5.1249 |
| 75 | 13.1934 | 8.7012 | 6.9607 | 1.5179 | 5.2102 |
| 76 | 13.4269 | 8.7165 | 6.4523 | 1.3491 | 5.1522 |
| 77 | 13.6604 | 8.9150 | 6.6498 | 1.4357 | 4.8349 |
| 78 | 13.5436 | 8.2258 | 6.4025 | 1.4324 | 4.7484 |
| 79 | 11.7923 | 6.4695 | 7.4277 | 1.1977 | 4.3373 |
| 80 | 12.3761 | 6.1921 | 6.8478 | 1.1187 | 4.6437 |
| 81 | 12.4928 | 5.3356 | 6.4375 | 1.0094 | 4.5055 |
| 82 | 11.4420 | 5.3669 | 6.1497 | 0.8518 | 4.0804 |
| 83 | 11.3253 | 5.8584 | 6.9291 | 0.8005 | 4.0920 |
| 84 | 10.3912 | 4.8981 | 5.8589 | 0.5807 | 4.0426 |
| 85 | 9.4572 | 4.6778 | 5.0014 | 0.4062 | 3.5495 |
| 86 | 8.2896 | 0.0 | 0.0 | 0.0 | 0.0 |
| 87 | 9.5739 | 0.0 | 0.0 | 0.0 | 0.0 |
| 88 | 9.3404 | 4.5 | 5.2 | 1.3 | 4.7 |
| 89 | 9.1069 | 0.0 | 0.0 | 0.0 | 0.0 |
| 90 | 8.6399 | 0.0 | 0.0 | 0.0 | 0.0 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=GLASS

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 7.6439 | 13.7537 | 133.399 | 16.0004 | 9.0009 |
| 59 | 9.0441 | 14.3365 | 151.606 | 16.5739 | 10.8059 |
| 60 | 9.1041 | 15.2502 | 157.696 | 16.4626 | 11.2597 |
| 61 | 9.0119 | 13.4100 | 154.679 | 14.8310 | 11.4132 |
| 62 | 9.4551 | 13.1343 | 160.967 | 13.3097 | 12.4983 |
| 63 | 10.1587 | 13.2695 | 167.074 | 11.8887 | 12.9623 |
| 64 | 10.6604 | 14.0718 | 175.379 | 10.9992 | 13.8767 |
| 65 | 11.5030 | 13.7386 | 182.487 | 10.4951 | 15.1665 |
| 66 | 12.3238 | 13.8387 | 199.405 | 10.0392 | 16.4528 |
| 67 | 12.3030 | 12.4679 | 198.647 | 9.0283 | 16.6166 |
| 68 | 12.5695 | 12.2575 | 207.941 | 8.2369 | 16.6166 |
| 69 | 13.2028 | 13.2254 | 218.636 | 7.3731 | 19.9842 |
| 70 | 12.8236 | 12.2516 | 226.355 | 5.6846 | 21.4036 |
| 71 | 13.4119 | 12.7587 | 240.335 | 4.4200 | 22.2600 |
| 72 | 14.6426 | 27.5614 | 235.776 | 3.7718 | 24.4028 |
| 73 | 15.8628 | 36.7186 | 224.460 | 2.6085 | 26.4057 |
| 74 | 14.8644 | 33.6322 | 220.138 | 0.7357 | 26.6752 |
| 75 | 14.4207 | 37.7946 | 201.245 | 0.4794 | 27.0608 |
| 76 | 15.6409 | 40.5573 | 212.415 | 0.2645 | 29.2922 |
| 77 | 16.0846 | 46.6721 | 203.073 | 0.4141 | 30.4762 |
| 78 | 16.9721 | 40.5628 | 214.440 | 0.2327 | 32.3823 |
| 79 | 16.3065 | 20.4635 | 223.781 | 0.2300 | 32.5095 |
| 80 | 15.5300 | 10.3781 | 217.979 | 0.3498 | 31.4777 |
| 81 | 15.5300 | 8.3076 | 212.616 | 0.2075 | 32.3553 |
| 82 | 14.0879 | 8.1903 | 203.013 | 0.2083 | 31.1857 |
| 83 | 14.3098 | 8.8612 | 223.471 | 0.2723 | 30.6070 |
| 84 | 14.4207 | 7.9003 | 205.523 | 0.2941 | 31.1952 |
| 85 | 14.5316 | 7.0484 | 177.069 | 0.2753 | 30.4251 |
| 86 | 14.6426 | 0.0000 | 0.000 | 0.0000 | 0.0000 |
| 87 | 16.1956 | 0.0000 | 0.000 | 0.0000 | 0.0000 |
| 88 | 16.4174 | 20.8000 | 213.800 | 8.4000 | 34.8000 |
| 89 | 16.4174 | 0.0000 | 0.000 | 0.0000 | 0.0000 |
| 90 | 16.4174 | 0.0000 | 0.000 | 0.0000 | 0.0000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=CEMENT

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|--------|---------|---------|---------|---------|
| 58 | 3.8479 | 27.2118 | 164.048 | 194.120 | 17.1182 |
| 59 | 4.2135 | 25.1487 | 183.022 | 201.203 | 18.2714 |
| 60 | 3.8863 | 24.0349 | 179.100 | 196.932 | 18.5034 |
| 61 | 3.8608 | 19.4952 | 174.522 | 187.174 | 19.0323 |
| 62 | 3.9532 | 19.1014 | 193.462 | 189.490 | 20.1753 |
| 63 | 4.1590 | 19.5349 | 203.062 | 203.640 | 22.2464 |
| 64 | 4.2704 | 20.2797 | 204.915 | 211.019 | 23.5737 |
| 65 | 4.4345 | 19.8706 | 207.704 | 225.735 | 24.8771 |
| 66 | 4.4496 | 18.8276 | 210.156 | 225.932 | 26.0542 |
| 67 | 4.3408 | 16.8192 | 205.611 | 223.362 | 25.5731 |
| 68 | 4.4718 | 23.5718 | 213.289 | 213.079 | 26.7946 |
| 69 | 4.5692 | 34.2076 | 213.892 | 199.252 | 28.3266 |
| 70 | 4.1489 | 36.3475 | 216.802 | 173.930 | 28.4119 |
| 71 | 4.3349 | 42.3494 | 223.542 | 175.778 | 29.0534 |
| 72 | 4.7952 | 63.9824 | 218.041 | 183.618 | 32.3426 |
| 73 | 4.9992 | 60.7655 | 199.547 | 179.498 | 33.4617 |
| 74 | 4.8972 | 45.3548 | 234.377 | 191.910 | 33.7961 |
| 75 | 4.1830 | 33.3328 | 165.827 | 192.275 | 30.0053 |
| 76 | 4.2851 | 36.6177 | 134.167 | 228.527 | 31.1859 |
| 77 | 4.5911 | 42.1052 | 95.347 | 292.103 | 33.5163 |
| 78 | 4.8972 | 39.4306 | 85.716 | 292.446 | 35.5305 |
| 79 | 4.9992 | 22.0879 | 76.000 | 311.967 | 35.2381 |
| 80 | 4.3871 | 14.3828 | 59.958 | 285.571 | 31.5197 |
| 81 | 3.9790 | 6.3644 | 47.821 | 299.145 | 30.4460 |
| 82 | 3.5709 | 5.2710 | 32.363 | 248.414 | 28.7318 |
| 83 | 3.6729 | 5.0819 | 26.129 | 257.254 | 28.3554 |
| 84 | 3.8770 | 5.3652 | 22.660 | 290.111 | 31.1519 |
| 85 | 3.9790 | 5.5093 | 15.973 | 276.160 | 32.0878 |
| 86 | 3.8770 | 0.0000 | 0.000 | 0.000 | 0.0000 |
| 87 | 4.0810 | 0.0000 | 0.000 | 0.000 | 0.0000 |
| 88 | 3.9790 | 13.3000 | 75.900 | 251.500 | 47.5000 |
| 89 | 3.8770 | 0.0000 | 0.000 | 0.000 | 0.0000 |
| 90 | 4.0810 | 0.0000 | 0.000 | 0.000 | 0.0000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=OTHER SCG

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 22.8571 | 55.4602 | 191.893 | 92.525 | 15.3507 |
| 59 | 25.9602 | 64.2639 | 237.123 | 106.946 | 19.0289 |
| 60 | 25.4566 | 64.7750 | 232.266 | 103.108 | 19.7011 |
| 61 | 25.4476 | 58.2971 | 224.646 | 94.616 | 19.8614 |
| 62 | 26.6776 | 55.3213 | 224.020 | 84.030 | 20.7349 |
| 63 | 28.7033 | 57.2605 | 242.494 | 86.063 | 20.7451 |
| 64 | 30.4245 | 63.0870 | 271.098 | 91.484 | 23.2530 |
| 65 | 32.5188 | 64.4298 | 296.923 | 98.066 | 24.1094 |
| 66 | 33.8582 | 63.6912 | 317.230 | 96.154 | 35.9389 |
| 67 | 32.1637 | 57.1137 | 311.017 | 88.467 | 25.0750 |
| 68 | 34.0224 | 62.8304 | 317.224 | 88.747 | 33.4242 |
| 69 | 34.3467 | 73.1227 | 321.672 | 88.856 | 32.6736 |
| 70 | 32.4984 | 71.3309 | 304.336 | 75.920 | 33.1308 |
| 71 | 33.3295 | 78.9162 | 316.528 | 80.352 | 33.8950 |
| 72 | 37.1902 | 88.6558 | 311.489 | 79.6912 | 36.1026 |
| 73 | 39.9329 | 81.4760 | 298.674 | 78.6886 | 37.8905 |
| 74 | 38.2873 | 63.6032 | 302.672 | 72.2553 | 38.5252 |
| 75 | 34.1185 | 69.0768 | 260.001 | 70.9446 | 37.7847 |
| 76 | 35.7641 | 78.0094 | 281.342 | 70.0209 | 39.2758 |
| 77 | 38.7261 | 88.4222 | 265.273 | 77.8851 | 41.5243 |
| 78 | 42.2367 | 95.3336 | 278.408 | 81.4247 | 43.8449 |
| 79 | 42.2367 | 61.9162 | 311.941 | 88.0889 | 44.8002 |
| 80 | 37.5194 | 45.1313 | 280.104 | 71.7393 | 41.0866 |
| 81 | 35.6544 | 45.1226 | 242.165 | 81.6561 | 39.9300 |
| 82 | 31.1564 | 38.6526 | 196.737 | 56.6377 | 35.1869 |
| 83 | 32.6923 | 43.0227 | 233.430 | 64.8605 | 36.3948 |
| 84 | 35.4350 | 40.1130 | 232.625 | 68.3527 | 40.1603 |
| 85 | 35.8738 | 38.7131 | 206.637 | 69.4566 | 49.9585 |
| 86 | 36.8611 | 0.0000 | 0.000 | 0.0000 | 0.0000 |
| 87 | 41.4688 | 0.0000 | 0.000 | 0.0000 | 0.0000 |
| 88 | 42.6755 | 19.3000 | 175.800 | 26.3000 | 32.9000 |
| 89 | 42.1270 | 0.0000 | 0.000 | 0.0000 | 0.0000 |
| 90 | 41.1397 | 0.0000 | 0.000 | 0.0000 | 0.0000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC-IRON AND STEEL

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 55.6846 | 244.091 | 248.249 | 216.114 | 85.548 |
| 59 | 63.6661 | 249.319 | 330.022 | 232.258 | 98.257 |
| 60 | 64.8321 | 269.216 | 381.746 | 251.247 | 104.443 |
| 61 | 61.4771 | 226.915 | 414.073 | 234.096 | 109.815 |
| 62 | 64.6327 | 231.105 | 480.287 | 244.714 | 113.587 |
| 63 | 67.5621 | 221.836 | 507.601 | 226.376 | 122.172 |
| 64 | 76.9795 | 249.500 | 553.044 | 236.676 | 141.380 |
| 65 | 84.2911 | 255.620 | 611.436 | 244.299 | 151.701 |
| 66 | 85.8217 | 241.403 | 657.332 | 223.534 | 164.983 |
| 67 | 79.6297 | 212.649 | 660.879 | 199.415 | 174.520 |
| 68 | 82.9687 | 219.320 | 691.755 | 214.134 | 185.159 |
| 69 | 84.7317 | 240.162 | 811.162 | 224.477 | 202.594 |
| 70 | 75.5996 | 212.348 | 760.115 | 202.061 | 197.509 |
| 71 | 71.5569 | 187.878 | 757.229 | 196.067 | 201.245 |
| 72 | 75.3951 | 264.015 | 746.693 | 171.045 | 210.717 |
| 73 | 91.4611 | 300.148 | 779.053 | 151.450 | 244.539 |
| 74 | 96.6065 | 290.420 | 794.320 | 133.798 | 251.146 |
| 75 | 70.4597 | 245.774 | 645.108 | 121.970 | 215.423 |
| 76 | 75.5001 | 278.861 | 653.840 | 119.919 | 229.651 |
| 77 | 74.8700 | 291.927 | 618.360 | 124.533 | 245.913 |
| 78 | 79.2803 | 314.940 | 716.832 | 96.580 | 262.273 |
| 79 | 81.8005 | 234.556 | 789.914 | 97.472 | 272.462 |
| 80 | 68.9896 | 119.932 | 669.025 | 98.077 | 238.251 |
| 81 | 71.2998 | 106.343 | 719.085 | 100.503 | 247.928 |
| 82 | 44.1030 | 71.376 | 518.001 | 68.536 | 178.749 |
| 83 | 42.8429 | 67.379 | 571.878 | 85.636 | 168.245 |
| 84 | 47.3582 | 56.386 | 580.982 | 83.643 | 204.389 |
| 85 | 43.5779 | 45.018 | 495.859 | 76.755 | 195.726 |
| 86 | 40.6377 | 0.0 | 0.0 | 0.0 | 0.0 |
| 87 | 46.6231 | 0.0 | 0.0 | 0.0 | 0.0 |
| 88 | 54.6037 | 50.6 | 539.2 | 51.2 | 229.5 |
| 89 | 52.6085 | 0.0 | 0.0 | 0.0 | 0.0 |
| 90 | 51.4534 | 0.0 | 0.0 | 0.0 | 0.0 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=PRIMARY ALUMINUM

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 4.1170 | 4.0070 | 122.046 | 15.6600 | 79.572 |
| 59 | 4.7687 | 3.6959 | 122.641 | 17.1770 | 103.524 |
| 60 | 4.6648 | 3.8848 | 124.886 | 20.3740 | 108.591 |
| 61 | 4.8793 | 3.3944 | 119.181 | 21.5769 | 102.275 |
| 62 | 5.3279 | 3.4272 | 132.802 | 33.2247 | 113.375 |
| 63 | 5.8091 | 3.6933 | 143.631 | 24.1728 | 122.451 |
| 64 | 6.2702 | 4.0063 | 153.435 | 24.0325 | 126.248 |
| 65 | 6.7581 | 3.9316 | 163.798 | 24.1877 | 138.211 |
| 66 | 7.5638 | 3.9450 | 177.538 | 22.9035 | 141.927 |
| 67 | 7.7811 | 3.1276 | 174.637 | 19.7967 | 159.628 |
| 68 | 7.9908 | 3.7164 | 183.139 | 21.3958 | 155.165 |
| 69 | 8.0613 | 4.4849 | 187.970 | 22.7002 | 179.544 |
| 70 | 7.4538 | 4.2479 | 181.206 | 20.5195 | 170.519 |
| 71 | 7.0579 | 4.1530 | 168.568 | 19.4940 | 158.233 |
| 72 | 9.4075 | 8.1362 | 155.331 | 12.4621 | 175.767 |
| 73 | 11.3317 | 10.5614 | 177.444 | 10.2293 | 217.424 |
| 74 | 9.7282 | 8.1354 | 184.490 | 7.7248 | 255.915 |
| 75 | 8.5523 | 7.8861 | 103.591 | 6.2316 | 211.092 |
| 76 | 10.2627 | 7.5153 | 91.459 | 5.2641 | 225.016 |
| 77 | 11.5455 | 8.0731 | 93.301 | 10.6571 | 244.686 |
| 78 | 12.1870 | 7.3847 | 81.802 | 10.7166 | 250.741 |
| 79 | 12.2939 | 5.4104 | 125.132 | 11.9423 | 261.194 |
| 80 | 11.8663 | 4.9441 | 128.425 | 9.3180 | 262.099 |
| 81 | 10.1558 | 2.9471 | 69.498 | 5.6441 | 256.629 |
| 82 | 7.5901 | 2.8059 | 49.360 | 4.1676 | 177.243 |
| 83 | 8.6592 | 2.4695 | 36.793 | 2.8135 | 180.391 |
| 84 | 9.3006 | 3.1926 | 43.802 | 1.3956 | 216.388 |
| 85 | 6.5211 | 2.2776 | 26.836 | 0.0000 | 189.797 |
| 86 | 5.8797 | 0.0000 | 0.000 | 0.0000 | 0.000 |
| 87 | 6.8418 | 0.0000 | 0.000 | 0.0000 | 0.000 |
| 88 | 8.1246 | 1.5000 | 99.100 | 1.8000 | 246.200 |
| 89 | 8.4454 | 0.0000 | 0.000 | 0.0000 | 0.000 |
| 90 | 9.0868 | 0.0000 | 0.000 | 0.0000 | 0.000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=OTHER PRIMARY METALS

| YEAR | OUTPUT | QOIL | QNGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 36.0478 | 38.4680 | 113.443 | 48.8165 | 27.5057 |
| 59 | 40.4543 | 38.7948 | 124.375 | 46.9365 | 29.5844 |
| 60 | 40.3419 | 41.6172 | 129.154 | 44.6510 | 29.4267 |
| 61 | 41.5916 | 38.7441 | 131.030 | 39.5663 | 32.0680 |
| 62 | 45.4424 | 42.0359 | 147.899 | 35.9394 | 35.1433 |
| 63 | 48.2586 | 42.3733 | 156.402 | 36.0934 | 33.3480 |
| 64 | 51.5051 | 44.9468 | 167.478 | 36.8991 | 38.0428 |
| 65 | 56.4632 | 43.6253 | 176.692 | 38.2676 | 47.1034 |
| 66 | 63.7898 | 43.8659 | 195.835 | 39.1053 | 58.7570 |
| 67 | 58.2932 | 39.0158 | 198.554 | 37.3885 | 51.5908 |
| 68 | 61.5637 | 40.4286 | 211.317 | 36.9279 | 57.6001 |
| 69 | 65.8560 | 45.0492 | 222.376 | 36.1844 | 58.3213 |
| 70 | 59.6293 | 40.5688 | 226.625 | 31.4162 | 70.0777 |
| 71 | 59.6104 | 39.3521 | 230.418 | 30.5936 | 62.8771 |
| 72 | 67.3548 | 55.7708 | 239.260 | 29.7523 | 65.2651 |
| 73 | 77.5018 | 58.3968 | 235.975 | 27.6299 | 69.9607 |
| 74 | 74.2613 | 45.4628 | 245.397 | 22.8336 | 71.2234 |
| 75 | 59.9831 | 44.0311 | 218.814 | 18.0733 | 63.4847 |
| 76 | 66.3257 | 46.4287 | 233.733 | 18.4102 | 72.6157 |
| 77 | 70.1764 | 49.4303 | 241.451 | 14.0536 | 71.1216 |
| 78 | 74.5799 | 48.8317 | 248.876 | 11.6208 | 73.4941 |
| 79 | 73.1441 | 38.2469 | 229.191 | 14.0649 | 76.9191 |
| 80 | 68.6065 | 23.2192 | 217.966 | 12.6749 | 75.5420 |
| 81 | 67.2781 | 23.4724 | 217.527 | 17.1082 | 76.4510 |
| 82 | 52.9927 | 19.3361 | 195.724 | 15.9295 | 64.4220 |
| 83 | 57.6921 | 18.8037 | 216.201 | 17.2978 | 61.8295 |
| 84 | 60.9514 | 15.2658 | 204.008 | 16.5186 | 69.2469 |
| 85 | 57.2044 | 11.2744 | 174.079 | 13.6880 | 68.5085 |
| 86 | 56.6669 | 0.0000 | 0.000 | 0.0000 | 0.0000 |
| 87 | 60.3142 | 0.0000 | 0.000 | 0.0000 | 0.0000 |
| 88 | 62.4986 | 7.0000 | 104.700 | 5.3000 | 33.4000 |
| 89 | 59.8264 | 0.0000 | 0.000 | 0.0000 | 0.0000 |
| 90 | 57.9490 | 0.0000 | 0.000 | 0.0000 | 0.0000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=FABRICATED METALS

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 73.080 | 74.3173 | 98.838 | 35.6481 | 26.734 |
| 59 | 81.212 | 71.3058 | 106.083 | 34.6718 | 30.388 |
| 60 | 80.514 | 69.5773 | 106.063 | 33.2267 | 31.127 |
| 61 | 78.914 | 60.5336 | 105.855 | 30.6923 | 31.695 |
| 62 | 85.972 | 66.9473 | 127.863 | 32.6816 | 34.378 |
| 63 | 88.690 | 60.3846 | 122.432 | 29.4122 | 35.993 |
| 64 | 94.587 | 65.5569 | 139.319 | 32.2453 | 39.815 |
| 65 | 104.392 | 63.9676 | 152.750 | 34.8545 | 43.675 |
| 66 | 112.504 | 67.7121 | 184.119 | 37.8718 | 50.057 |
| 67 | 114.608 | 68.8590 | 213.021 | 43.6054 | 62.182 |
| 68 | 119.501 | 72.9257 | 234.013 | 39.5819 | 71.168 |
| 69 | 122.401 | 74.6872 | 236.921 | 35.1763 | 76.872 |
| 70 | 115.024 | 69.1911 | 251.072 | 28.3523 | 81.025 |
| 71 | 115.113 | 62.0155 | 248.821 | 23.9162 | 78.263 |
| 72 | 125.904 | 73.9605 | 251.830 | 20.4364 | 82.196 |
| 73 | 138.886 | 68.8646 | 241.624 | 17.0425 | 87.389 |
| 74 | 133.766 | 48.9955 | 234.718 | 12.4403 | 85.450 |
| 75 | 118.531 | 51.8466 | 216.292 | 10.8893 | 83.231 |
| 76 | 128.185 | 53.9303 | 217.795 | 10.5778 | 87.807 |
| 77 | 136.471 | 59.7798 | 209.359 | 12.6469 | 89.829 |
| 78 | 142.876 | 58.4287 | 222.584 | 10.8538 | 89.970 |
| 79 | 146.384 | 46.8905 | 223.605 | 11.3499 | 89.721 |
| 80 | 138.691 | 36.0169 | 215.594 | 10.2058 | 86.391 |
| 81 | 137.229 | 29.7704 | 212.290 | 10.1511 | 87.139 |
| 82 | 126.713 | 28.7263 | 208.991 | 11.3090 | 87.113 |
| 83 | 128.509 | 26.9276 | 210.705 | 11.6883 | 84.733 |
| 84 | 139.003 | 24.5876 | 213.460 | 10.9389 | 103.635 |
| 85 | 138.486 | 20.4560 | 186.952 | 9.6285 | 95.448 |
| 86 | 136.800 | 0.0000 | 0.000 | 0.0000 | 0.000 |
| 87 | 141.264 | 0.0000 | 0.000 | 0.0000 | 0.000 |
| 88 | 146.185 | 15.8000 | 203.300 | 9.2000 | 105.600 |
| 89 | 143.491 | 0.0000 | 0.000 | 0.0000 | 0.000 |
| 90 | 141.867 | 0.0000 | 0.000 | 0.0000 | 0.000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=INDUSTRIAL MACHINERY

| YEAR | OUTPUT | QOIL | QNGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 82.137 | 44.6764 | 53.622 | 62.1049 | 26.129 |
| 59 | 91.384 | 44.0135 | 59.493 | 60.2403 | 31.022 |
| 60 | 89.850 | 46.1721 | 62.824 | 58.7950 | 31.776 |
| 61 | 88.124 | 43.8707 | 65.587 | 55.6785 | 31.868 |
| 62 | 96.438 | 49.3200 | 77.556 | 56.8395 | 35.386 |
| 63 | 102.173 | 48.2891 | 81.399 | 53.2147 | 37.737 |
| 64 | 113.878 | 54.2300 | 94.713 | 56.4525 | 42.992 |
| 65 | 125.484 | 52.1317 | 102.209 | 54.1258 | 47.366 |
| 66 | 142.241 | 53.2856 | 117.559 | 53.0716 | 53.978 |
| 67 | 144.777 | 53.3082 | 139.738 | 54.6489 | 57.008 |
| 68 | 143.957 | 50.5257 | 147.704 | 48.8437 | 62.948 |
| 69 | 150.793 | 51.8599 | 153.640 | 43.5318 | 69.953 |
| 70 | 144.523 | 50.4237 | 177.559 | 38.6704 | 74.116 |
| 71 | 138.087 | 46.8967 | 184.316 | 36.3054 | 76.538 |
| 72 | 156.416 | 57.0053 | 183.652 | 33.6146 | 82.093 |
| 73 | 182.198 | 55.4861 | 180.767 | 30.0997 | 90.531 |
| 74 | 190.226 | 41.9279 | 184.174 | 23.0166 | 88.539 |
| 75 | 170.441 | 47.3470 | 159.685 | 22.0770 | 93.281 |
| 76 | 174.344 | 46.9197 | 156.802 | 17.9087 | 95.417 |
| 77 | 190.502 | 50.9114 | 149.159 | 21.2864 | 97.045 |
| 78 | 207.436 | 49.3107 | 160.642 | 22.9285 | 102.687 |
| 79 | 220.888 | 40.6439 | 165.061 | 24.5807 | 103.633 |
| 80 | 215.035 | 31.7473 | 158.487 | 24.2493 | 104.330 |
| 81 | 219.638 | 29.4517 | 152.124 | 21.1479 | 107.714 |
| 82 | 194.516 | 28.9261 | 149.802 | 19.3994 | 104.283 |
| 83 | 188.381 | 26.5842 | 139.218 | 18.9469 | 100.232 |
| 84 | 234.849 | 24.2130 | 138.809 | 19.4847 | 103.043 |
| 85 | 247.634 | 21.2188 | 118.719 | 16.5775 | 103.515 |
| 86 | 256.463 | 0.0 | 0.0 | 0.0 | 0.0 |
| 87 | 279.400 | 0.0 | 0.0 | 0.0 | 0.0 |
| 88 | 319.185 | 14.8 | 126.9 | 17.7 | 114.2 |
| 89 | 342.724 | 0.0 | 0.0 | 0.0 | 0.0 |
| 90 | 348.649 | 0.0 | 0.0 | 0.0 | 0.0 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=ELECTRONIC

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 45.373 | 31.2606 | 38.844 | 43.6486 | 25.510 |
| 59 | 52.959 | 30.0135 | 43.708 | 42.8218 | 31.954 |
| 60 | 55.674 | 32.0766 | 46.530 | 41.8868 | 32.853 |
| 61 | 58.366 | 29.3666 | 46.886 | 37.3255 | 33.266 |
| 62 | 65.947 | 32.6969 | 54.303 | 36.4030 | 38.974 |
| 63 | 68.491 | 32.5012 | 59.012 | 36.6301 | 41.575 |
| 64 | 71.163 | 33.2038 | 62.917 | 36.7393 | 44.599 |
| 65 | 81.005 | 34.4461 | 71.805 | 39.8401 | 52.286 |
| 66 | 92.002 | 35.4326 | 83.060 | 41.4935 | 61.277 |
| 67 | 94.948 | 35.2079 | 95.555 | 44.0821 | 63.731 |
| 68 | 99.931 | 36.0285 | 103.035 | 39.6025 | 70.420 |
| 69 | 104.631 | 40.5546 | 112.286 | 34.5931 | 77.030 |
| 70 | 100.426 | 37.9919 | 119.002 | 25.9548 | 79.555 |
| 71 | 98.299 | 37.8643 | 124.748 | 20.2349 | 78.786 |
| 72 | 109.717 | 44.0142 | 122.294 | 21.2288 | 84.118 |
| 73 | 123.581 | 40.4358 | 115.403 | 21.8140 | 88.765 |
| 74 | 119.148 | 27.6322 | 108.804 | 17.6040 | 84.452 |
| 75 | 104.408 | 30.6520 | 96.803 | 13.0225 | 80.988 |
| 76 | 114.199 | 33.4915 | 98.097 | 14.1259 | 80.901 |
| 77 | 132.569 | 37.5740 | 95.462 | 15.9305 | 85.467 |
| 78 | 145.136 | 38.7943 | 101.560 | 14.2270 | 88.896 |
| 79 | 157.036 | 29.0914 | 105.362 | 15.5974 | 93.216 |
| 80 | 161.208 | 22.4283 | 106.402 | 12.2299 | 92.750 |
| 81 | 165.822 | 19.8297 | 102.147 | 12.3097 | 95.628 |
| 82 | 165.937 | 20.0077 | 105.117 | 11.5092 | 98.537 |
| 83 | 171.755 | 18.8746 | 110.202 | 12.5194 | 99.570 |
| 84 | 199.889 | 16.6433 | 110.539 | 11.7205 | 111.953 |
| 85 | 199.194 | 14.8023 | 101.609 | 10.6108 | 111.991 |
| 86 | 199.861 | 0.0000 | 0.000 | 0.0000 | 0.000 |
| 87 | 215.137 | 0.0000 | 0.000 | 0.0000 | 0.000 |
| 88 | 228.237 | 12.7000 | 84.600 | 7.1000 | 108.700 |
| 89 | 229.939 | 0.0000 | 0.000 | 0.0000 | 0.000 |
| 90 | 231.748 | 0.0000 | 0.000 | 0.0000 | 0.000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=TRANSP EQUIP

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 144.332 | 49.7548 | 63.016 | 95.970 | 47.887 |
| 59 | 162.580 | 46.1677 | 66.217 | 96.281 | 54.305 |
| 60 | 168.045 | 47.7919 | 69.211 | 100.829 | 56.752 |
| 61 | 155.210 | 46.6138 | 72.775 | 97.638 | 55.547 |
| 62 | 178.303 | 45.1678 | 78.888 | 101.020 | 62.644 |
| 63 | 193.054 | 43.0403 | 82.729 | 96.888 | 66.563 |
| 64 | 202.912 | 46.7645 | 95.381 | 102.948 | 68.695 |
| 65 | 234.396 | 45.5764 | 102.941 | 103.709 | 77.078 |
| 66 | 249.566 | 44.2880 | 113.232 | 99.986 | 76.986 |
| 67 | 245.305 | 43.3523 | 124.398 | 96.766 | 85.118 |
| 68 | 274.419 | 46.4300 | 138.624 | 95.284 | 99.057 |
| 69 | 272.374 | 52.3925 | 140.240 | 84.253 | 100.866 |
| 70 | 228.294 | 47.5482 | 145.283 | 71.640 | 94.828 |
| 71 | 249.949 | 48.4465 | 157.649 | 71.327 | 99.452 |
| 72 | 261.760 | 62.2651 | 153.847 | 67.147 | 102.696 |
| 73 | 299.722 | 61.8385 | 144.324 | 59.041 | 110.534 |
| 74 | 265.546 | 46.6886 | 152.802 | 52.286 | 97.158 |
| 75 | 243.706 | 49.0802 | 139.133 | 48.352 | 94.734 |
| 76 | 279.192 | 53.7275 | 152.102 | 51.702 | 101.162 |
| 77 | 305.455 | 57.3700 | 145.555 | 52.694 | 106.030 |
| 78 | 321.130 | 57.6946 | 155.745 | 50.495 | 108.399 |
| 79 | 315.848 | 48.8224 | 151.742 | 50.539 | 109.090 |
| 80 | 262.826 | 39.4991 | 134.116 | 47.598 | 102.251 |
| 81 | 256.419 | 35.6240 | 125.969 | 47.735 | 102.669 |
| 82 | 238.318 | 32.8823 | 117.262 | 42.909 | 98.322 |
| 83 | 270.106 | 32.8389 | 135.193 | 48.311 | 103.939 |
| 84 | 313.099 | 28.1721 | 135.430 | 51.444 | 114.241 |
| 85 | 322.966 | 25.6651 | 123.357 | 47.935 | 117.839 |
| 86 | 329.546 | 0.0000 | 0.000 | 0.000 | 0.000 |
| 87 | 351.494 | 0.0000 | 0.000 | 0.000 | 0.000 |
| 88 | 364.778 | 31.2000 | 138.300 | 36.200 | 127.200 |
| 89 | 365.235 | 0.0000 | 0.000 | 0.000 | 0.000 |
| 90 | 348.995 | 0.0000 | 0.000 | 0.000 | 0.000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=INSTRUMENTS

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 13.0851 | 8.8144 | 7.8396 | 18.6023 | 5.0450 |
| 59 | 14.9082 | 8.6047 | 8.3594 | 17.4182 | 5.8920 |
| 60 | 15.2865 | 8.8540 | 8.5513 | 15.8932 | 6.2594 |
| 61 | 14.9221 | 8.5915 | 9.0808 | 14.7071 | 6.7234 |
| 62 | 14.7764 | 9.8971 | 10.7855 | 15.0976 | 7.1189 |
| 63 | 15.4882 | 8.4672 | 10.0188 | 13.0010 | 6.6366 |
| 64 | 16.3950 | 8.1997 | 10.1293 | 12.1544 | 7.2941 |
| 65 | 18.6663 | 8.5380 | 11.7062 | 13.7957 | 8.1507 |
| 66 | 20.6128 | 7.6222 | 11.9706 | 12.7129 | 8.9804 |
| 67 | 22.1688 | 9.0228 | 16.2645 | 22.9994 | 9.7674 |
| 68 | 23.5847 | 8.8115 | 14.8377 | 15.7958 | 10.9803 |
| 69 | 25.1291 | 12.4203 | 17.4574 | 22.1195 | 12.4098 |
| 70 | 24.1572 | 12.8336 | 20.4661 | 17.3282 | 13.4193 |
| 71 | 24.8107 | 13.9493 | 22.2726 | 20.3116 | 13.7790 |
| 72 | 27.7339 | 18.8197 | 21.3615 | 20.5153 | 14.8854 |
| 73 | 31.6996 | 17.4438 | 18.4818 | 16.3157 | 15.8641 |
| 74 | 34.0626 | 15.3539 | 19.9196 | 15.7911 | 15.4212 |
| 75 | 32.2282 | 15.7516 | 18.9687 | 13.4752 | 16.8727 |
| 76 | 34.9388 | 16.3182 | 21.6295 | 13.9936 | 17.2561 |
| 77 | 38.5257 | 19.0602 | 24.5401 | 6.4605 | 18.7055 |
| 78 | 42.8871 | 17.6195 | 22.7096 | 8.8434 | 19.3385 |
| 79 | 43.9584 | 11.6271 | 23.2701 | 20.3112 | 19.9305 |
| 80 | 44.1421 | 9.6837 | 24.3463 | 21.0968 | 20.4270 |
| 81 | 45.8945 | 8.9874 | 23.9188 | 18.7309 | 20.9073 |
| 82 | 48.3253 | 8.7852 | 24.9629 | 19.8178 | 21.6611 |
| 83 | 47.0845 | 8.6645 | 27.6433 | 22.7669 | 22.5714 |
| 84 | 49.7924 | 7.5629 | 29.1393 | 23.8297 | 24.9304 |
| 85 | 51.1518 | 6.6025 | 26.6744 | 21.0712 | 25.0103 |
| 86 | 51.8641 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 87 | 54.8743 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 88 | 59.2865 | 8.6000 | 32.0000 | 21.5000 | 48.9000 |
| 89 | 60.6405 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 90 | 61.5025 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

Table E-22C. Manufacturing Consumption and Output, 1958-1990

SIC=MISC MFG

| YEAR | OUTPUT | QOIL | QNATGAS | QCOAL | QELEC |
|------|---------|---------|---------|---------|---------|
| 58 | 13.9146 | 14.0793 | 10.6963 | 10.0428 | 4.5141 |
| 59 | 15.1558 | 12.0019 | 9.1356 | 8.5161 | 5.2272 |
| 60 | 15.5411 | 11.8508 | 8.3631 | 7.9713 | 5.3978 |
| 61 | 16.0854 | 9.6144 | 7.1060 | 6.5971 | 5.3159 |
| 62 | 16.9291 | 11.6186 | 8.7877 | 7.4991 | 6.4487 |
| 63 | 17.8649 | 10.1786 | 8.5923 | 5.6601 | 7.8511 |
| 64 | 18.9604 | 9.9971 | 8.9602 | 4.6458 | 8.2742 |
| 65 | 20.7133 | 9.9806 | 10.0584 | 4.2290 | 8.6324 |
| 66 | 21.6439 | 12.8059 | 14.6301 | 4.6917 | 8.2196 |
| 67 | 22.0478 | 12.8052 | 16.5188 | 4.1106 | 8.3970 |
| 68 | 23.2608 | 13.8004 | 17.9511 | 3.9427 | 9.5571 |
| 69 | 24.5258 | 14.6388 | 17.9153 | 3.4088 | 11.2665 |
| 70 | 23.6673 | 15.1920 | 20.7458 | 3.0667 | 11.2290 |
| 71 | 23.9065 | 15.6012 | 22.6634 | 2.8104 | 12.7268 |
| 72 | 28.5771 | 19.5292 | 24.5167 | 2.8543 | 14.2588 |
| 73 | 28.5771 | 16.2684 | 21.4962 | 2.3016 | 14.2725 |
| 74 | 26.5282 | 11.6293 | 22.1265 | 1.6290 | 13.5014 |
| 75 | 24.4793 | 12.0196 | 19.1418 | 0.8788 | 13.0271 |
| 76 | 27.8222 | 12.6700 | 17.7183 | 1.3491 | 12.6996 |
| 77 | 31.7044 | 12.0417 | 17.2893 | 1.3805 | 14.0678 |
| 78 | 32.3514 | 12.1201 | 18.7511 | 1.2618 | 13.6108 |
| 79 | 30.7339 | 9.9763 | 19.5549 | 1.3623 | 12.6029 |
| 80 | 27.9301 | 7.7559 | 19.6104 | 1.6775 | 12.3545 |
| 81 | 28.6849 | 6.0984 | 18.6637 | 1.9596 | 12.3883 |
| 82 | 28.2536 | 4.9170 | 16.4249 | 1.6340 | 12.4627 |
| 83 | 26.8517 | 5.0938 | 17.6174 | 2.0981 | 12.3763 |
| 84 | 27.1752 | 4.3240 | 18.3814 | 1.6749 | 12.6548 |
| 85 | 26.2047 | 3.6127 | 15.6577 | 1.4098 | 11.8939 |
| 86 | 26.6360 | 0.0 | 0.0 | 0.0 | 0.0 |
| 87 | 30.7339 | 0.0 | 0.0 | 0.0 | 0.0 |
| 88 | 31.9201 | 3.3 | 19.6 | 1.8 | 14.3 |
| 89 | 32.2436 | 0.0 | 0.0 | 0.0 | 0.0 |
| 90 | 32.1358 | 0.0 | 0.0 | 0.0 | 0.0 |

Table E-22D. Manufacturing Prices, 1958-1990

Sources:

Prices: [97]

Notes:

All dollar values are expressed in constant 1987 dollars. Prices are per million Btu.

The mnemonics are as follows: NATGAS and NATGS--Natural Gas; COAL--Coal; ELEC--Electricity; OIL--All Oil Products; DOL87--Deflator for 1987 Dollars

SIC=FOOD

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.18053 | 1.39057 | 1.23994 | 16.2434 |
| 59 | 3.90625 | 2.17615 | 1.45144 | 1.23367 | 16.1788 |
| 60 | 3.84615 | 2.14240 | 1.48710 | 1.16515 | 16.8922 |
| 61 | 3.80228 | 2.16616 | 1.53369 | 1.14061 | 14.6831 |
| 62 | 3.71747 | 2.10078 | 1.55297 | 1.09737 | 15.4348 |
| 63 | 3.67647 | 2.05830 | 1.52812 | 1.07445 | 15.5591 |
| 64 | 3.61011 | 1.90852 | 1.46057 | 1.04509 | 15.2681 |
| 65 | 3.52113 | 1.83342 | 1.41899 | 0.97156 | 14.9603 |
| 66 | 3.40136 | 1.80959 | 1.36444 | 0.95192 | 15.1576 |
| 67 | 3.30033 | 1.82586 | 1.31762 | 0.92597 | 12.5342 |
| 68 | 3.14465 | 1.80220 | 1.28322 | 0.90906 | 11.2621 |
| 69 | 2.95858 | 1.73800 | 1.23746 | 0.90752 | 10.4675 |
| 70 | 2.84091 | 1.87293 | 1.22207 | 1.03611 | 10.1329 |
| 71 | 2.84091 | 2.09973 | 1.27207 | 1.11538 | 10.3578 |
| 72 | 2.57732 | 2.26160 | 1.38444 | 0.98720 | 10.1165 |
| 73 | 2.42131 | 2.71380 | 1.54447 | 0.93772 | 10.0526 |
| 74 | 2.22717 | 4.51188 | 1.67305 | 1.38558 | 11.1218 |
| 75 | 2.03252 | 4.39950 | 2.16233 | 1.74866 | 12.3481 |
| 76 | 1.91205 | 4.24397 | 2.63213 | 1.81665 | 12.9487 |
| 77 | 1.78891 | 4.31622 | 3.04743 | 1.79724 | 13.7679 |
| 78 | 1.66113 | 4.01271 | 3.17615 | 1.81663 | 14.5950 |
| 79 | 1.52439 | 4.82072 | 3.46803 | 1.69475 | 14.8783 |
| 80 | 1.39470 | 5.85006 | 3.96276 | 1.72964 | 15.8163 |
| 81 | 1.26743 | 6.41837 | 4.35641 | 1.78296 | 16.4534 |
| 82 | 1.19332 | 6.23400 | 4.48819 | 1.80232 | 16.7583 |
| 83 | 1.14811 | 5.94439 | 4.25820 | 1.69327 | 17.9321 |
| 84 | 1.09890 | 6.12488 | 4.28582 | 1.65542 | 17.1742 |
| 85 | 1.05932 | 5.73922 | 4.42153 | 1.69222 | 17.0351 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 3.42011 | 2.80347 | 1.48362 | 14.3931 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=TOBACCO

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.48049 | 1.88591 | 1.45625 | 15.3211 |
| 59 | 3.90625 | 2.38274 | 1.90522 | 1.43650 | 15.1848 |
| 60 | 3.84615 | 2.38601 | 1.89236 | 1.34489 | 15.8429 |
| 61 | 3.80228 | 2.34994 | 1.89152 | 1.30315 | 13.5768 |
| 62 | 3.71747 | 2.28613 | 1.86296 | 1.24151 | 14.2813 |
| 63 | 3.67647 | 2.23022 | 1.82608 | 1.24617 | 14.1661 |
| 64 | 3.61011 | 2.06454 | 1.74522 | 1.23815 | 13.6490 |
| 65 | 3.52113 | 1.87487 | 1.68903 | 1.18101 | 13.1360 |
| 66 | 3.40136 | 1.83826 | 1.61744 | 1.18439 | 13.1603 |
| 67 | 3.30033 | 1.84464 | 1.55530 | 1.17616 | 10.3668 |
| 68 | 3.14465 | 1.79205 | 1.53960 | 1.29928 | 9.4104 |
| 69 | 2.95858 | 1.65755 | 1.50727 | 1.41362 | 8.9248 |
| 70 | 2.84091 | 1.74793 | 1.50771 | 1.66563 | 8.8438 |
| 71 | 2.84091 | 1.97404 | 1.58420 | 1.86335 | 9.2606 |
| 72 | 2.57732 | 2.03681 | 1.58320 | 1.69095 | 9.6696 |
| 73 | 2.42131 | 2.40475 | 1.65314 | 1.61858 | 10.1478 |
| 74 | 2.22717 | 4.17853 | 1.69940 | 2.01479 | 11.6826 |
| 75 | 2.03252 | 4.26456 | 2.26869 | 2.58012 | 13.5151 |
| 76 | 1.91205 | 4.11226 | 2.58894 | 2.59787 | 13.3610 |
| 77 | 1.78891 | 4.29533 | 3.21467 | 2.37292 | 13.7572 |
| 78 | 1.66113 | 3.76045 | 3.49010 | 2.15254 | 13.9617 |
| 79 | 1.52439 | 4.09378 | 3.57946 | 2.53529 | 14.1676 |
| 80 | 1.39470 | 5.45185 | 4.45395 | 2.48648 | 15.8469 |
| 81 | 1.26743 | 6.25194 | 4.90507 | 2.50647 | 14.1060 |
| 82 | 1.19332 | 5.90603 | 5.05251 | 2.48493 | 14.6894 |
| 83 | 1.14811 | 5.56957 | 4.81461 | 2.22729 | 14.8938 |
| 84 | 1.09890 | 5.73971 | 4.88320 | 2.15600 | 15.2431 |
| 85 | 1.05932 | 5.11391 | 5.00882 | 2.12455 | 15.1233 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 2.86657 | 3.33333 | 1.96532 | 13.4489 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=TEXTILE MILLS

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 1.80914 | 1.39283 | 1.43040 | 11.2760 |
| 59 | 3.90625 | 1.83424 | 1.45361 | 1.40840 | 11.1181 |
| 60 | 3.84615 | 1.81840 | 1.48745 | 1.31541 | 11.7823 |
| 61 | 3.80228 | 1.86889 | 1.53376 | 1.27180 | 9.5659 |
| 62 | 3.71747 | 1.83892 | 1.55422 | 1.20903 | 10.3806 |
| 63 | 3.67647 | 1.79092 | 1.53300 | 1.21896 | 10.6770 |
| 64 | 3.61011 | 1.64767 | 1.47169 | 1.21750 | 10.6572 |
| 65 | 3.52113 | 1.58356 | 1.43473 | 1.16654 | 10.5898 |
| 66 | 3.40136 | 1.57361 | 1.38643 | 1.17540 | 11.0745 |
| 67 | 3.30033 | 1.57582 | 1.34964 | 1.17230 | 8.6952 |
| 68 | 3.14465 | 1.60377 | 1.36154 | 1.18659 | 8.0048 |
| 69 | 2.95858 | 1.54245 | 1.34543 | 1.20520 | 7.6786 |
| 70 | 2.84091 | 1.71779 | 1.35940 | 1.36281 | 7.7712 |
| 71 | 2.84091 | 1.97544 | 1.44178 | 1.47098 | 8.2659 |
| 72 | 2.57732 | 2.14205 | 1.54489 | 1.65140 | 8.4858 |
| 73 | 2.42131 | 2.59399 | 1.70100 | 1.87213 | 8.6819 |
| 74 | 2.22717 | 4.35864 | 1.81471 | 2.51159 | 10.0118 |
| 75 | 2.03252 | 4.24037 | 2.20400 | 2.92195 | 11.7162 |
| 76 | 1.91205 | 4.06497 | 2.67275 | 2.30689 | 11.8415 |
| 77 | 1.78891 | 4.28351 | 3.15053 | 2.29998 | 12.4336 |
| 78 | 1.66113 | 3.95365 | 3.38180 | 2.62841 | 12.8998 |
| 79 | 1.52439 | 4.54560 | 3.79294 | 2.44313 | 13.0369 |
| 80 | 1.39470 | 5.77032 | 4.22756 | 2.38792 | 13.3459 |
| 81 | 1.26743 | 6.41058 | 4.82043 | 2.31378 | 13.7726 |
| 82 | 1.19332 | 6.12640 | 4.93252 | 2.35561 | 14.8334 |
| 83 | 1.14811 | 5.82390 | 4.66768 | 2.16562 | 14.7275 |
| 84 | 1.09890 | 6.03597 | 4.69360 | 2.14340 | 15.0391 |
| 85 | 1.05932 | 5.51506 | 4.78677 | 2.16470 | 14.7687 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 3.12356 | 3.27553 | 1.86898 | 13.4200 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC-APPAREL & OTHER

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.37164 | 1.84284 | 1.60926 | 21.0352 |
| 59 | 3.90625 | 2.39780 | 1.88405 | 1.56260 | 20.8084 |
| 60 | 3.84615 | 2.38579 | 1.89313 | 1.43949 | 21.2708 |
| 61 | 3.80228 | 2.43763 | 1.91637 | 1.37095 | 18.8291 |
| 62 | 3.71747 | 2.38384 | 1.91502 | 1.28120 | 19.2926 |
| 63 | 3.67647 | 2.35673 | 1.89075 | 1.27309 | 19.3848 |
| 64 | 3.61011 | 2.21701 | 1.82112 | 1.25338 | 19.0266 |
| 65 | 3.52113 | 2.16077 | 1.78023 | 1.18610 | 18.6300 |
| 66 | 3.40136 | 2.15092 | 1.72005 | 1.18215 | 18.7006 |
| 67 | 3.30033 | 2.29523 | 1.66954 | 1.16908 | 15.9698 |
| 68 | 3.14465 | 2.17733 | 1.59401 | 1.19447 | 14.2543 |
| 69 | 2.95858 | 2.05037 | 1.50103 | 1.21240 | 12.9276 |
| 70 | 2.84091 | 2.06042 | 1.45228 | 1.35322 | 12.1695 |
| 71 | 2.84091 | 2.15746 | 1.46896 | 1.43782 | 12.0096 |
| 72 | 2.57732 | 2.40119 | 1.61965 | 1.54571 | 11.5158 |
| 73 | 2.42131 | 2.92330 | 1.81003 | 1.72036 | 11.0678 |
| 74 | 2.22717 | 4.81384 | 1.94440 | 2.33862 | 11.7582 |
| 75 | 2.03252 | 4.52717 | 2.33386 | 3.12187 | 12.4861 |
| 76 | 1.91205 | 4.41007 | 2.84439 | 2.97103 | 13.1369 |
| 77 | 1.78891 | 4.61766 | 3.20942 | 2.71570 | 14.7692 |
| 78 | 1.66113 | 4.50566 | 3.27606 | 2.75307 | 17.9981 |
| 79 | 1.52439 | 5.47883 | 3.58895 | 2.84666 | 19.0398 |
| 80 | 1.39470 | 6.85334 | 3.83801 | 2.76599 | 19.6355 |
| 81 | 1.26743 | 7.33415 | 4.10230 | 2.67939 | 19.6749 |
| 82 | 1.19332 | 7.18956 | 4.52804 | 2.70022 | 20.9187 |
| 83 | 1.14811 | 6.78784 | 4.60733 | 2.45589 | 22.2557 |
| 84 | 1.09890 | 7.07441 | 4.90318 | 2.41523 | 19.2461 |
| 85 | 1.05932 | 6.59218 | 5.28748 | 2.42335 | 20.6466 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 4.43443 | 4.02697 | 2.19653 | 19.4220 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=LUMBER & WOOD

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.84727 | 1.90367 | 1.49691 | 16.4322 |
| 59 | 3.90625 | 2.87991 | 1.86270 | 1.47688 | 16.2930 |
| 60 | 3.84615 | 2.89339 | 1.78796 | 1.38073 | 16.9586 |
| 61 | 3.80228 | 2.94812 | 1.72713 | 1.33457 | 14.6990 |
| 62 | 3.71747 | 2.89451 | 1.63509 | 1.27163 | 15.3939 |
| 63 | 3.67647 | 2.78150 | 1.60906 | 1.27042 | 15.3546 |
| 64 | 3.61011 | 2.57387 | 1.54071 | 1.25634 | 14.9109 |
| 65 | 3.52113 | 2.43850 | 1.49826 | 1.19318 | 14.4938 |
| 66 | 3.40136 | 2.35511 | 1.44199 | 1.18989 | 14.5755 |
| 67 | 3.30033 | 2.31206 | 1.39438 | 1.17562 | 11.8249 |
| 68 | 3.14465 | 2.25926 | 1.35743 | 1.24488 | 10.7523 |
| 69 | 2.95858 | 2.17801 | 1.30946 | 1.31406 | 10.1600 |
| 70 | 2.84091 | 2.30483 | 1.29401 | 1.52002 | 9.9919 |
| 71 | 2.84091 | 2.49228 | 1.34689 | 1.67253 | 10.3782 |
| 72 | 2.57732 | 2.55086 | 1.43302 | 1.70255 | 9.3661 |
| 73 | 2.42131 | 2.94407 | 1.56684 | 1.80824 | 8.6138 |
| 74 | 2.22717 | 4.76847 | 1.67117 | 2.35860 | 9.0932 |
| 75 | 2.03252 | 4.52959 | 2.14320 | 3.45439 | 10.4677 |
| 76 | 1.91205 | 4.58466 | 2.65694 | 2.91186 | 10.9399 |
| 77 | 1.78891 | 4.89015 | 3.06831 | 2.30746 | 11.8604 |
| 78 | 1.66113 | 4.65902 | 3.31125 | 2.15693 | 12.6557 |
| 79 | 1.52439 | 5.75499 | 3.53237 | 2.60555 | 12.9452 |
| 80 | 1.39470 | 7.10914 | 3.94643 | 2.58542 | 14.1157 |
| 81 | 1.26743 | 7.92077 | 4.53233 | 2.46905 | 14.7508 |
| 82 | 1.19332 | 7.61662 | 4.74762 | 2.47971 | 14.9518 |
| 83 | 1.14811 | 6.94865 | 4.57222 | 2.24922 | 15.2487 |
| 84 | 1.09890 | 6.93875 | 4.67300 | 2.18835 | 15.2795 |
| 85 | 1.05932 | 6.42184 | 4.82796 | 2.17300 | 15.2961 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 4.78011 | 3.44894 | 1.65703 | 15.5106 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=FURNITURE & FIXTURES

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.84790 | 1.96490 | 1.59391 | 20.0560 |
| 59 | 3.90625 | 2.82455 | 2.03708 | 1.51624 | 19.6797 |
| 60 | 3.84615 | 2.74410 | 2.07517 | 1.36757 | 20.0772 |
| 61 | 3.80228 | 2.68151 | 2.12858 | 1.27350 | 17.5494 |
| 62 | 3.71747 | 2.52195 | 2.14753 | 1.16055 | 17.9426 |
| 63 | 3.67647 | 2.50347 | 2.14695 | 1.16560 | 18.0281 |
| 64 | 3.61011 | 2.39430 | 2.08850 | 1.16620 | 17.6135 |
| 65 | 3.52113 | 2.33697 | 2.05263 | 1.11509 | 17.2200 |
| 66 | 3.40136 | 2.34860 | 2.00199 | 1.12480 | 17.2757 |
| 67 | 3.30033 | 2.37723 | 1.96035 | 1.12330 | 14.5556 |
| 68 | 3.14465 | 2.26254 | 1.85625 | 1.19011 | 13.0618 |
| 69 | 2.95858 | 2.08279 | 1.74884 | 1.25338 | 12.0909 |
| 70 | 2.84091 | 2.09130 | 1.67181 | 1.44336 | 11.4930 |
| 71 | 2.84091 | 2.19396 | 1.69224 | 1.57762 | 11.5833 |
| 72 | 2.57732 | 2.40082 | 1.72172 | 1.79740 | 11.2613 |
| 73 | 2.42131 | 2.89933 | 1.86141 | 2.06977 | 11.2248 |
| 74 | 2.22717 | 4.79661 | 1.94760 | 2.75813 | 12.3284 |
| 75 | 2.03252 | 4.59550 | 2.34732 | 3.13052 | 13.4622 |
| 76 | 1.91205 | 4.76260 | 2.83301 | 2.68975 | 14.3306 |
| 77 | 1.78891 | 4.92247 | 3.10942 | 2.50565 | 15.3032 |
| 78 | 1.66113 | 4.75951 | 3.31244 | 2.64014 | 16.4655 |
| 79 | 1.52439 | 5.85885 | 3.58301 | 2.59147 | 17.0277 |
| 80 | 1.39470 | 7.14550 | 4.06754 | 2.51889 | 17.6370 |
| 81 | 1.26743 | 7.63389 | 4.46899 | 2.42216 | 18.1374 |
| 82 | 1.19332 | 7.41556 | 4.82041 | 2.47366 | 19.0715 |
| 83 | 1.14811 | 6.93617 | 4.78968 | 2.26985 | 19.0732 |
| 84 | 1.09890 | 7.02606 | 5.00982 | 2.27645 | 19.2665 |
| 85 | 1.05932 | 6.69815 | 5.31860 | 2.32028 | 19.3563 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 4.51399 | 3.75723 | 2.10019 | 17.2254 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=PAPER

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 1.73778 | 0.97467 | 1.37225 | 10.7010 |
| 59 | 3.90625 | 1.69868 | 1.03396 | 1.36508 | 10.5837 |
| 60 | 3.84615 | 1.62396 | 1.07406 | 1.28980 | 11.2774 |
| 61 | 3.80228 | 1.62117 | 1.12085 | 1.26197 | 9.1322 |
| 62 | 3.71747 | 1.53986 | 1.14484 | 1.21285 | 9.9591 |
| 63 | 3.67647 | 1.51745 | 1.13614 | 1.19804 | 10.1725 |
| 64 | 3.61011 | 1.39703 | 1.08678 | 1.17352 | 10.0438 |
| 65 | 3.52113 | 1.36161 | 1.06262 | 1.10120 | 9.8961 |
| 66 | 3.40136 | 1.36535 | 1.02896 | 1.08767 | 10.2997 |
| 67 | 3.30033 | 1.41119 | 1.00027 | 1.06478 | 7.8403 |
| 68 | 3.14465 | 1.39722 | 1.00146 | 1.05284 | 7.0902 |
| 69 | 2.95858 | 1.31487 | 0.99190 | 1.05188 | 6.8240 |
| 70 | 2.84091 | 1.51094 | 1.00507 | 1.18673 | 6.9257 |
| 71 | 2.84091 | 1.78865 | 1.07140 | 1.27194 | 7.4007 |
| 72 | 2.57732 | 1.99568 | 1.19680 | 1.34611 | 7.3690 |
| 73 | 2.42131 | 2.50735 | 1.35948 | 1.47712 | 7.4146 |
| 74 | 2.22717 | 4.35971 | 1.48994 | 2.05253 | 8.6452 |
| 75 | 2.03252 | 3.67305 | 1.98248 | 2.36495 | 9.8762 |
| 76 | 1.91205 | 3.45525 | 2.47463 | 2.08505 | 10.0296 |
| 77 | 1.78891 | 3.68935 | 2.95141 | 1.94796 | 10.8695 |
| 78 | 1.66113 | 3.30001 | 3.13086 | 2.28750 | 11.1734 |
| 79 | 1.52439 | 4.02967 | 3.41730 | 2.27003 | 11.6994 |
| 80 | 1.39470 | 5.06718 | 3.92447 | 2.18881 | 12.4568 |
| 81 | 1.26743 | 6.01165 | 4.38170 | 2.18808 | 12.9744 |
| 82 | 1.19332 | 5.60209 | 4.40207 | 2.17344 | 13.6139 |
| 83 | 1.14811 | 5.24780 | 4.10107 | 1.95108 | 13.7610 |
| 84 | 1.09890 | 5.36860 | 4.06140 | 1.89181 | 15.6782 |
| 85 | 1.05932 | 4.71030 | 4.08137 | 1.86930 | 14.0740 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 2.45308 | 2.38921 | 1.71484 | 11.4355 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=PRINTING

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.48786 | 1.93620 | 1.69375 | 19.6616 |
| 59 | 3.90625 | 2.52273 | 2.04471 | 1.68889 | 19.4780 |
| 60 | 3.84615 | 2.52109 | 2.11686 | 1.59837 | 20.0228 |
| 61 | 3.80228 | 2.55786 | 2.20414 | 1.56547 | 17.6618 |
| 62 | 3.71747 | 2.49630 | 2.25443 | 1.50895 | 18.2333 |
| 63 | 3.67647 | 2.42423 | 2.25378 | 1.49701 | 18.2445 |
| 64 | 3.61011 | 2.24467 | 2.20385 | 1.46453 | 17.8242 |
| 65 | 3.52113 | 2.12971 | 2.17856 | 1.38139 | 17.3746 |
| 66 | 3.40136 | 2.07506 | 2.12961 | 1.36875 | 17.4136 |
| 67 | 3.30033 | 2.05614 | 2.09029 | 1.34031 | 14.6493 |
| 68 | 3.14465 | 2.02997 | 1.99347 | 1.42753 | 13.2475 |
| 69 | 2.95858 | 1.95883 | 1.88184 | 1.50821 | 12.3072 |
| 70 | 2.84091 | 2.12492 | 1.81757 | 1.73021 | 11.8723 |
| 71 | 2.84091 | 2.38126 | 1.84411 | 1.89861 | 12.0701 |
| 72 | 2.57732 | 2.52222 | 1.83829 | 1.66231 | 11.8569 |
| 73 | 2.42131 | 2.97590 | 1.91408 | 1.53180 | 11.8632 |
| 74 | 2.22717 | 4.88703 | 1.95537 | 1.88266 | 12.9488 |
| 75 | 2.03252 | 4.86126 | 2.43974 | 2.59497 | 13.6166 |
| 76 | 1.91205 | 4.98185 | 2.95416 | 2.71571 | 14.4206 |
| 77 | 1.78891 | 4.94861 | 3.29117 | 2.30267 | 15.2956 |
| 78 | 1.66113 | 4.80858 | 3.46935 | 2.16116 | 16.8843 |
| 79 | 1.52439 | 5.40348 | 3.81223 | 2.07538 | 18.1096 |
| 80 | 1.39470 | 6.55299 | 4.17480 | 2.06094 | 18.8774 |
| 81 | 1.26743 | 7.02978 | 4.54848 | 2.43226 | 19.4055 |
| 82 | 1.19332 | 7.00013 | 4.87466 | 2.44676 | 20.5378 |
| 83 | 1.14811 | 6.76606 | 4.78963 | 2.22218 | 20.6451 |
| 84 | 1.09890 | 7.22048 | 4.98769 | 2.16621 | 20.3565 |
| 85 | 1.05932 | 7.62808 | 5.24307 | 2.16161 | 19.8174 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 4.84739 | 3.86320 | 0.00000 | 18.0925 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=BULK CHEMICALS

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.07619 | 0.81891 | 1.13429 | 5.5979 |
| 59 | 3.90625 | 2.01939 | 0.85831 | 1.11523 | 5.7052 |
| 60 | 3.84615 | 1.94083 | 0.88194 | 1.04020 | 6.7256 |
| 61 | 3.80228 | 1.91037 | 0.91315 | 1.00681 | 4.7474 |
| 62 | 3.71747 | 1.79203 | 0.92594 | 0.95554 | 5.8945 |
| 63 | 3.67647 | 1.75407 | 0.91426 | 0.94638 | 6.5060 |
| 64 | 3.61011 | 1.61439 | 0.86469 | 0.93335 | 6.8062 |
| 65 | 3.52113 | 1.53276 | 0.84198 | 0.87730 | 7.0328 |
| 66 | 3.40136 | 1.51727 | 0.81028 | 0.87105 | 7.8520 |
| 67 | 3.30033 | 1.53182 | 0.78544 | 0.86025 | 5.7658 |
| 68 | 3.14465 | 1.54094 | 0.78415 | 0.86712 | 5.2923 |
| 69 | 2.95858 | 1.47968 | 0.77594 | 0.88871 | 5.3237 |
| 70 | 2.84091 | 1.63885 | 0.78520 | 1.03806 | 5.6331 |
| 71 | 2.84091 | 1.86904 | 0.84202 | 1.13804 | 6.2299 |
| 72 | 2.57732 | 2.04499 | 0.96959 | 1.21811 | 6.0028 |
| 73 | 2.42131 | 2.50028 | 1.12298 | 1.34975 | 5.9306 |
| 74 | 2.22717 | 4.27595 | 1.26081 | 1.95042 | 7.1049 |
| 75 | 2.03252 | 4.16817 | 1.60689 | 2.04658 | 8.2622 |
| 76 | 1.91205 | 3.87892 | 2.00456 | 1.94223 | 8.4814 |
| 77 | 1.78891 | 4.02137 | 2.38650 | 1.87672 | 9.2857 |
| 78 | 1.66113 | 3.58489 | 2.44597 | 2.16456 | 10.1971 |
| 79 | 1.52439 | 4.36452 | 2.57246 | 2.04353 | 10.6376 |
| 80 | 1.39470 | 5.64094 | 2.81143 | 1.98048 | 11.6884 |
| 81 | 1.26743 | 6.44256 | 3.17908 | 2.01911 | 12.6631 |
| 82 | 1.19332 | 6.03350 | 3.34613 | 2.01343 | 14.5786 |
| 83 | 1.14811 | 5.63653 | 3.20356 | 1.80649 | 13.2007 |
| 84 | 1.09890 | 5.75670 | 3.21153 | 1.75087 | 12.7187 |
| 85 | 1.05932 | 5.21414 | 3.35774 | 1.73691 | 12.6192 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 2.66121 | 1.89783 | 1.57033 | 10.2312 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=OTHER CHEMICALS

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 1.77753 | 1.22066 | 1.24900 | 15.0168 |
| 59 | 3.90625 | 1.80041 | 1.26137 | 1.22566 | 14.9934 |
| 60 | 3.84615 | 1.78105 | 1.28239 | 1.14216 | 15.6899 |
| 61 | 3.80228 | 1.82973 | 1.31271 | 1.10297 | 13.4525 |
| 62 | 3.71747 | 1.79397 | 1.31467 | 1.04409 | 14.2296 |
| 63 | 3.67647 | 1.76117 | 1.30414 | 1.06632 | 14.4077 |
| 64 | 3.61011 | 1.62786 | 1.25090 | 1.07447 | 14.1710 |
| 65 | 3.52113 | 1.57968 | 1.22297 | 1.03196 | 13.9402 |
| 66 | 3.40136 | 1.57200 | 1.18587 | 1.04018 | 14.2161 |
| 67 | 3.30033 | 1.60700 | 1.15593 | 1.03780 | 11.6063 |
| 68 | 3.14465 | 1.59137 | 1.13884 | 1.04763 | 10.5800 |
| 69 | 2.95858 | 1.52543 | 1.11327 | 1.06237 | 10.0028 |
| 70 | 2.84091 | 1.67781 | 1.11378 | 1.20929 | 9.9289 |
| 71 | 2.84091 | 1.92059 | 1.18003 | 1.30268 | 10.3843 |
| 72 | 2.57732 | 2.12264 | 1.30142 | 1.29177 | 10.5076 |
| 73 | 2.42131 | 2.59864 | 1.45949 | 1.34415 | 10.7885 |
| 74 | 2.22717 | 4.33997 | 1.60967 | 1.85699 | 12.2214 |
| 75 | 2.03252 | 4.38562 | 2.01907 | 2.40205 | 13.4782 |
| 76 | 1.91205 | 4.07996 | 2.39947 | 2.13613 | 13.9123 |
| 77 | 1.78891 | 4.17519 | 2.88400 | 2.01499 | 14.7682 |
| 78 | 1.66113 | 3.86403 | 3.16826 | 2.23312 | 15.3330 |
| 79 | 1.52439 | 4.87191 | 3.29396 | 2.30017 | 14.9729 |
| 80 | 1.39470 | 6.29602 | 3.66854 | 2.21677 | 16.7865 |
| 81 | 1.26743 | 6.80017 | 4.15066 | 2.20072 | 17.1567 |
| 82 | 1.19332 | 6.30595 | 4.07633 | 2.17958 | 18.6934 |
| 83 | 1.14811 | 5.79801 | 3.75338 | 1.95047 | 18.3927 |
| 84 | 1.09890 | 5.77671 | 3.66449 | 1.88775 | 17.8474 |
| 85 | 1.05932 | 4.98726 | 3.67531 | 1.86322 | 17.3856 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 3.07696 | 1.89788 | 1.57033 | 10.2312 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=SIC 29, COAL & MISC

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.43076 | 1.39757 | 1.22466 | 18.4993 |
| 59 | 3.90625 | 2.37623 | 1.44459 | 1.22261 | 18.4341 |
| 60 | 3.84615 | 2.27950 | 1.46773 | 1.15712 | 19.1408 |
| 61 | 3.80228 | 2.25201 | 1.50306 | 1.13557 | 16.9744 |
| 62 | 3.71747 | 2.14115 | 1.51275 | 1.09544 | 17.7999 |
| 63 | 3.67647 | 2.10318 | 1.48025 | 1.09522 | 18.2005 |
| 64 | 3.61011 | 1.96305 | 1.40928 | 1.08705 | 18.1641 |
| 65 | 3.52113 | 1.90422 | 1.36476 | 1.03388 | 18.0883 |
| 66 | 3.40136 | 1.88344 | 1.30810 | 1.03550 | 18.4725 |
| 67 | 3.30033 | 1.90695 | 1.25920 | 1.02875 | 16.0282 |
| 68 | 3.14465 | 1.87881 | 1.23703 | 1.14078 | 14.3616 |
| 69 | 2.95858 | 1.81143 | 1.20114 | 1.24773 | 13.1525 |
| 70 | 2.84091 | 1.95044 | 1.19261 | 1.48122 | 12.4794 |
| 71 | 2.84091 | 2.17015 | 1.24784 | 1.66785 | 12.4956 |
| 72 | 2.57732 | 2.29310 | 1.35419 | 1.44932 | 12.0970 |
| 73 | 2.42131 | 2.71365 | 1.51146 | 1.32556 | 11.9527 |
| 74 | 2.22717 | 4.48257 | 1.62927 | 1.68712 | 12.9065 |
| 75 | 2.03252 | 4.44998 | 1.96692 | 1.43102 | 14.0321 |
| 76 | 1.91205 | 4.38317 | 2.54520 | 2.05452 | 14.8676 |
| 77 | 1.78891 | 4.47914 | 3.06229 | 2.02098 | 16.0012 |
| 78 | 1.66113 | 4.33908 | 3.20044 | 2.15230 | 16.9612 |
| 79 | 1.52439 | 5.37459 | 3.44615 | 1.98341 | 16.3682 |
| 80 | 1.39470 | 6.60037 | 3.89219 | 1.65786 | 18.2430 |
| 81 | 1.26743 | 6.81480 | 4.17487 | 1.66493 | 19.3909 |
| 82 | 1.19332 | 7.30509 | 4.42864 | 1.66805 | 18.3269 |
| 83 | 1.14811 | 6.65715 | 4.30754 | 1.51182 | 19.3906 |
| 84 | 1.09890 | 6.55680 | 4.47498 | 1.47874 | 19.6794 |
| 85 | 1.05932 | 5.89561 | 4.67065 | 1.47349 | 19.8707 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 4.19912 | 2.01349 | 1.95568 | 11.9557 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=RUBBER & MISC

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.45127 | 1.33043 | 1.09565 | 13.9067 |
| 59 | 3.90625 | 2.31772 | 1.41964 | 1.09405 | 13.8582 |
| 60 | 3.84615 | 2.14413 | 1.48356 | 1.03677 | 14.6197 |
| 61 | 3.80228 | 2.03413 | 1.55746 | 1.01983 | 12.4519 |
| 62 | 3.71747 | 1.84407 | 1.60287 | 0.98494 | 13.2683 |
| 63 | 3.67647 | 1.80481 | 1.61204 | 0.98410 | 13.5363 |
| 64 | 3.61011 | 1.66308 | 1.57673 | 0.97804 | 13.3987 |
| 65 | 3.52113 | 1.59269 | 1.56590 | 0.92726 | 13.2486 |
| 66 | 3.40136 | 1.57708 | 1.53849 | 0.92785 | 13.6137 |
| 67 | 3.30033 | 1.59740 | 1.51748 | 0.92086 | 11.1417 |
| 68 | 3.14465 | 1.63394 | 1.46919 | 0.90122 | 10.0644 |
| 69 | 2.95858 | 1.60646 | 1.40832 | 0.89723 | 9.4629 |
| 70 | 2.84091 | 1.78819 | 1.38210 | 1.02349 | 9.2843 |
| 71 | 2.84091 | 2.03498 | 1.42806 | 1.09993 | 9.6260 |
| 72 | 2.57732 | 2.12159 | 1.49370 | 1.09071 | 9.8117 |
| 73 | 2.42131 | 2.50780 | 1.61769 | 1.14452 | 10.1038 |
| 74 | 2.22717 | 4.22304 | 1.71217 | 1.66969 | 11.4792 |
| 75 | 2.03252 | 4.16562 | 2.13714 | 2.17313 | 12.7392 |
| 76 | 1.91205 | 3.98025 | 2.59915 | 1.79763 | 13.1626 |
| 77 | 1.78891 | 4.20133 | 3.05201 | 1.72737 | 13.9529 |
| 78 | 1.66113 | 3.96641 | 3.20479 | 2.04764 | 14.7007 |
| 79 | 1.52439 | 4.53436 | 3.52681 | 1.92566 | 15.2352 |
| 80 | 1.39470 | 5.78022 | 4.00381 | 1.74040 | 16.2215 |
| 81 | 1.26743 | 6.71893 | 4.50311 | 1.72524 | 16.9395 |
| 82 | 1.19332 | 6.43263 | 4.64289 | 1.86790 | 13.2745 |
| 83 | 1.14811 | 6.07610 | 4.42476 | 1.82589 | 13.2734 |
| 84 | 1.09890 | 6.26463 | 4.48465 | 1.90559 | 15.3576 |
| 85 | 1.05932 | 5.83866 | 4.60217 | 2.01785 | 15.2829 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 3.22645 | 3.03468 | 2.17726 | 15.2023 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=LEATHER

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 1.98783 | 1.59388 | 1.25731 | 21.7624 |
| 59 | 3.90625 | 1.97460 | 1.71732 | 1.30918 | 21.3296 |
| 60 | 3.84615 | 1.92161 | 1.78710 | 1.29801 | 21.6125 |
| 61 | 3.80228 | 1.93813 | 1.85325 | 1.32641 | 19.1494 |
| 62 | 3.71747 | 1.86681 | 1.87695 | 1.33203 | 19.5447 |
| 63 | 3.67647 | 1.79954 | 1.89752 | 1.31278 | 19.3337 |
| 64 | 3.61011 | 1.63734 | 1.87250 | 1.28690 | 18.7190 |
| 65 | 3.52113 | 1.55200 | 1.86602 | 1.21168 | 18.0908 |
| 66 | 3.40136 | 1.51841 | 1.83578 | 1.20037 | 18.0619 |
| 67 | 3.30033 | 1.52708 | 1.80673 | 1.17939 | 15.0860 |
| 68 | 3.14465 | 1.58281 | 1.73250 | 1.12876 | 13.8417 |
| 69 | 2.95858 | 1.58609 | 1.66453 | 1.08758 | 12.9852 |
| 70 | 2.84091 | 1.77756 | 1.66000 | 1.18087 | 12.5816 |
| 71 | 2.84091 | 1.99136 | 1.68000 | 1.24311 | 12.8821 |
| 72 | 2.57732 | 2.27394 | 1.71295 | 1.04857 | 12.2812 |
| 73 | 2.42131 | 2.81828 | 1.82048 | 0.94303 | 11.9790 |
| 74 | 2.22717 | 4.62064 | 1.87772 | 1.36037 | 12.7814 |
| 75 | 2.03252 | 4.33467 | 2.10181 | 1.71396 | 13.6919 |
| 76 | 1.91205 | 4.27452 | 2.75533 | 1.45838 | 14.6211 |
| 77 | 1.78891 | 4.26669 | 3.20076 | 1.49398 | 16.9822 |
| 78 | 1.66113 | 4.03356 | 3.27574 | 2.05252 | 17.2816 |
| 79 | 1.52439 | 4.85809 | 3.52163 | 2.07575 | 18.6274 |
| 80 | 1.39470 | 5.95058 | 4.13555 | 2.03439 | 19.4922 |
| 81 | 1.26743 | 6.69867 | 4.56766 | 2.13456 | 20.2822 |
| 82 | 1.19332 | 6.39165 | 4.79029 | 2.10561 | 20.9395 |
| 83 | 1.14811 | 5.98558 | 4.62026 | 1.88028 | 20.7905 |
| 84 | 1.09890 | 6.14201 | 4.74722 | 1.79397 | 19.1912 |
| 85 | 1.05932 | 5.54431 | 4.94315 | 1.75771 | 19.7569 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 2.9332 | 3.37187 | 1.88825 | 17.5723 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=GLASS

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 1.96660 | 1.52798 | 1.17697 | 11.3170 |
| 59 | 3.90625 | 1.96690 | 1.57615 | 1.18150 | 11.0881 |
| 60 | 3.84615 | 1.94310 | 1.59733 | 1.12586 | 11.7174 |
| 61 | 3.80228 | 1.96996 | 1.63076 | 1.11241 | 9.4071 |
| 62 | 3.71747 | 1.91154 | 1.63614 | 1.08007 | 10.1197 |
| 63 | 3.67647 | 1.88685 | 1.61341 | 1.23449 | 10.4466 |
| 64 | 3.61011 | 1.75054 | 1.54720 | 1.37128 | 10.3891 |
| 65 | 3.52113 | 1.67119 | 1.50688 | 1.44400 | 10.3390 |
| 66 | 3.40136 | 1.66355 | 1.45236 | 1.57918 | 10.8267 |
| 67 | 3.30033 | 1.68827 | 1.40583 | 1.69032 | 8.4609 |
| 68 | 3.14465 | 1.77609 | 1.37580 | 1.52978 | 7.7310 |
| 69 | 2.95858 | 1.77615 | 1.33267 | 1.38477 | 7.4748 |
| 70 | 2.84091 | 1.96336 | 1.32124 | 1.39931 | 7.5756 |
| 71 | 2.84091 | 2.17908 | 1.37893 | 1.37096 | 8.1168 |
| 72 | 2.57732 | 2.34595 | 1.46000 | 1.19306 | 8.3519 |
| 73 | 2.42131 | 2.80993 | 1.59599 | 1.10553 | 8.6469 |
| 74 | 2.22717 | 4.61779 | 1.70169 | 1.51061 | 10.0607 |
| 75 | 2.03252 | 4.45072 | 2.13811 | 1.26768 | 11.3264 |
| 76 | 1.91205 | 4.22741 | 2.64283 | 2.16867 | 11.4230 |
| 77 | 1.78891 | 4.50887 | 3.18275 | 1.72368 | 12.6084 |
| 78 | 1.66113 | 4.16369 | 3.34227 | 2.47064 | 13.0039 |
| 79 | 1.52439 | 4.76221 | 3.61202 | 1.96845 | 12.7871 |
| 80 | 1.39470 | 6.10737 | 4.11703 | 2.02666 | 13.8993 |
| 81 | 1.26743 | 7.07889 | 4.45175 | 2.07614 | 14.5838 |
| 82 | 1.19332 | 6.91713 | 4.59790 | 2.10478 | 15.6389 |
| 83 | 1.14811 | 6.52879 | 4.37556 | 1.93150 | 15.8597 |
| 84 | 1.09890 | 6.67536 | 4.42429 | 1.91644 | 15.4363 |
| 85 | 1.05932 | 6.45782 | 4.54064 | 1.93202 | 15.4972 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 4.21965 | 2.64933 | 1.47399 | 11.8497 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=CEMENT

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 1.21861 | 1.04107 | 1.23192 | 10.1979 |
| 59 | 3.90625 | 1.33829 | 1.05800 | 1.21842 | 10.2066 |
| 60 | 3.84615 | 1.42436 | 1.05713 | 1.14364 | 11.0834 |
| 61 | 3.80228 | 1.57878 | 1.06483 | 1.11259 | 9.0117 |
| 62 | 3.71747 | 1.64954 | 1.05218 | 1.06339 | 9.9594 |
| 63 | 3.67647 | 1.62390 | 1.02939 | 1.05013 | 10.3293 |
| 64 | 3.61011 | 1.49909 | 0.96779 | 1.03071 | 10.3147 |
| 65 | 3.52113 | 1.45847 | 0.93217 | 0.96656 | 10.3063 |
| 66 | 3.40136 | 1.45751 | 0.88965 | 0.95556 | 10.8333 |
| 67 | 3.30033 | 1.49846 | 0.85258 | 0.93780 | 8.5046 |
| 68 | 3.14465 | 1.38712 | 0.86036 | 0.93908 | 7.6646 |
| 69 | 2.95858 | 1.22438 | 0.85827 | 0.95309 | 7.3106 |
| 70 | 2.84091 | 1.31959 | 0.87609 | 1.09744 | 7.3203 |
| 71 | 2.84091 | 1.49635 | 0.94430 | 1.19186 | 7.7638 |
| 72 | 2.57732 | 1.56516 | 1.01037 | 1.16604 | 7.7452 |
| 73 | 2.42131 | 1.92974 | 1.11599 | 1.20750 | 7.8078 |
| 74 | 2.22717 | 3.63223 | 1.21346 | 1.71873 | 9.0414 |
| 75 | 2.03252 | 3.61057 | 1.77110 | 1.91861 | 10.6146 |
| 76 | 1.91205 | 3.29073 | 2.11201 | 1.78715 | 11.3793 |
| 77 | 1.78891 | 3.43008 | 2.56851 | 1.70314 | 12.2493 |
| 78 | 1.66113 | 3.23121 | 2.70924 | 1.97725 | 12.6418 |
| 79 | 1.52439 | 3.83992 | 3.42470 | 1.92075 | 12.8654 |
| 80 | 1.39470 | 4.86968 | 3.57083 | 2.00223 | 14.3852 |
| 81 | 1.26743 | 5.65965 | 4.31742 | 2.02055 | 14.8448 |
| 82 | 1.19332 | 5.80089 | 4.39758 | 2.00421 | 15.8905 |
| 83 | 1.14811 | 5.73716 | 4.14433 | 1.79668 | 16.2567 |
| 84 | 1.09890 | 6.07241 | 4.15111 | 1.73917 | 15.8811 |
| 85 | 1.05932 | 5.67780 | 4.21014 | 1.71619 | 14.8361 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 3.91731 | 1.99422 | 1.45472 | 11.8497 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC-OTHER SCG

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.86546 | 1.47450 | 1.44678 | 15.5004 |
| 59 | 3.90625 | 2.74364 | 1.51252 | 1.40027 | 15.3699 |
| 60 | 3.84615 | 2.59049 | 1.52478 | 1.28495 | 16.0317 |
| 61 | 3.80228 | 2.49479 | 1.54900 | 1.21893 | 13.7701 |
| 62 | 3.71747 | 2.31300 | 1.54648 | 1.13519 | 14.4809 |
| 63 | 3.67647 | 2.32803 | 1.53207 | 1.11751 | 14.7590 |
| 64 | 3.61011 | 2.23208 | 1.47455 | 1.09214 | 14.6216 |
| 65 | 3.52113 | 2.20612 | 1.44257 | 1.02119 | 14.4646 |
| 66 | 3.40136 | 2.23181 | 1.39677 | 1.00590 | 14.8101 |
| 67 | 3.30033 | 2.28989 | 1.35825 | 0.98293 | 12.3249 |
| 68 | 3.14465 | 2.14649 | 1.32444 | 0.97602 | 11.0601 |
| 69 | 2.95858 | 1.97882 | 1.27864 | 0.98160 | 10.2754 |
| 70 | 2.84091 | 2.00507 | 1.26387 | 1.11912 | 9.9468 |
| 71 | 2.84091 | 2.11500 | 1.31613 | 1.20719 | 10.1696 |
| 72 | 2.57732 | 2.40331 | 1.44602 | 1.27667 | 10.2096 |
| 73 | 2.42131 | 2.96686 | 1.62353 | 1.40133 | 10.3882 |
| 74 | 2.22717 | 4.91556 | 1.76434 | 1.97376 | 11.6593 |
| 75 | 2.03252 | 4.84972 | 2.09505 | 2.40652 | 12.9800 |
| 76 | 1.91205 | 4.64091 | 2.49963 | 2.22001 | 13.5726 |
| 77 | 1.78891 | 4.72276 | 2.96180 | 2.04648 | 13.6868 |
| 78 | 1.66113 | 4.49492 | 3.16882 | 2.31713 | 14.3893 |
| 79 | 1.52439 | 5.77270 | 3.47429 | 2.15511 | 14.8117 |
| 80 | 1.39470 | 7.17695 | 3.92425 | 2.12774 | 15.9543 |
| 81 | 1.26743 | 7.87602 | 4.24299 | 2.08299 | 16.6514 |
| 82 | 1.19332 | 7.77752 | 4.37720 | 2.11315 | 17.5029 |
| 83 | 1.14811 | 7.28946 | 4.15413 | 1.93898 | 17.5111 |
| 84 | 1.09890 | 7.44092 | 4.20203 | 1.92192 | 17.2249 |
| 85 | 1.05932 | 7.05790 | 4.30876 | 1.94018 | 14.0689 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 3.79307 | 2.64933 | 1.47399 | 11.8497 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=IRON AND STEEL

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.13909 | 1.62190 | 1.11479 | 10.5731 |
| 59 | 3.90625 | 2.13297 | 1.64286 | 1.11032 | 10.5796 |
| 60 | 3.84615 | 2.08517 | 1.63657 | 1.04644 | 11.3167 |
| 61 | 3.80228 | 2.11008 | 1.64796 | 1.02781 | 9.1461 |
| 62 | 3.71747 | 2.05011 | 1.63647 | 0.99430 | 10.0657 |
| 63 | 3.67647 | 2.01187 | 1.62050 | 0.98730 | 10.2604 |
| 64 | 3.61011 | 1.86616 | 1.56202 | 0.97569 | 10.0576 |
| 65 | 3.52113 | 1.79450 | 1.52440 | 0.91709 | 9.8787 |
| 66 | 3.40136 | 1.77247 | 1.47402 | 0.91195 | 10.2491 |
| 67 | 3.30033 | 1.79147 | 1.43456 | 0.90258 | 7.7336 |
| 68 | 3.14465 | 1.74045 | 1.42453 | 0.86558 | 7.2887 |
| 69 | 2.95858 | 1.64103 | 1.39618 | 0.84857 | 7.2925 |
| 70 | 2.84091 | 1.75014 | 1.40229 | 0.95992 | 7.6265 |
| 71 | 2.84091 | 1.96873 | 1.48016 | 1.02606 | 8.3880 |
| 72 | 2.57732 | 2.24190 | 1.51816 | 1.20702 | 8.2295 |
| 73 | 2.42131 | 2.78971 | 1.61528 | 1.42220 | 8.1644 |
| 74 | 2.22717 | 4.60595 | 1.69196 | 2.08507 | 9.2645 |
| 75 | 2.03252 | 4.33118 | 2.11403 | 2.73328 | 10.9523 |
| 76 | 1.91205 | 3.76424 | 2.58224 | 2.13892 | 11.1426 |
| 77 | 1.78891 | 4.03185 | 3.09235 | 2.03031 | 12.2904 |
| 78 | 1.66113 | 3.80037 | 3.21294 | 2.01295 | 13.0738 |
| 79 | 1.52439 | 4.40985 | 3.36956 | 2.02542 | 13.1328 |
| 80 | 1.39470 | 5.44797 | 3.98236 | 2.05302 | 14.2912 |
| 81 | 1.26743 | 6.29050 | 4.15473 | 2.11232 | 14.5857 |
| 82 | 1.19332 | 5.87207 | 4.32153 | 2.16562 | 16.9315 |
| 83 | 1.14811 | 5.45516 | 4.13189 | 1.94739 | 16.8390 |
| 84 | 1.09890 | 5.53072 | 4.19362 | 1.95102 | 15.1731 |
| 85 | 1.05932 | 4.89388 | 4.32385 | 1.94555 | 14.7360 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 2.69921 | 2.56262 | 1.6763 | 11.0597 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC-PRIMARY ALUMINUM

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.29549 | 0.67854 | 1.43229 | 4.2010 |
| 59 | 3.90625 | 2.27596 | 0.69811 | 1.36333 | 4.0951 |
| 60 | 3.84615 | 2.23227 | 0.70575 | 1.22781 | 4.9537 |
| 61 | 3.80228 | 2.21199 | 0.71884 | 1.14138 | 2.8407 |
| 62 | 3.71747 | 2.10475 | 0.71560 | 1.03855 | 3.8174 |
| 63 | 3.67647 | 2.06107 | 0.72886 | 1.08624 | 4.3421 |
| 64 | 3.61011 | 1.91152 | 0.70440 | 1.12438 | 4.5208 |
| 65 | 3.52113 | 1.80561 | 0.70451 | 1.11132 | 4.7386 |
| 66 | 3.40136 | 1.79733 | 0.69871 | 1.15361 | 5.5355 |
| 67 | 3.30033 | 1.83008 | 0.69543 | 1.18348 | 3.4424 |
| 68 | 3.14465 | 1.75747 | 0.67289 | 1.11216 | 2.9324 |
| 69 | 2.95858 | 1.65361 | 0.64622 | 1.05713 | 2.9443 |
| 70 | 2.84091 | 1.80136 | 0.63830 | 1.14207 | 3.2101 |
| 71 | 2.84091 | 2.01908 | 0.67242 | 1.18029 | 3.7362 |
| 72 | 2.57732 | 2.10809 | 0.80623 | 1.35835 | 3.2990 |
| 73 | 2.42131 | 2.49605 | 0.96225 | 1.57739 | 2.8865 |
| 74 | 2.22717 | 4.30090 | 1.10941 | 2.21973 | 3.8301 |
| 75 | 2.03252 | 4.35373 | 1.24982 | 3.71794 | 4.4234 |
| 76 | 1.91205 | 4.28424 | 1.42577 | 2.28795 | 4.7883 |
| 77 | 1.78891 | 4.27518 | 1.68533 | 1.91344 | 5.1535 |
| 78 | 1.66113 | 3.98658 | 2.03869 | 2.13318 | 5.7823 |
| 79 | 1.52439 | 4.50409 | 1.70902 | 2.17676 | 5.7626 |
| 80 | 1.39470 | 5.57516 | 2.26494 | 2.23085 | 6.3938 |
| 81 | 1.26743 | 6.55337 | 1.94222 | 2.31683 | 6.6354 |
| 82 | 1.19332 | 6.32749 | 2.69904 | 2.31250 | 8.3505 |
| 83 | 1.14811 | 5.98823 | 3.18621 | 2.08642 | 8.6437 |
| 84 | 1.09890 | 6.13837 | 3.79893 | 2.03276 | 8.3514 |
| 85 | 1.05932 | 5.70734 | 4.42576 | . | 7.4946 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 3.75080 | 2.56262 | 6.44509 | 11.0597 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC-OTHER PRIMARY METALS

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELECS7 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.09399 | 1.54481 | 1.42256 | 10.6636 |
| 59 | 3.90625 | 2.06526 | 1.55697 | 1.36378 | 10.5472 |
| 60 | 3.84615 | 2.01902 | 1.54321 | 1.23814 | 11.2961 |
| 61 | 3.80228 | 2.02524 | 1.54233 | 1.16152 | 9.1003 |
| 62 | 3.71747 | 1.93529 | 1.51565 | 1.06781 | 9.9271 |
| 63 | 3.67647 | 1.90100 | 1.51253 | 1.07105 | 10.2222 |
| 64 | 3.61011 | 1.75659 | 1.46607 | 1.06688 | 10.1356 |
| 65 | 3.52113 | 1.67392 | 1.44469 | 1.01606 | 10.0596 |
| 66 | 3.40136 | 1.66826 | 1.40888 | 1.01933 | 10.5255 |
| 67 | 3.30033 | 1.68332 | 1.37973 | 1.01418 | 8.1385 |
| 68 | 3.14465 | 1.69454 | 1.34269 | 1.00655 | 7.3893 |
| 69 | 2.95858 | 1.64704 | 1.29375 | 1.01102 | 7.1208 |
| 70 | 2.84091 | 1.82277 | 1.27639 | 1.14868 | 7.2045 |
| 71 | 2.84091 | 2.08392 | 1.32666 | 1.23682 | 7.7146 |
| 72 | 2.57732 | 2.20130 | 1.39194 | 1.23545 | 7.8530 |
| 73 | 2.42131 | 2.61873 | 1.51171 | 1.29910 | 8.0524 |
| 74 | 2.22717 | 4.46071 | 1.60648 | 1.82457 | 9.3981 |
| 75 | 2.03252 | 4.38791 | 1.91186 | 3.01726 | 10.8408 |
| 76 | 1.91205 | 4.49896 | 2.27471 | 2.29975 | 10.6845 |
| 77 | 1.78891 | 4.44213 | 2.65388 | 1.96257 | 11.4718 |
| 78 | 1.66113 | 4.27206 | 2.76263 | 2.12671 | 12.0086 |
| 79 | 1.52439 | 4.86170 | 3.41841 | 2.15887 | 12.2040 |
| 80 | 1.39470 | 6.39257 | 3.81224 | 2.20462 | 12.9478 |
| 81 | 1.26743 | 6.80356 | 4.07682 | 2.24472 | 13.8860 |
| 82 | 1.19332 | 6.61203 | 4.31110 | 2.29743 | 14.6595 |
| 83 | 1.14811 | 6.18100 | 4.21118 | 2.18401 | 15.2599 |
| 84 | 1.09890 | 6.31821 | 4.36013 | 2.21240 | 14.5744 |
| 85 | 1.05932 | 6.11125 | 4.57287 | 2.23802 | 13.9411 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 3.27264 | 2.65896 | 1.69557 | 10.0096 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=FABRICATED METALS

| YEAR | DOL87 | POIL87 | PNA'GS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.36389 | 2.03334 | 1.39539 | 17.1609 |
| 59 | 3.90625 | 2.36808 | 2.07441 | 1.37251 | 17.1143 |
| 60 | 3.84615 | 2.34654 | 2.08211 | 1.27557 | 17.8352 |
| 61 | 3.80228 | 2.38238 | 2.10742 | 1.22604 | 15.6128 |
| 62 | 3.71747 | 2.30705 | 2.08755 | 1.15942 | 16.3613 |
| 63 | 3.67647 | 2.28410 | 2.07051 | 1.15830 | 16.4807 |
| 64 | 3.61011 | 2.14611 | 2.00480 | 1.14944 | 16.1509 |
| 65 | 3.52113 | 2.07383 | 1.96316 | 1.08835 | 15.7777 |
| 66 | 3.40136 | 2.06045 | 1.89972 | 1.08522 | 15.7382 |
| 67 | 3.30033 | 2.06880 | 1.85963 | 1.06793 | 12.8680 |
| 68 | 3.14465 | 1.98187 | 1.77945 | 1.07147 | 11.5119 |
| 69 | 2.95858 | 1.85374 | 1.68310 | 1.08038 | 10.8070 |
| 70 | 2.84091 | 1.94025 | 1.62763 | 1.22426 | 10.5455 |
| 71 | 2.84091 | 2.11954 | 1.66028 | 1.32026 | 10.8277 |
| 72 | 2.57732 | 2.30853 | 1.72174 | 1.44067 | 10.7304 |
| 73 | 2.42131 | 2.78699 | 1.84571 | 1.60488 | 10.8093 |
| 74 | 2.22717 | 4.74153 | 1.93229 | 2.23351 | 11.9951 |
| 75 | 2.03252 | 4.73163 | 2.38536 | 2.65665 | 13.5444 |
| 76 | 1.91205 | 4.70744 | 2.85509 | 2.41400 | 14.1464 |
| 77 | 1.78891 | 4.83792 | 3.26694 | 2.26991 | 14.7682 |
| 78 | 1.66113 | 4.58532 | 3.45173 | 2.54212 | 15.7970 |
| 79 | 1.52439 | 5.43307 | 3.66142 | 2.44894 | 16.3532 |
| 80 | 1.39470 | 6.80857 | 4.12596 | 2.32364 | 17.5904 |
| 81 | 1.26743 | 7.44609 | 4.31471 | 2.24741 | 18.3426 |
| 82 | 1.19332 | 7.29040 | 4.57928 | 2.32951 | 19.2559 |
| 83 | 1.14811 | 6.91197 | 4.49351 | 2.16504 | 19.7351 |
| 84 | 1.09890 | 7.16332 | 4.64566 | 2.16252 | 18.4990 |
| 85 | 1.05932 | 7.02123 | 4.87069 | 2.21102 | 18.5577 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 4.55635 | 3.46821 | 1.86898 | 16.7437 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=INDUSTRIAL MACHINERY

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.33114 | 1.89433 | 1.38406 | 17.3419 |
| 59 | 3.90625 | 2.33159 | 1.94776 | 1.35869 | 17.0330 |
| 60 | 3.84615 | 2.29041 | 1.97192 | 1.26993 | 17.6051 |
| 61 | 3.80228 | 2.29102 | 2.01669 | 1.23147 | 15.1385 |
| 62 | 3.71747 | 2.20595 | 2.02143 | 1.17281 | 15.5850 |
| 63 | 3.67647 | 2.13881 | 2.01757 | 1.15708 | 15.6727 |
| 64 | 3.61011 | 1.96143 | 1.95570 | 1.12986 | 15.2970 |
| 65 | 3.52113 | 1.87765 | 1.92560 | 1.06188 | 14.9664 |
| 66 | 3.40136 | 1.84780 | 1.87187 | 1.04986 | 15.1350 |
| 67 | 3.30033 | 1.85495 | 1.80902 | 1.02955 | 12.6049 |
| 68 | 3.14465 | 1.83918 | 1.71731 | 1.00803 | 11.4982 |
| 69 | 2.95858 | 1.76214 | 1.61684 | 0.99295 | 10.7881 |
| 70 | 2.84091 | 1.89881 | 1.56480 | 1.10954 | 10.5973 |
| 71 | 2.84091 | 2.10716 | 1.57724 | 1.16937 | 10.9691 |
| 72 | 2.57732 | 2.28323 | 1.64838 | 1.19126 | 10.8169 |
| 73 | 2.42131 | 2.74484 | 1.78517 | 1.25539 | 10.8576 |
| 74 | 2.22717 | 4.67137 | 1.87997 | 1.78945 | 11.9912 |
| 75 | 2.03252 | 4.69511 | 2.27314 | 2.12574 | 12.9665 |
| 76 | 1.91205 | 4.63494 | 2.78987 | 2.24479 | 13.6422 |
| 77 | 1.78891 | 4.75313 | 3.20330 | 2.04426 | 14.6787 |
| 78 | 1.66113 | 4.41289 | 3.41795 | 2.20826 | 15.5214 |
| 79 | 1.52439 | 5.23214 | 3.62849 | 2.02214 | 15.9392 |
| 80 | 1.39470 | 6.74631 | 4.02482 | 2.10688 | 16.8438 |
| 81 | 1.26743 | 7.19100 | 4.28741 | 2.01263 | 17.7922 |
| 82 | 1.19332 | 6.99294 | 4.55442 | 1.99359 | 18.9017 |
| 83 | 1.14811 | 6.59275 | 4.49769 | 1.79629 | 18.8254 |
| 84 | 1.09890 | 6.77670 | 4.66389 | 1.74213 | 19.5097 |
| 85 | 1.05932 | 6.45976 | 4.91037 | 1.71899 | 19.1991 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 4.31228 | 3.46821 | 1.52216 | 15.8478 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC-ELECTRONIC

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.11687 | 1.99152 | 1.31143 | 14.2112 |
| 59 | 3.90625 | 2.13512 | 2.04837 | 1.28594 | 13.9313 |
| 60 | 3.84615 | 2.06433 | 2.07511 | 1.19691 | 14.5506 |
| 61 | 3.80228 | 2.12860 | 2.12010 | 1.15498 | 12.2409 |
| 62 | 3.71747 | 2.11421 | 2.13001 | 1.09156 | 12.8556 |
| 63 | 3.67647 | 2.06816 | 2.07369 | 1.09190 | 12.9929 |
| 64 | 3.61011 | 1.91457 | 1.97012 | 1.08315 | 12.7164 |
| 65 | 3.52113 | 1.82133 | 1.89599 | 1.03124 | 12.4761 |
| 66 | 3.40136 | 1.79064 | 1.80181 | 1.03172 | 12.7641 |
| 67 | 3.30033 | 1.78682 | 1.71728 | 1.02217 | 10.1944 |
| 68 | 3.14465 | 1.79857 | 1.64688 | 0.98693 | 9.3602 |
| 69 | 2.95858 | 1.74929 | 1.56402 | 0.96780 | 8.9725 |
| 70 | 2.84091 | 1.89600 | 1.52305 | 1.08132 | 8.9777 |
| 71 | 2.84091 | 2.13003 | 1.56071 | 1.14971 | 9.4836 |
| 72 | 2.57732 | 2.32883 | 1.67120 | 1.19100 | 9.6367 |
| 73 | 2.42131 | 2.80233 | 1.83698 | 1.27204 | 9.8743 |
| 74 | 2.22717 | 4.72145 | 1.96118 | 1.87900 | 11.1889 |
| 75 | 2.03252 | 4.53281 | 2.35260 | 2.29372 | 12.5642 |
| 76 | 1.91205 | 4.52383 | 2.78443 | 2.12444 | 13.1129 |
| 77 | 1.78891 | 4.65263 | 3.28278 | 2.02029 | 14.0804 |
| 78 | 1.66113 | 4.33255 | 3.40315 | 2.36679 | 14.6500 |
| 79 | 1.52439 | 4.93325 | 3.67230 | 2.16496 | 14.7817 |
| 80 | 1.39470 | 6.46653 | 4.11400 | 2.21363 | 16.1755 |
| 81 | 1.26743 | 6.85175 | 4.53261 | 2.01805 | 17.2961 |
| 82 | 1.19332 | 6.57985 | 4.78905 | 2.06545 | 18.1037 |
| 83 | 1.14811 | 6.17437 | 4.65818 | 1.87749 | 18.1169 |
| 84 | 1.09890 | 6.31643 | 4.80093 | 1.87458 | 17.9333 |
| 85 | 1.05932 | 5.79195 | 5.02552 | 1.87633 | 18.0639 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 3.93663 | 3.30443 | 1.61850 | 15.3276 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=TRANSP EQUIP

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 1.96942 | 1.77499 | 1.31515 | 13.1265 |
| 59 | 3.90625 | 2.00503 | 1.84651 | 1.30640 | 12.9556 |
| 60 | 3.84615 | 2.00868 | 1.87640 | 1.23208 | 13.6017 |
| 61 | 3.80228 | 2.04793 | 1.90628 | 1.19941 | 11.2869 |
| 62 | 3.71747 | 1.99719 | 1.91299 | 1.15307 | 11.9970 |
| 63 | 3.67647 | 1.96792 | 1.89544 | 1.15567 | 12.2323 |
| 64 | 3.61011 | 1.82467 | 1.83197 | 1.14786 | 12.0970 |
| 65 | 3.52113 | 1.75211 | 1.79040 | 1.09019 | 11.9425 |
| 66 | 3.40136 | 1.74222 | 1.73115 | 1.09020 | 12.2762 |
| 67 | 3.30033 | 1.75925 | 1.67349 | 1.07825 | 9.7526 |
| 68 | 3.14465 | 1.72735 | 1.62006 | 1.11059 | 9.0085 |
| 69 | 2.95858 | 1.64132 | 1.55303 | 1.14382 | 8.7247 |
| 70 | 2.84091 | 1.79945 | 1.52661 | 1.31571 | 8.8458 |
| 71 | 2.84091 | 2.02949 | 1.57348 | 1.43989 | 9.4580 |
| 72 | 2.57732 | 2.21021 | 1.66224 | 1.51275 | 9.8030 |
| 73 | 2.42131 | 2.68774 | 1.79980 | 1.63794 | 10.2094 |
| 74 | 2.22717 | 4.56832 | 1.89976 | 2.21133 | 11.6844 |
| 75 | 2.03252 | 4.36571 | 2.41401 | 2.83728 | 13.1859 |
| 76 | 1.91205 | 4.28019 | 2.83296 | 2.44100 | 13.6002 |
| 77 | 1.78891 | 4.42965 | 3.32335 | 2.19344 | 14.3320 |
| 78 | 1.66113 | 4.13385 | 3.39423 | 2.55971 | 14.8063 |
| 79 | 1.52439 | 4.85891 | 3.65226 | 2.49399 | 14.8162 |
| 80 | 1.39470 | 6.03655 | 4.08384 | 2.46235 | 16.4471 |
| 81 | 1.26743 | 6.91990 | 4.47633 | 2.34538 | 17.2914 |
| 82 | 1.19332 | 6.62357 | 4.73153 | 2.40104 | 18.2659 |
| 83 | 1.14811 | 6.21727 | 4.59388 | 2.22500 | 18.5019 |
| 84 | 1.09890 | 6.34763 | 4.70962 | 2.20440 | 17.3135 |
| 85 | 1.05932 | 5.79046 | 4.92190 | 2.22187 | 17.0704 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 3.51607 | 3.35260 | 1.97495 | 12.9480 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=INSTRUMENTS

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.65679 | 2.26734 | 1.51779 | 17.4773 |
| 59 | 3.90625 | 2.54744 | 2.26920 | 1.51848 | 16.9301 |
| 60 | 3.84615 | 2.38597 | 2.23389 | 1.43869 | 17.3380 |
| 61 | 3.80228 | 2.27832 | 2.21581 | 1.41004 | 14.8308 |
| 62 | 3.71747 | 2.07530 | 2.15969 | 1.35894 | 15.2017 |
| 63 | 3.67647 | 2.03389 | 2.17070 | 1.34633 | 15.4226 |
| 64 | 3.61011 | 1.88543 | 2.12929 | 1.32026 | 15.1650 |
| 65 | 3.52113 | 1.80605 | 2.10662 | 1.24069 | 14.8355 |
| 66 | 3.40136 | 1.77810 | 2.05646 | 1.22753 | 14.9649 |
| 67 | 3.30033 | 1.79311 | 2.01865 | 1.20178 | 12.3107 |
| 68 | 3.14465 | 1.73740 | 1.88471 | 1.17319 | 11.4490 |
| 69 | 2.95858 | 1.67958 | 1.75557 | 1.15831 | 10.9988 |
| 70 | 2.84091 | 1.82394 | 1.66176 | 1.27862 | 10.9857 |
| 71 | 2.84091 | 2.11944 | 1.66381 | 1.35894 | 11.5355 |
| 72 | 2.57732 | 2.39618 | 1.81971 | 1.36936 | 11.7706 |
| 73 | 2.42131 | 2.91281 | 2.02213 | 1.43298 | 12.1806 |
| 74 | 2.22717 | 4.70258 | 2.17981 | 1.95199 | 13.5394 |
| 75 | 2.03252 | 4.41324 | 2.52280 | 2.60928 | 13.9326 |
| 76 | 1.91205 | 4.14572 | 2.91170 | 2.63682 | 14.9329 |
| 77 | 1.78891 | 4.29361 | 3.20105 | 2.32845 | 15.3863 |
| 78 | 1.66113 | 3.96175 | 3.46943 | 3.81090 | 15.9168 |
| 79 | 1.52439 | 4.62564 | 3.77308 | 2.45995 | 16.4673 |
| 80 | 1.39470 | 6.03026 | 4.23859 | 2.42064 | 17.6155 |
| 81 | 1.26743 | 6.85370 | 4.69480 | 2.46977 | 18.7865 |
| 82 | 1.19332 | 6.43423 | 4.85795 | 2.42710 | 19.8491 |
| 83 | 1.14811 | 5.95283 | 4.65703 | 2.15563 | 20.5547 |
| 84 | 1.09890 | 6.01496 | 4.73243 | 2.06661 | 19.8663 |
| 85 | 1.05932 | 5.34988 | 4.88061 | 2.01889 | 19.4920 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 3.36952 | 3.60308 | 1.65703 | 17.3988 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

Table E-22D. Manufacturing Prices, 1958-1990

SIC=MISC MFG

| YEAR | DOL87 | POIL87 | PNATGS87 | PCOAL87 | PELEC87 |
|------|---------|---------|----------|---------|---------|
| 58 | 3.90625 | 2.32003 | 1.75039 | 1.36019 | 20.7345 |
| 59 | 3.90625 | 2.34048 | 1.95578 | 1.37011 | 20.2098 |
| 60 | 3.84615 | 2.32974 | 2.12472 | 1.31047 | 20.4079 |
| 61 | 3.80228 | 2.37215 | 2.30513 | 1.29795 | 17.7107 |
| 62 | 3.71747 | 2.29494 | 2.44470 | 1.26459 | 17.9564 |
| 63 | 3.67647 | 2.26484 | 2.40597 | 1.26661 | 18.0628 |
| 64 | 3.61011 | 2.12300 | 2.31791 | 1.25652 | 17.7364 |
| 65 | 3.52113 | 2.03525 | 2.25619 | 1.19563 | 17.3772 |
| 66 | 3.40136 | 2.00030 | 2.17169 | 1.19766 | 17.5013 |
| 67 | 3.30033 | 2.00916 | 2.09922 | 1.18666 | 14.8171 |
| 68 | 3.14465 | 1.91907 | 2.04294 | 1.13497 | 13.5051 |
| 69 | 2.95858 | 1.79201 | 1.96701 | 1.09619 | 12.6413 |
| 70 | 2.84091 | 1.88319 | 1.93632 | 1.19687 | 12.2813 |
| 71 | 2.84091 | 2.06593 | 1.99987 | 1.25043 | 12.5672 |
| 72 | 2.57732 | 2.29250 | 2.00074 | 1.17024 | 12.3996 |
| 73 | 2.42131 | 2.80355 | 2.08866 | 1.16563 | 12.4590 |
| 74 | 2.22717 | 4.72758 | 2.13381 | 1.63927 | 13.5759 |
| 75 | 2.03252 | 4.64103 | 2.59074 | 2.07924 | 14.8844 |
| 76 | 1.91205 | 4.60175 | 3.10780 | 2.12450 | 15.7634 |
| 77 | 1.78891 | 4.74389 | 3.39368 | 2.35584 | 16.1115 |
| 78 | 1.66113 | 4.50849 | 3.62061 | 2.15112 | 17.5989 |
| 79 | 1.52439 | 5.57863 | 3.87723 | 2.22029 | 18.4094 |
| 80 | 1.39470 | 7.00684 | 4.22774 | 2.21132 | 19.3155 |
| 81 | 1.26743 | 7.00385 | 4.72644 | 2.13437 | 20.1548 |
| 82 | 1.19332 | 6.95862 | 4.98103 | 2.38349 | 20.4620 |
| 83 | 1.14811 | 6.40600 | 4.84538 | 2.25068 | 21.6610 |
| 84 | 1.09890 | 6.71710 | 4.96935 | 2.34280 | 20.4414 |
| 85 | 1.05932 | 6.09130 | 5.17172 | 2.37773 | 20.0751 |
| 86 | 1.03199 | . | . | . | . |
| 87 | 1.00000 | . | . | . | . |
| 88 | 0.96339 | 4.44824 | 3.60308 | 1.75337 | 18.4875 |
| 89 | 0.92081 | . | . | . | . |
| 90 | 0.88339 | . | . | . | . |

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