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**DOE/MC/23174-3068  
(DE92001149)**

**INTEGRATED SYSTEM DESIGN REPORT**

**Topical Report**

**July 1989**

**Work Performed Under Contract No. AC21-88MC23174**

**For  
U.S. Department of Energy  
Morgantown Energy Technology Center  
Morgantown, West Virginia**

**By  
General Electric Company  
Erie, Pennsylvania**

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## **Integrated System Design Report**

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For  
U.S. Department of Energy  
Office of Fossil Energy  
Morgantown Energy Technology Center  
P.O. Box 880  
Morgantown, West Virginia 26507-0880

By  
General Electric Company  
GE Transportation Systems  
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**July 1989**

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## 1. Overview

The primary objective of the integrated system test phase is to demonstrate the commercial potential of a coal fueled diesel engine in its actual operating environment. The integrated system in this project is defined as a coal fueled diesel locomotive. This locomotive, shown on drawing 41D715542, is described in the separate Concept Design Report. The test locomotive will be converted from an existing oil fueled diesel locomotive in three stages, until it nearly emulates the concept locomotive.

The first of the three development stages will consist of a modified locomotive and a fuel tender car. GE 607, a General Electric Engineering test locomotive, will be used, with modifications, for all three stages. For Stage I, the 16 cylinder engine on GE 607 has been replaced with a 12 cylinder engine. This has been done to provide additional space on the locomotive to accommodate the extra equipment needed for handling the coal-water-slurry (CWS). In addition to GE 607, Stage I will use a railroad flatcar with a special CWS tank, purge water tanks, and associated pumps and controls. The flatcar will serve as a testbed for working with the CWS. The CWS tank has special features which will allow the effectiveness of recirculation at various rates to be evaluated. In addition, it has features such as a removable top and baffles which will allow flexibility to modify during the testing process which would not be possible if the tank were in the location of a standard locomotive fuel tank. The CWS handling systems will be completely tested prior to the installation of the actual coal-fired engine. After the coal-fired engine is installed, locomotive testing will include both stationary testing and testing on the General Electric test track.

Knowledge gained during testing of the Stage I locomotive will be used to design a new, segmented, CWS/diesel tank for the Stage II locomotive. In addition, the recirculating and purge pumps and associated piping and controls will be relocated from the Stage I tender (flatcar) to GE607, thus eliminating the need for the tender. The engine will be modified to convert the fuel system to an accumulator type system. Locomotive testing will include stationary tests, tests on the General Electric test track, and limited running on a commercial railroad.

For Stage III, the locomotive will be modified to allow the installation of emission control equipment. In addition, electrical control functions will be further integrated into the locomotive's control system.

Refer to drawing number 41D715472 for a view of the locomotive equipment location for the three stages.

## 2. Locomotive Design Details

### 2.1 Description of GE 607

GE 607 is a C39-8 Engineering test locomotive used for conducting experimental tests. It forms the basis for the coal-fired locomotive, and is used for all three stages of the program. It is a microprocessor controlled, six axle locomotive, having motor driven blowers and radiator fans. The air compressor is shaft driven.

#### 2.1.1 12-Cylinder Engine Design Description

The engine will be a modified General Electric model 7FDL12, which is normally diesel-fired and rated at 3300 brake horsepower at 1050 rpm. It is a 4-stroke per cycle compression-ignition type engine of 45 degree bank angle, 9 inch cylinder bore and 10.5 inch piston stroke, having a 12.7:1 compression ratio. Some of the standard design features include: unitized cylinder assemblies using welded head-to-liners with four valves per head and external jackets having individual cooling water, intake air, and exhaust gas connections; 3-ring pistons using steel crowns and aluminum skirts on articulated connecting rods; a cast-iron main frame with internal oil passages; aftercooled free-wheeling turbocharger run from a constant-pressure exhaust manifold; hydraulic overspeed and speed control governors.

##### 2.1.1.1 Fuel Injection Systems

The coal-fired engine will be provided with dual fuel injection systems. One is a pilot system for diesel fuel, which will be used to start the engine and run it at lower power levels. The other is the main system for CWS fuel, which will be used only at the higher power levels. For Stage I locomotive testing, the pilot system will be mechanically linked to the main system. The pilot system should change to an electrically operated one for Stage II and later locomotive versions.

The pilot fuel system will be a modified version of the standard engine diesel fuel delivery system. This includes an electrically driven fuel transfer pump which is able to operate from battery power. It pumps the pilot fuel from the internally-baffled tank (standard locomotive tank) located under the locomotive platform, then through a large fuel filter with regulator and pressure relief valve, feeding parallel low-pressure lines to each cylinder bank. Jerk-type high-pressure fuel injections pumps will be specially mounted in the main frame sidecovers, directly cam-driven by an additional lobe per camshaft section, and connected by high pressure fuel lines to the individual pilot fuel injectors. Each pilot fuel injector is sleeve-mounted at the 9 o'clock posi-

tion on the cylinder head and sprays into the combustion chamber from the side. These special pilot fuel pump/injector combinations will be in addition to the CWS jerk-pump/diaphragm pump/injectors provided for each cylinder.

A special fuel rack linkage will be used to control the amount of both CWS and diesel fuel delivered to the cylinders. Refer to the engine Fuel Linkage Layout, drawing number 41D715542. The load control governor power piston will rotate two layshafts (one per cylinder bank) just as on a standard diesel engine. However, this layshaft rotation will control only the pilot (diesel) fuel delivery during the first half of its rotation, and only the main (CWS) fuel delivery during the second half. As previously stated, the pilot fuel will be used to start the engine and run it at lower power levels. Additionally, a second layshaft on each bank will be provided to allow small amounts of pilot fuel to be added to the cylinders, as deemed necessary, during CWS combustion (the second half of the primary layshaft rotation). This secondary layshaft will be rotated by electrically operated actuators, to allow manual control over this feature.

## 2.1.2 CWS Delivery System

The locomotive/tender fuel system includes a CWS storage tank, a recirculation pump, and flow-through heater, all located on the tender (Stage I only). Refer to the Hydraulic Schematic on drawing number 41D715526. A progressive cavity (Moyno) pump is used as a charge pump to pump CWS from the CWS tank to the diaphragm pumps on the diesel engine. Control valves located on the tender determine whether the CWS is just recirculated through the tank and heater on the tender, or also supplied to the charge pump on the locomotive. Control valves on the locomotive determine whether the CWS supplied to the charge pump is then recirculated back to the tender, or supplied to the engine for combustion. A thermostatically controlled water/CWS heater on the locomotive controls the temperature of the CWS supplied to the engine. A strainer is also located on the locomotive to filter any larger contaminants prior to supply of the CWS to the engine. Drain valves are located throughout the tender and locomotive to allow draining of the system.

### 2.1.2.1 CWS Charge Pump

A Moyno progressive-cavity pump has been selected as the engine CWS charge pump. This pump will supply up to 13 gpm at 400 psi to all the diaphragm pumps on the engine. The basis for selecting this pump is its ability to provide such a relatively high flow rate at the high pressure required to complete filling of the CWS injection pumps. A progressive-cavity pump is specifically designed for difficult pumping applications such that of the abrasive CWS slurry. A smaller Moyno progressive-cavity pump has been used in a similar application on the 2-cylinder combustion research engine in the General Electric Transportation Systems Engine Laboratory. The major disadvantage of the

Moyno pump is its great length, which requires it to be mounted on top of the locomotive fuel tank. No other location on the locomotive could accommodate its approximate 20 foot length.

The primary difficulty in pumping CWS fuel is that it is a non-Newtonian fluid (not constant viscosity). Neither is it a normally viscous fluid. The CWS fuels used to date exhibit a characteristic in which above a certain shear rate its viscosity rises very sharply. At the concentration of 50 percent coal (by weight) used, this occurs just above the range of maximum pumping shear rates. Consequently, unless local anomalies in the concentration of the CWS are totally avoided, this has a direct bearing on pump selection. Use of a progressive-cavity pump will provide capability to handle coal-water slurries having non-Newtonian characteristics.

Centrifugal pumps have a high ratio of peak to average velocities inside the pump casing, precluding their use except for very low concentrations of coal. Gear pumps have a pocket at the base of the gear tooth which can fill with coal particles and eventually lock the gears. In vane pumps, the shear rate at the tip of the vanes is high, but the vane motion avoids clogging. Lobe pumps have close clearances, both between lobes and the casing and between other lobes, which would seem to cause high shear rates. However, satisfactory operation has been observed at Otisca. This satisfactory operation may be due to its low rpm. A lobe type pump will be used for the multi-cylinder engine charge pump in the Engine Laboratory.

#### 2.1.2.2 Drain Valves

Drain valves will be provided at the low points in the CWS piping system. They will enable the piping to be drained when the locomotive will be shutdown for a long period of time, preventing the water from freezing in the pipes and equipment. The drain valves will also provide a back-up to the water purge capability, enabling the piping to be drained if the pipes cannot be purged for some reason. This is essential, since the CWS piping must be either purged or drained when the engine will remain unloaded for any length of time to prevent the coal particles from settling out of the slurry. The drain valves themselves will be of a type which will, as near as possible, provide no dead volume in which the coal particles might collect. Details of the drain valves are shown on drawings 41D715494 and 41D715559.

Two types of drain valves will be used on the locomotive and tender. The first type will simply be tees located in the piping, fitted with special drain plugs which extend up into the tee to the extent that they are relatively flush with the inside of the piping, to minimize the dead volume into which coal could settle during normal operation. If this were not done, removal of a standard pipe plug might not allow draining of the system if an accumulation of coal particles had solidified above the standard pipe plug.

The second type of drain valve which will be used is a General Electric design specifically for use with the CWS. The basis for its design is to provide zero dead volume for coal to settle in. In addition, it provides a smooth surface for normal flow of the CWS. Refer to drawing 41D715559 for details of the valve.

#### 2.1.2.3 CWS Control Valves

Full port ball valves were selected for use as control valves throughout the system because of their wide-open flow path, with no trapped volume for coal to settle into. The design of the valves allows the valve ball and seals to be removed as a cartridge, without disturbing the piping. This will simplify any maintenance needed. Stainless steel was specified for both the ball and the seat.

Double-acting air actuators will be used to operate the valves.

#### 2.1.2.4 Piping

The CWS piping will require measures to prevent corrosion, since the base liquid for the coal slurry is water. The most expedient solution is to use anti-corrosive steel pipe, since steel pipe is presently used on production locomotives for both cooling water and lubricating oil. Consequently, hot-dip galvanized steel pipe will be used for the majority of the Stage I CWS piping. However, the piping in the immediate area of the flow control valves on the locomotive will be stainless steel. This more expensive anti-corrosive steel will be used because this area of the CWS piping system is not expected to be changed between Stage I and Stages II or III. The use of both stainless and galvanized steel pipe will allow us to gain experience with both throughout the program.

#### 2.1.2.5 Pipe Couplings

The pipe couplings used for the CWS piping for the Stage I locomotive and tender have been specified as Victaulic-type end-groove style couplings. Refer to Figure 1 in the appendages for details of Victaulic-type couplings. The technical justification for their selection is threefold. First, GE Transportation Systems presently uses Victaulic brand end-groove style couplings successfully for both cooling water and lubricating oil piping on production locomotives. Our operating experience with them has been good.

Second, Victaulic has a seal for their couplings which will allow them to act virtually as a continuation of the pipe wall. The seal fills the gap between the two mating pipes, eliminating any dead volume. This may prove to be beneficial in handling a non-Newtonian fluid such as the CWS.

Lastly, Victaulic style couplings will allow us to pipe the locomotive much faster and easier than other couplings or joining methods. This is important, in that the piping must be routed around existing cabling, equipment, and structures on the locomotive. They also are reusable, and allow quick, easy disassembly, which will be beneficial not only during the changes between the three stages of construction, but may be helpful at times during testing. They will expedite changes and disassembly for cleaning of pipe or equipment.

#### **2.1.2.6 CWS Heater**

A tube-in-shell heat exchanger was selected for heating of the CWS on the locomotive, using the engines cooling water as the source of heat. The construction of the heat exchanger is very similar to that of the one used on production GE locomotives for heating the diesel fuel. The CWS flows on the tube side because the coal would settle out in non-turbulent areas if it were to flow through the shell side. The heat exchanger is designed to raise the CWS temperature 40 degrees-F at a flow rate of 18 gpm, with engine water of 150 degrees-F. Actual flow through the heater will be approximately 13 gpm at most. The engine cooling water is approximately 150 degrees-F at idle, and 180 to 210 degrees-F when operating under load. The temperature of the CWS will be controlled thermostatically. Based on our experience to date in the Engine Laboratory, an operating temperature of approximately 80 degrees-F has been chosen. At CWS temperatures above 80, the engine cooling water will bypass the heat exchanger. The thermostatic control valve has not yet been selected, but will be similar in nature to the AMOT valve used on production GE locomotives. The heat exchanger will be located under the locomotive platform, just behind the CWS charge pump. Refer to drawings 41E914186 and 41E914188.

#### **2.1.2.7 Back-Pressure Orifice**

An orifice is used in the CWS supply header to the engine to provide sufficient back-pressure to allow supply of the CWS to the engine at approximately 400 psi. At full load, the engine will burn approximately 5 gpm of CWS. At this flow rate, it has been calculated that an orifice size of 0.5 inches in diameter will provide the desired 400 psi pressure. A pressure transducer located upstream of the orifice will be used to control the charge pump speed to maintain 400 psi. Excess flow through the orifice will provide recirculation to maintain the coal in suspension.

#### **2.1.2.8 CWS Strainer**

A filtration strainer will be used to remove solid particles larger than fuel injection and control orifices. This strainer will have a removable stainless steel wire mesh basket, capable of passing all particles 0.030 inches

in diameter and smaller. It will be located on the pressure side of the CWS engine charge pump, easily accessible for cleaning.

### **2.1.3 Lubricating Oil Centrifugal Filter**

The standard engine lubrication system utilizes a single engine-driven helical gear pump in tandem with a pressure relief valve. Lubricating oil is supplied from the engine sump through a strainer to the suction side of the pump. It is then pumped through a large tube-in-shell heat exchanger, where it is cooled by the engine cooling water, and then filtered in a large paper element filter housing. The lubricating oil is then distributed throughout the engine from an oil gallery cast in the main frame, and then through drilled passages.

To remove the additional contaminants caused by the combustion of coal, a bypass centrifugal filtration system is being added to the system described above. The larger particles from the oil will be filtered by the ten, standard paper element filters. The centrifugal filter will be used to further clean the lubricating oil, bypassing the paper element filter housing, and then returning to the engine crankcase after cleaning. Approximately 10 percent of the total lubricating oil flow will pass through the centrifugal filter. The centrifugal filter is driven by the high-pressure oil supplied to it (approximately 100 psi at full engine speed).

### **2.1.4 Modifications Necessary to GE 607**

It is necessary to make a number of modifications to the locomotive (GE 607) to accommodate conversion to a coal-fired locomotive. Refer to drawing 41E914186 for details of the modifications.

#### **2.1.4.1 Engine Mounting**

GE 607 was originally designed and built with a GE 16 cylinder engine. To provide sufficient room on the locomotive for the CWS handling equipment, especially for Stages II and III, the engine has been changed from a 16 cylinder to a 12 cylinder. This was done by keeping the location of the rear of the engine in its original position, and shifting the front of the engine and alternator rearward 32 inches. This created sufficient room forward of the alternator of the necessary equipment. After removal of the 16 cyl. engine, the forward two engine supports were removed, and new ones were welded in place 32 inches rearward. This also included the addition of a bulkhead inside the platform, between the new supports, to provide the necessary strength to support the engine.

#### 2.1.4.2 Blower Cab

To provide additional equipment room over the alternator, the traction motor blower and alternator blower package was shifted forward on the blower cab. A new cab was then fabricated to fit over the alternator. Incorporated into this new cab is a full width platform, which will provide a location for mounting the air-operated control valves which are used on the locomotive. The platform is equipped with a drip-pan and drain to catch any potential CWS leaks from the valves and piping. Refer to drawing number 41E914189.

Because of the relocation of the traction motor and alternator blowers, it was necessary to fabricate a new alternator air duct (connecting the blower to the alternator) and modify the traction motor air duct. Refer to drawing number 41D715501 and 41D715502 for construction details.

Relocation of the alternator rearward by 32 inches results in the need to re-route the cables from the locomotive to the alternator. They are being re-routed to the other side of the locomotive to allow the use of a full height doorway into the new CWS equipment area. Because it was not previously necessary to provide easy access to this area before, these cables were previously located at a height of about 4 feet.

#### 2.1.4.3 Traction Motor Cables

The traction motor cables have been raised approximately 8 inches to provide the necessary height over the fuel tank for the charge pump. Because of its extreme length (approximately 20 feet), the only acceptable location for the engine charge pump is on top of the locomotive fuel tank. As originally built, there was not sufficient height to allow installation of the pump over the fuel tank.

#### 2.1.4.4 Air Compressor

The air compressor on a locomotive is used to charge the train air brake lines and provide air for locomotive air brake equipment and pneumatically controlled devices. The original three cylinder air compressor on GE 607 was shaft-driven off the free-end of the diesel engine. The shaft and couplings used were specifically designed to provide the necessary torsional stiffness to allow satisfactory operation of the air compressor with the 16 cylinder engine. The change to a 12 cylinder engine would necessitate changing the driveshaft and couplings to those providing the necessary torsional stiffness for use with a 12 cylinder engine. For the Stage III locomotive, installation of the emission control equipment will necessitate lengthening of the locomotive platform, and relocation of the equipment rearward of the engine. This would involve relocation of the air compressor, which, if shaft-driven, would be either diffi-

cult or impossible. For this reason, it has been decided to replace the present shaft-driven air compressor with a motor-driven one as is currently used on current DASH 8 locomotives. This will allow locating the air compressor without concern for the ability to drive it with a shaft. Making the change at this time will eliminate the need to replace the drive shaft and couplings.

The new air compressor will be driven by a special dual winding 6/12-pole AC electric motor. This motor allows the air compressor to run about twice engine speed during no-load and low power levels (6-pole operation). When the engine speed increases, the motor becomes a 12-pole machine, running at about the same speed as the engine. The use of a motor driven air compressor also reduces the locomotives' auxiliary losses by not rotating the compressor when it is not needed. A shaft-driven compressor is driven at all times.

Conversion to a motor-driven air compressor necessitates the addition of a electrical control box for control of the drive motor.

## 2.2 Description of Fuel Tender Car

A railroad flatcar serves as the mounting base for the CWS tank, heater, recirculating pump, purge water tanks, and purge water pump for Stage I. It will serve as a test bed for the development of CWS handling techniques which will be incorporated into the Stage II locomotive. It will provide the room and flexibility needed to allow experimentation with CWS tank design and recirculation techniques. The electrical control cabinet for system control is located on the tender car (Stage I only). The types of valves, piping, and couplings are the same as those defined for the locomotive. An engine-generator set is located on the tender car to provide AC power for the pumps and electrical controls. The location of equipment is shown on 41E914197, and the piping layout is shown on 41E914191.

### 2.2.1 CWS Tank

The CWS tank is a one quarter segment of a full size 4000 gallon locomotive fuel tank. This was done to minimize problems when scaling it up to locomotive size for Stage II. The main stiffeners and load carrying members are placed outside of the tank. Consequently, all baffles are stress-free and replaceable. Various cutouts between the six compartments will be tested by measuring concentration of the coal in each of the compartments.

The tank is designed to allow testing of three methods of maintaining the coal in suspension in the CWS:

Recirculation  
Bubbling of compressed air in the CWS  
Stirrers

When the baffles are removed, it is possible to exchange the recirculating and compressed air tubes. This exchange will be required if the preliminary location and sizes of the holes in the recirculating tubes are not satisfactory. The fuel inlet mechanism will be incorporated into one compartment of the tank.

#### 2.2.1.1 CWS Tank Construction

The tank walls are made of 0.1875 inch thick mild steel plate. All stiffeners are external. Both sides of the tank are fitted with raised walkways to allow easy access and inspection of the tank. It is equipped with handrails on both sides for safety. Two, removable covers allow access to the top of the tank for observation and modification. The internal baffles can be removed through these covers. Each of the two covers is equipped with three, 4 inch diameter inspection holes, with covers, to allow a quick check to be made into each of the tank's six compartments. Refer to drawing number 41E914098 for details of the tank.

The tanks four transverse baffles are removable, and are made of aluminum to allow modification of hole sizes and locations without concern for corrosion. They will be tested in many configurations including completely blanked off and completely open.

The recirculating tubes consist of a longitudinal placed 2 inch I.D. pipe each running through three of the tanks compartments. Each of the tubes has drilled holes spaced 4 inches apart, at angles between 10 and 30 degrees, to discharge the CWS towards the bottom of the tank.

One of the compartments is fitted with a suction line to supply the CWS to the recirculation pump. It is intended that the CWS be drawn off the top of liquid level in the tank. In the event the coal settles to the bottom during a period of non-recirculation, the pump would be able to draw water off the top, discharging it into the bottom of the tank and providing the necessary action to re-disperse the coal.

The inside of the tank will be epoxy coated to prevent corrosion. The outside will initially be painted, and perhaps insulated at a later time to reduce heat loss during cold weather operation.

#### 2.2.2 Purge Water Tanks

A clean purge water tank and a dirty purge water tank will be located on the tender. During periods of inoperation, the CWS must be purged from the systems. One tank provides a source of clean water for the purging, while the other tank provides a place to store the dirty purge water. Both tanks are

fabricated steel, epoxy coated on the inside for corrosion protection. Refer to drawing number 41D715481 for details of these tanks.

#### **2.2.3 Purge Water Pump**

A motor-driven centrifugal pump having a 10 gpm capacity at 50 psi is used to pump the purge water.

#### **2.2.4 CWS Recirculation Pump**

A motor-driven lobe type pump having a capacity of 100 gpm at 50 psi is used to recirculate the CWS. Its speed will be varied to determine the optimum recirculation rate for the CWS.

#### **2.2.5 CWS Electric Heater**

An electric circulation heater will be used in the CWS fuel storage tank recirculation line to prevent freezing of the CWS during low ambient temperatures. This heater is a pass-through type, with several individual elements, allowing the CWS flow to be thoroughly heated. The electric heater is sized to make maximum use of the heat added by the recirculation pump. It will be located between the pressure side of the recirculation pump and the pipe branch-off for transferring CWS to the locomotive, permitting heating of the total CWS flow through the recirculation pump.

#### **2.2.6 Engine Generator Set**

A diesel engine driven generator set will be located on the CWS tender to provide power for pumps and controls. Details are given in the electrical section.

### **2.3 Electrical System**

The electrical system provides the necessary control and sequencing logic for operation of the CWS and purge water systems in their various modes of operation. All pumps and the electric heater are 220 VAC.

### 2.3.1 Power Sources

The fuel tender will require AC power as follows:

CWS Heater.....	220VAC, 3-phase
Recirculation pump.....	220VAC, 3-phase
Engine Charge pump.....	220VAC, 3-phase
Purge Pump.....	220VAC, 1-phase
Instrumentation.....	110VAC, 1-phase

Power will be supplied initially from the Locomotive Test building, and then later by a portable diesel-powered source mounted on the tender car.

### 2.3.2 DC Control System

The electrical control system schematics for CWS control are shown on sketches GRC-890106C (sheets 1-3) and GRC-881222K (sheets 1-5). The CWS hydraulic schematic is shown on sketch 41D715526. Main control is through a selector switch with the following 6 positions:

- [1] Startup/Shutdown
- [2] Charge Recirculation System
- [3] Charge Engine
- [4] Run
- [5] Purge Engine
- [6] Standby

#### 2.3.2.1 Start

The cycle begins in the Startup position. Circuit breakers CB1,2, and 4 are open and no pumps are running. Note that Start and Shutdown are the same switch position except that in Start the lockout relay (LOR) is dropped out to prevent initiation of a purge cycle when the circuit breakers are first closed. The circuit breakers are then closed.

#### 2.3.2.2 Charge Recirculation

Moving the switch to position [2] picks up relay RECR to start the recirculation pump and closes valves V4, V8, and V10 to initiate the charging of the recirculation lines. Purge water is cleared from the recirculation lines by pumping CWS from the CWS tank through the valves V4, V8, and V10. When all purge water has been pushed into the dirty water tank, time delay relay TD20 picks up. V10 is opened and V9 is closed to re-route the slurry back into the CWS tank. Picking up TD20 also latches in relay RCCR to indicate

that the recirculation lines are fully charged. The pump continues recirculating CWS from the tank through the electric heater and the CWS heat exchanger on the locomotive. Pump speed is controlled by an inverter drive control. The pump may be shut off manually, if required by opening switch RPSD.

#### 2.3.2.3 Charge Engine

Moving to position [3] picks up ECR1 to start the engine charge pump at slow speed. A second inverter drive control is used to regulate engine charge pump speed. Valve V4 is opened and valves V2 and V5 are closed to pump CWS to the engine charge pump. The charge pump then pumps the CWS through the engine pushing purge water through V2 and into the dirty water tank. Valve V4 is opened to preclude starving the charge pump.

When all the purge water has been pushed into the dirty water tank, TD30 picks up to open V2 and close V3. This re-routes CWS from the engine back to the CWS tank where it is recirculated. Picking up TD30 also latches in relay ECCR to indicate the engine is fully charged.

#### 2.3.2.4 Run

Moving to position [4] picks up ECR4 to run the engine charge pump at high speed to run the engine. Note that both RCCR and ECCR must be picked up in order to pick up ECR4. Feedback from pressure transducer PT1 mounted near the orifice is used to control pump speed to maintain a CWS pressure of 400 psi at the engine.

#### 2.3.2.5 Purge Engine

Moving to position [5] drops out ECR4 to return the engine charge pump to low speed and picks up relay PURP to start the purge pump. Valves V2 and V6 are closed, and V3 and V5 are opened. This routes water from the clean water tank through the engine to the dirty water tank. CWS in the engine will be pushed through V2 into the dirty water tank. Valve V4 is also closed to resume recirculating the CWS through the heat exchanger. When the engine purge is complete, TD52 picks up to stop the purge and charge pumps and to open valves V2 and V6. Note that the EPR relay is picked up at the start of the engine purge cycle causing ECCR to drop out. This prevents running the engine until another full engine charge cycle has been completed.

### 2.3.2.6 Stand By

Moving to position [6] puts the system in a standby mode. The recirculation pump continues to recirculate CWS through the heaters while the engine idles on diesel fuel. It is possible to move directly from Run to Standby without initiating an engine shutdown sequence by holding the engine purge bypass switch (EPBS) open while moving from [4] to [2]. This is useful when a temporary engine shutdown is desired. In this case EPRB must also be held open when moving from [6] back to [4].

### 2.3.2.7 Shutdown

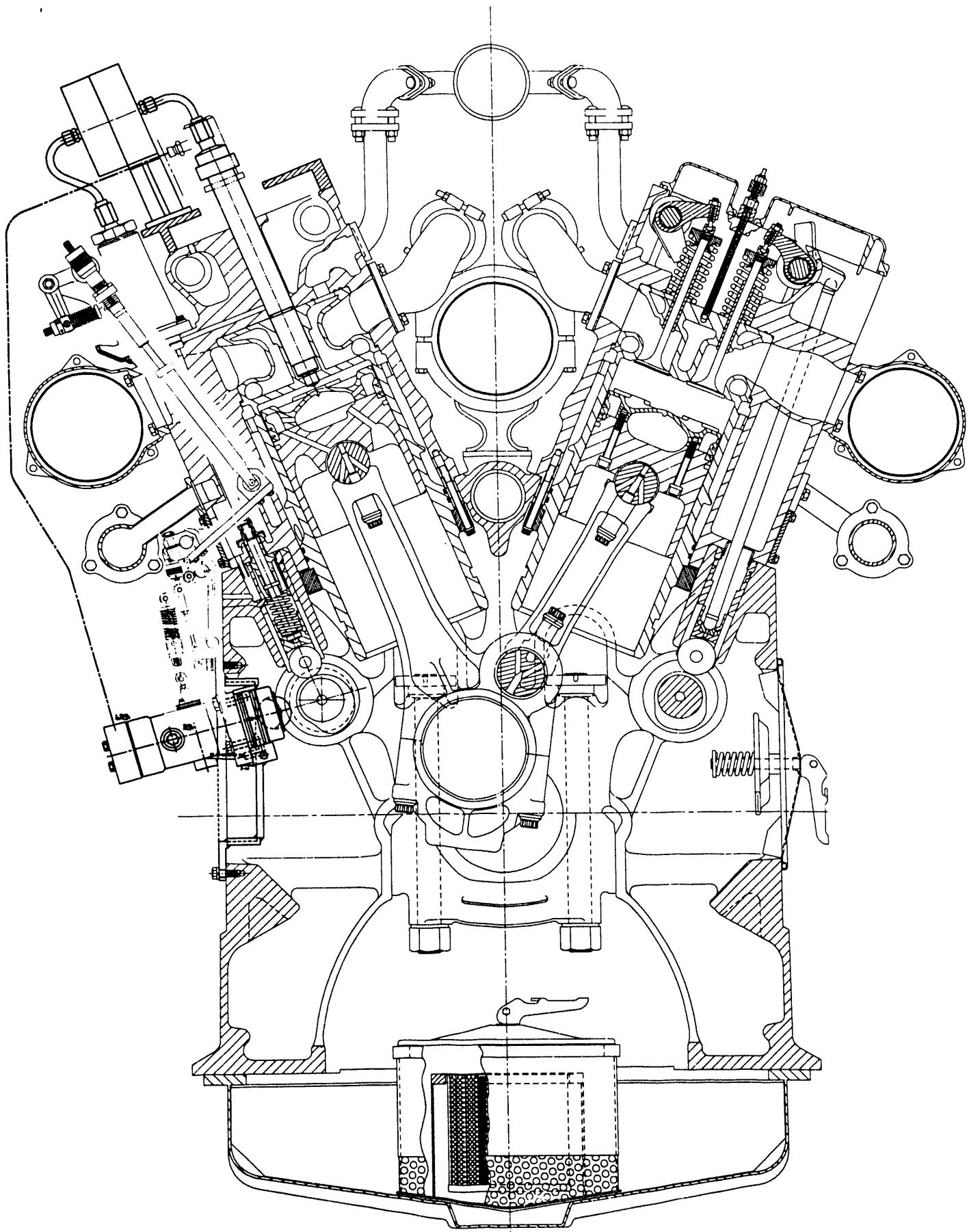
Moving to position [1] with LOR picked up initiates the shutdown sequence. The purge pump is re-started while valve V7 is closed and valve V8 is opened. This pumps water from the clean water tank through the recirculation lines. Prior to complete purging of the CWS, TD11 picks up to open V9 and close V10. This is done to route the purge water into the dirty water tank and not into the CWS tank. When all lines have been purged, TD12 picks up to stop the purge pump and open V4, V7, and V10. The shutdown cycle is now complete. Note that the relay RPR is picked up at the start of the purge cycle causing RCCR to drop out. This prevents running the engine until another full recirculation line charge cycle has been completed. Removing DC power will allow the LOR relay to drop out to avoid another purge cycle on re-start.

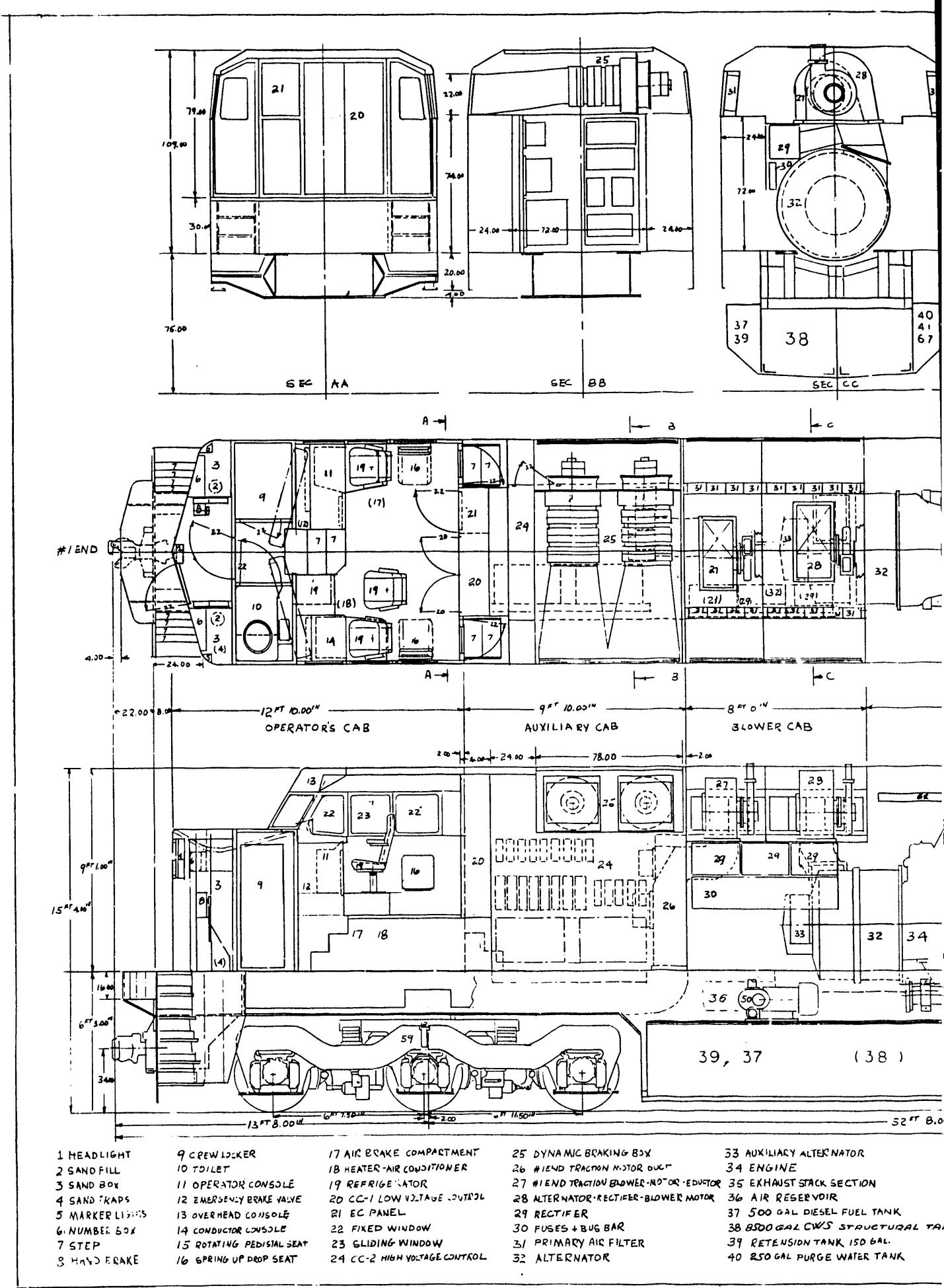
### 2.3.3 Status Indicators

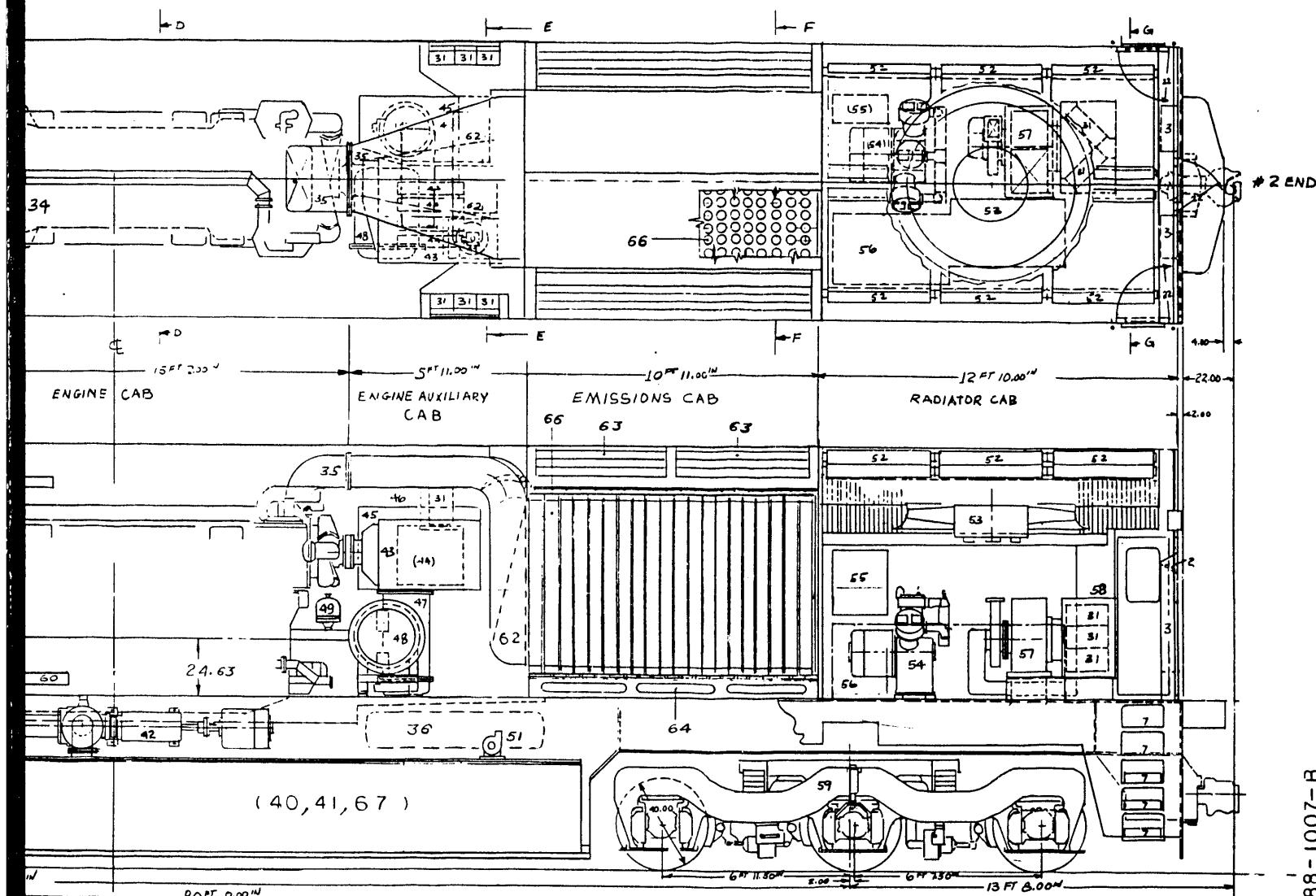
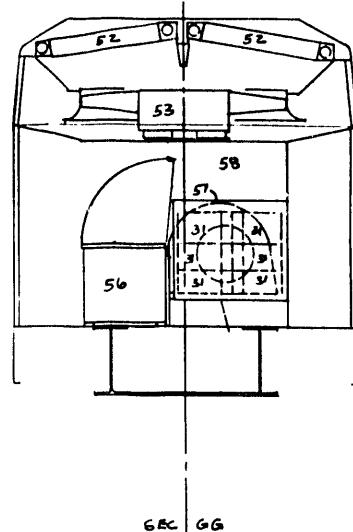
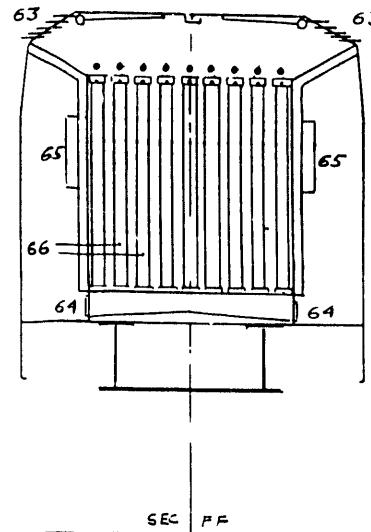
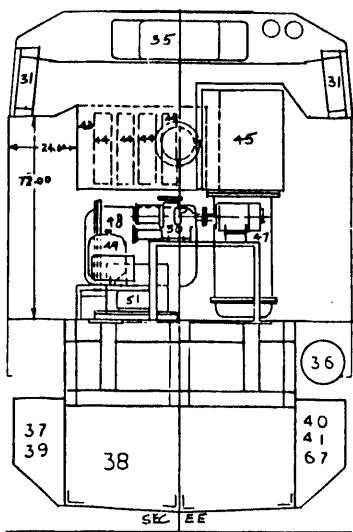
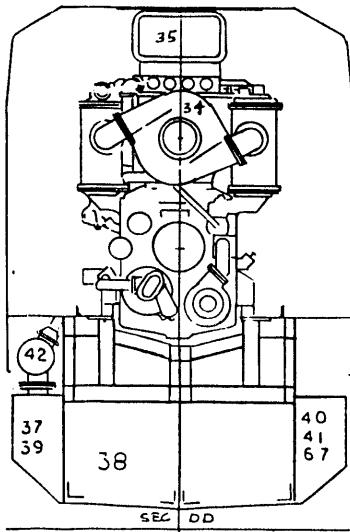
Control Status is displayed by status lamps mounted on the door of the fuel tender control box, as shown on sketch CRC-890106C, sheet 3. Indicator lights are used to show the following:

- Shutdown Complete
- Recirculation Charge Complete
- Engine Charge Complete
- Running
- Engine Purge Complete
- Standby
- V10 Closed
- AC Power
- DC Power (Wayside)
- DC Power (Locomotive)
- Water Heater
- Recirculating Pump Running
- Purge Pump Running
- Charge Pump Running
- Charge Pump Running Hi Speed
- Full Pressure at Orifice

Control Air  
V3 Closed  
V4 Closed  
V5 Closed  
V8 Closed  
V9 Closed  
Purging Engine  
Purging Recirculation Lines  
V6 Closed  
V7 Closed  
V2 Closed







- 41 250 GAL WASTE/URGE WATER TANK
- 42 MYNO PUMB-MOTOR
- 43 ENGINE AIR FILTER COMPARTMENT
- 44 SECONDARY FILTER
- 45 ENGINE WATER TANK
- 46 FLOW CONTROL VALVE
- 47 LUBE OIL COOLER
- 48 LUBE OIL FILTER

49 LUBE-OIL CENTRIFUGE  
 50 TUTHILL LOBE PUMP - MOTOR  
 51 PURGE WATER PUMP - MOTOR  
 52 RADIATOR  
 53 RADIATOR FAN - MOTOR  
 54 AIR COMPRESSOR - MOTOR  
 55 AIR COMPRESSOR CONTROL  
 56 BATTERY BOX

57 #2 END TRACTION BLOWER-MOTOR-EDUCTOR	66
58 #2 END TRACTION FILTER- DUCT	67
59 'C' 3 MOTOR TRUCK	
60 CWS HEAT EXCHANGER	
61 HYDRAULIC CONTROL UNIT	
62 DIFFUSOR INLET	
63 AUTOMATIC LOUVERS	
64 PARTICULATE VACUUM EXTRACTION	
65 INSPECTION HATCHES	

66 STAINLESS STEEL BAG FILTERS  
67 500 GAL. SORBENT TANK

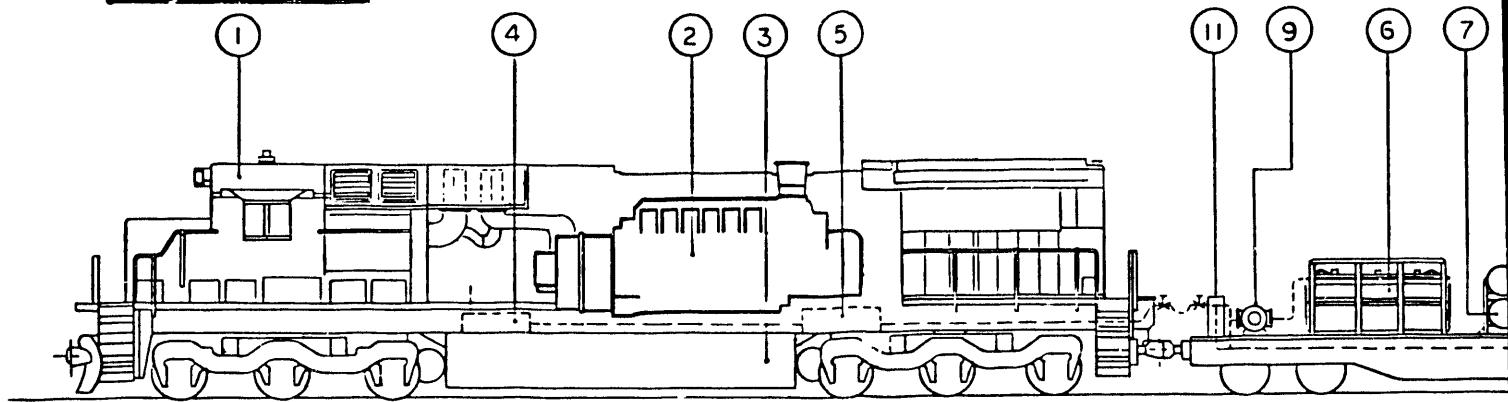
SCALE 3/8 = 10'

4000 HP CWS FUELED CONCEPT  
LOCOMOTIVE — PRELIMINARY  
LOCATION OF APPARATUS

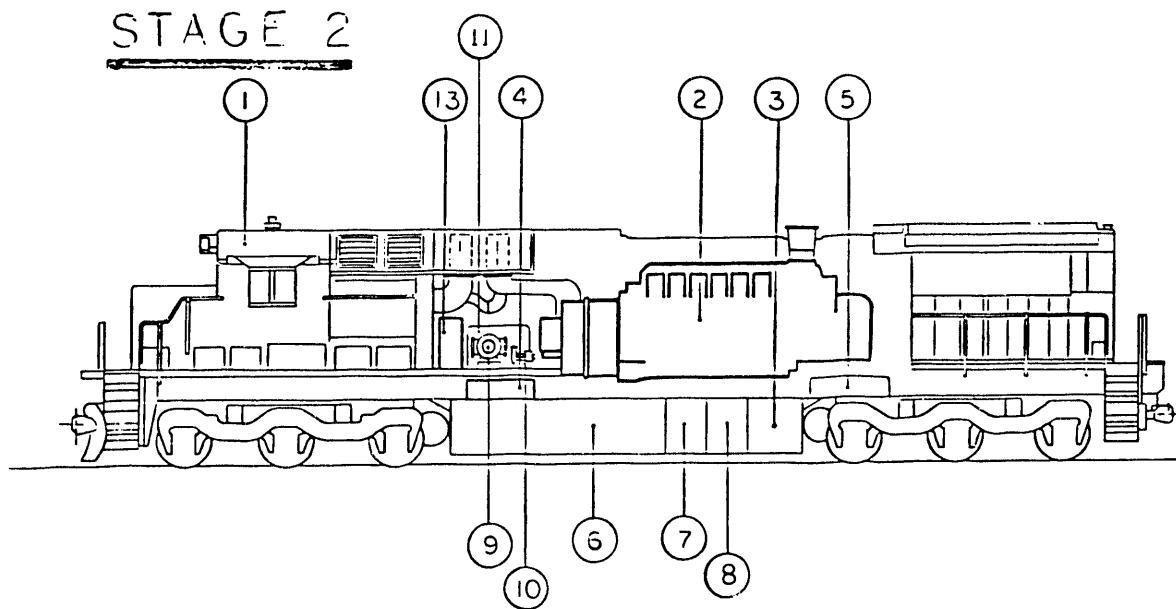
LOCATION OF APPARATUS		
MASSIE	J.R. CHAM so add name //, V/V = B	41D715543
ISSUED (C) 10/7/88		
ISSUED (UNC) 10/7/88		

SK-1988-1007-B

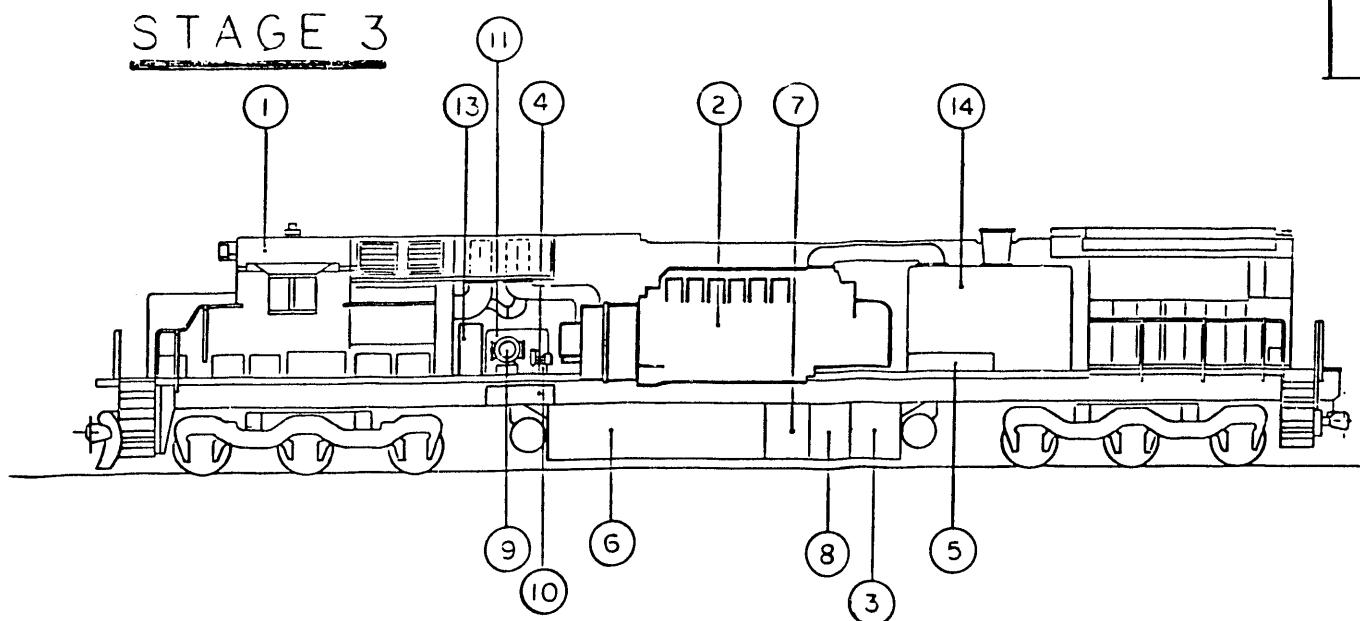
## STAGE I

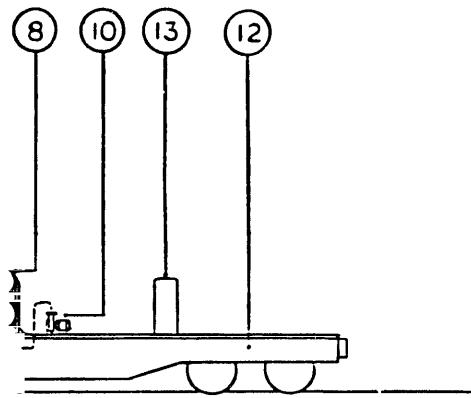


## STAGE 2

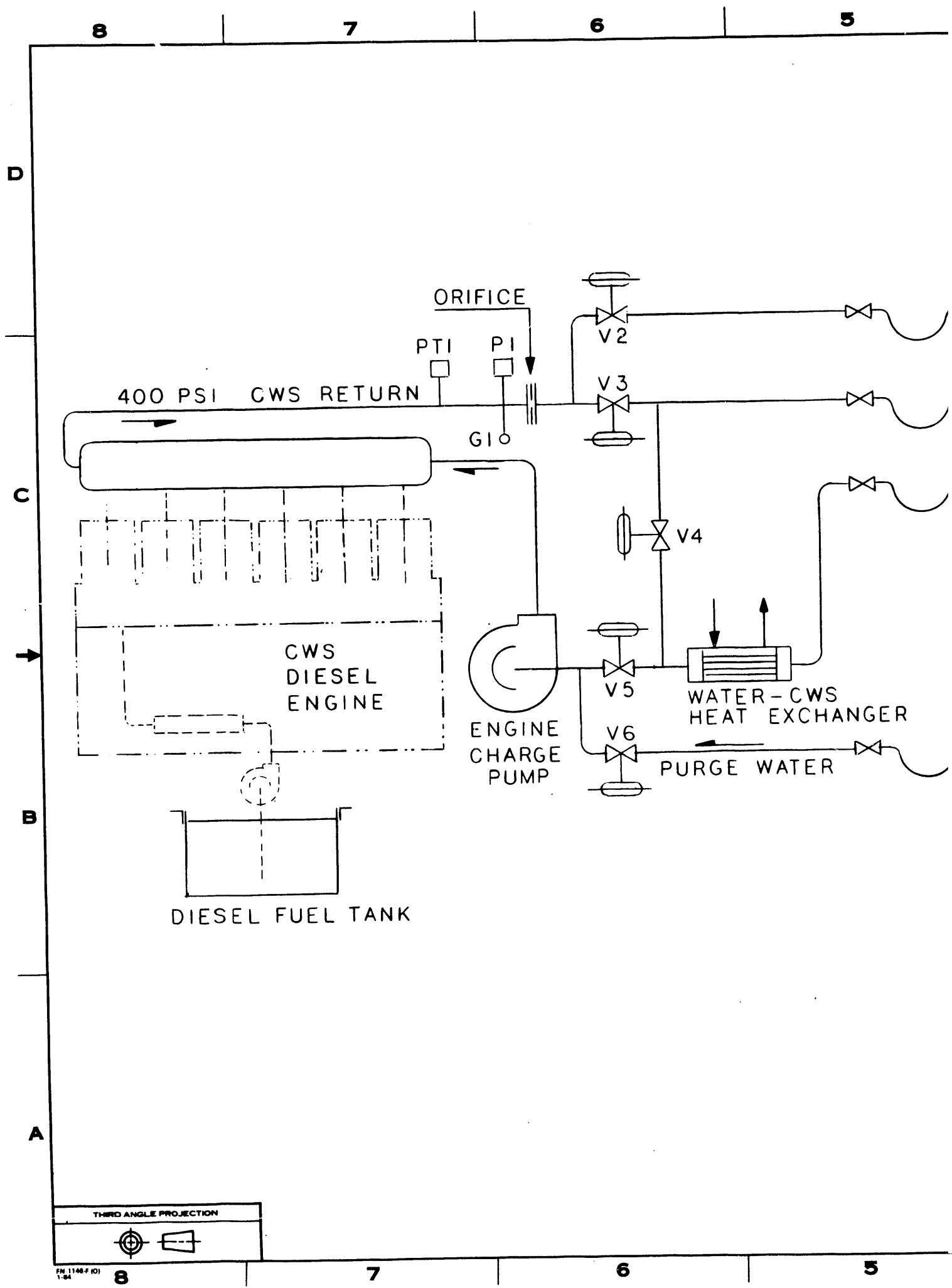


## STAGE 3





CONTROL		
CONTROLS		
HEATER & THERMOSTAT		
LARGE PUMP		
COOLING PUMP		
WATER TANK		
WATER TANK		
EXTRIMENTAL FUEL TANK		
SHEAT EXCHANGER		
LARGE PUMP		
FUEL TANK		
DIESEL ENGINE		
407 LOCOMOTIVE		
INITIALS	DATE	
GENERAL ELECTRIC		
CWS DIESEL LOCOMOTIVE STAGES 1,2 & 3		
SCALE	PILOT NO.	410715472
SCALE	PILOT NO.	410715472

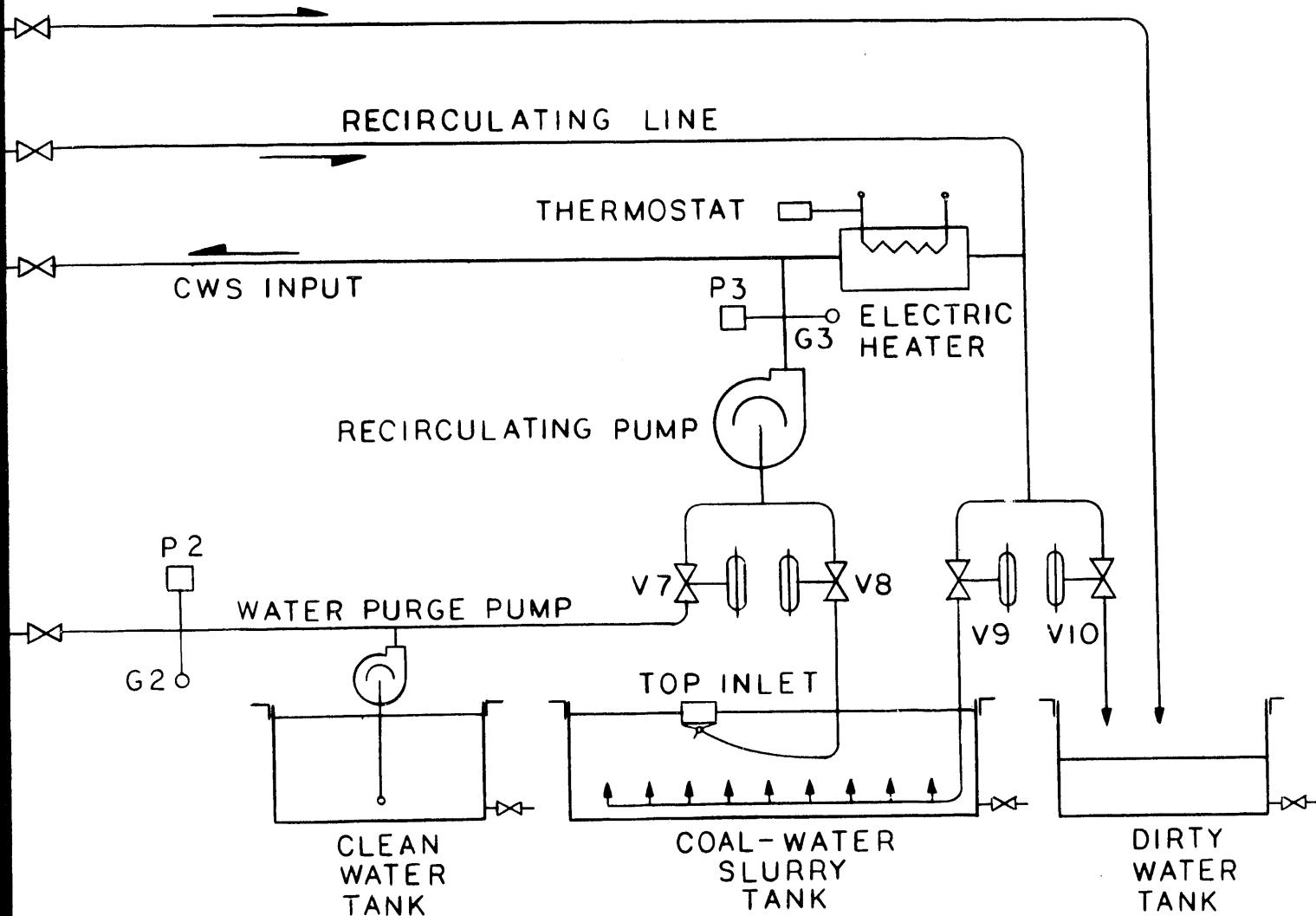


1

1

1

1



UNLESS OTHERWISE SPECIFIED		SIGNATURES	DATE
DIMENSIONS ARE IN INCHES		DRAWN	S.L.O. 3,2089
TOLERANCES ON:		CHECKED	
2 PL. DECIMALS $\pm$		SHIPPED	
3 PL. DECIMALS $\pm$		ISSUED	
ANGLES $\pm$			
FRACTIONS $\pm$			

**GENERAL ELECTRIC**  
DEPT. LOC.

**COAL-WATER SLURRY  
DIESEL ENGINE  
HYDRAULIC SCHEMATIC**

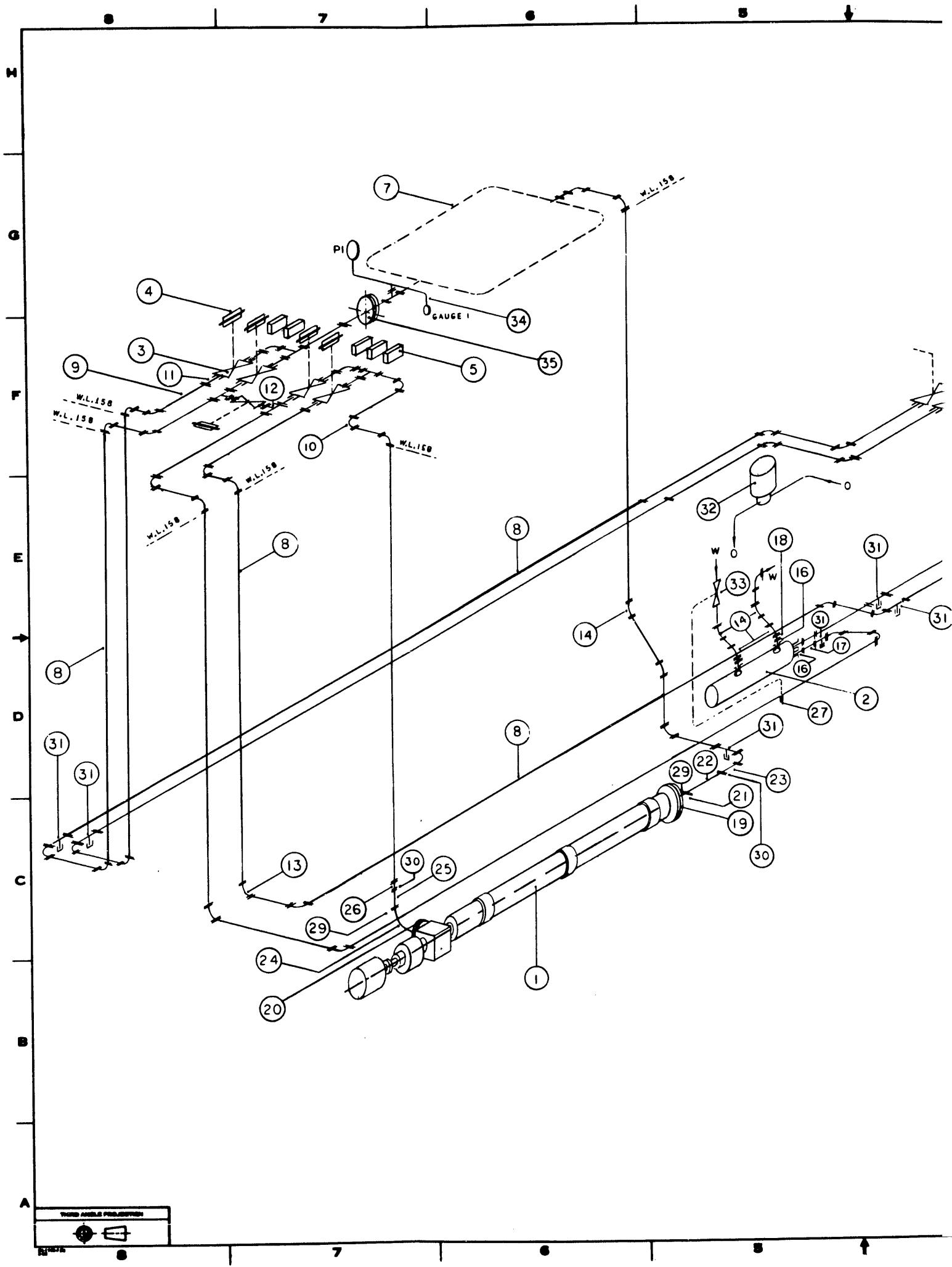
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4

3

2

1



REVERSE			
ITEM	DESCRIPTION	DATE	APPROVAL

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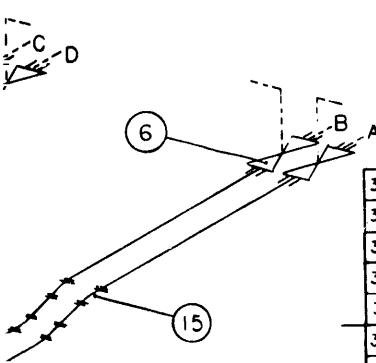
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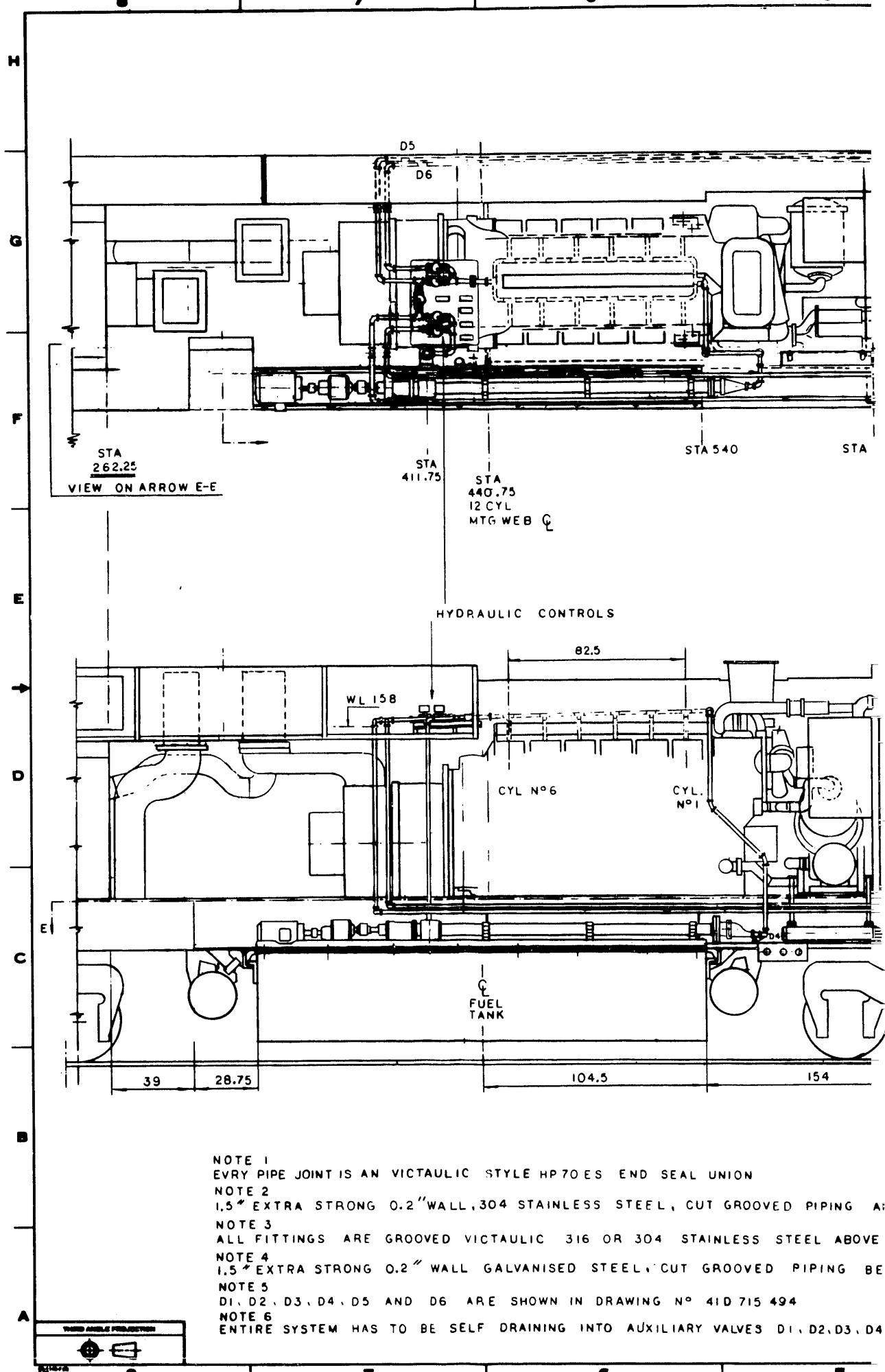
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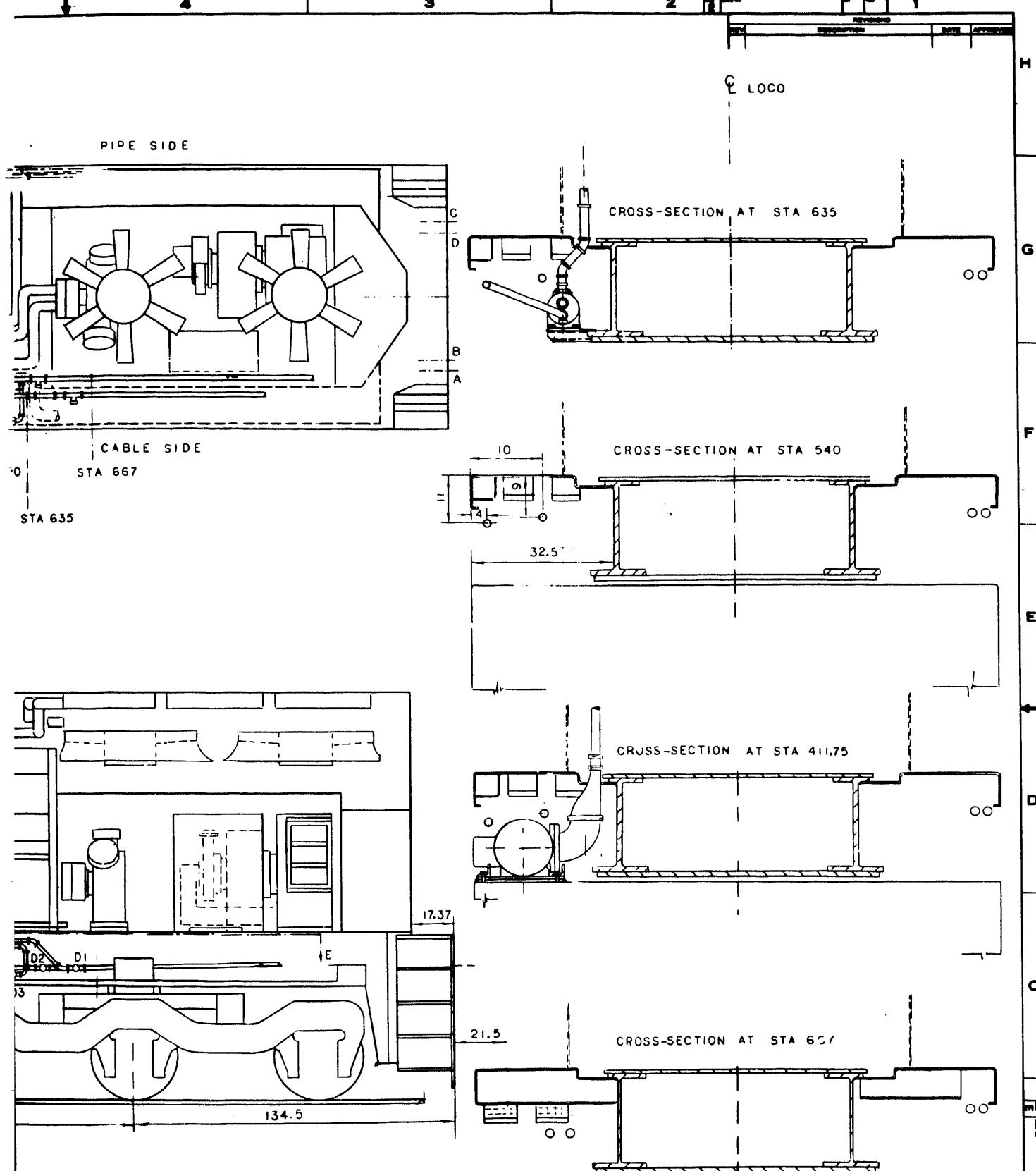
1

10



35	1	TUBE LINE	ORIFICE FLANGES 1.5" WELDING NECK 300 LB
34	1	RED VALVE COMPANY	PRESSURE SWITCH AND GAUGE COMBINATION
33	1		1.5" THERMOSTATIC VALVE
32	1	SPINNER II	OIL CLEANING CENTRIFUGE MODEL 600
31	6	GENERAL ELECTRIC	DRAWING N° 410 715 494
30	2	VICTAULIC COMPANY OF AMERICA	2" STYLE HP 70 ES END SEAL COUPLING H.D.G.
29	2	— II —	6" STYLE HP 70 ES END SEAL COUPLING H.D.G.
28	131	— II —	1.5" STYLE HP 70 ES END SEAL COUPLING H.D.G.
27	1	— II —	VIC-O-WELL STYLE 924
26	1	— II —	2" x 1.5" CONCENTRIC REDUCER N° 50
25	1	— II —	6" x 2" ECCENTRIC REDUCER N° 51 H.D.G.
24	1	— II —	6" 90° ELBOW N° 10 H.D.G.
23	1	— II —	2" x 1.5" ECCENTRIC REDUCER N° 51 H.D.G.
22	1	— II —	6" x 2" ECCENTRIC REDUCER N° 51 H.D.G.
21	1	— II —	5" x 6" CONCENTRIC REDUCER N° 50 (DIVERGING) H.D.G.
20	1	— II —	6" STYLE 742 VIC FLANGE ADAPTER 125 LB H.D.G.
19	1	— II —	5" STYLE 743 VIC FLANGE ADAPTER 300 LB H.D.G.
19	2	— II —	2" x 1.5" CONCENTRIC REDUCER N° 50 H.D.G.
17	2	— II —	2" x 1.5" ECCENTRIC REDUCER N° 51 H.D.G.
16	4	— II —	2" THREADED ADAPTER NIPPLE N° 40 H.D.G.
15	4	— II —	1.5" 22° ELBOW N° 12 H.D.G.
14	6	— II —	1.5" 45° ELBOW N° 11 H.D.G.
13	22	— II —	1.5" 90° ELBOW N° 10 HOT-DIP GALVANISED (H.D.G.)
12	4	— II —	1.5" TEE N° 20 SST 304, OR, 314
11	10	— II —	1.5" THREADED ADAPTER NIPPLE N° 40 SST 304 OR 316
10	15	— II —	1.5" 90° ELBOW N° 10, SST 304 OR 316
9	20	— II —	1.5" I.D. 0.2" WALL STAINLESS STEEL TUBE ABOVE W.L. 158 FT
8	250	— II —	1.5" I.D. 0.2" WALL GALVANIZED STEEL TUBE BELOW W.L. 158 FT CUT GROOVED
7	1	GENERAL ELECTRIC	DIESEL ENGINE FUEL DISTRIBUTION LINKAGE
6	4	JAMESBURY Co	1.5" FULL PORT SERIES 4000 BALL VALVE
5	5	MAC VALVES INC	SOLENOID VALVE MAC 82 INDIVIDUAL BASE
4	5	JAMESBURY Co	DOUBLE ACTING PNEUMATIC VANE ACTUATOR 105-1
3	5	— II —	1.5" FULL PORT SERIES 4000 BALL VALVE
2	1	YOUNG	WATER CWS HEAT EXCHANGER 804-ER-2P-CNTB PART NUMBER 287 982
1	1	ROBBINS MYERS	MOYNO PUMP DWG 385 039480
ITEM	QTY	VENDOR	DESCRIPTION





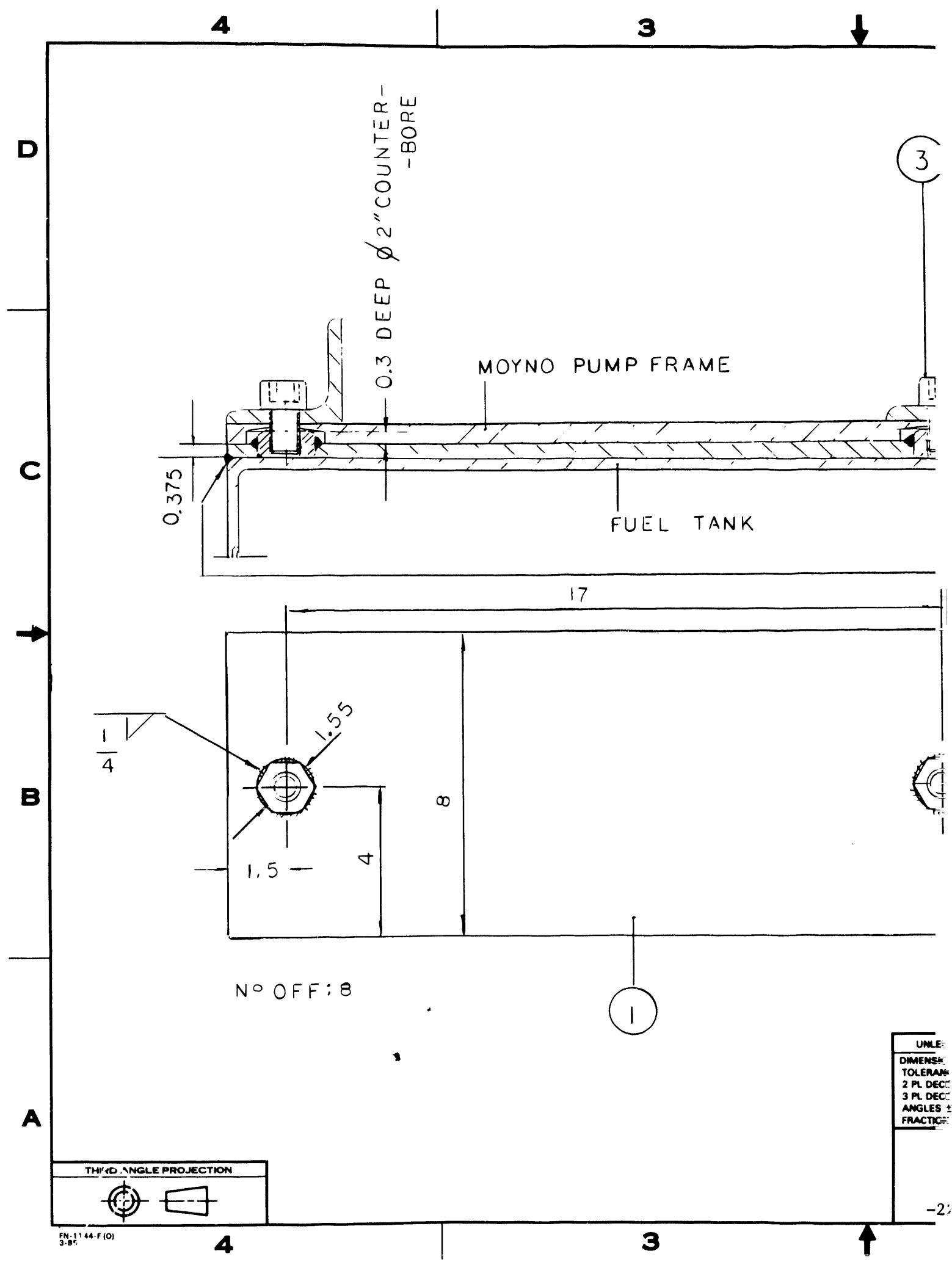
OVE W.L. 158

W.L. 158 AND GALVANISED BELOW W.L. 158

DW W.L. 158

D5 AND D6

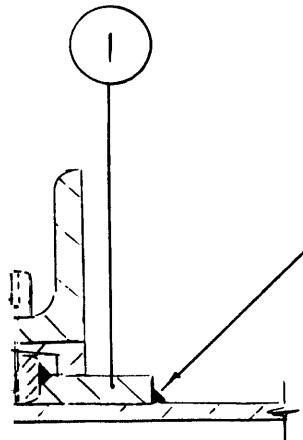
UNLESS OTHERWISE SPECIFIED EQUIPMENT IS IN STORES TELEGRAMS ON 2 FL. INSTRUMENTS 3 FL. INSTRUMENTS ADDITIONAL FRACTIONAL ✓	SIGNATURES SLO	DATE 10/27/65	<b>GENERAL ELECTRIC</b> CWS FUELED LOCOMOTIVE MODIFIED 607 STAGE 1 LAYOUT E 41E 914 186 SCALE 1:20 AND 1:10 AND 1:1
--	-------------------	------------------	--



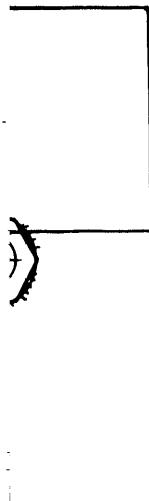
## REVISIONS

REV	DESCRIPTION	DATE	APPROVED

UNC STANDARD OR ALTERNATEVLY  
ALLAN  $\frac{7}{8}$ " x 1.5"



SPOT WELD IN ASSEMBLY  
WITH THE MOYNO PUMP FRAME  
THEN REMOVE THE MOYNO  
PUMP FOR A BETTER ACCESS  
DURING FINAL INTERMITTENT  
WELDING OF THE PLATE (1) TO  
THE FUEL TANK



UNC STANDARD HEXAGONAL NUT  
 $\frac{7}{8}$

REMOVE SHARP EDGES

OTHERWISE SPECIFIED  
IS ARE IN INCHES  
ES ON:  
MATERIAL:  
MATERIAL:  
±

## SIGNATURES

## DATE

DRAWN S.L.O.

2.24.

CHECKED

89

ENGRD

ISSUED

GENERAL  ELECTRIC  
DEPT LOC

MODIFIED LOCO 607  
MOYNO PUMP ATTACHMENT  
DETAIL

SIZE

PROM NO

DRAW NO

C

41C 640 505

SCALE 1:2

SHEET

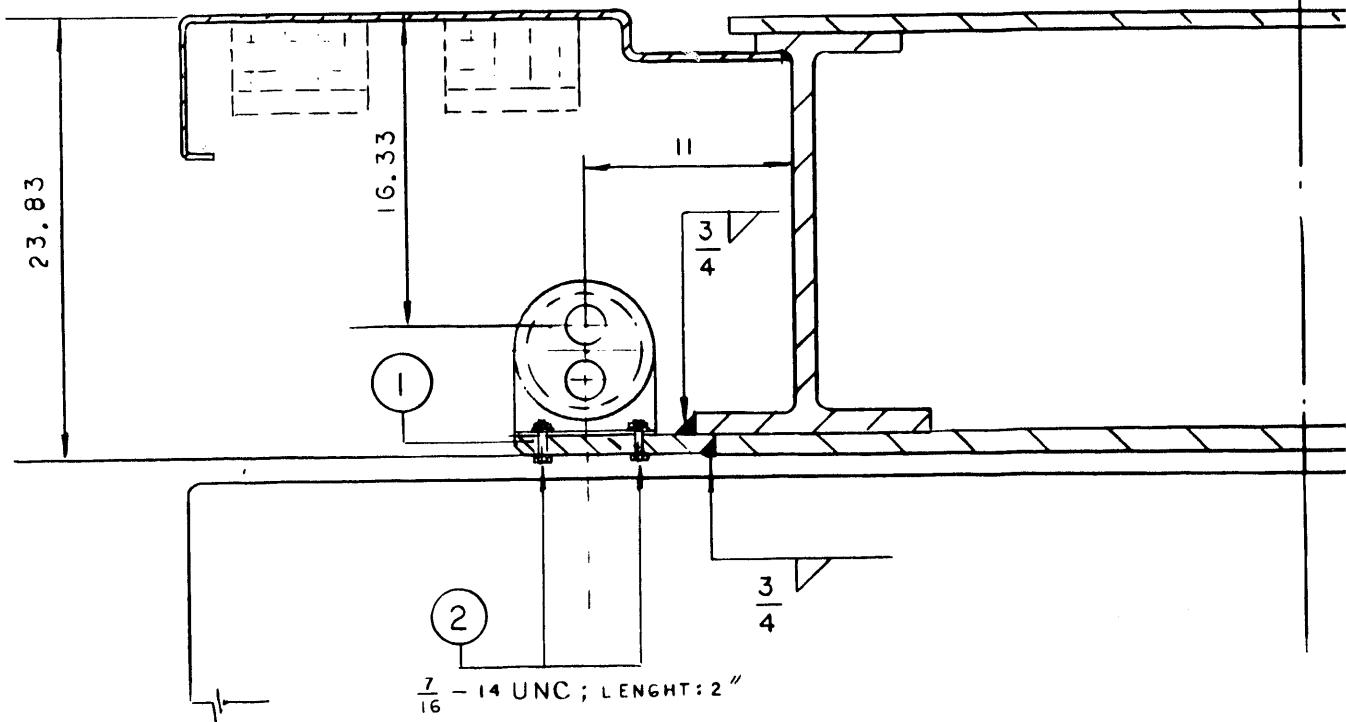
DISTR TO

8 7 6 5

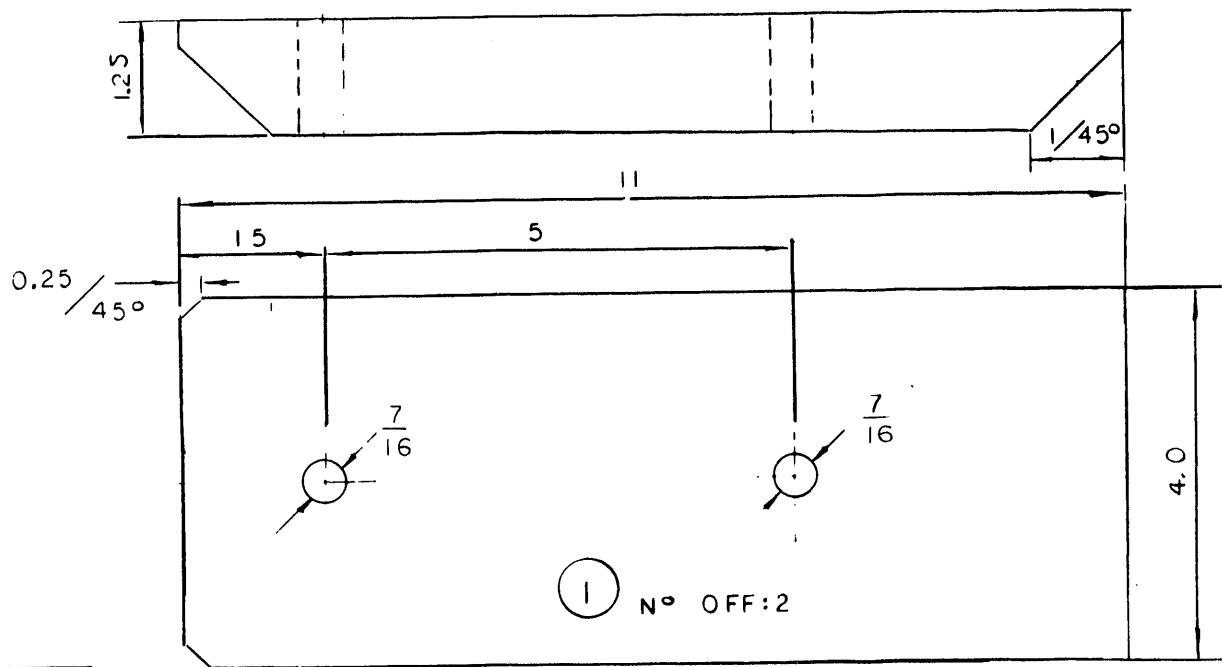
D

CROSS-SECTION AT STA 640

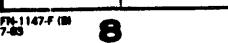
$$f_{NAT} = 122 \text{ Hz}$$



B



THIRD ANGLE PROJECTION



7-83



8

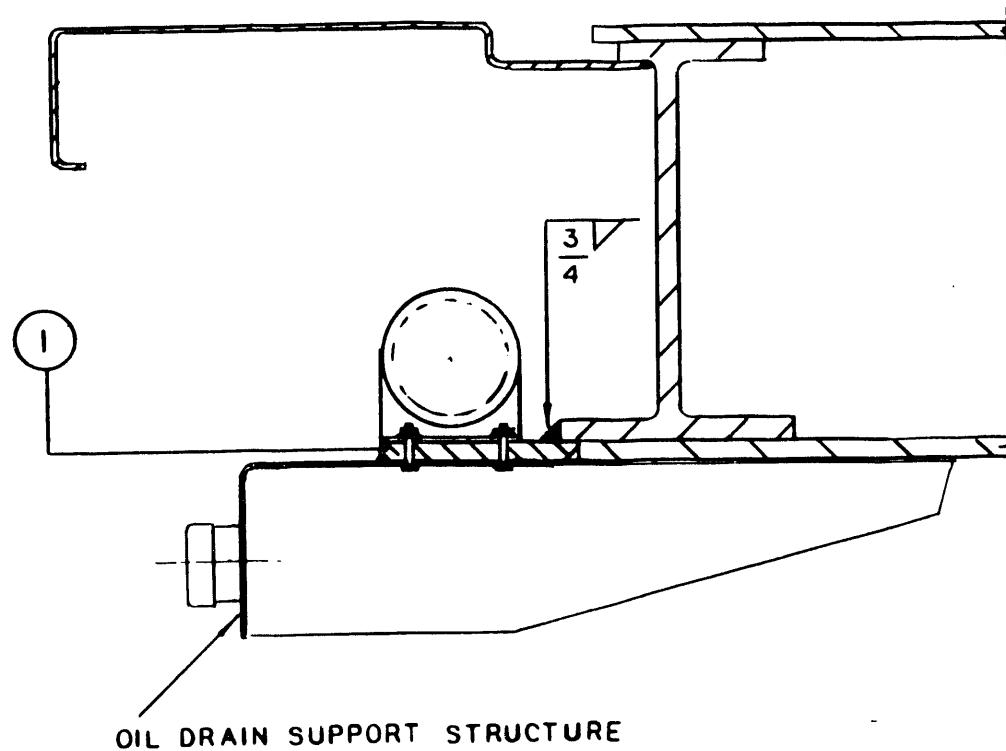
7

6

5

REF ID	SHEET NO	REV	REV	1
REVISIONS				
REV	DESCRIPTION		DATE	APPROVED

CROSS-SECTION AT STA 578



-23-

WILSON ENGINEERING CORPORATION GENERAL AND IN CONTROL WILSON ENGINEERING CORP. 122, WILSON AVENUE NEW YORK 100-122 TELEGRAMS: WILSON TELEPHONE: 2-1212 TELETYPE: ✓	SIGNATURES S.L.O. C.R.D. C.R.D. C.R.D. C.R.D. C.R.D. C.R.D. C.R.D. C.R.D.	DATE 2,9, 89       	GENERAL ELECTRIC DEPT. LOC MODIFIED LOCO 607 WATER CWS HEAT EXCHANGER ATTACHMENTS
			PRINTED FEB. 1960 SHEET NO. 41D715 508 SCALE 1:85 AND 1:1 INCHES

8 7 6 5

D  
C  
B  
A

VIEW ON ARROW E-E

26.5

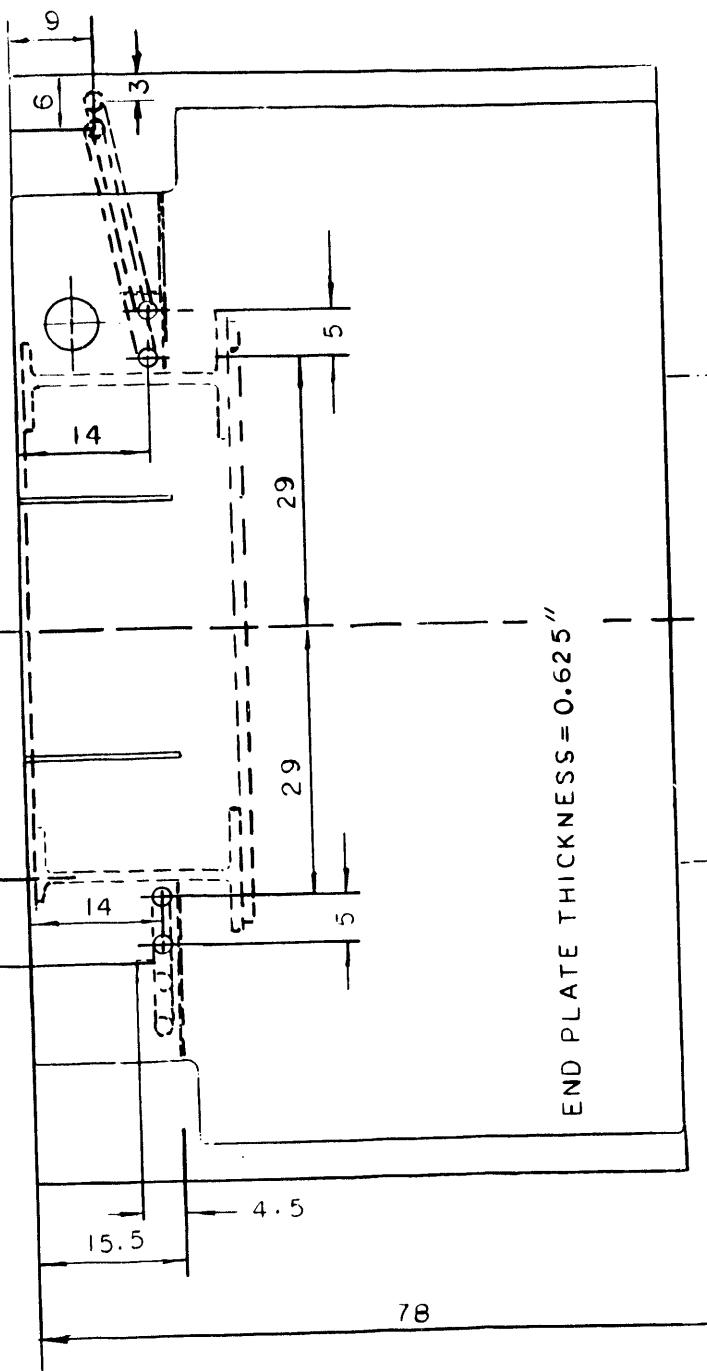
9

15.5

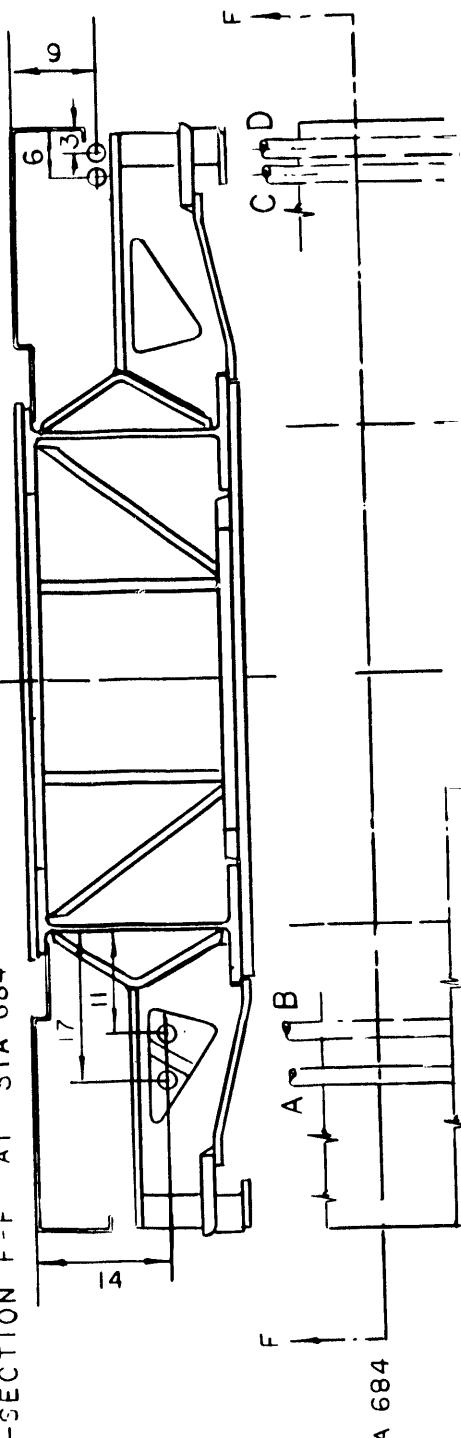
4.5

78

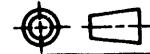
END PLATE THICKNESS = 0.625"



CROSS-SECTION F-F AT STA 684



THIRD ANGLE PROJECTION



784

8

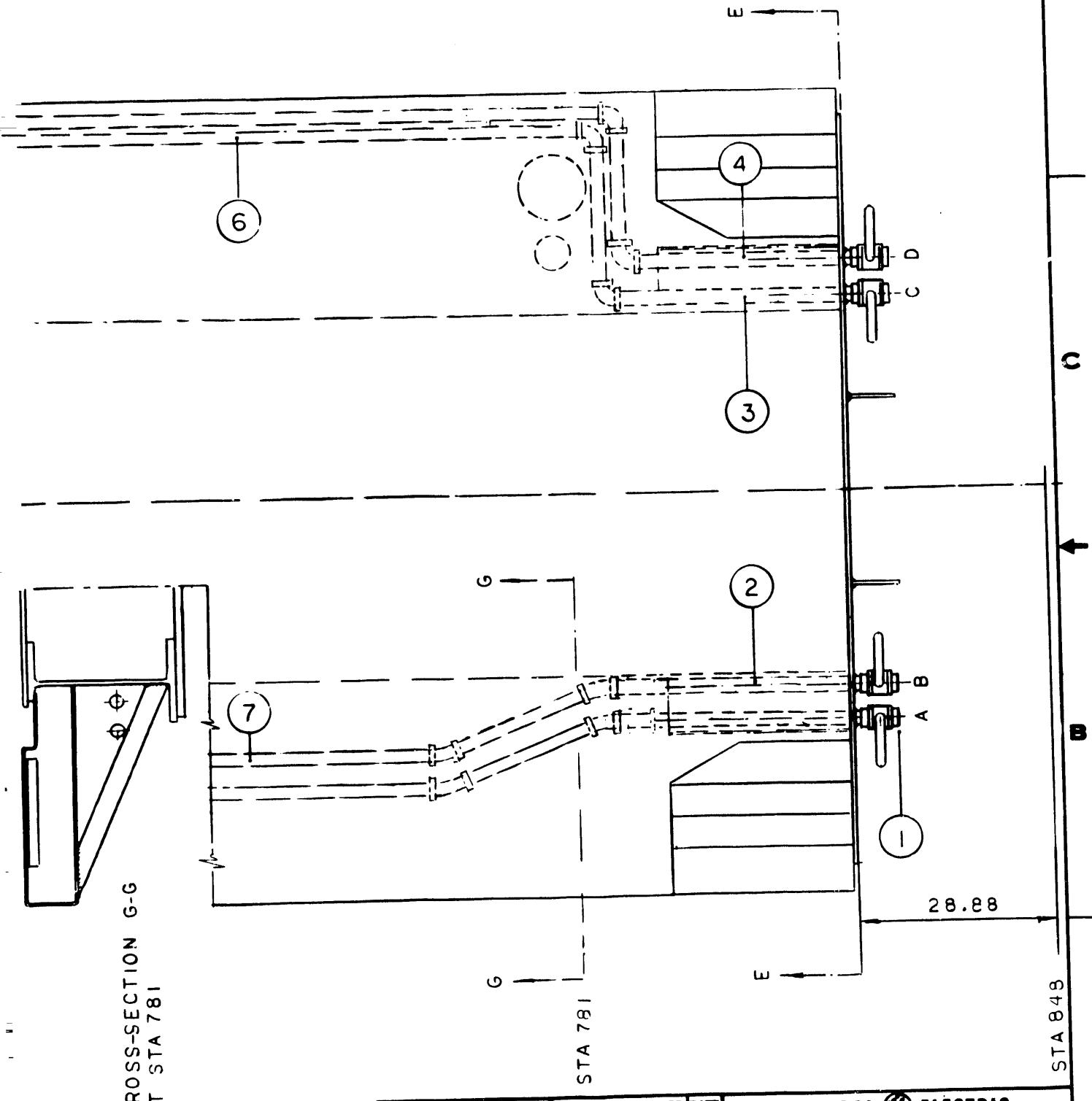
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6

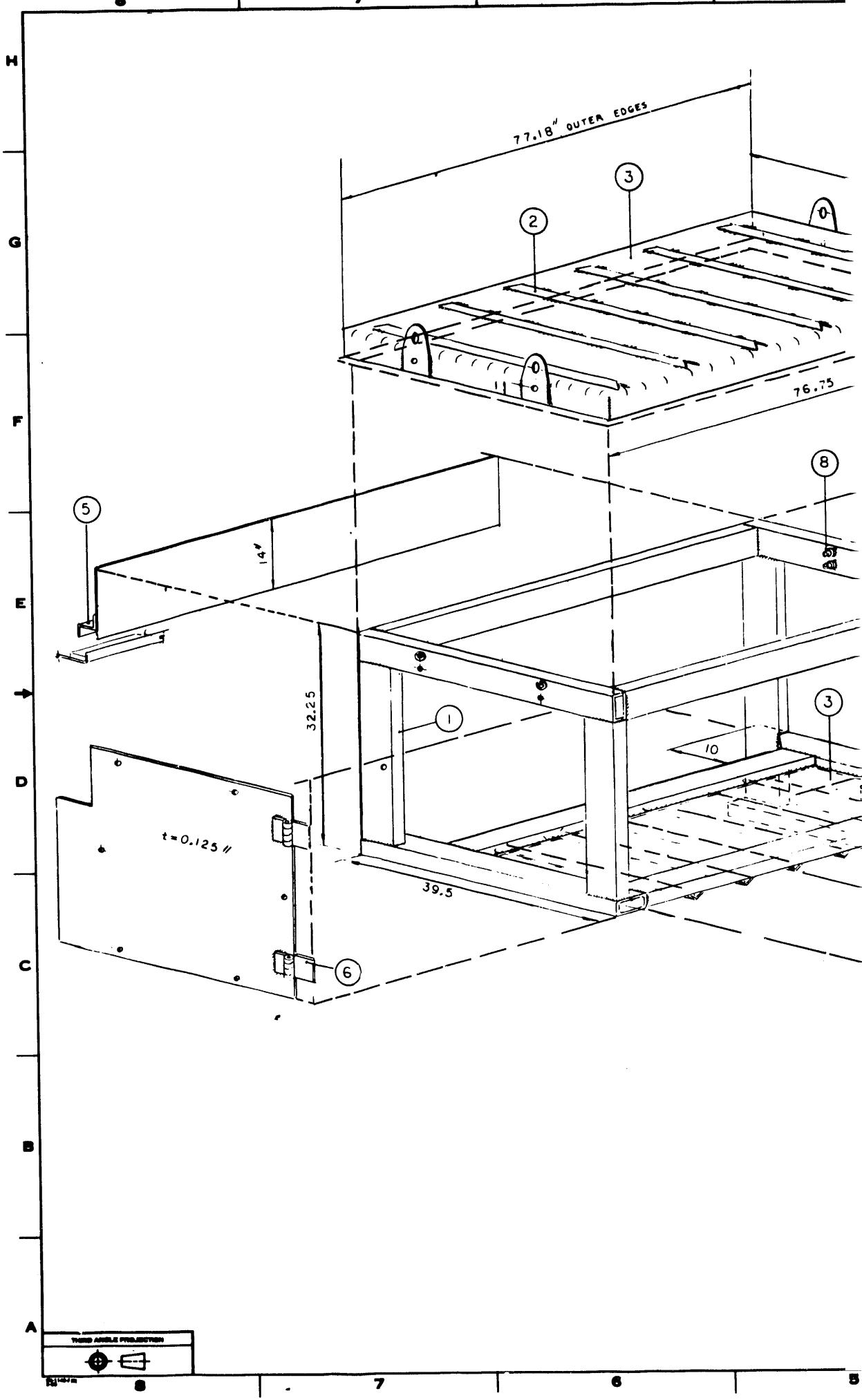
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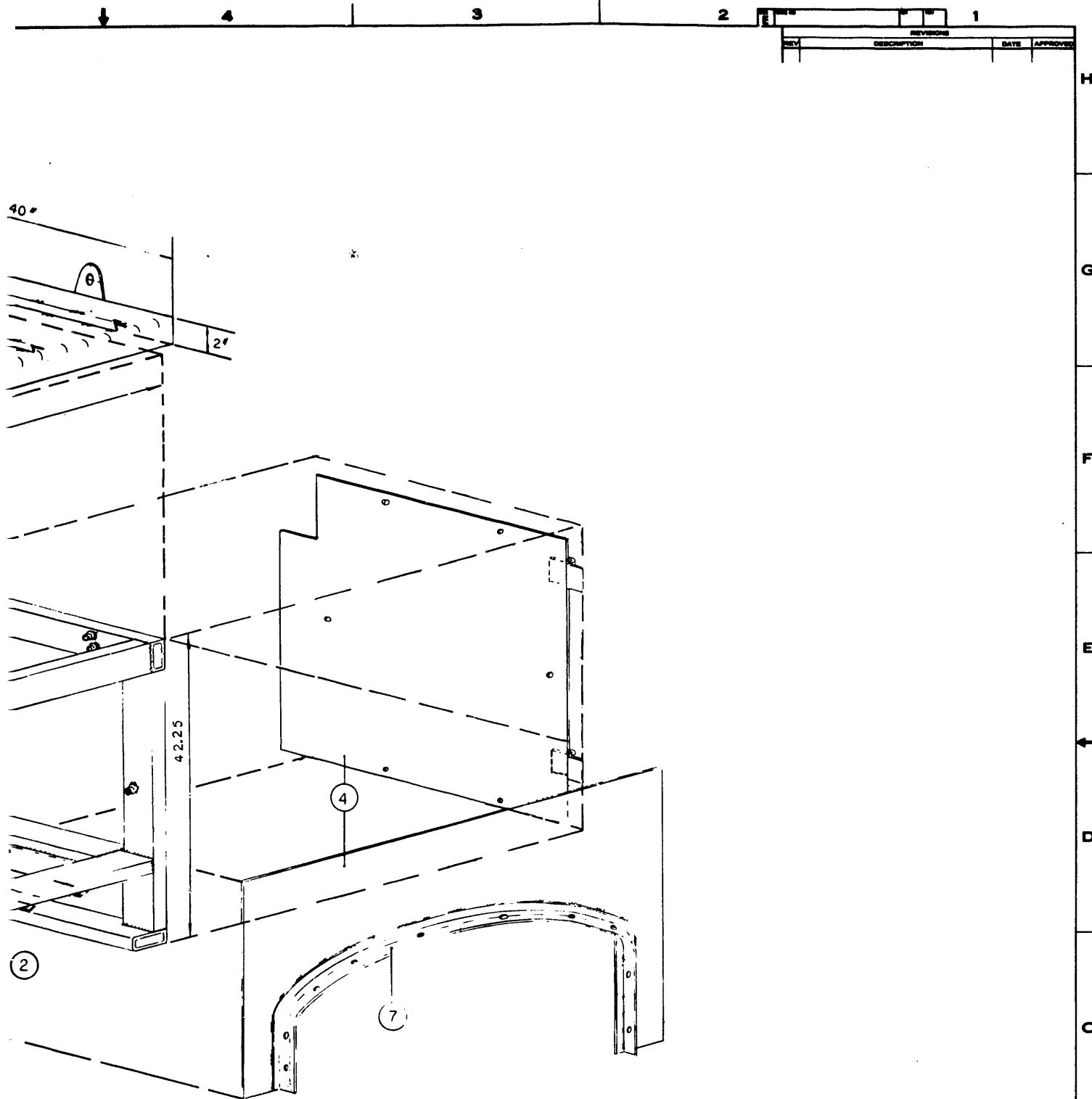
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DATE	ISSUE NO.	BY	REV.	1
REVISIONS				
REV.	DESCRIPTION	DATE	APPROVAL	

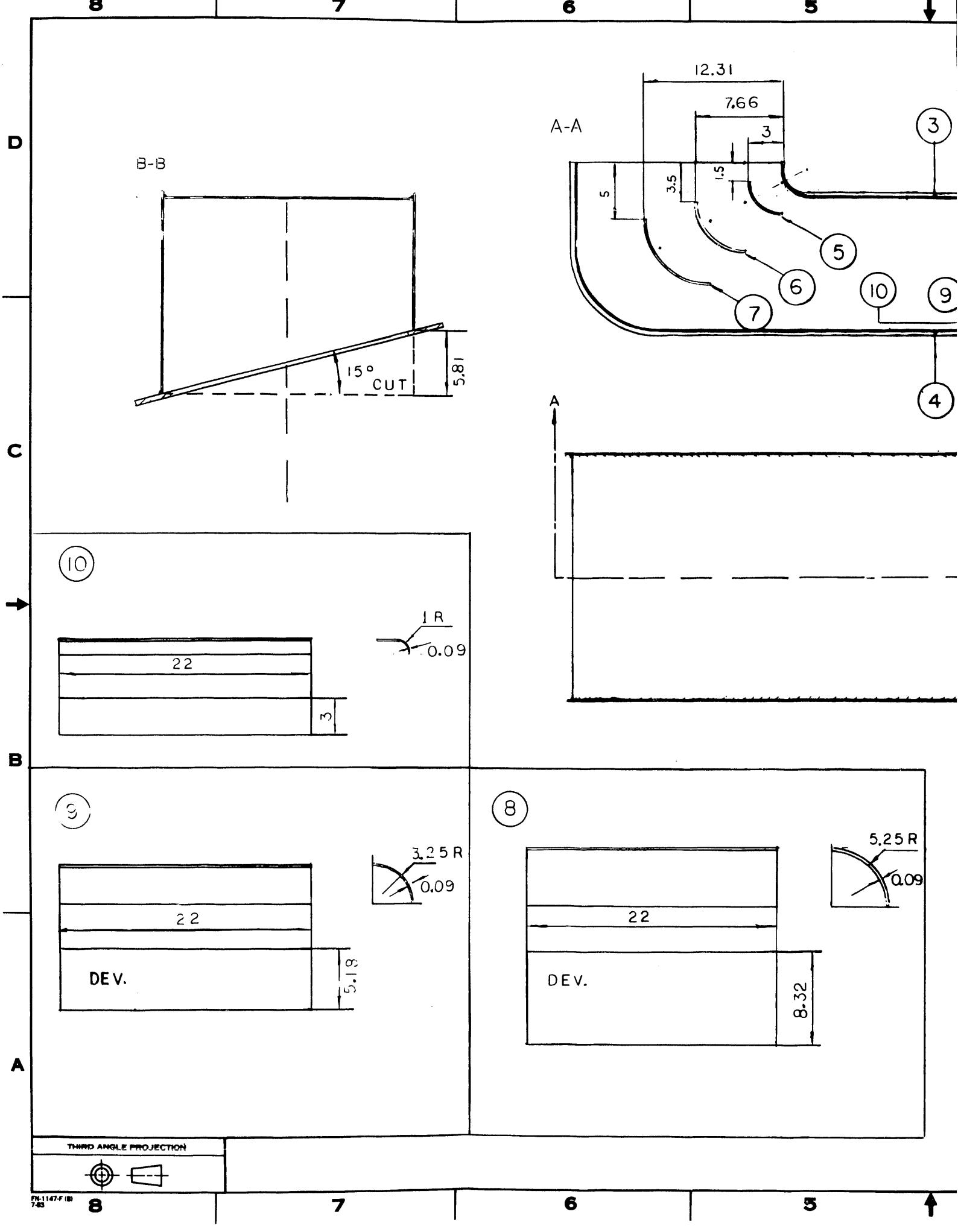


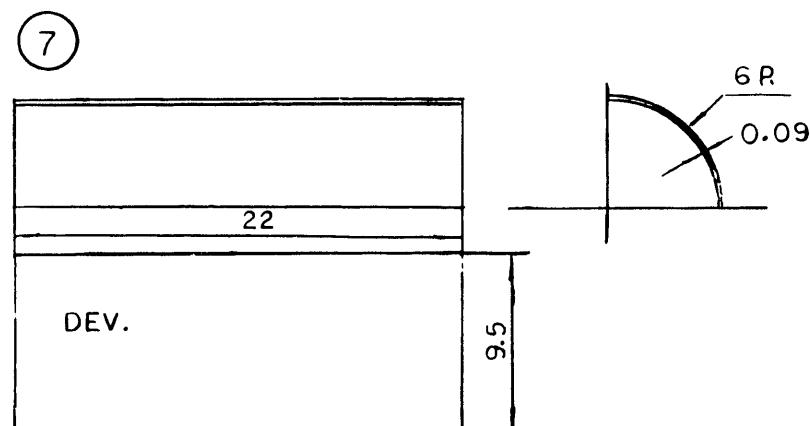
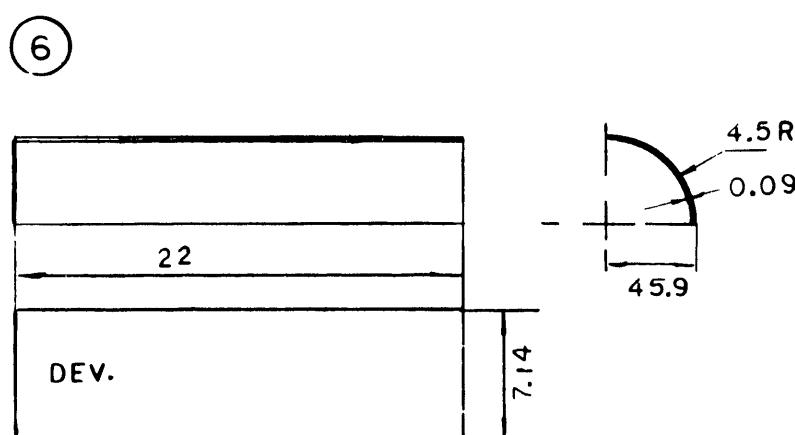
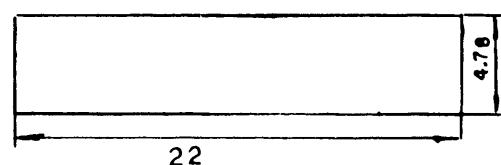
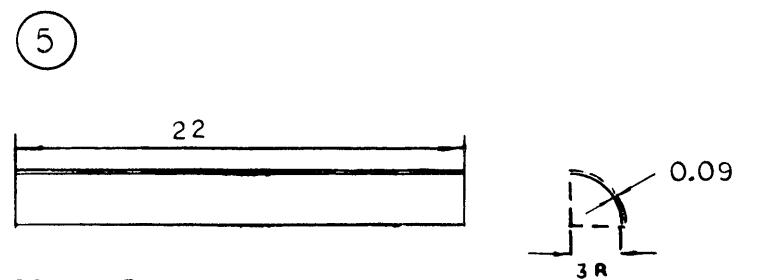
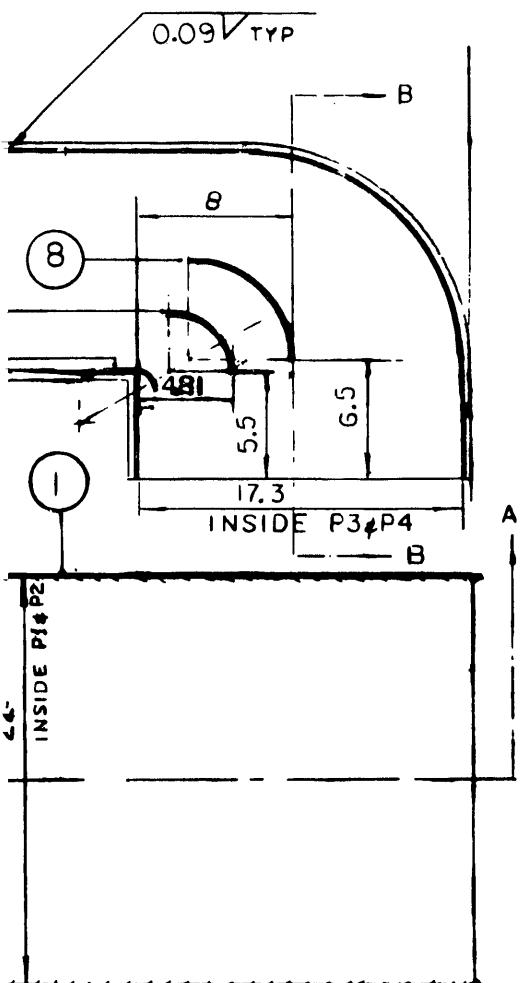
CROSS-SECTION G-6  
AT STA 781



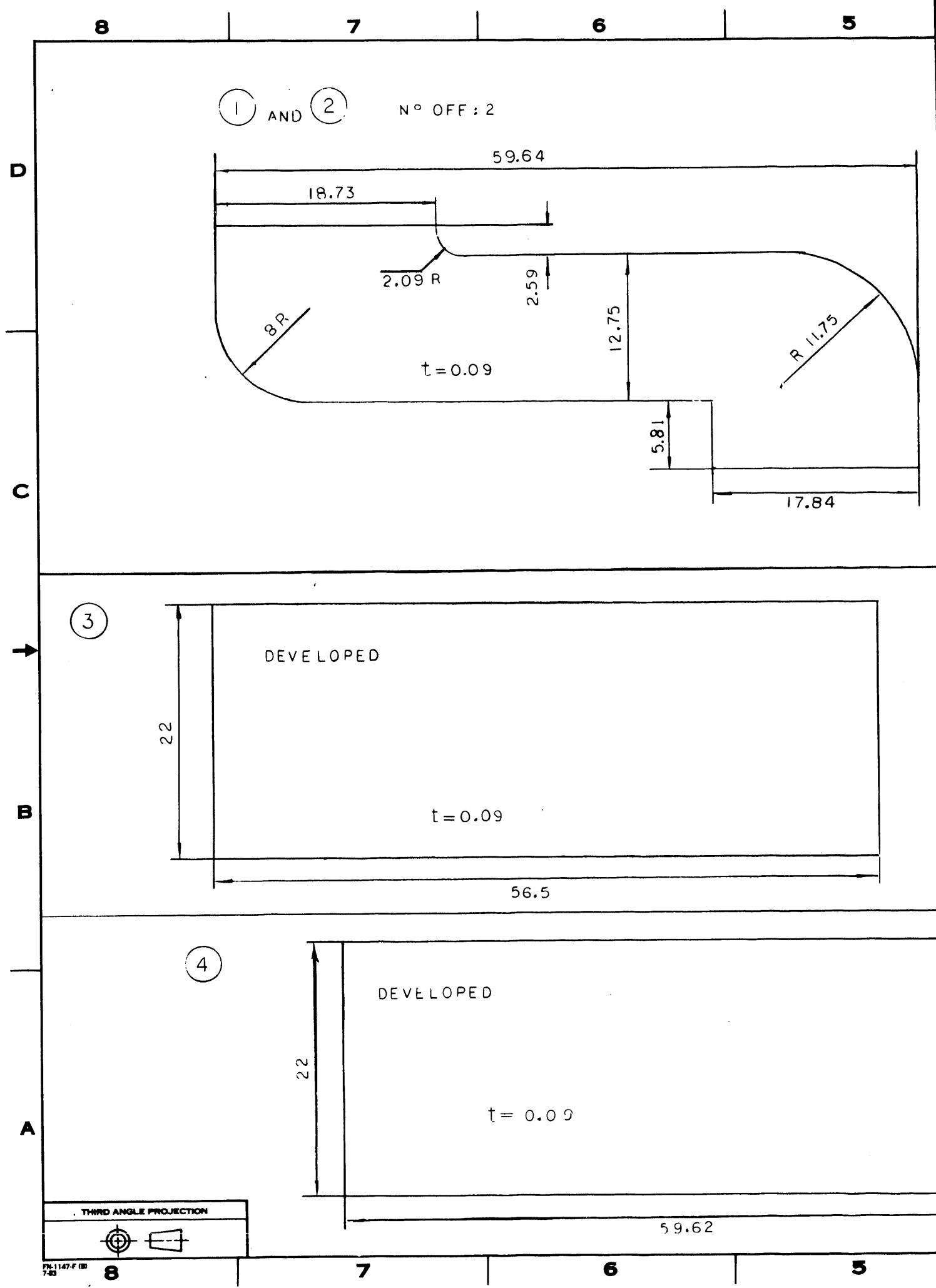


9	16	0.5" 6"-12 GALVANISED STEEL BOLTS
8	16	0.5" WELD NUTS
7	1	DASH 8 ENGINE CAB JOINT MEMBER
6	4	WELDING HINGES
5	7 FT	1'1.5" ZEE
4	62 SQFT	0.125" WALL ACCESS AND SIDE PLATES
3	50 SQFT	0.09" WALL ROOF AND Drip FLOOR PLATE
2	44 FT	1.5, 1.5, 0.125 EQUAL ANGLE STIFFENERS
1	55 FT	4 2" x 3/16" STEEL BOX BEAM
ITEM	QTY	VENDOR
		DESCRIPTION
DRAWING APPROVED BY: <u>SLD</u> DATE: <u>1-26-89</u> DESIGNER AND IN CHARGE: <u>SLD</u> APPROVAL: <u>SLD</u> DRAWN BY: <u>SLD</u> CHECKED BY: <u>SLD</u> REVISED: <u>SLD</u> DRAWN: <u>SLD</u> FUNCTION: <u>SLD</u> DRAWN: <u>SLD</u>		
<b>GENERAL ELECTRIC</b> CWS FIRED LOCOMOTIVE MODIFIED 607 HYDRAULIC CONTROL MODULE DRAWING NO: 41E 914 189 SCALE: 1 DRAFTED BY: <u>SLD</u>		



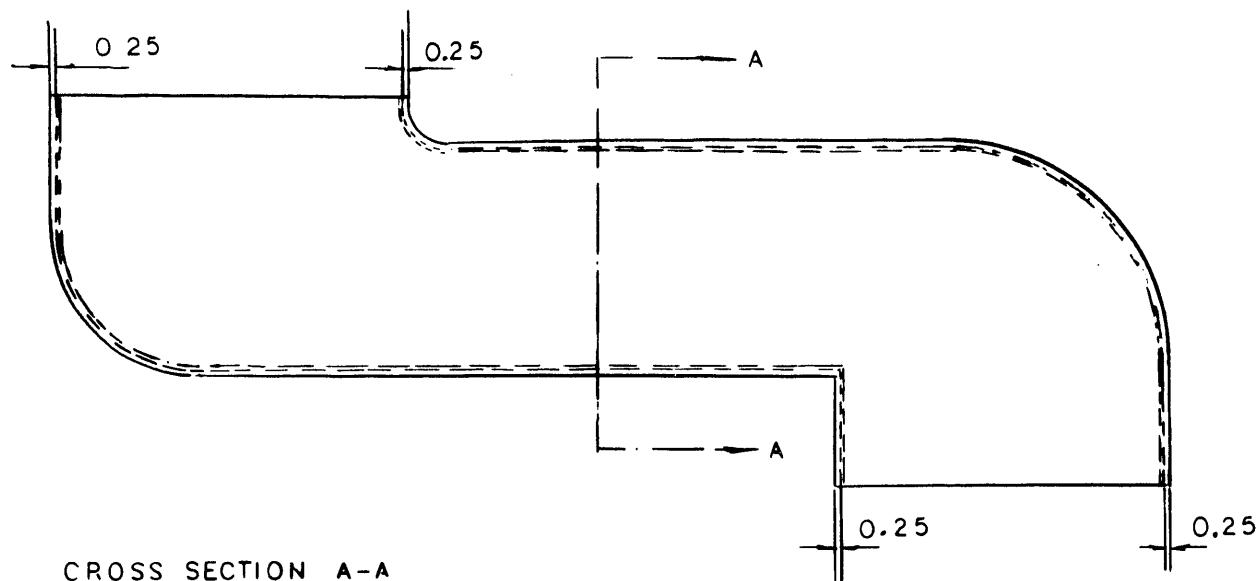


UNLESS OTHERWISE SPECIFIED	SIGNATURES	DATE	<b>GENERAL ELECTRIC</b> <small>DEPT LOC</small>	
DIMENSIONS ARE IN INCHES. TOLERANCES ON: 2 PL. DECIMALS 2; 3 PL. DECIMALS 2; ANGLES 2; FRACTIONS 2;	DR. BR.	1.31.		
	CHIEF S.L.O.	89	<b>MODIFIED LOCOMOTIVE 607</b> <b>ALTERNATOR COOLING DUCT</b> <b>MODIFICATION; DETAILS 5 to 10</b>	
	DR. BR.	89		
			PRINT. NO.	DRAW. NO.
			<b>D</b>	<b>41D 715 502</b>
			SCALE	SMITH

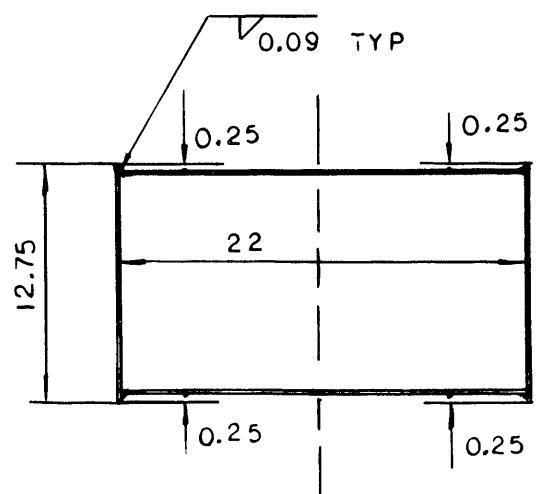


REF	DRG NO	SH	REV	1
REVISIONS				
REV	DESCRIPTION	DATE	APPROVED	

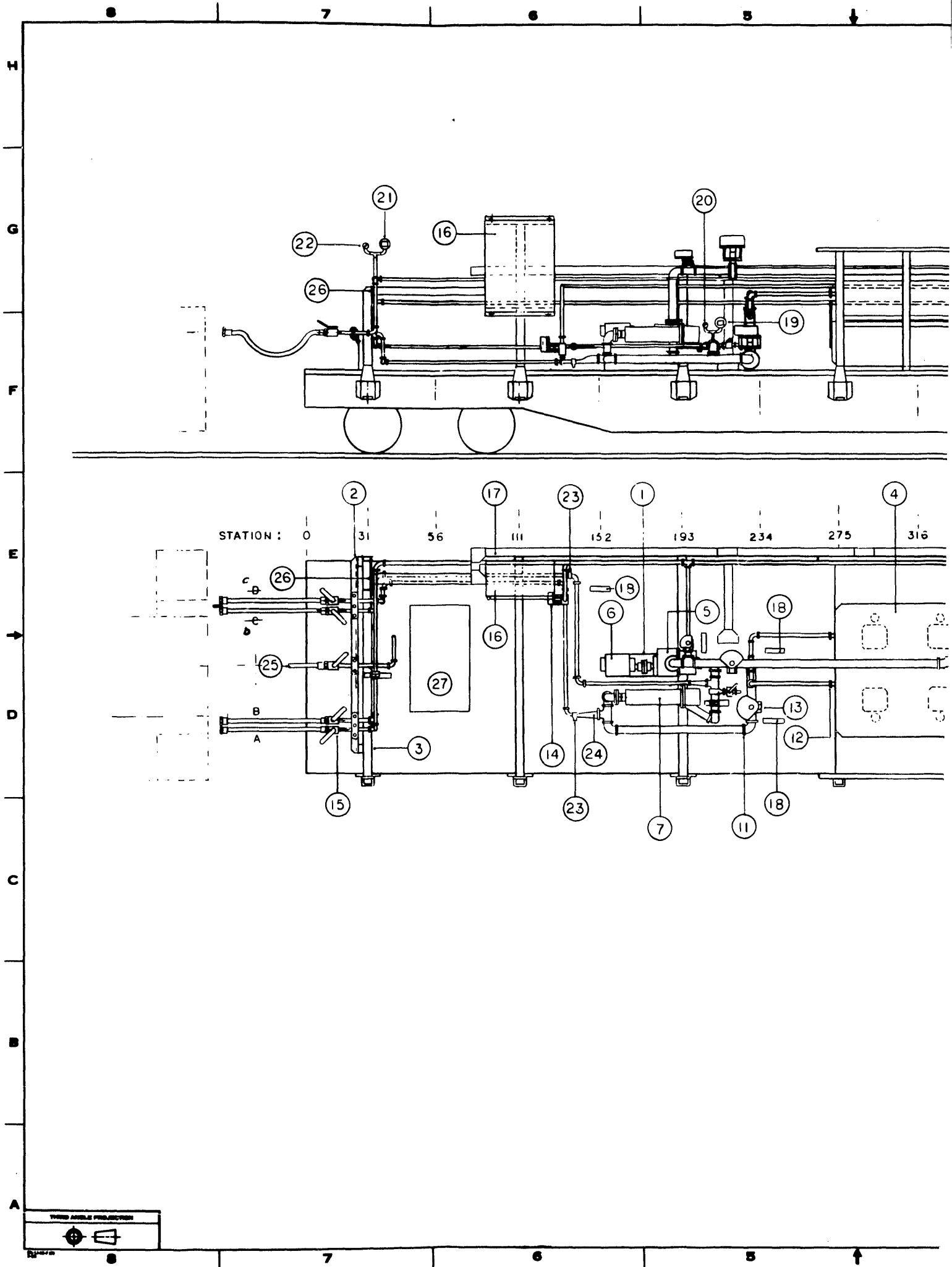
SIDE VIEW (VANES NOT SHOWN)



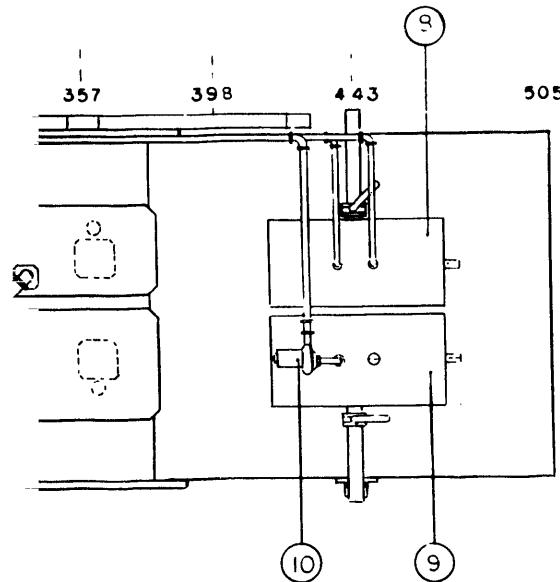
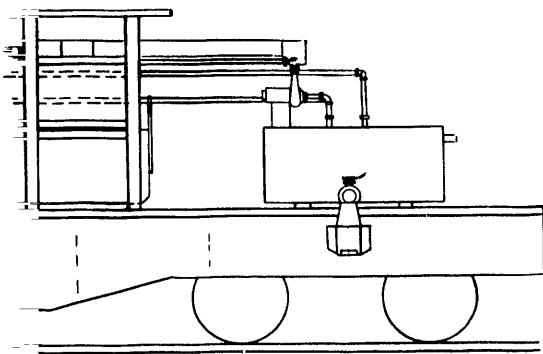
CROSS SECTION A-A



UNLESS OTHERWISE SPECIFIED	INITIALS	DATE	GENERAL ELECTRIC	
DIMENSIONS ARE IN INCHES.	S.L.O.	1.31.	DEPT	LOC
TOLERANCES 0.010		89	MODIFIED LOCOMOTIVE 607 ALTERNATOR COOLING DUCT MODIFICATION; DETAILS 1 TO 4	
2 PL. DECIMALS 2				
2 PL. DECIMALS 2				
ANGLES 1				
FRACTION 2				
			SIZE	PCBA NO.
			D	DRW. NO.
			41D715501	
			SCALE 1:5	BLANK

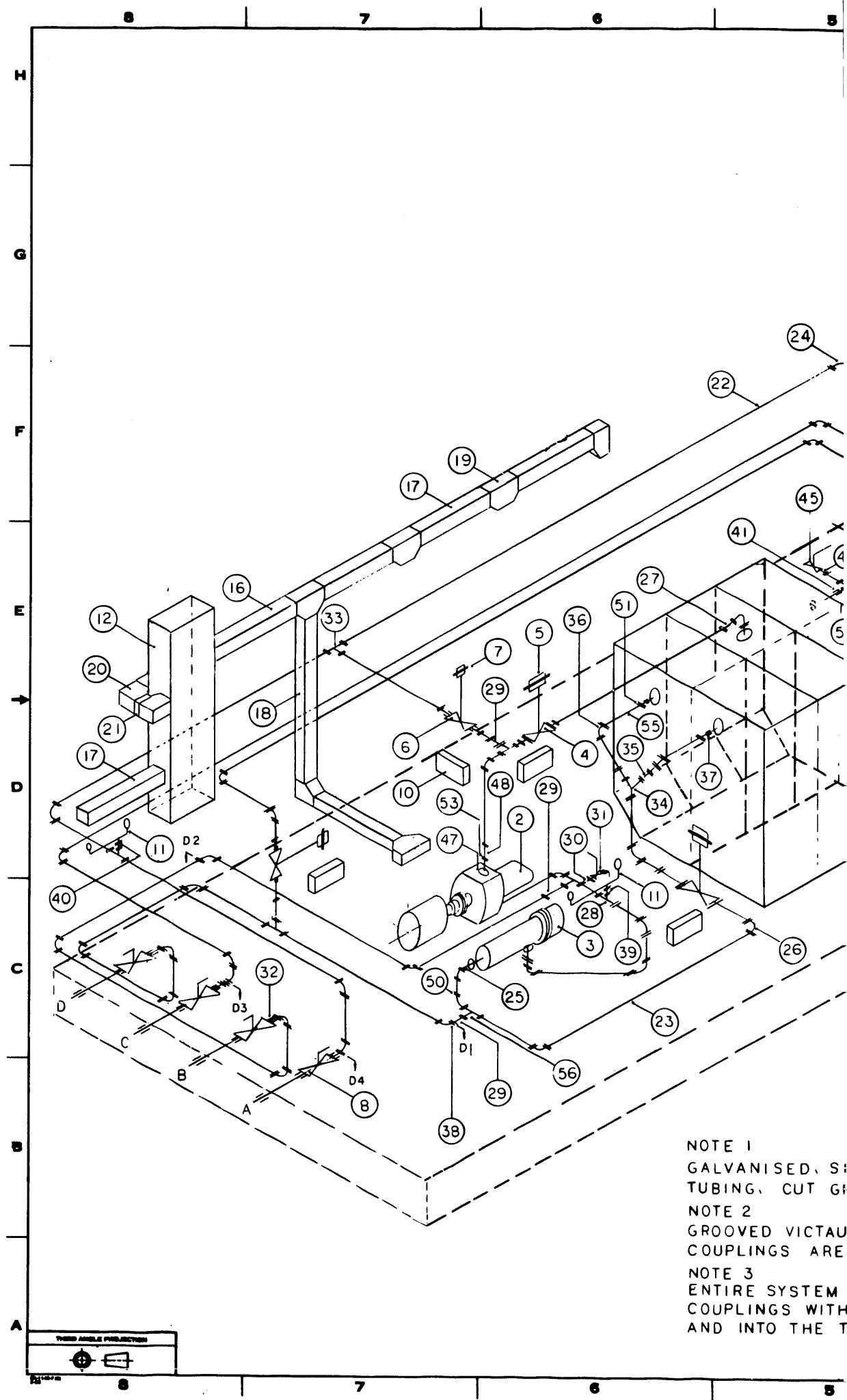


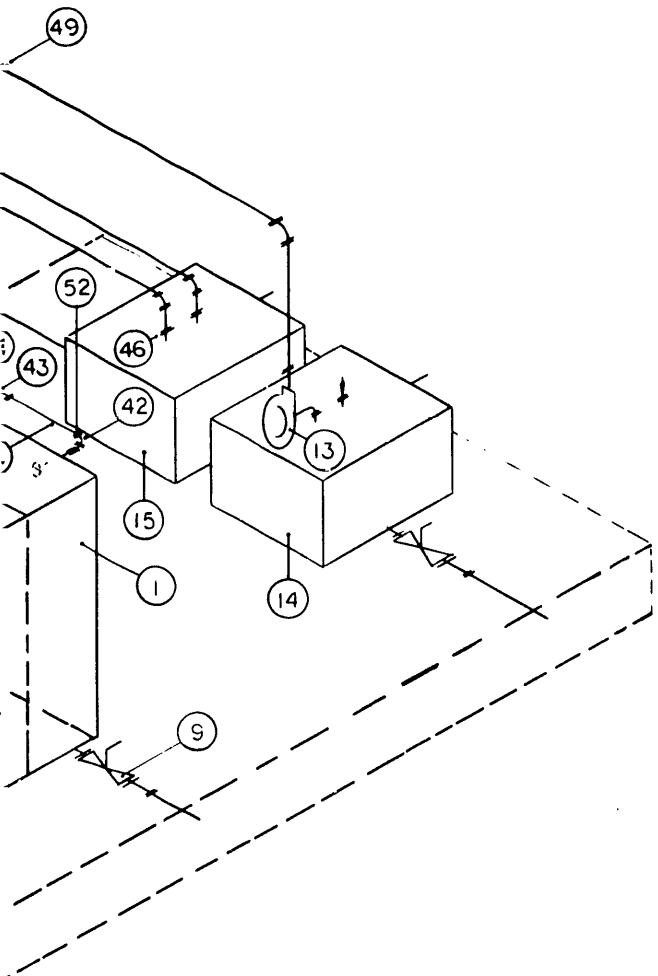
DESCRIPTION		DATE	APPROVED
1	VICTAULIC COUPLINGS AND FITTINGS, INCORPORATED, PIPING LAYOUT MOD. ELECTRIC HEATER (ITEM 7) REPLACED	01/20/89	
2	DETAILS OF ELECTRIC CONTROLS AND WIREWAYS INCLUDED	01/25/89	



27	DIESEL ENGINE POWERED AUXILIARY GENERATOR
26	ELECTRIC CONECTIONS TO LOCOMOTIVE
25	COMPRESSED AIR
24	ECCENTRIC REDUCER
23	VICTAULIC OUTLET COUPLING
22	PRESSURE GAUGE
21	PRESSURE SWITCH P2
20	PRESSURE GAUGE
19	PRESSURE SWITCH P3
18	SOLENOID PILOT VALVE
17	CABLE WAY BOX
16	ELECTRIC CONTROLS
15	1.5" FULL PORT VALVES
14	1.5" FULL PORT BALL VALVE WITH PNEUMATIC ACTUATOR
13	4" BUTTERFLY VALVE WITH PNEUMATIC ACTUATOR
12	1.5" VICTAULIC COUPLING
11	4" VICTAULIC COUPLING
10	WATER PURGE PUMP
9	CLEAN WATER TANK
8	DIRTY WATER TANK
7	ELECTRIC HEATER AND THERMOSTAT
6	ELECTROMOTOR
5	RECIRCULATING PUMP GEAR BOX
4	EXPERIMENTAL CWS FUEL TANK
3	FLOOR AND FENCE BEAMS
2	VALVE AND TUBING SUPPORT PORTAL FRAME
1	RECIRCULATING PUMP TUTHILL 330 H700-3

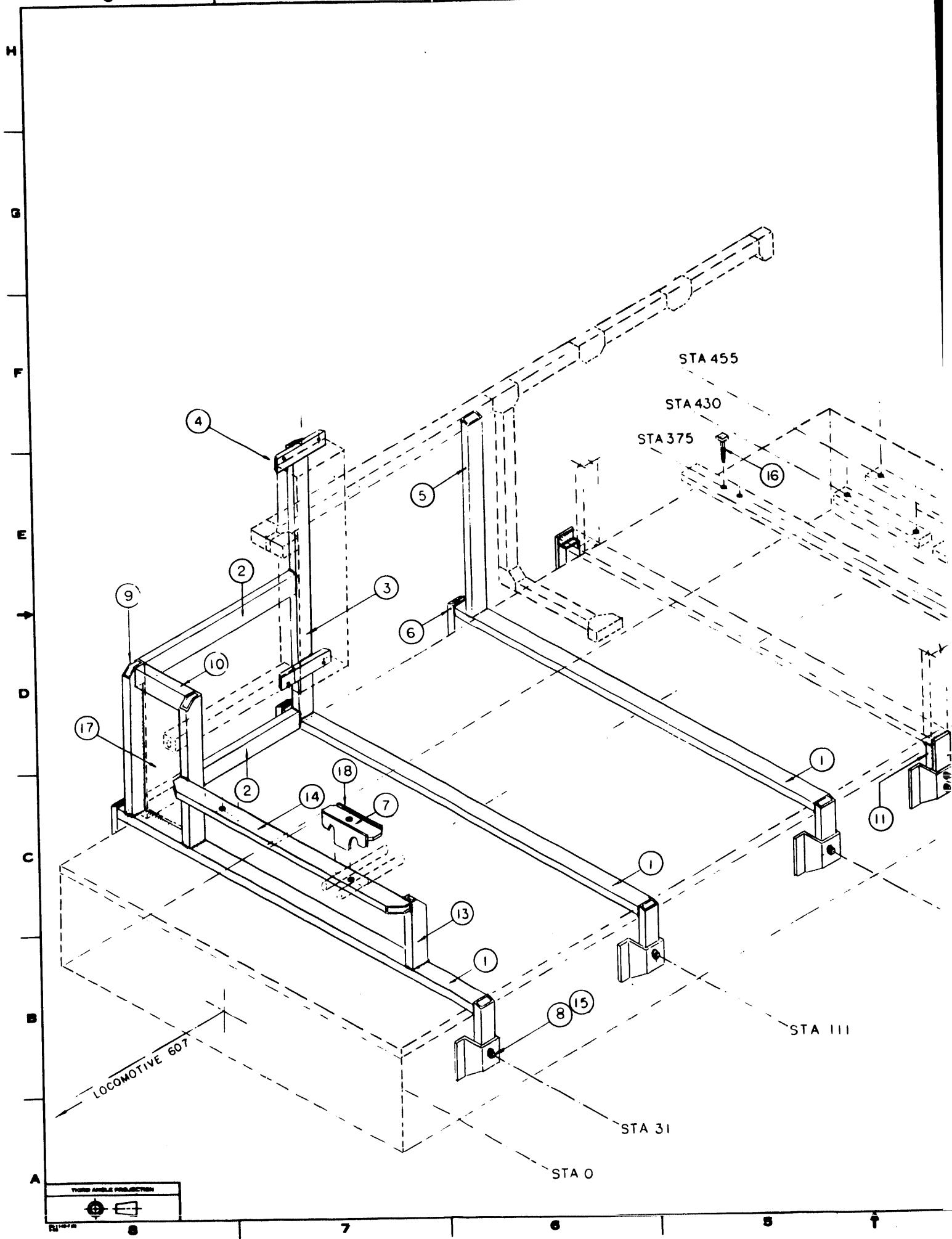
UNLESS OTHERWISE SPECIFIED UNLESS OTHERWISE SPECIFIED UNLESS OTHERWISE SPECIFIED 2 PL. INCHES : 2 PL. INCHES : 2 PL. INCHES : ANGLE : FRACTION : <input checked="" type="checkbox"/>	SIGNATURES SLO	DATE 10.21.85	GENERAL ELECTRIC LCM
FLAT CAR LAY OUT			PRINTED 41E914197
E			SCALE 1/20
			SHR





ITEM	QTY	VENDOR	DESCRIPTION	REVISIONS	DATE	APPROVAL
				1		
56	3	VICTAULIC COMPANY OF AMERICA	4" TEE N° 20 H.D.G.			H
55	12	FT	2" I.D. 0.1875 WALL GALVANISED STEEL PIPE			
54	18	FT	1" I.D. 0.1575 WALL GALVANISED STEEL PIPE			
53	1	VICTAULIC COMPANY OF AMERICA	5" STYLE HP-70 ES END SEAL COUPLING H.D.G.			
52	8	-	1" STYLE 77 STANDARD COUPLING H.D.G.			
51	10	-	2" STYLE HP 70 ES END SEAL COUPLING H.D.G.			
50	33	-	4" STYLE HP-70 ES END SEAL COUPLING H.D.G.			
49	77	-	1.5" STYLE HP-70 ES ENDSEAL COUPLING H.D.G.			
48	1	-	5" 4" CONCENTRIC REDUCER N° 50 H.D.G.			G
47	1	-	5" FLANGED ADAPTOR NIPPLE N° 41 H.D.G.			
46	4	-	1.5" FEMALE THREADED ADAPTER N° 80 H.D.G.			
45	1	-	1" GAS VALVE			
44	1	-	1" NIPPLE N° 40 H.D.G.			
43	1	-	1" TEE N° 20 H.D.G.			
42	1	-	1" 90° ELBOW N° 10 H.D.G.			
41	2	-	1" FEMALE THREADED ADAPTERS N° 80 H.D.G.			
40	1	-	1.5" 3/4" REDUCER THREADED SMALL END N° 52 H.D.G.			F
39	1	-	2" 3/4" REDUCER THREADED SMALL END N° 52 H.D.G.			
38	4	-	1.5" 3/4" STYLE 72 WITH F THREADED OUTLET H.D.G.			
37	2	-	2" FEMALE THREADED ADAPTER N° 80 H.D.G.			
36	2	-	2" 90° ELBOW N° 10 H.D.G.			
35	2	-	4" 2" CONCENTRIC REDUCER N° 50 H.D.G.			
34	1	-	4" TRUE "Y" N° 33 H.D.G.			
33	2	-	1.5" TEE N° 20 H.D.G.			
32	8	-	1.5" NIPPLE N° 40 H.D.G.			
31	1	-	1.5" STYLE 700 BUTTERFLY VALVE			E
30	1	-	4" 1.5" STYLE 72 GROOVED OUTLET COUPLING H.D.G.			
29	3	-	4" 1.5" ECCENTRIC REDUCER N° 51 H.D.G.			
28	1	-	4" x 4" x 2" REDUCING TEE N° 25 H.D.G.			
27	1	-	4" 45° ELBOW N° 11 H.D.G.			
26	10	-	4" 90° ELBOW N° 10 H.D.G.			
25	11	-	FLANGED ADAPTER NIPPLE N° 41 H.D.G.; 4"			
24	24	-	1.5" 90° ELBOW N° 10 HOT DIP GALVANISED			
23	50	FT	4" I.D. 0.25" GALVANISED STEEL PIPE			
22	200	FT	1.5" I.D. 0.2" WALL GALVANISED STEEL PIPE			D
21	1	HOFFMAN ENGINEERING COMPANY	F - 44WN4 NIPPLE			
20	4	-	F - 44WE 90° ELBOW			
19	4	-	F - 44WT TEE			
18	2	-	F - 44W36" STRAIGHT SECTION			
17	4	-	F - 44W60" STRAIGHT SECTION			
16	1	HOFFMAN ENGINEERING COMPANY	F - 44W120" STRAIGHT SECTION			
15	1	GENERAL ELECTRIC	DIRTY WATER TANK DWG N° 41D7154B1			
14	1	-	CLEAN WATER TANK DWG N° 41D7154B1			C
13	1	POWER DRIVES INC	WATER PURGE PUMP SERIES 80 STRAIGHT CENTRIFUGAL			
12	1	HOFFMAN ENGINEERING COMPANY	A-48H36FLP ENCLOSURE A48P36 PANEL ELECTRICAL CONTROLS			
11	2	RED VALVE COMPANY INC	PRESSURE SWITCH AND GAUGE COMBINATION			
10	4	MAC VALVES INC	SOLENOID VALVE MAC 82 - INDIVIDUAL BASE			
9	3	JAMESBURY CO	4" BUTTERFLY VALVE TYPE 815 W			
8	4	-	1.5" FULL PORT SERIES 4000 BALL VALVE			
7	2	-	1.5" DOUBLE ACTING PNEUMATIC ACTUATOR 105-1			
6	2	-	1.5" FULL PORT SERIES 4000 BALL VALVE			
5	2	-	1.5" DOUBLE ACTING PNEUMATIC ACTUATOR 105-1			
4	2	-	4" BUTTERFLY VALVE TYPE 815 W			
3	1	HY-TECH SALES INC	ELECTRIC HEATER WITH THERMOSTAT, 4" FLANGES			
2	1	TUTHILL PUMP COMPANY	RECIRCULATING AND FEED PUMP TUTHILL 330 H70J-3			
1	1	GENERAL ELECTRIC	CWS EXPERIMENTAL' FUEL TANK DWG N° 41E914098			

ITEM	QTY	VENDOR	DESCRIPTION	UNLESS OTHERWISE SPECIFIED	SIGNATURES	DATE	GENERAL ELECTRIC
				CONNECTIONS ARE AS SHOWN	SL0	01.23.	
				TOLERANCES ARE AS SHOWN		89	
				1" I.D. 0.1575			
				2" I.D. 0.3125			
				3" I.D. 0.4375			
				4" I.D. 0.5625			
				5" I.D. 0.6875			
				6" I.D. 0.8125			
				7" I.D. 0.9375			
				8" I.D. 1.0625			
				9" I.D. 1.1875			
				10" I.D. 1.3125			
				11" I.D. 1.4375			
				12" I.D. 1.5625			
				13" I.D. 1.6875			
				14" I.D. 1.8125			
				15" I.D. 1.9375			
				16" I.D. 2.0625			
				17" I.D. 2.1875			
				18" I.D. 2.3125			
				19" I.D. 2.4375			
				20" I.D. 2.5625			
				21" I.D. 2.6875			
				22" I.D. 2.8125			
				23" I.D. 2.9375			
				24" I.D. 3.0625			
				25" I.D. 3.1875			
				26" I.D. 3.3125			
				27" I.D. 3.4375			
				28" I.D. 3.5625			
				29" I.D. 3.6875			
				30" I.D. 3.8125			
				31" I.D. 3.9375			
				32" I.D. 4.0625			
				33" I.D. 4.1875			
				34" I.D. 4.3125			
				35" I.D. 4.4375			
				36" I.D. 4.5625			
				37" I.D. 4.6875			
				38" I.D. 4.8125			
				39" I.D. 4.9375			
				40" I.D. 5.0625			
				41" I.D. 5.1875			
				42" I.D. 5.3125			
				43" I.D. 5.4375			
				44" I.D. 5.5625			
				45" I.D. 5.6875			
				46" I.D. 5.8125			
				47" I.D. 5.9375			
				48" I.D. 6.0625			
				49" I.D. 6.1875			
				50" I.D. 6.3125			
				51" I.D. 6.4375			
				52" I.D. 6.5625			
				53" I.D. 6.6875			
				54" I.D. 6.8125			
				55" I.D. 6.9375			
				56" I.D. 7.0625			
				57" I.D. 7.1875			
				58" I.D. 7.3125			
				59" I.D. 7.4375			
				60" I.D. 7.5625			
				61" I.D. 7.6875			
				62" I.D. 7.8125			
				63" I.D. 7.9375			
				64" I.D. 8.0625			
				65" I.D. 8.1875			
				66" I.D. 8.3125			
				67" I.D. 8.4375			
				68" I.D. 8.5625			
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				119" I.D. 14.9375			
				120" I.D. 15.0625			
				121" I.D. 15.1875			
				122" I.D. 15.3125			
				123" I.D. 15.4375			
				124" I.D. 15.5625			
				125" I.D. 15.6875			
				126" I.D. 15.8125			
				127" I.D. 15.9375			
				128" I.D. 16.0625			
				129" I.D. 16.1875			
				130" I.D. 16.3125			
				131" I.D. 16.4375			
				132" I.D. 16.5625			
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				136" I.D. 17.0625			
				137" I.D. 17.1875			
				138" I.D. 17.3125			
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				140" I.D. 17.5625			
				141" I.D. 17.6875			
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				144" I.D. 18.0625			
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				156" I.D. 19.5625			
				157" I.D. 19.6875			
				158" I.D. 19.8125			
				159" I.D. 19.9375			



ITEM	DESCRIPTION	DATE
HEGHT OF ITEM 3 HAS BEEN REDUCED SIMPLIFICATION AND IMPROVEMENT OF ITEMS 10,17, ITEM 18 INCLUDED		02.08.69

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E

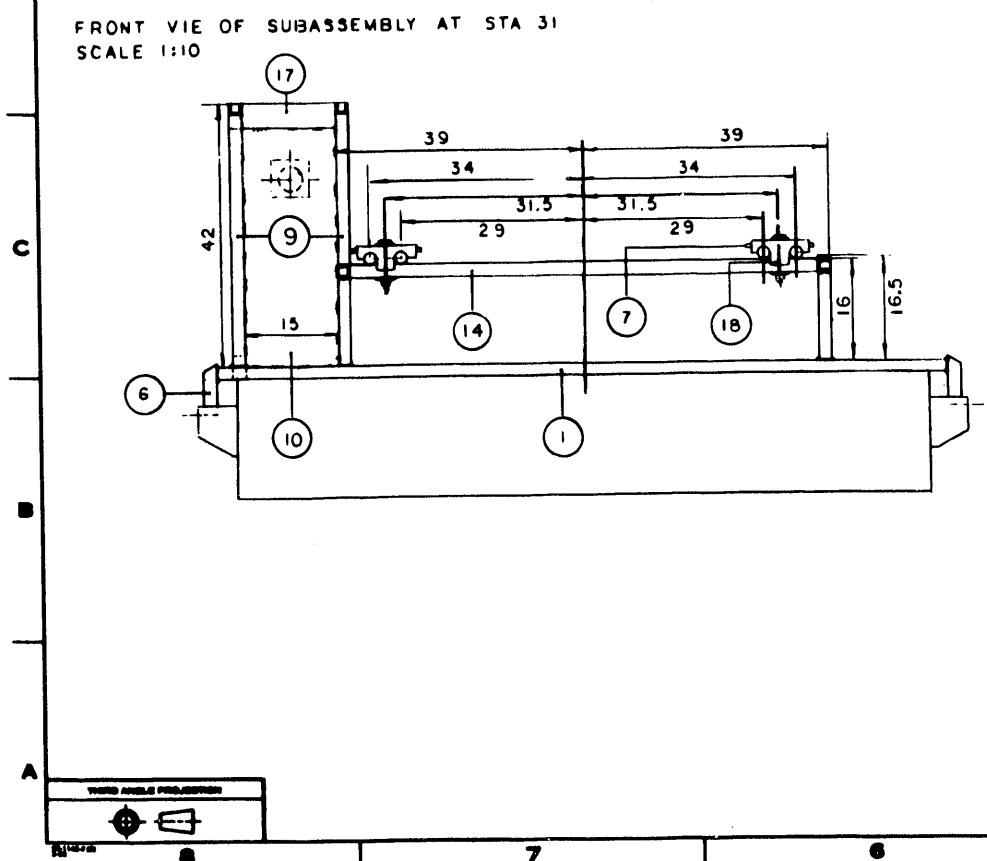
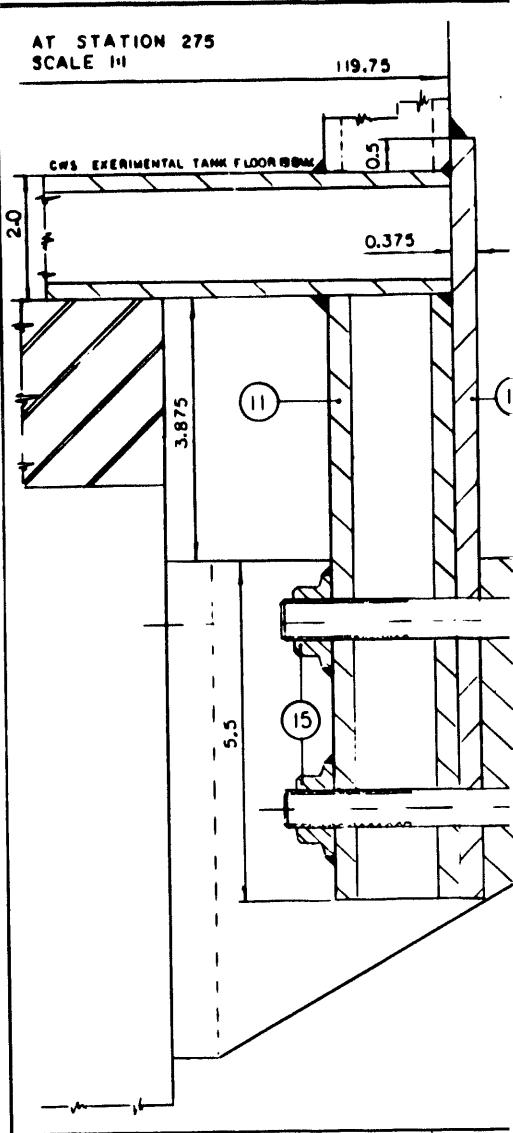
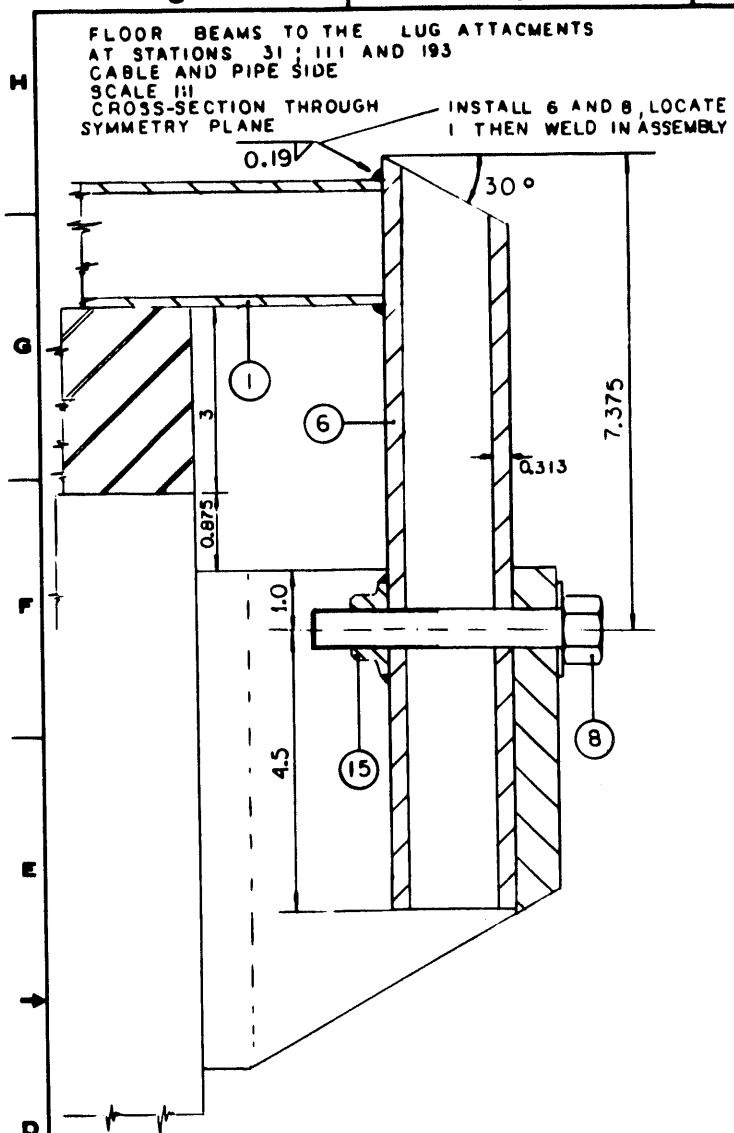
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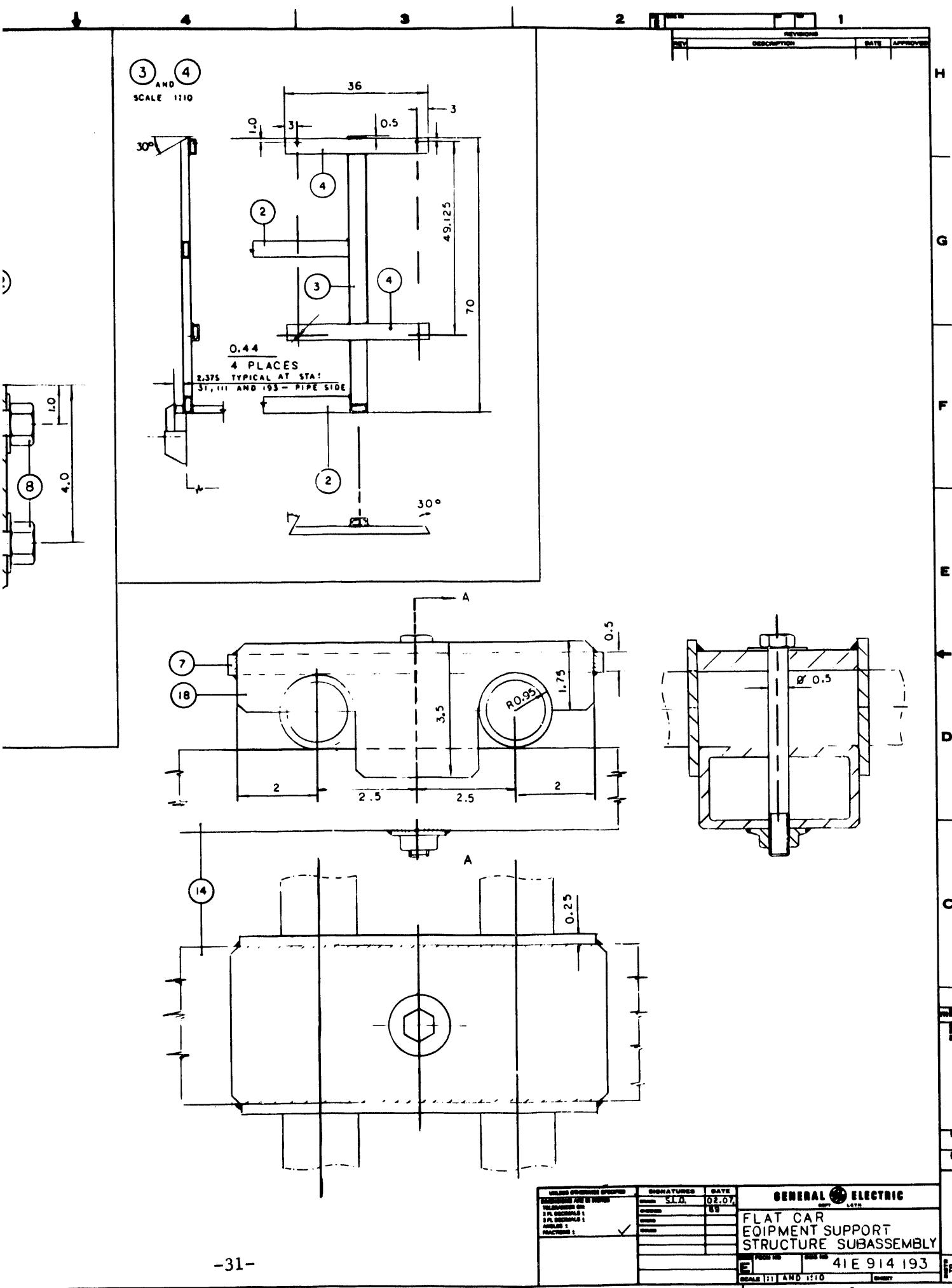
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STA 275

STA 193

ITEM	QTY	VENDOR	DESCRIPTION
18	4		PIPE GRIP PLATE
17	1		0.125" WALL WEB PLATE 38" x 15"
16	12		1/2" SQUARE HEAD WOOD SCREW; LENGTH 5"
15	20		5/8" - 11 WELD NUT
14	1		BOX BEAM - PIPE SUPPORT
13	1		STRUT
12	2		REINFORCEMENT WELD PLATE
11	2		THE MAIN STAKE POST LUG LINK
9	2		END LOAD MEMBERS 9:452" 0.19" WALL LENGTH 42" 2.65" TOP
10	1		10 42" 0.19" WALL LENGTH 15"
8	10		5/8" - 11 BOLT
7	2		PIPE CLAMP PLATE
6	6		STAKE POST LUG LINK
5	1		WIREWAY POST 4"2" 0.19" WALL; LENGTH: 55"; 3G" SH. TOP
4	2		CROSS BEAM
3	1		ELECTRICAL CONTROL UNIT POST BOX BEAM 42" 0.1875" WALL; LENGTH 70"
2	2		LONGITUDINAL BOX TIES 4"2" 0.1875" WALL; LENGTH 76" ; STL
1	3		TRANSVERSE FLOOR BOX BEAMS 4"2" 0.1875" WALL; 116.5" LENGTH; STEEL A36
ITEM QTY VENDOR DESCRIPTION			
NAME ORGANIZATION SPONSORED DESIGNERS AND ENGINEERS APPROVALS 2 PL. APPROVALS: 2 PL. APPROVALS: APPROVAL: APPROVAL:  ✓		SIGNATURES	DATE
		GENERAL ELECTRIC	
		FLAT CAR	
		CWS EXPERIMENTAL EQUIPMENT	
		SUPPORT STRUCTURE	
		41E914192	
		SCALE -	
		EQUIPMENT	





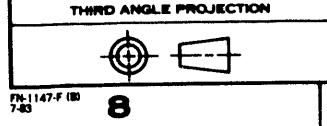
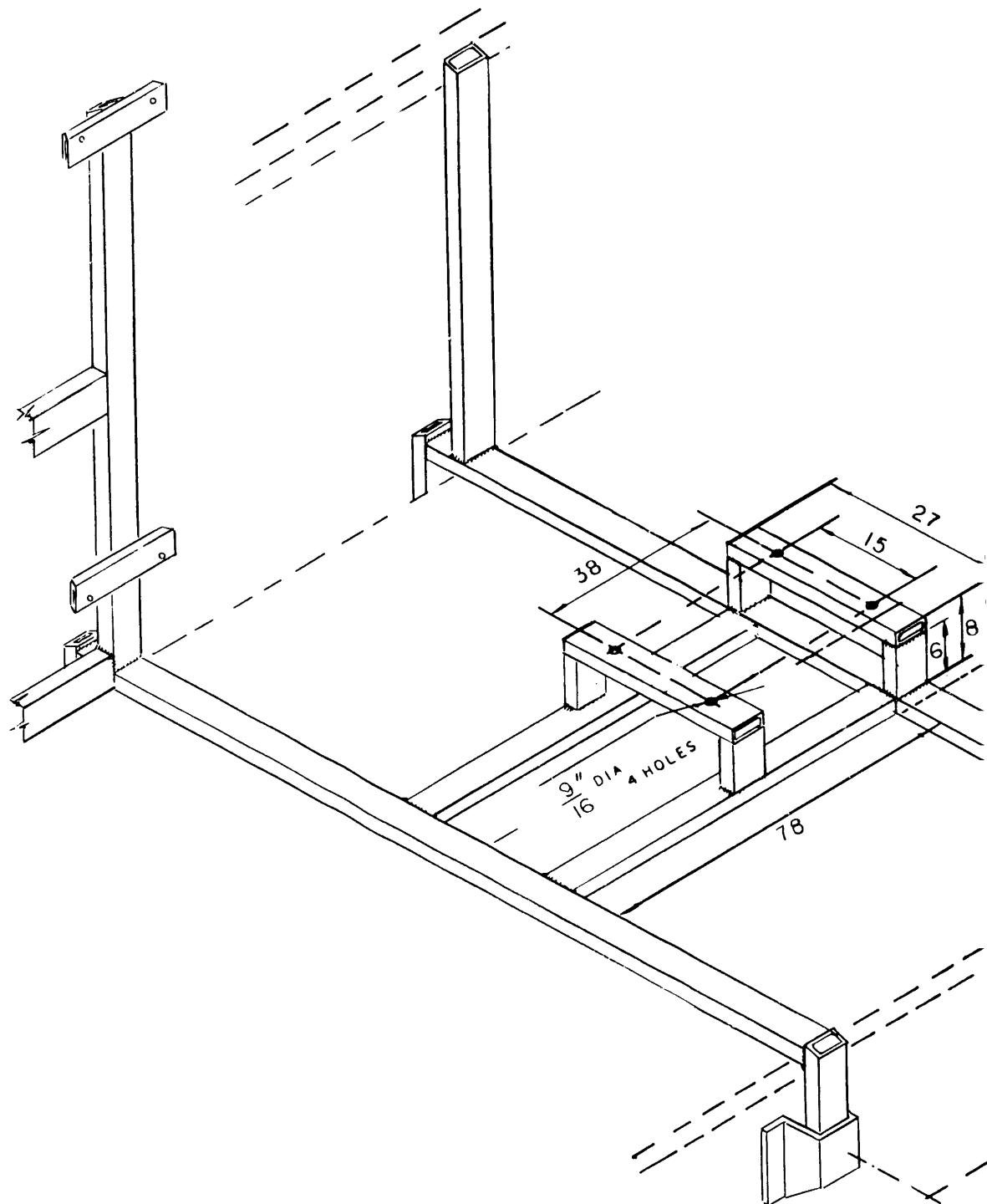
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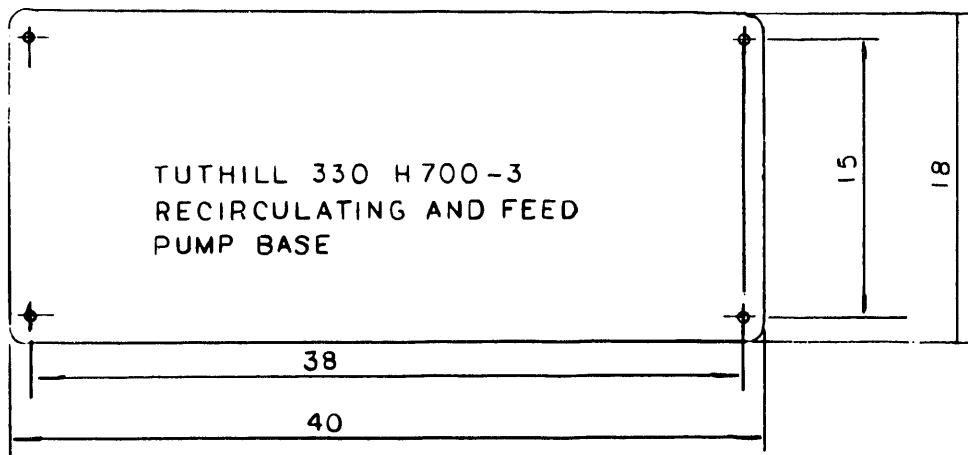
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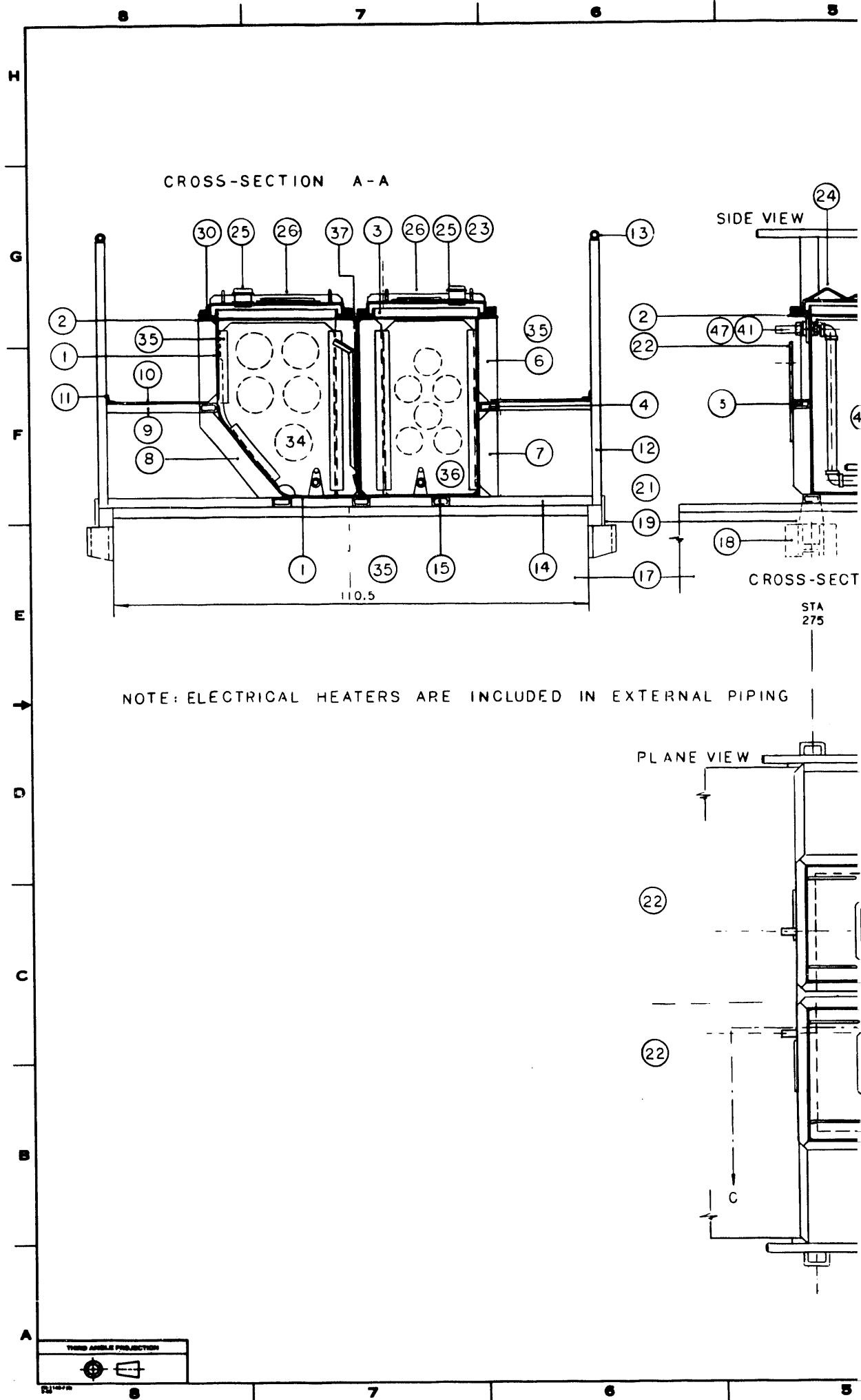
TUTHILL 330 H700-3  
RECIRCULATING AND FEED  
PUMP BASE

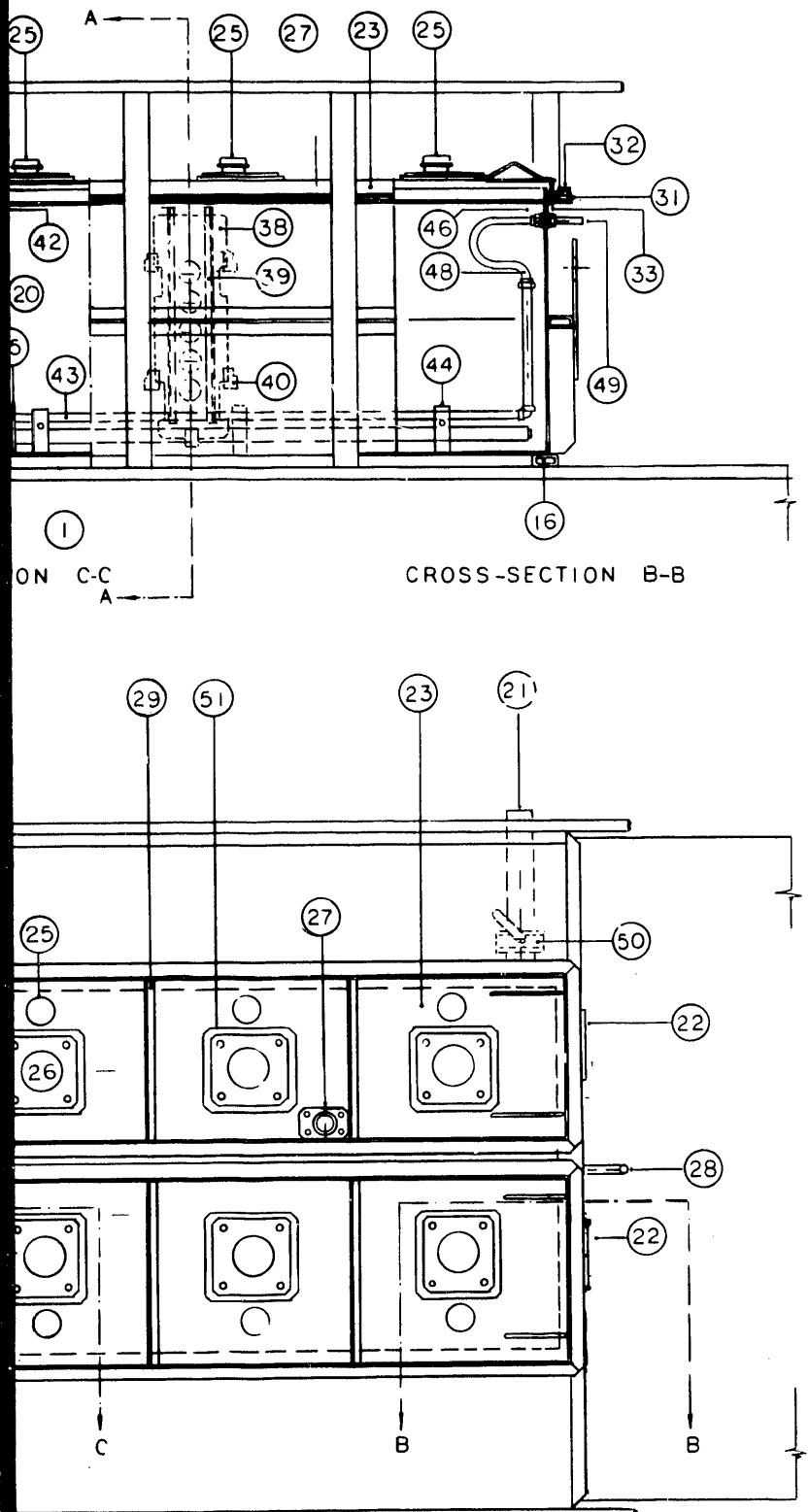


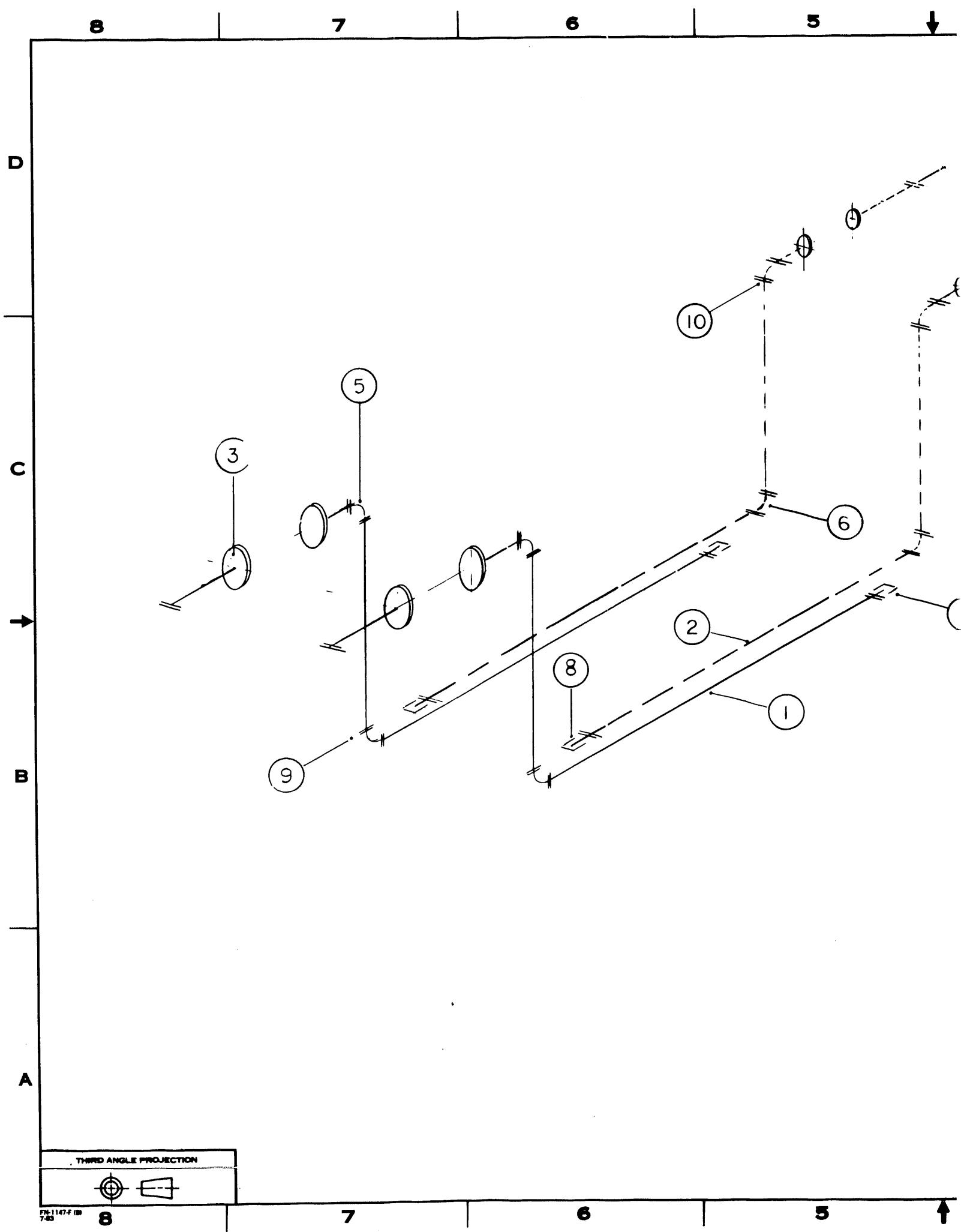
STA 193

### STA III

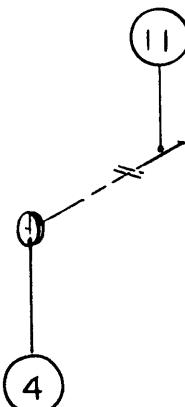
32-



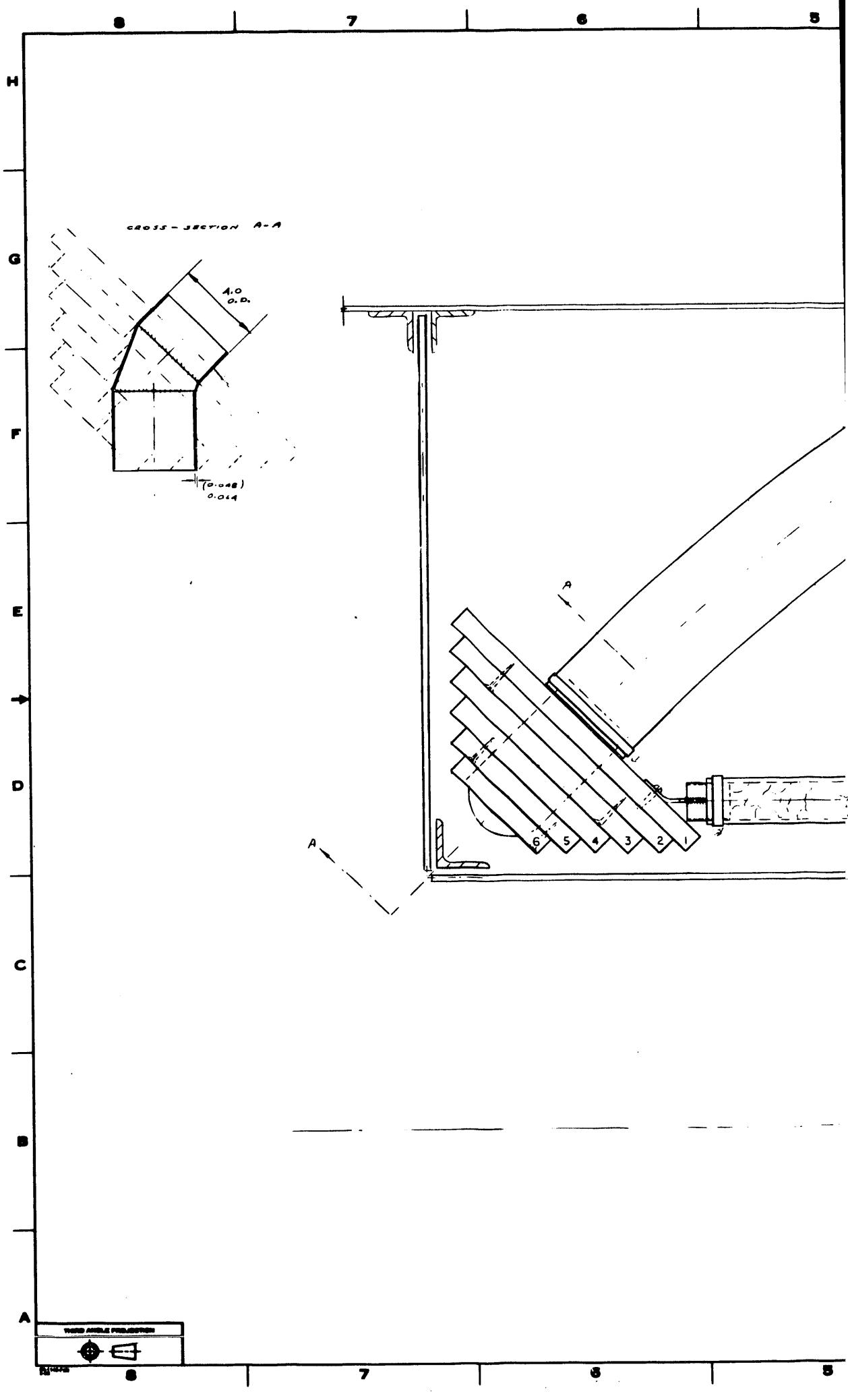




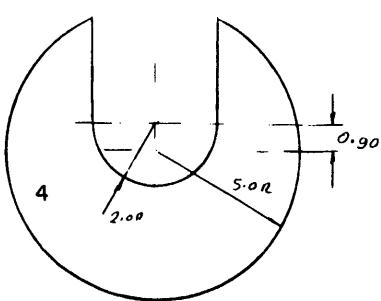
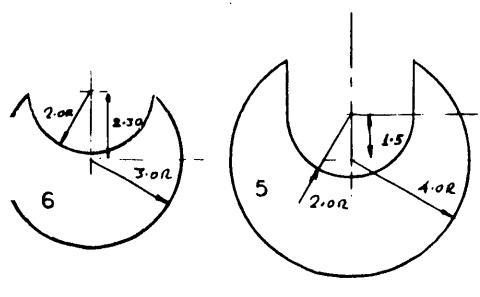
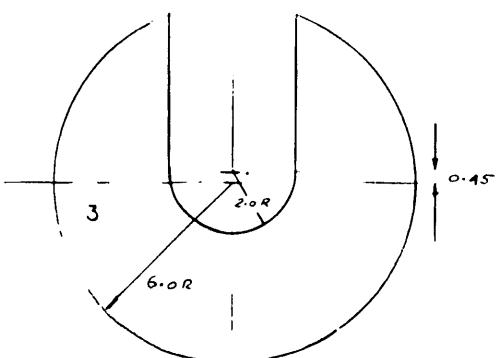
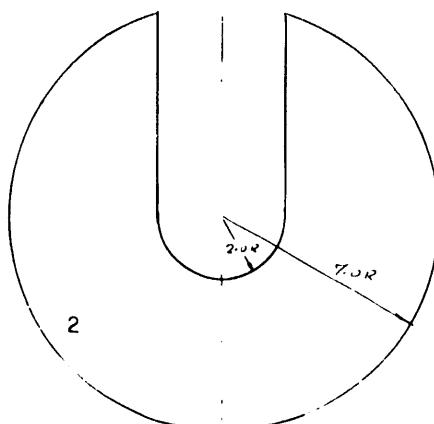
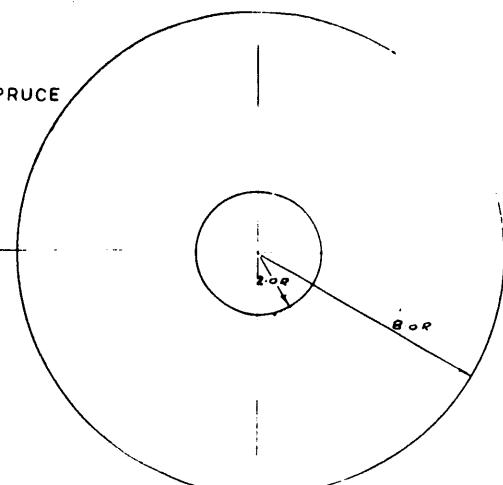
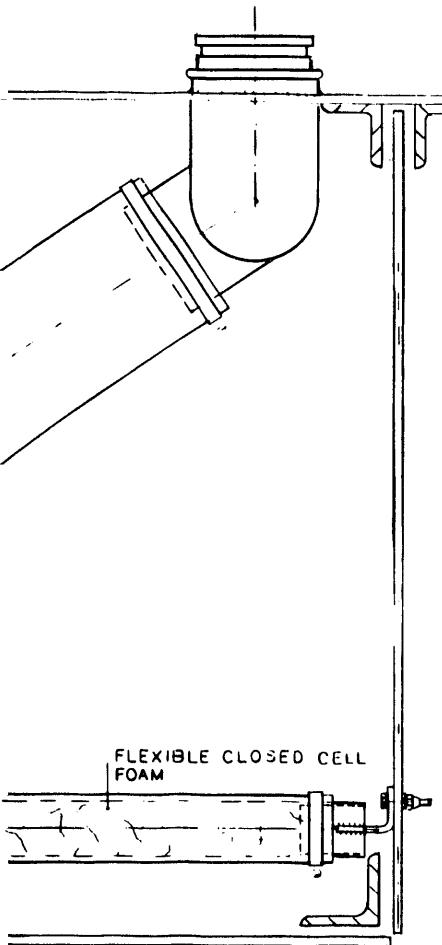
<b>D</b>	ITEM NO	SK	REV	<b>1</b>
	REVISIONS			
REV	DESCRIPTION		DATE	APPROVED



11	2	VICTAULIC COMPANY OF AMERICA	1" NIPPLE N° 40
10	12	VICTAULIC COMPANY OF AMERICA	1" STYLE 77 STANDARD COUPLING
9	12	— II —	2" STYLE HP-70 ES END SEAL COUPLING HOT DIP GALVANISED
8	2	— II —	1" N° 60
7	2	— II —	2" CAP N° 60
6	4	— II —	1" N° 10
5	4	— II —	2" 90° ELBOW N° 10
4	4	— II —	1" N° 41
3	4	— II —	FLANGED ADAPTER NIPPLE N° 41 ; 2" I.D.
2	25 FT		1" I.D. 0.1575 WALL GALVANISED STEEL PIPE
1	25 FT		2" I.D. 0.1875 WALL GALVANISED STEEL PIPE
ITEM	QTY	VENDOR	DESCRIPTION

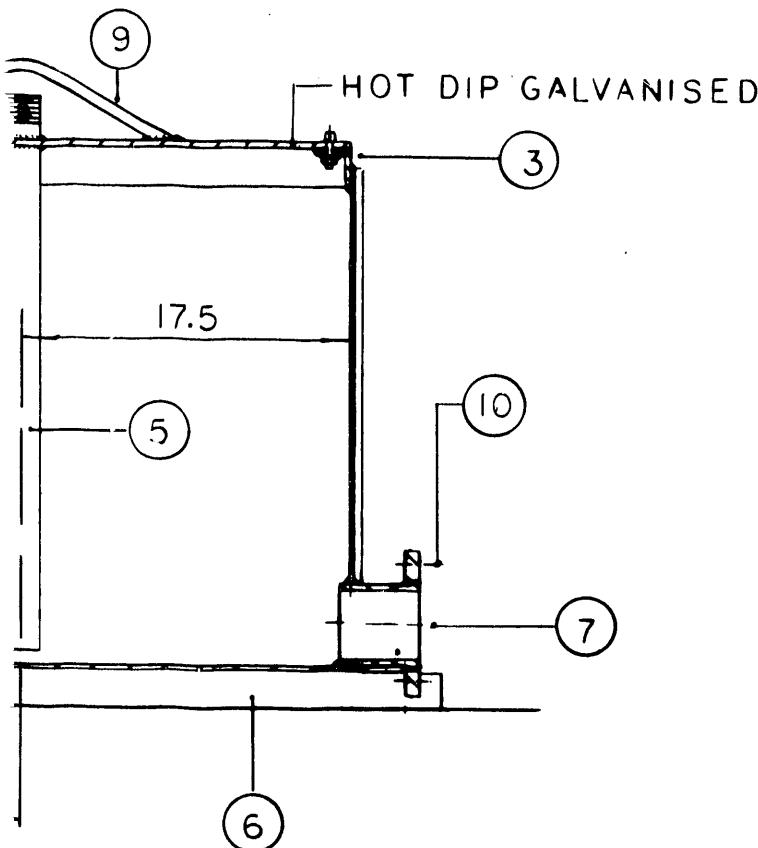


MTL., ITEMS 1-6: SPRUCE



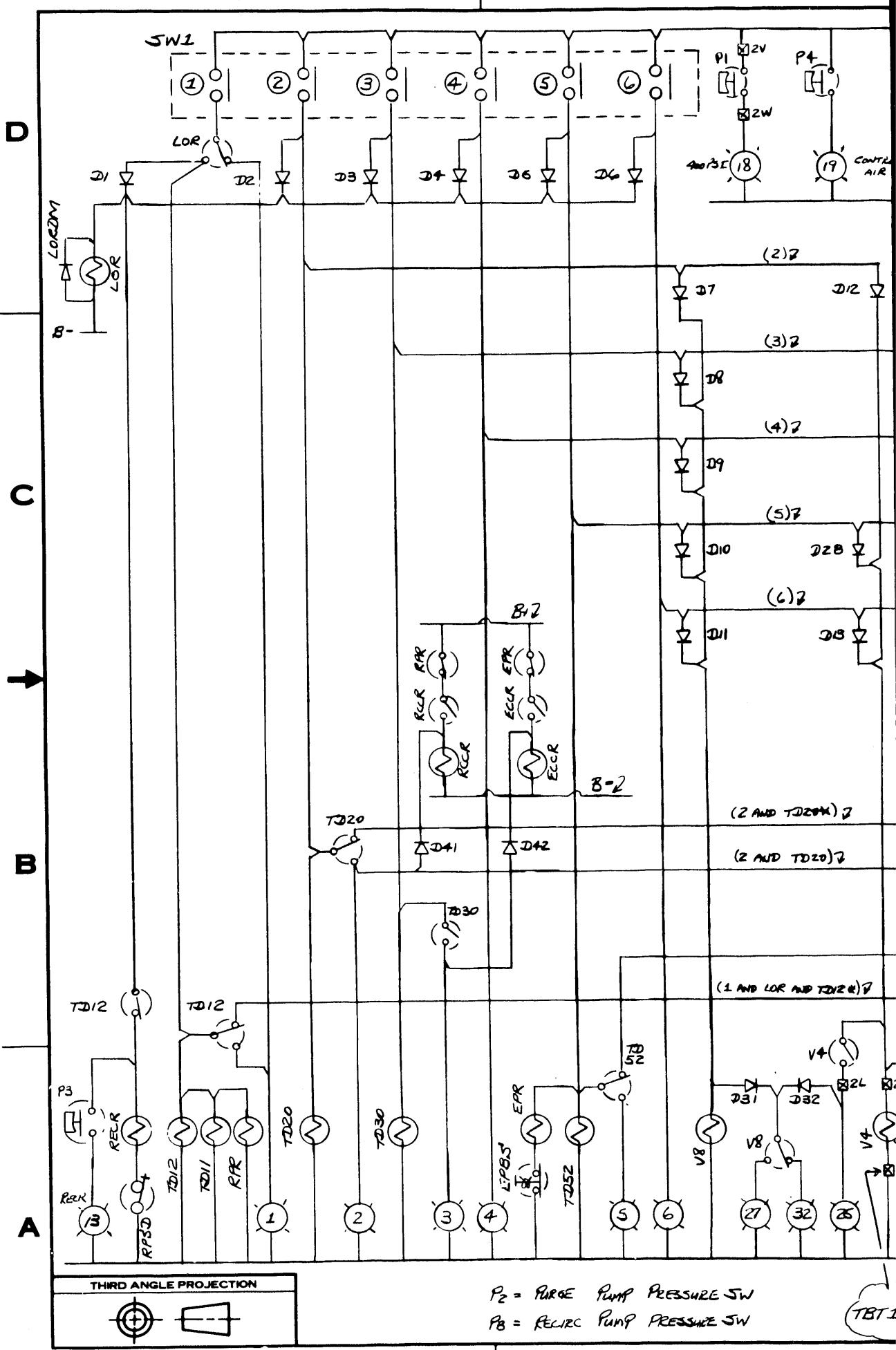


ISON B-B



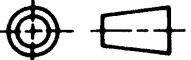
10	4" THREADED FLANGE 150 LB
9	LUG
8	SEAL
7	4" BUTTERFLY VALVE 815W ATTACH. FLANGE
6	MOUNTING BEAMS
5	1.5" I.D. TUBE
4	WELD NUT N 264
3	BOLT 5/16-18 N22
2	COVER PLATE
1	TANK WALLS-EPOXY COATED FROM INSIDE

4	3	2	1
GENERAL ELECTRIC	CLEAN WATER AND COAL SLURRY TANK		
41 D 715 481	4	3	2



$P_2$  = PURGE PUMP PRESSURE JW  
 $P_3$  = RECIRC PUMP PRESSURE JW

### THIRD ANGLE PROJECTION



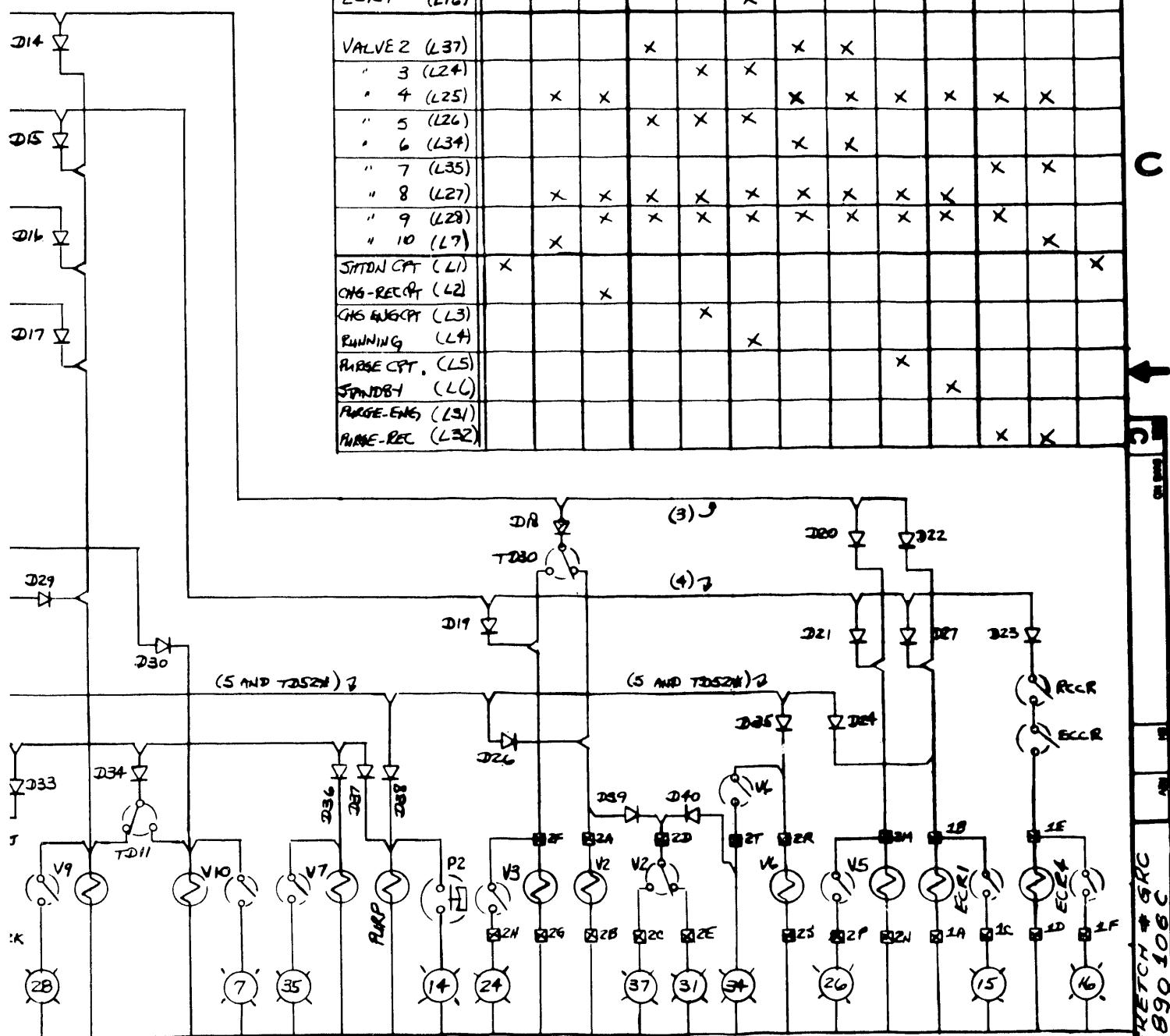
REV A 03/08/89 DEC  
DEL TDSI, ADD EPDS, RPSI

2

SIZE C DING NCO

1

		REVISIONS A						DATE		APPROVED	
		DESCRIPTION									
		①	②	③	④	⑤	⑥	⑦	⑧	⑨	⑩
DEVICE	START	CHARGE RECIRC	CHARGE ENGINE	RUN	PURGE ENGINE	STOP	SHUT DOWN				
	TO	T <sub>AO</sub>	TO	T <sub>SO</sub>	TO	T <sub>IO</sub>	TO	T <sub>IE</sub>	T <sub>SO</sub>		
TD11											X X
TD12											X
TD20		X									
TD30			X								
TD52							X				
REC R (L13)		X	X	X	X	X	X	X	X	X	X
PURP (L14)						X	X			X	X
ECR1 (L15)			X	X	X	X					
ECR4 (L16)				X							
VALVE 2 (L37)			X		X						
" 3 (L24)		X	X		X	X					
" 4 (L25)						X	X	X	X	X	X
" 5 (L26)			X	X	X						
" 6 (L34)						X	X				
" 7 (L35)										X	X
" 8 (L27)		X	X	X	X	X	X	X	X		
" 9 (L28)			X	X	X	X	X	X	X	X	X
" 10 (L7)		X									X
SATION CPT (L1)	X										
CHG-RECPT (L2)			X								
CHG-FUELCPT (L3)				X							
RUNNING (L4)					X						
PURGE CPT. (L5)								X			
STANDBY (L6)									X		
PURGE-ENG (L31)											
PURGE-REC (L32)								X			



18-

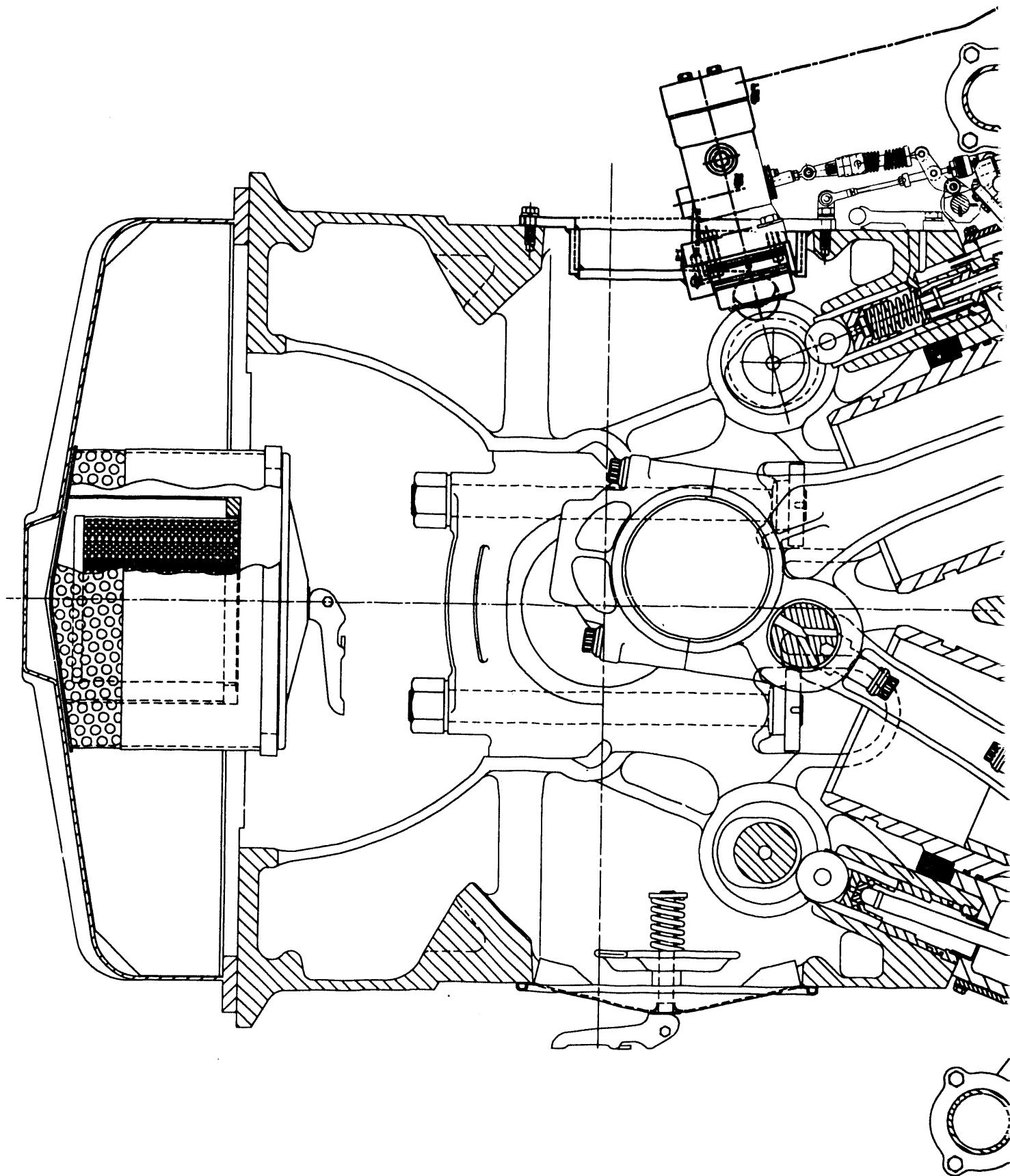
-37-

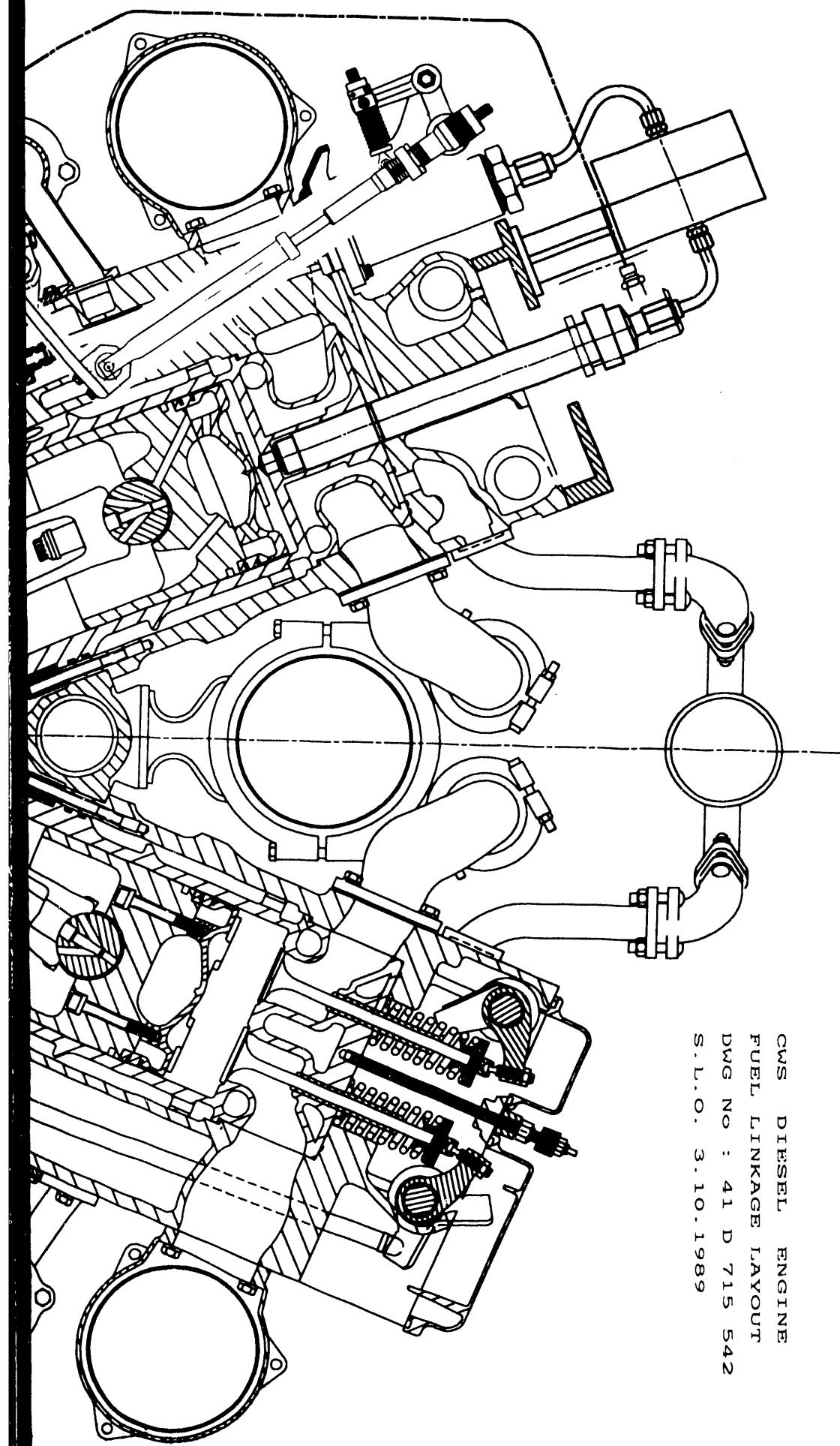
REFERENCE: RMS SKETCH 1026

SIZE	PCBM NO	DWG NO	DRAFTS 1 OF 1
C	48C 1-6-89	41C 640527	
SCALE		SHEET 1 OF 3	

2

1





CWS DIESEL ENGINE  
FUEL LINKAGE LAYOUT  
DWG NO : 41 D 715 542  
S. L. O. 3.10.1989

# END

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DATE  
FILMED

6/24/92