

INTERIM FINAL TECHNICAL REPORT

September 1, 1991 through August 31, 1992

**Project Title:** CFBC Evaluation of Fuels Processed from Illinois Coals

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**ABSTRACT**

The fuels studied in this project are (a) flotation slurry fuel beneficiated from coal fines at various stages of the cleaning process and (b) coal-sorbent pellets made from the flotation concentrate of the same beneficiation process using corn starch as binder. These fuels are investigated in a 4-inch internal diameter circulating fluidized bed combustor (CFBC). Combustion data such as  $\text{SO}_2$ ,  $\text{NO}_x$  emissions, combustion efficiency and ash mineral matter analyses from these fuels are compared with similar parameters from a reference coal burnt in the same fluidized bed combustor.

The combustion experiments demonstrated that the three coal-water slurry fuels and the pellet fuel employed in the present tests could burn well in the CFBC unit. Bed temperature control could easily be maintained with the slurry fuels, and provided the bed temperature did not fall below 1100-1200°F, it could be brought up to operating conditions solely on the slurry fuel. Bed temperature control was even better with the pellet fuel tested, and the bed could be slumped to even lower temperatures.

The combustion tests showed that the combustion efficiency of the slurry fuels and the pellets were quite comparable with that of the standard coal in the range of 91-98%.

Sulfur dioxide emissions in lbs per million Btu from the slurry fuels were low enough to satisfy EPA emissions requirements with Ca/S ratios of 1.5 or less. At these low Ca/S ratios, the slurry fuels and the pellet emitted less  $\text{SO}_2$  than the standard coal. Increasing the Ca/S ratios showed that the standard coal  $\text{SO}_2$  emissions reduced at a faster rate than the  $\text{SO}_2$  emissions from the pellet and slurry fuels, because of the more efficient dispersion and gas-solid contact of the standard coal particles.

Oxides of nitrogen emissions were generally on the order of 0.3 lbs per million Btu from the slurry fuels under the conditions of the present tests, while that from the pellets were between 0.6 to 0.75 lbs per million Btu depending on bed temperature. In comparison, the oxides of nitrogen emissions from the standard coal varied from 0.5 to 0.8 lbs per million Btu in the bed temperature range of 1475-1625°F.

**MASTER**

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## EXECUTIVE SUMMARY

Combustion experiments were conducted in a 4-inch internal diameter circulating fluidized bed combustor on three coal-water slurry fuels, a standard reference coal and a coal-sorbent pellet fuel. The three coal-water slurry fuels were obtained by taking samples at various stages of recovery from the Galatia preparation plant of Kerr-McGee Corporation. Particle size analysis of dried coal from the slurries were made and the results were reported in previous quarterly reports. Proximate and ultimate analyses results and mineral matter distribution in the above coal samples have also been reported.

In the combustion tests conducted this quarter, the coal-water slurry fuels were prepared by either adding or decanting water such that the solids concentration of the slurries varied from 42-46%, as this solids loading was found best for injection and for slurry transport into the combustor. Using a peristaltic pump and an in-house fabricated pneumatic injection system, the three slurries were fed into the fluidized bed combustor once it had been brought up to steady state operating conditions on a run-of-mine coal. The combustor was then operated entirely on the coal-water slurry fuel and the combustion and emissions properties of the slurry fuels investigated. The variables measured during a test included temperatures at various points within the combustor, CO, CO<sub>2</sub>, O<sub>2</sub>, SO<sub>2</sub> and NO<sub>x</sub> emissions, coal-water slurry and air feed rates, recycle ratios and exit cyclone ash rejection rates.

Similar experiments were conducted on the standard coal and the coal-sorbent pellets made by using cornstarch as binder.

Results from the combustion experiments show that the three coal-water slurry fuels and the coal-sorbent pellets are excellent fuels with combustion and emissions properties equal to or better than the standard run-of-mine coal.

### Sulfur Dioxide Emissions

The SO<sub>2</sub> emissions of the slurry fuels were measured to be lower than those from the standard coal, except at high Ca/S ratios. At a temperature of 1550°F and a Ca/S ratio of 2.5, slurry fuel A yielded 0.8 lb/10<sup>6</sup> Btu, slurry fuel B emitted about 1 lb/10<sup>6</sup> Btu and slurry fuel C (which had the highest sulfur content) emitted about 1.15 lb/10<sup>6</sup> Btu.

The standard run-of-mine coal emitted 1.2 lb/10<sup>6</sup> Btu. These values are comparable values under the conditions of the test and are not the lowest emissions levels that can be achieved when the system is optimized. Under similar conditions of operation, the pellet fuel emitted about 1.15 lb/10<sup>6</sup> Btu.

### Oxides of Nitrogen Emissions

Oxides of nitrogen emissions for the slurry fuels were uniformly lower than for the standard coal. For the three slurry fuels tested, NO<sub>x</sub> emissions varied between 0.25 to 0.4 lb/10<sup>6</sup> Btu; and for the pellet fuel, the measured NO<sub>x</sub> emissions were on the order of 0.6 lb/10<sup>6</sup> Btu. In comparison, the

oxides of nitrogen emissions for the standard coal varied between 0.48 to 0.85 lb/10<sup>6</sup> Btu, depending on bed temperature.

### Combustion Efficiency

Carbon conversion efficiencies ranging from 91 to 98% were measured for the slurry fuels and the standard coal. The pellets burnt extremely well and had a uniform carbon conversion efficiency of over 98%.

It may be concluded from the results of these comparative tests that the coal-water slurry fuels processed from the preparation plant fines considered in the present tests are desirable fuels with good combustion and emissions characteristics. The coal-sorbent pellets also exhibited good carbon conversion efficiencies in the CFBC burner with emissions of SO<sub>2</sub> and NO<sub>x</sub> somewhat lower than those of the standard coal.

## OBJECTIVES

The overall objectives for this one-year project are:

1. to demonstrate that new fuels derived from Illinois high sulfur coal, namely (a) coal-sorbent pellets and (b) coal-water slurry produced from froth flotation feed can be effectively utilized in a circulating fluidized bed combustor,
2. to compare the carbon conversion efficiencies,  $\text{SO}_2$  and  $\text{NO}_x$  emission levels and Ca/S ratios needed to meet EPA regulations from the above fuels with those measured under similar operating conditions with a standard IBCSP coal, and
3. to analyze ash and spent limestone residues with a view to proposing waste disposal strategies for the combustion residues resulting from these new fuel forms.

The specific goals to be achieved as stated in the proposal are as follows:

1. determination of the carbon conversion efficiency of (a) the froth flotation coal water slurry fuel developed at the ISGS under CRSC sponsorship, and (b) the coal-sorbent pelletized fuel developed by ISGS under CRSC funding.
2. determination of the Ca/S mole ratio requirements for the coal-water slurry fuel to meet EPA  $\text{SO}_2$  emissions requirements.
3. determination of the sulfur capture efficiency of the coal-sorbent pellet fuel
4. evaluation of the mineral matter elemental distribution in the combustion residues from the above fuels when burned in a laboratory scale 4" internal diameter circulating fluidized bed combustor
5. determination of the  $\text{NO}_x$  emission levels when burning the coal-water slurry and the pelletized fuel in a CFBC unit
6. comparison of the carbon conversion efficiency, carbon balances,  $\text{SO}_2$  and  $\text{NO}_x$  emission levels and combustion waste analyses of the coal water slurry and pelletized fuel with equivalent values obtained from a standard coal

The accomplishment of these goals involve the following tasks: (a) fuels procurement, (b) fuel testing and analysis, (c) fuels preparation, (d) installation of limestone feeder, (e) combustion testing in a 4" internal diameter circulating fluidized bed combustor, (f) combustion residues analysis using EDX, and (g) data analysis and report preparation.

## INTRODUCTION AND BACKGROUND

Increased utilization of Illinois coals can be promoted by developing clean burning coal-based fuels which are low in sulfur and high in heating value. One such project, funded by CRSC, is aimed at developing coal-sorbent pellets from coal fines. A second CRSC supported project recovers fine coal from plant waste employing various flotation techniques, producing a slurry with higher solids concentration and Btu content. The market potential of these fuels will depend on the combustion and emissions characteristics of the coal/sorbent pellets and the coal slurry. This can be established only by combustion testing under conditions simulating actual boiler firing. Because of the small quantities of the fuels being produced, laboratory-scale combustors are best suited to demonstrate their utility and emissions characteristics.

There is a need to evaluate the burning characteristics of the coal-sorbent pellets and the coal water slurry to determine whether they can be burned easily and with good carbon conversion efficiencies. In the case of the coal-sorbent pellets, it is necessary to quantitatively evaluate the sulfur capture efficiency of the pellets, in comparison with the case where the coal and sorbent are fed separately, to establish the merits of the coal-sorbent pelletization process. Additionally, it is necessary to investigate how the pelletization process, namely the mixing of the sorbent with the coal matrix influences the porosity and carbon burnout histories of the coal. The sorbent Ca/S ratios needed to meet EPA requirements with the coal water slurry and its carbon conversion efficiency needs to be evaluated in comparison with standard Illinois coals to demonstrate the usefulness of the separation process.

The research currently being performed in this project addresses the above needs to improve the usefulness of fuels produced from high sulfur coals.

## EXPERIMENTAL PROCEDURES

### I. Equipment and Instrumentation

The experiments are being conducted in the 4" internal diameter circulating fluidized bed combustor shown schematically in Figure 1(a). The combustor is lined with a castable refractory to reduce heat losses. As shown in Figure 1(a), a blower supplies fluidizing air which is split into two streams. The main stream enters the fast fluidized bed section of the combustor through a distributor plate specially designed to provide even fluidization. This section of the air duct also houses a propane-fired preheat system, which is utilized to bring the bed solids up to temperatures required to ignite the main fuel. Unburnt fuel, limestone and ash entrained by the gases in the main bed column pass through a refractory-lined hot cyclone, which traps the larger particles and deposits them into an auxiliary bubbling bed attached to the bottom end of the hot cyclone. The second smaller air stream enters this bubbling bed into which the carry-over solids from the fast fluidized bed trapped by the hot cyclone are deposited. A non-mechanical seal ensures that this unburnt fuel and bed solids flow from the bubbling bed into the fast fluidized bed and not vice-versa. Both air streams are metered with ASME nozzles and incorporate

control valves for adjusting the flow velocities in the fast fluidizing and bubbling bed sections of the combustor.

Crushed and sieved coal is fed from a pressurized hopper via a screw feeder pneumatically into the dense portion of the fast fluidized bed, using metered high pressure air. Sized limestone, stored in a separate hopper, is fed simultaneously into the air stream, conveying the coal into the bed. Both coal and limestone feed systems have been calibrated individually.

Two quartz glass-lined observation ports, one located in the dense bed at the bottom, and the other located near the top in the dilute phase or transport section of the bed, serve for visual monitoring of the combustion process. The circulating fluidized bed combustor is instrumented with chromel-alumel thermocouples at various positions for measuring temperature. The thermocouples are connected to a selector switch and, thence, to a digital readout meter.

Solids too small to be captured by the hot cyclone are trapped in a multiclone, mounted at the hot cyclone exit. In the present system, these multiclone solids are not reinjected into the bed. The multiclone solids are later analyzed for heat content, using an adiabatic calorimeter. Combustion gases are drawn off from a point at the exit of the multiclone, filtered through 2-5 micron particulate filters, and conveyed via heated lines to an instrument panel for determining gas composition. Carbon monoxide and carbon dioxide are measured with Beckman NDIR analyzers, oxygen with a Beckman 755 paramagnetic analyzer, oxides of nitrogen,  $\text{NO}_x$ , with a Thermoelectron 10 AR chemiluminescent analyzer and sulfur dioxide with a Beckman IR analyzer.

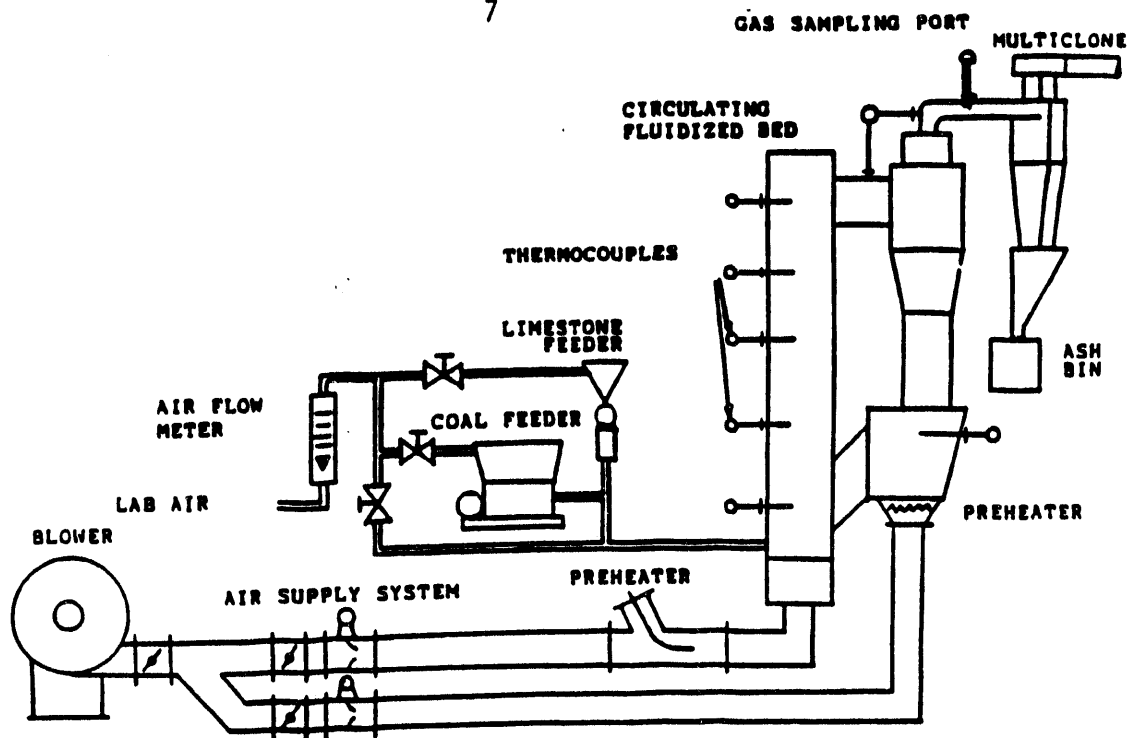
#### Coal Water Slurry Feed System

When firing coal-water slurry (CWS) fuels, the feed system shown in Figure 1(b) is used. The CWS fuel is stored in a container fitted with a motor-driven stirrer, to maintain uniformity of slurry composition. The slurry is pumped by a speed-controlled peristaltic pump to the CFBC and injected pneumatically into the region above the dense portion of the bed, using a water-cooled injector. Due to the longer residence times in the fluidized bed, and the effective mixing of the slurry droplets and the bed material, it is not necessary to provide a finely atomized slurry to the bed. Hence, a low pressure system such as the one illustrated in Figure 1(b) has been found adequate in previous tests, and is the one used in the present tests.

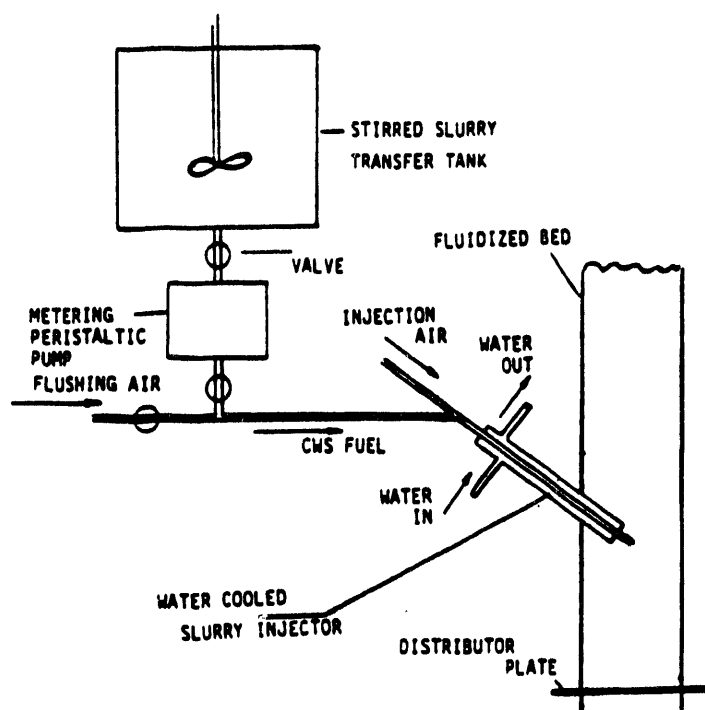
#### Pellet Feed System

The coal-sorbent pellets are injected pneumatically into the dense bed using a vibrating feeder. Feed rates are controlled by changing the frequency of vibration. Feed rates are measured by feeding a known weight of pellets and measuring the time in which this known weight of pellets is utilized by the burner.





**Figure 1(a). Schematic of 4" Diameter Circulating Fluidized Bed Facility Used for Fuels Testing**



**Figure 1(b). Schematic of CWS Slurry Injection System**

## II. Test Procedures

### CFBC Combustion and Emissions Tests

The combustion testing of the coal slurry and pellet fuels involves the following steps:

- \* The CO, CO<sub>2</sub>, O<sub>2</sub>, NO<sub>x</sub> and SO<sub>2</sub> analyzers are calibrated at the beginning and at several times during a test burn.
- \* The CFBC combustor is filled with the proper amount of bed material (sand or limestone).
- \* The propane preheat system is fired the bed material and unit is brought up to about 1100-1200°F. This step takes several hours.
- \* Coal and limestone hoppers are filled with prepared standard coal and limestone sorbent, respectively.
- \* The coal feed is initiated and the CFBC unit is brought up to operating temperatures of around 1500°F on the standard coal. The operation of all sampling and control systems are checked.
- \* For tests with standard coal and the slurry and pellet fuels, typical values of operating variables are as follows:

fluidization velocity 9 ft/sec  
Ca/S ratio 1-4  
Bed temperature ≈ 1450-1650°F

These parameters are kept constant with all the fuels, so that comparison of the combustion and emissions parameters can be made under identical conditions of operation.

- \* During the coal-sorbent pellet tests, the pellets are injected pneumatically into the bed. No additional limestone sorbent will be injected during initial tests. If SO<sub>2</sub> emissions are higher than EPA limits, further tests will be conducted with limestone injection.
- \* With the coal-water slurry fuels, a special in-house fabricated pneumatic slurry injection system, Figure 1(b), is employed to inject the slurry fuel into the combustor.
- \* Six to ten test runs are planned to be made. Each test run is made after the combustor has reached steady state conditions. Combustor steady state conditions are usually achieved after 30-48 hours of operation. Where test fuel supplies are limited, the procedure adopted is to first bring the combustor to steady state operation on the standard coal or another Illinois coal, and then change the fuel feed to the test coal, slurry or pellet fuel only for the duration of the steady state data acquisition period.

\* The variables measured during a test include:

- fuel and air mass flows
- air superficial velocity
- bed temperature
- other temperatures at various combustor locations
- combustion gas analysis comprised of CO, CO<sub>2</sub>, O<sub>2</sub>, NO<sub>x</sub> and SO<sub>2</sub> emissions
- test duration time
- quantity of ash collected in cyclones during test period

Combustion generated ash and spent limestone from the slurry fuel, pellets and standard coal tested are analyzed. The heat content of the elutriated unburnt carbon is determined from calorimetry tests. Spent limestone and ash are prepared on metal stubs and subjected to energy dispersive x-ray (EDX) analysis to determine the elements present in the samples.

### Sample Analysis

#### (a) Solids Concentration Determination of Slurry Samples

Three samples of slurry fuel were analyzed to determine their solids concentration. This are:

- (1) the dilute coal-water stream from the flotation cell,
- (2) a flotation concentrate obtained by gravity concentration, and
- (3) the centrifuge product containing a high solids loading.

In each case, the solids concentration loading was determined by taking a known weight of well-mixed sample of each of the above fuels, and driving off the moisture by heating in a vacuum oven maintained at less than 100°C and measuring the weight of the dried sample at regular intervals till no weight change was detected in the dried sample.

#### (b) Proximate and Ultimate Analyses

Proximate and ultimate analyses of the above three slurry fuels and the size graded reference Illinois No. 5 coal were obtained using standard ASTM procedures at the Coal Technology Laboratory at Carterville, Illinois.

#### (c) Particle Size Analysis

Particle size analysis in the range below 125 microns was obtained utilizing a Leeds and Northrup Microtrak Model 7995-10 particle size analyzer. A schematic of the instrument is shown in Figure 2. In this version of the instrument, a laser beam is projected through a transparent cell which contains a stream of moving particles suspended in a liquid. Light rays which strike particles are scattered through angles which are inversely proportional to their sizes. The rotating optical filter transmits light at a number of predetermined angles and directs it to a photodetector. Electrical signals proportional to the transmitted light flux values are processed by a microcomputer system to form a multi-channel histogram of the particle size distribution.

#### (d) Mineral Matter Analysis

The mineral matter analysis of the coal in the three slurry fuels and the reference Illinois No. 5 coal was conducted with a Hitachi H-600 analytical electron microscope operating both in the transmission and the scanning-transmission electron microscopy (STEM) modes. With STEM, a Tracor-Northern energy dispersive x-ray (EDX) Model 5500 analysis system was employed. The specimen samples were mounted on adhesive copper grids and examined at 100kV in the electron microscope. The samples were uncoated.

#### Data Analysis

From the measured data the following parameters will be computed:

- \* excess-air ratios
- \* Ca/S mole ratios
- \* carbon conversion efficiency
- \* sulfur capture efficiency %
- \* SO<sub>2</sub> emissions levels in lb/10<sup>6</sup> Btu
- \* carbon balances

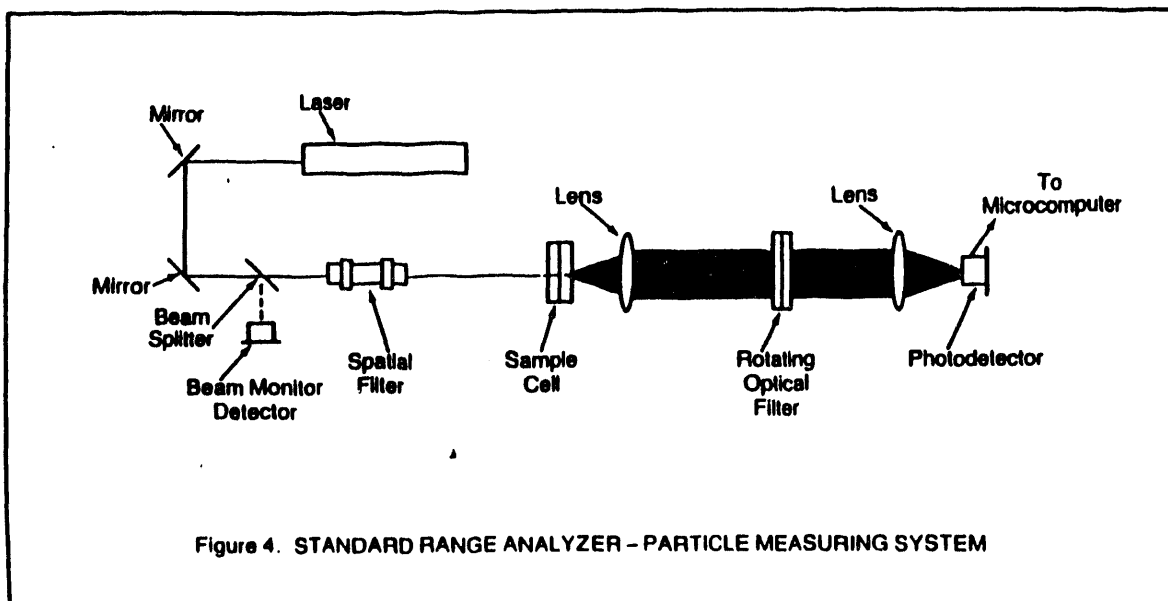


Figure 2. Schematic of Microtrak Particle Size Measurement System

## RESULTS AND DISCUSSION

### Fuels Preparation

Experiments were conducted with the CFBC brought up to operating temperature to determine if the coal-water slurry fuels had the proper solids concentration loading for smooth and continuous operation. Solids concentration loading was varied between 40 to 60% by adding or decanting water from the as-received coal-water slurry samples. If the solids loading was too high, some difficulty was experienced in transporting the slurry from the pump to the injector. Also, the injector tip which was in contact with the hot combustion gases tended to clog. If the solids concentration was too low, excessive amounts of water was being fed into the bed; and bed temperature was difficult to maintain, especially at higher bed temperatures. As a result of these experiments, it was determined that a solids concentration loading of 42-46% was best suited for the comparison experiments that were being performed. Therefore, the slurry fuels solids loading was altered to fall in this range. It was also determined that a common household detergent such as Cheer added in the amount of 15gms/50kg of slurry fuel also enhanced the flow properties of the slurry fuels.

The coal-sorbent pellets were obtained from researchers at ISGS. They contained ground limestone so that the Ca/S ratio of the pellet was 2.0. The pellets were 0.125 inches in diameter and 0.375 inches long. As received, the pellets were quite moist and fragmented easily. They were dried by blowing air over them until the moisture content was less than 5%.

### Combustion Test Results

The slurry fuels, standard coal and pellets were burnt in the CFBC unit under the conditions described above. Results of the combustion tests are discussed in the following sections, under the headings of Sulfur Dioxide Emissions, Oxides of Nitrogen Emissions and Combustion Efficiency.

### Sulfur Dioxide Emissions

Two types of tests were conducted with the fuels. In one series of experiments, the effect of bed temperature on  $\text{SO}_2$  emissions were investigated. In the second series, the influence of Ca/S ratio was measured. Where supplies of the fuel were limited, only one of the tests was possible.

Figures 3 and 4 illustrate the influence of bed temperature on  $\text{SO}_2$  emissions from slurry fuels A and B, respectively. Slurry fuel A is derived from the very low (5.6%) solids loading flotation column effluent of the preparation plant. Slurry B is the flotation concentrate fuel as developed by ISGS under ICCI sponsorship. The Ca/S mole ratios for the data of Figures 3 and 4 are 2.5 and 2.7, respectively. As seen from the figures, the effect of bed temperature on  $\text{SO}_2$  emissions is very similar for the two slurry fuels shown. These trends were also found to be similar for the standard coal and slurry fuel C.

The effect of bed temperature on the  $\text{SO}_2$  emissions from the pellet fuel for a Ca/S ratio of 2.0 is shown in Figure 5. Figure 6 depicts the comparative emissions levels of  $\text{SO}_2$  from the standard coal, slurry fuel A and slurry

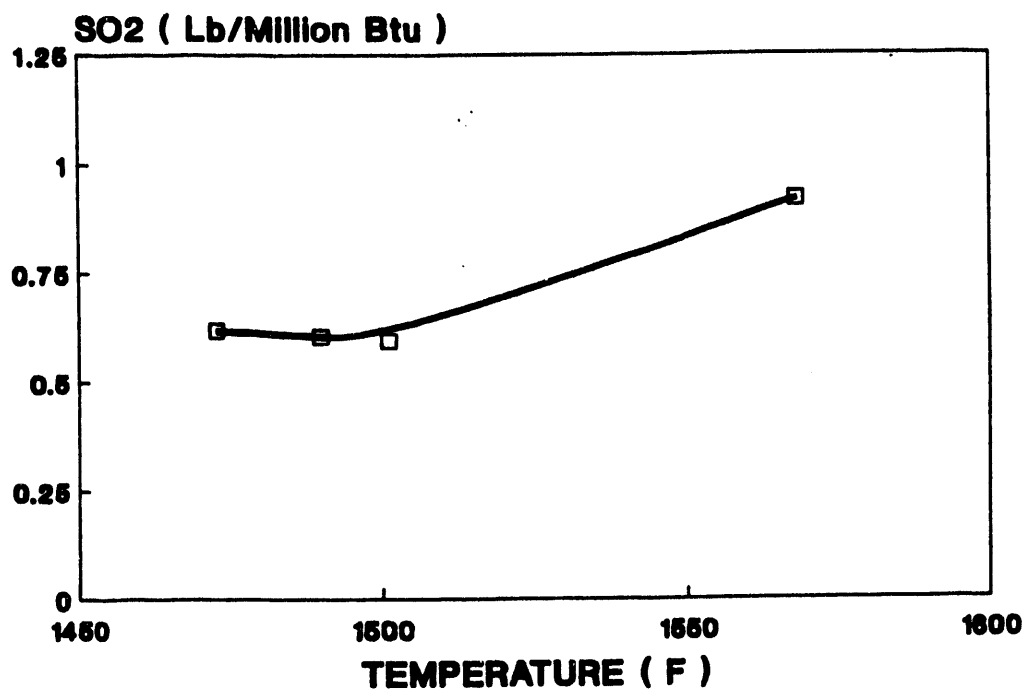


Figure 3. Variation of SO<sub>2</sub> Emissions with Bed Temperature;  
Slurry A, Ca/S = 2.5

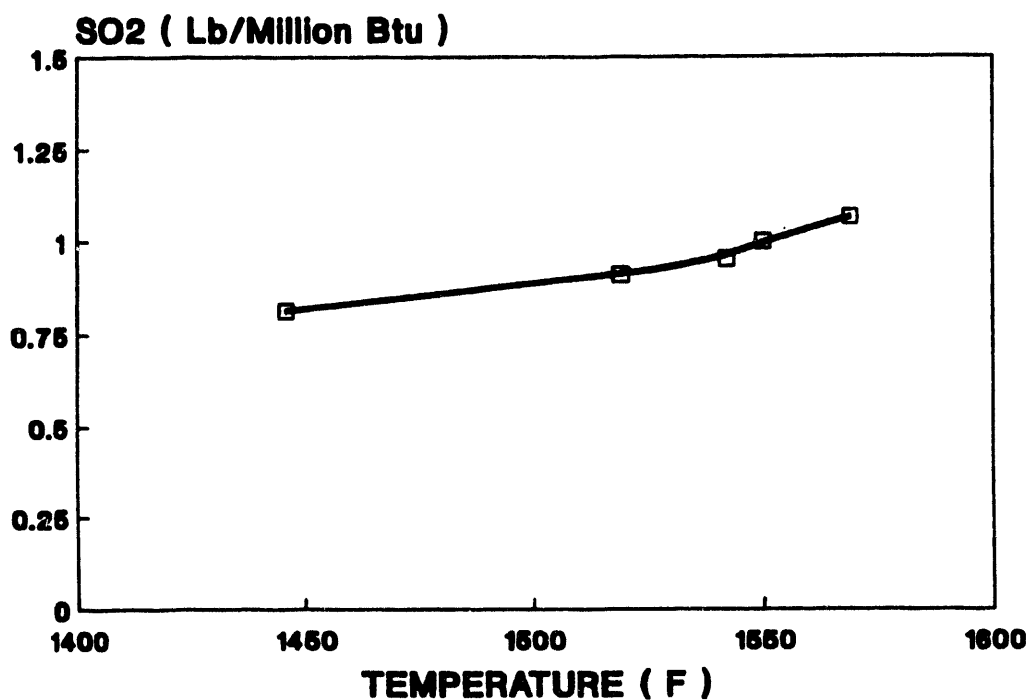


Figure 4. Variation of SO<sub>2</sub> Emissions with Bed Temperature  
Slurry B, Ca/S = 2.5

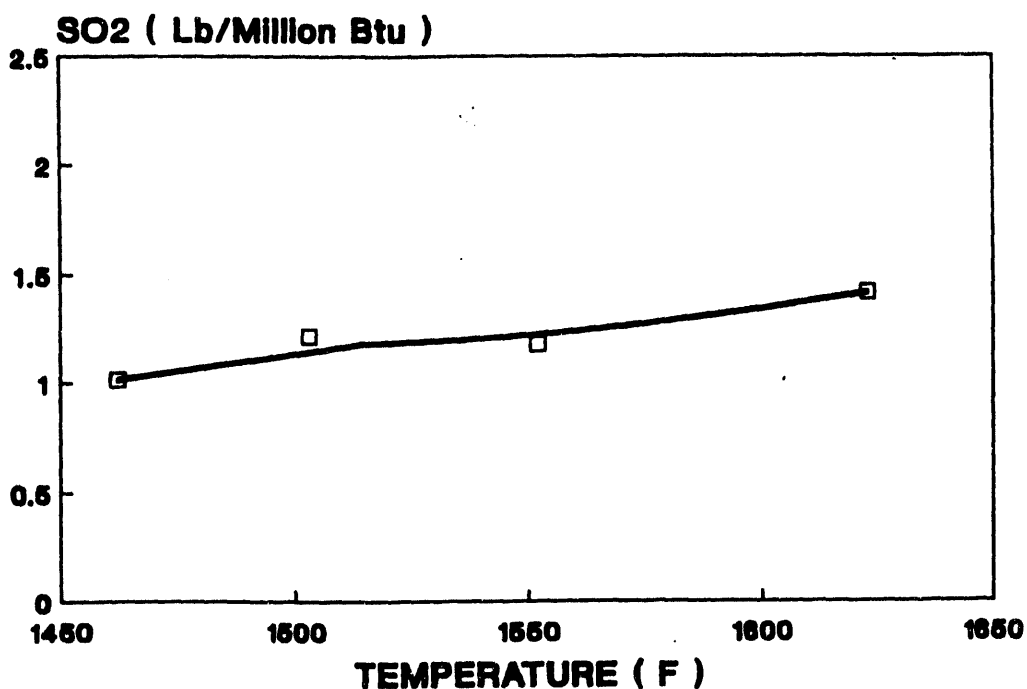


Figure 5. Effect of Bed Temperature on SO<sub>2</sub> Emissions;  
Coal-Sorbent Pellets, Ca/S = 2.0

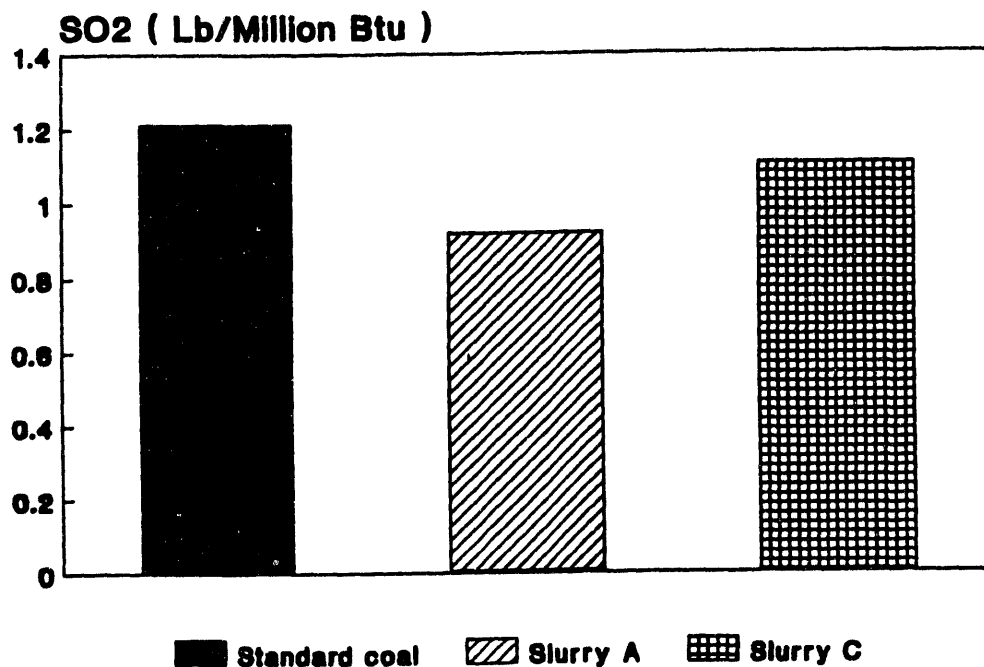


Figure 6. Comparative SO<sub>2</sub> Emissions for Standard Coal, Slurry A and  
Slurry C; Bed Temperature 1575°F, Ca/S = 2.5

fuel C at a bed temperature of 1575°F and a Ca/S ratio of 2.5. Generally, the slurry fuels yielded lower levels of SO<sub>2</sub> emissions than the standard coals, especially at lower Ca/S ratios.

The effect of Ca/S ratio on the slurry fuels and the pellets is shown in Figures 7 and 8 for a bed temperature of 1550°F. Slurry A coal contained about 1% sulfur, while slurry C coal contained 1.5% sulfur. The standard coal and the coal used in the pellets also contained 1.5% sulfur. At low Ca/S ratios less than Ca/S = 2.5, the slurry fuels emit lower levels of SO<sub>2</sub> in lbs per million Btu. Thus, with slurries of this type, and with fuel and operating conditions optimized, it may be possible to meet EPA emissions limits on SO<sub>2</sub> with very small Ca/S ratios.

With higher Ca/S ratios, it was found that the standard coal exhibited a more rapid decline in SO<sub>2</sub> emissions than the slurry fuels. This is seen in Figure 7 by comparing the levels from the standard coal and slurry C which has the same percentage of sulfur in the coal. This is attributed to the dispersion characteristics of the fuel and limestone in the fluidized bed. The slurry fuel is in the form of larger droplets than the standard coal. As the Ca/S ratio is increased, more limestone particles are dispersed in the bed; and since the coal particles are also more dispersed, the probability of SO<sub>2</sub> capture increases. This effect is not so strong for the slurry fuels, and the rate of decrease of SO<sub>2</sub> emissions with increasing Ca/S ratios is slower. Figure 8 shows the influence of Ca/S ratios on the pelletized coal fuel. Again, the decrease of SO<sub>2</sub> emissions with increasing Ca/S ratios is not as prominent as with the standard coal for similar reasons. However, the SO<sub>2</sub> release and absorption characteristics and histories are different for the slurries, standard coal and pellet fuels, and is evidenced by the lower SO<sub>2</sub> emissions levels for the pellets and slurry fuels at lower Ca/S ratios.

### Oxides of Nitrogen Emissions

Oxides of nitrogen emissions in lbs per million Btu are shown in Figures 9-12 as a function of bed temperature. Nitrogen content of the slurry coals varied from 1.22 to 1.76% while that of the standard coal and the pellet coal was 1.71%. Regardless of fuel nitrogen content, the NO<sub>x</sub> emissions of the slurry fuels were uniformly lower than those from the standard coal. This can clearly be attributed to the lower temperature environment of the burning coal-water slurry droplet, especially in the preliminary combustion stages encompassing the volatiles release phase. For the slurry fuels, NO<sub>x</sub> levels were on the order of 0.3 lbs/10<sup>6</sup> Btu. Oxides of nitrogen levels for the pellet fuel did not vary much with bed temperature in the range of 1460 to 1625°F and were on the order of 0.55 lbs/10<sup>6</sup> Btu. NO<sub>x</sub> emissions for the standard coal at lower temperatures were similar in magnitude for the standard coal and pellet fuel. For the standard coal, they increased somewhat more rapidly with bed temperature increase to a value of 0.85 lb/10<sup>6</sup> Btu at a bed temperature of 1625°F.

### Combustion Efficiency

Figures 13-15 show the range of combustion efficiencies measured in the present experiments. Slurry B coal had the lowest heating value of 9550 Btu/lb, but yielded the highest efficiency among the slurry fuels, Figures



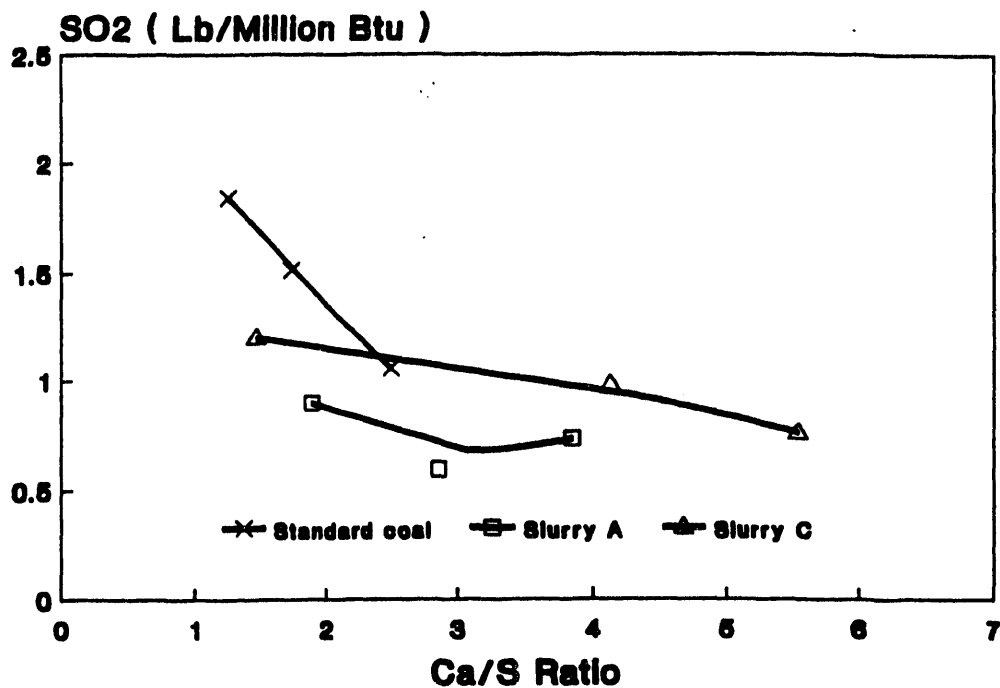


Figure 7. Influence of Ca/S Ratio on SO<sub>2</sub> Emissions for Slurry Fuels

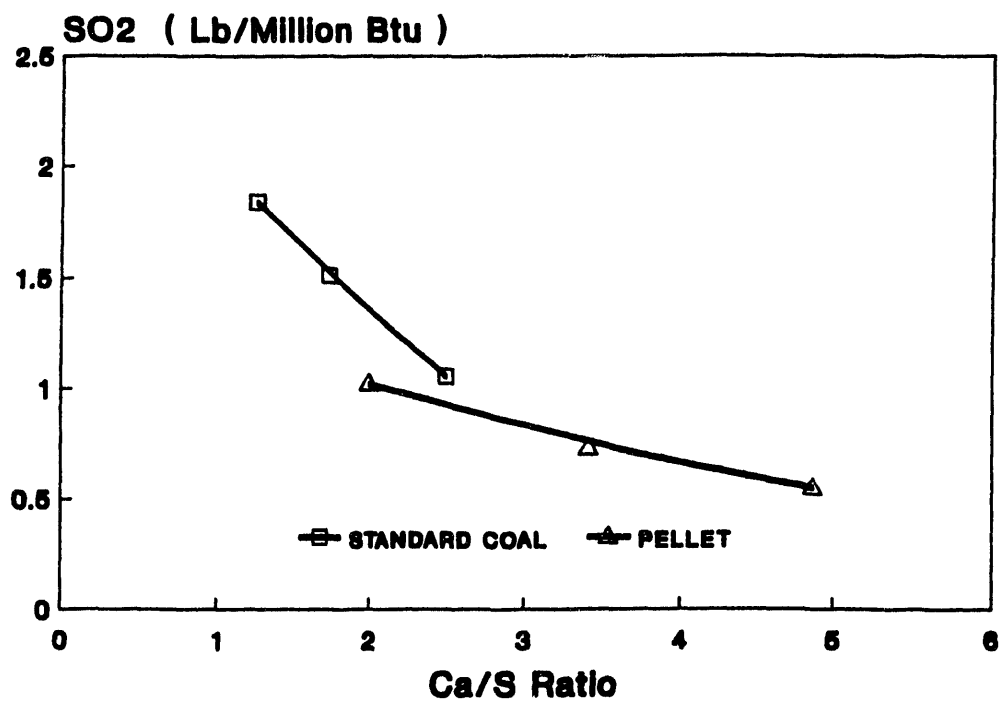


Figure 8. Influence of Ca/S Ratio on SO<sub>2</sub> Emissions for Pellets with Additional Limestone Injection

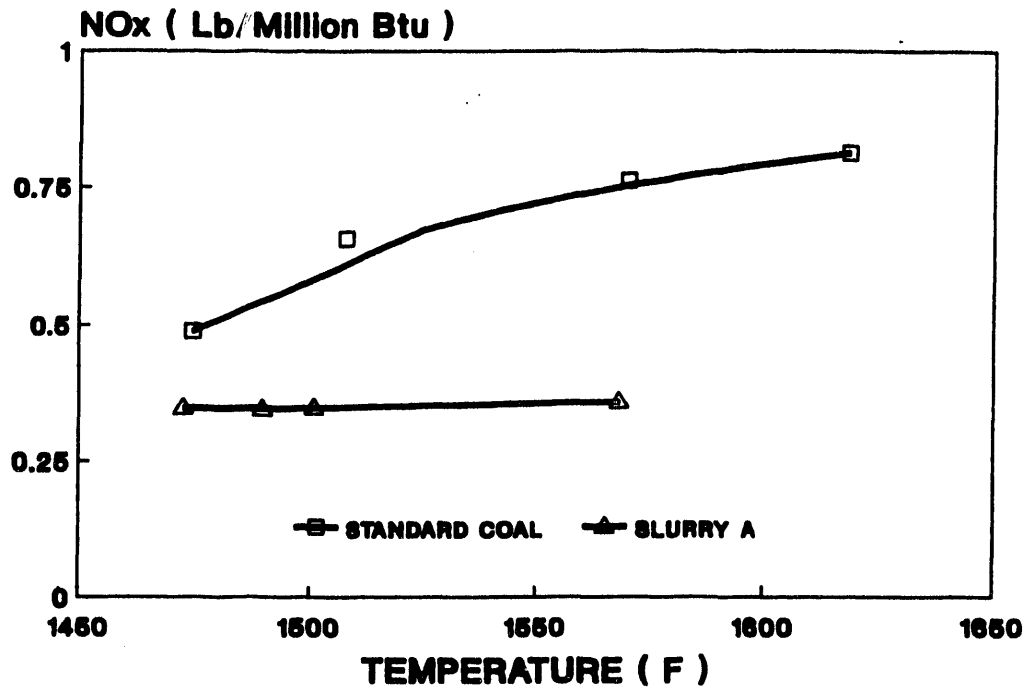


Figure 9. Comparison of NO<sub>x</sub> Emissions for Standard Coal and Slurry A

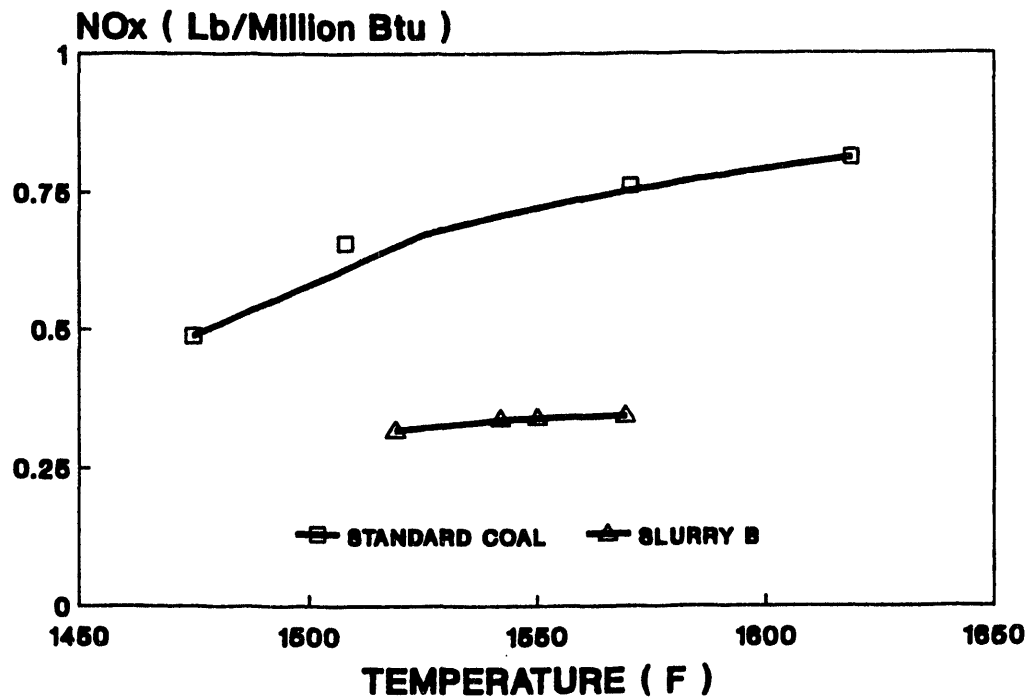


Figure 10. Comparison of NO<sub>x</sub> Emissions for Standard Coal and Slurry B

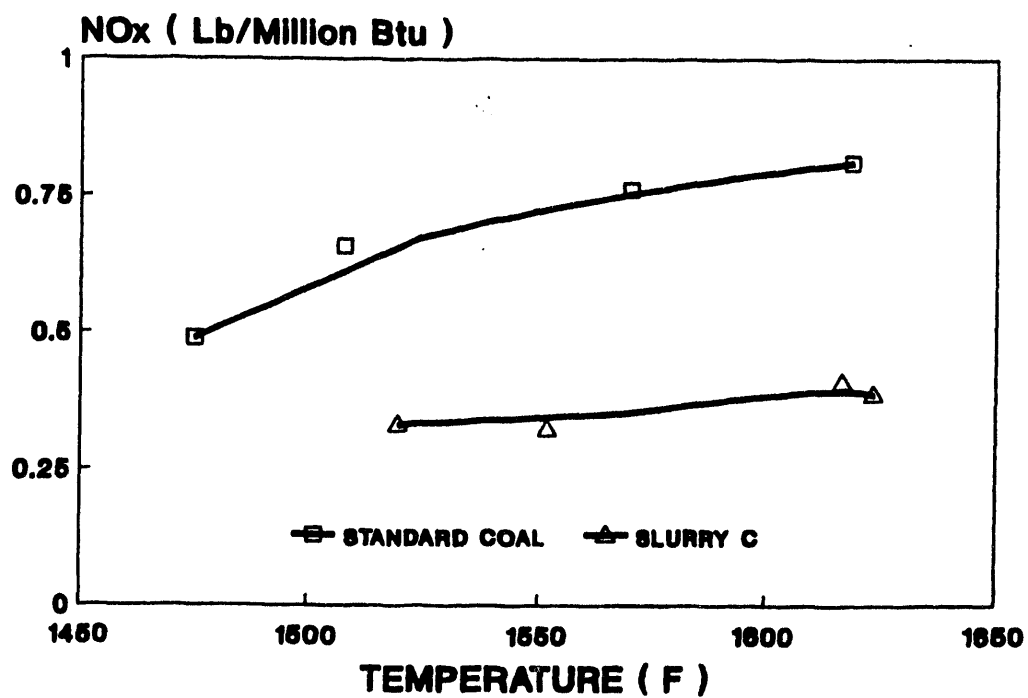


Figure 11. Comparison of NO<sub>x</sub> Emissions for Standard Coal and Slurry C

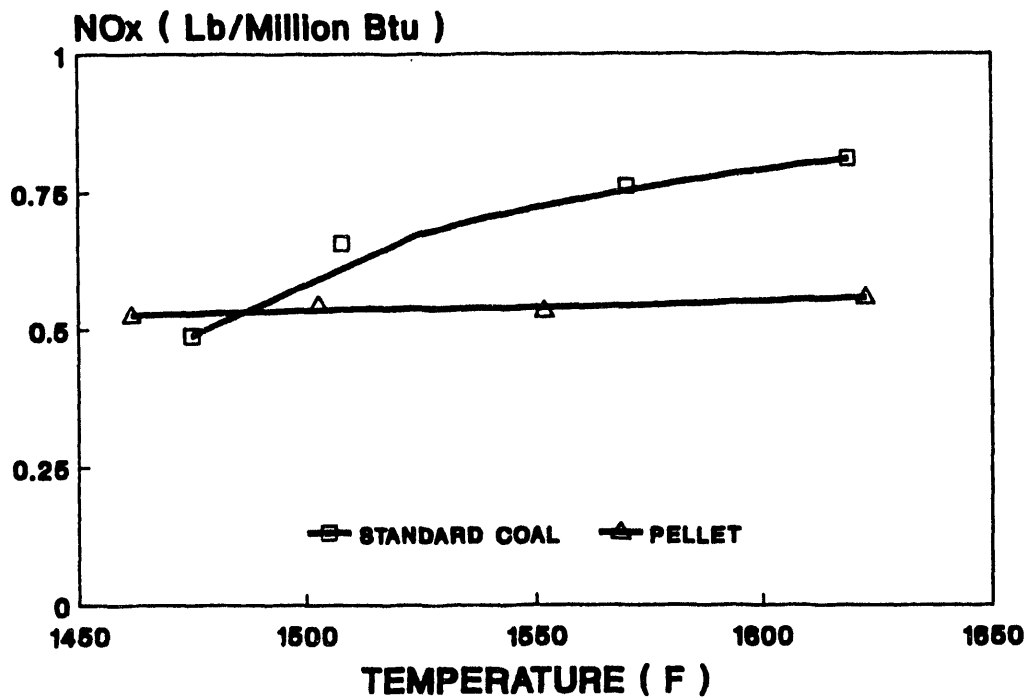


Figure 12. Comparison of NO<sub>x</sub> Emissions for Standard Coal and the Pellets

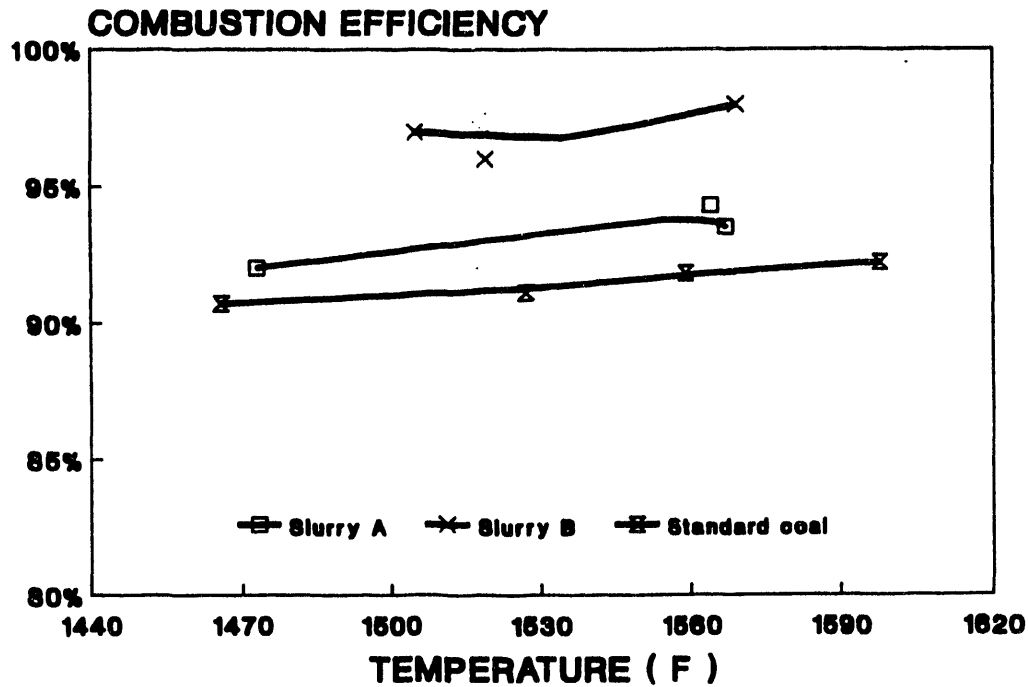


Figure 13. Influence of Bed Temperature on Combustion Efficiency for Slurry Fuels

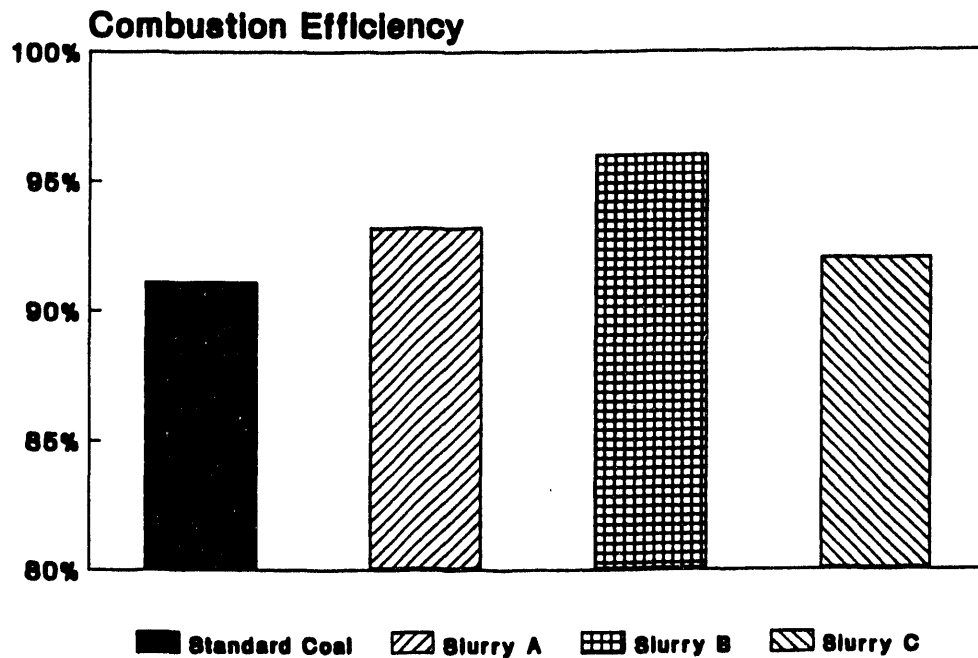


Figure 14. Comparison of Combustion Efficiencies at Bed Temperature of 1550°F

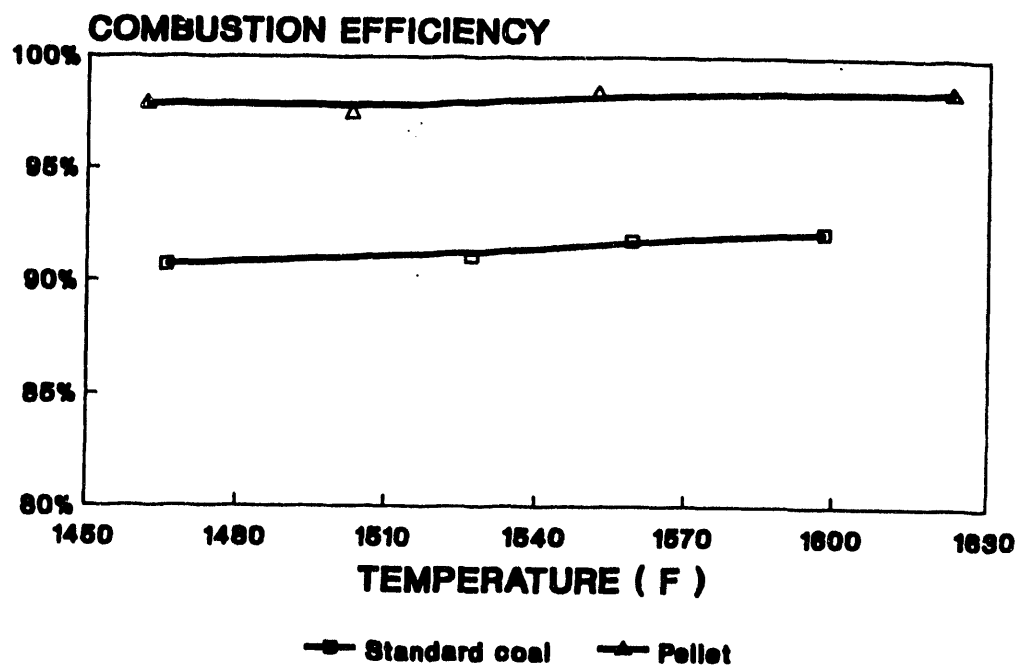


Figure 15. Effect of Bed Temperature on Combustion Efficiency of the Pellet Fuel

13 and 14. The longer residence time of the slurry droplets in the hotter regions of the bed generally results in higher combustion efficiencies for the slurries. Figures 14 and 15 show that the combustion efficiency varies almost linearly with bed temperature under the conditions of the present tests. Very good efficiencies were also measured for the pellet fuels, on the order of 98% as seen from Figure 15.

### Mineral Matter Analysis

At the present time, EDX analysis of the mineral matter in the ash from the combustion tests is being done. Also, trace elemental analysis of selected samples is being performed by professional laboratories. Results of these tests will be submitted in the final report.

### CONCLUSIONS

Evaluation of the combustion and emissions properties of three coal-water slurry fuels processed from preparation plant waste streams have been performed. Compared with similar performance from a standard run-of-mine coal, the coal-water slurry fuels generally emit lower levels of  $\text{SO}_2$  emissions. The advantage of the slurry fuels over the run-of-mine coal, in respect to  $\text{SO}_2$  emissions, appears greater at low levels of Ca/S ratio because of the  $\text{SO}_2$  release history from the slurry fuels. For the size of standard coal and limestone employed in these experiments, dispersion of the fuel particles/droplets and the limestone particles in the bed influences  $\text{SO}$  emissions from the standard coal more strongly as Ca/S ratio is increased, in comparison to that from the slurries and the pellet fuel.

Oxides of nitrogen emissions from the slurry fuels are markedly lower than from the standard coal as measured in the present tests. The coal-sorbent pellet also emits lower  $\text{NO}_x$  levels, especially at the typical FBC operation temperature of 1500-1550°F. Combustion efficiencies measured with the slurry fuels and the coal-sorbent pellets were generally 2-5 percentage points higher than with the standard coal.

## **PROJECT MANAGEMENT REPORT**

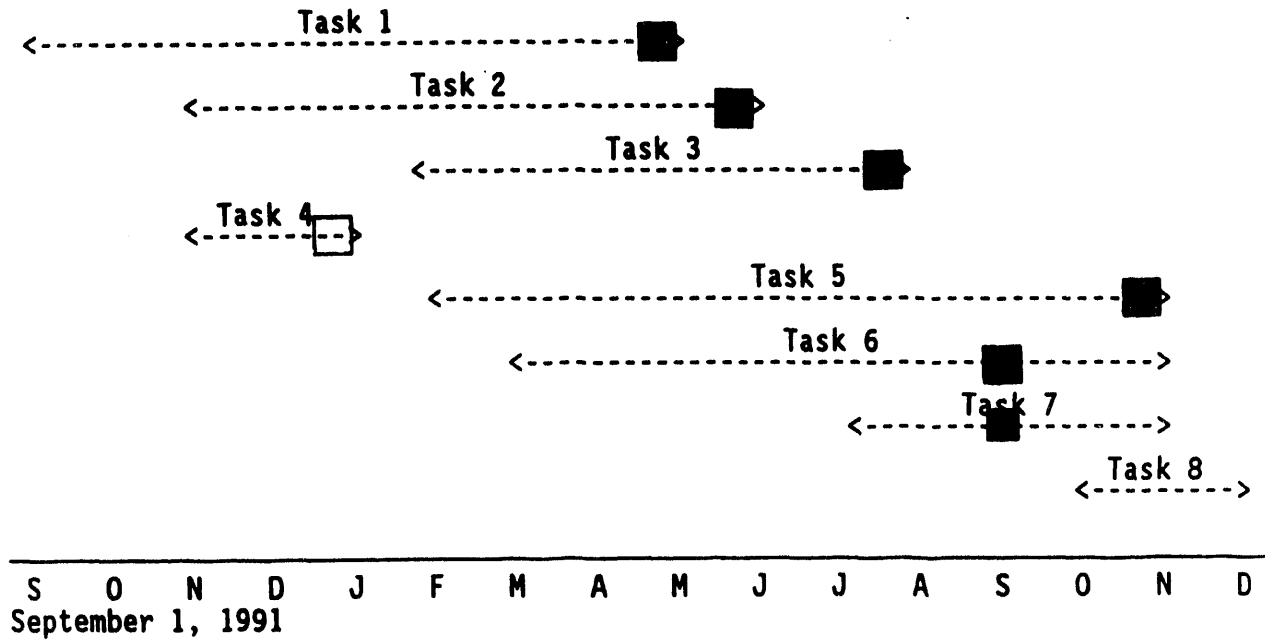
September 1, 1991 through August 31, 1992

**Project Title: CFBC Evaluation of Fuels Processed from Illinois Coals**

**Principal Investigator: Dr. S. Rajan**  
**Mechanical Engineering and Energy Processes**  
**Southern Illinois University**  
**Carbondale, Illinois 62901**

**Project Monitor: Dr. Ken Ho**

This project is funded by the U. S. Department of Energy (METC) and by the Illinois Department of Energy and Natural Resources as part of their cost-shared program.

**MODIFIED SCHEDULE**

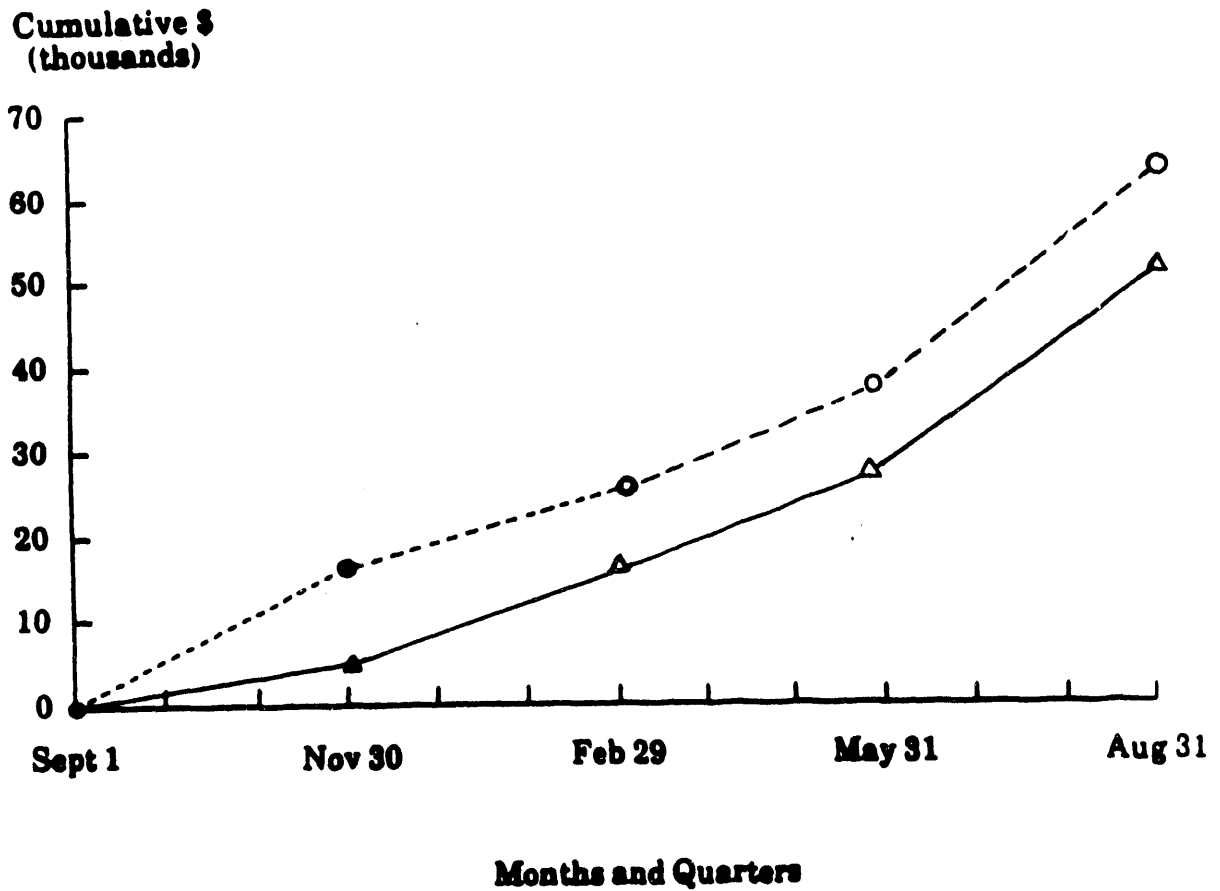
- Task 1: Fuels Procurement
- Task 2: Fuels Testing and Analysis
- Task 3: Fuels Preparation
- Task 4: Limestone Feeder Purchase and Installation
- Task 5: Fuel Combustion Testing
- Task 6: Combustion Residues Analysis
- Task 7: Data Analysis
- Task 8: Final Report and Recommendations



# Projected and Estimated Expenditures by Quarter

Quarter*	Types of Cost	Direct Labor	Materials & Supplies	Travel	Major Equipment	Other Direct Costs	Indirect Cost	Total
Sept. 1, 1991 to Nov. 30, 1991	Projected	6667	1125	0	4500	2375	1467	16134
	Estimated	3500	400	0	0	500	1000	5400
Sept. 1, 1991 to Feb. 29, 1992	Projected	13334	2250	0	4500	4750	2843	27317
	Estimated	5900	1300	0	4000	2800	1600	15600
Sept. 1, 1991 to May 31, 1992	Projected	20001	3375	700	4500	7125	3570	39271
	Estimated	11000	2500	150	4000	4500	2700	24850
Sept. 1, 1991 to Aug. 31, 1992	Projected	41775	4500	1200	4500	9500	6148	67623
	Estimated	33000	3400	1200	0	8500	4200	50300

\*Cumulative by quarter

**COSTS BY QUARTER - EXHIBIT C****CFBC Evaluation of Fuels Processed from Illinois Coals**

O = Projected Expenditures .....

Δ = Actual Expenditures \_\_\_\_\_

**Total CRSC Award \$67,623**

**DATE  
FILMED**

*2 / 24 / 94*

**END**