

Sloshing Response of Nonuniform Density Liquid in a Laterally Excited Tank

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ABSTRACT

A study on the sloshing response of nonuniform density liquid in a tank undergoing lateral base excitations is presented. The system considered is a circular cylindrical tank containing a liquid whose density increases with the liquid depth. The density distribution along the depth can be of any arbitrary continuous function. In the analysis, the liquid field is divided into n layers. The thicknesses of the liquid layers can be different, but the density of each liquid layer is considered to be uniform and its value is assigned to be the value of the original liquid density at the mid-height of that layer. The problem is solved by the transfer matrix technique. The effect of the nonuniform liquid density on the sloshing response is illustrated in a numerical example in which the linear and cosine distributions of the liquid density are assumed. The response functions examined include the sloshing frequencies, surface wave height, and the associated convective hydrodynamic pressure. The results are presented in tabular and graphical forms. It is found that the natural frequencies of the sloshing motion for nonuniform density liquid are lower than those of the uniform density liquid of the same total depth contained in an identical tank. Also, it is shown that for nonuniform density liquid, the maximum sloshing wave height may increase significantly and the magnitude of the convective hydrodynamic pressure may be quite different compared with that of a uniform liquid contained in an identical tank.

INTRODUCTION

The sloshing motion associated with the dynamic response of a homogeneous liquid in a rigid tank undergoing lateral base motion has been studied by Housner (1957), Bauer (1964) and Yang (1976). It is found that the natural frequencies of the sloshing motion can be computed by a very simple closed-form equation, and these frequencies are independent of the liquid density. For more information about this topic, the reader is referred to the above mentioned references. However, these previous studies were based on the assumption that the liquid has a constant density. Recently a paper by Bandyopadhyay (1991) indicates that a large number of

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high level waste (HLW) storage tanks at various U.S. Department of Energy (DOE) facilities contain liquid with nonuniform density. Thus, there is a need to understand the effect of nonuniform density on the seismic response of the contained liquid. Exploratory studies on the dynamic response of tanks containing two liquids have been performed by Tang (1993a, 1993b). Those studies show that the dynamic response of a tank containing two liquids is quite different from that of an identical tank containing only one liquid. Especially, the sloshing wave height may increase significantly in a tank that contains two liquids. Therefore, to design and evaluate the HLW storage tanks it is necessary to understand the sloshing response of tanks that contain liquid with nonuniform density.

The objectives of this paper are (1) to present a method of analysis for the computation of the sloshing frequencies, the sloshing displacement and the convective hydrodynamic pressure of nonuniform density liquid contained in a tank undergoing lateral base excitations; and (2) to present the numerical results with which the effect of nonuniform density of the liquid on the sloshing response can be elucidated. In the proposed approach, the liquid field is divided into n layers along its height. These liquid layers may have different thicknesses, but the liquid density of each layer is assumed to be uniform. The tank wall is assumed to be rigid. For each layer the so-called impulsive component of the response is solved first and then followed by the convective component of the response quantity. For the definitions of impulsive and convective components, the reader is referred to Housner (1957) and Veletsos (1984). Response functions examined include the sloshing frequencies, sloshing wave height and the convective hydrodynamic pressure. Even though, the solutions presented herein are for rigid tanks, they are also applicable for flexible tanks because it has been shown by Haroun and Housner (1981) that the sloshing motion is insensitive to the flexibility of the tank wall.

SYSTEM DESCRIPTION

The tank-liquid system investigated is shown in Fig. 1. It is a ground-supported upright circular cylindrical tank of radius R which is filled with a nonuniform liquid to a height of H . The density of the liquid is assumed to have a minimum value, denoted by ρ_a , at the top of the liquid surface. The liquid density is assumed to increase monotonously with the increase of the liquid depth and reaches a maximum value, denoted by ρ_b , at bottom of the liquid. The tank is assumed to be rigid and clamped to a rigid base. The liquid is considered to be incompressible

and inviscid. The response of the liquid is assumed to be linear. The cylindrical coordinate system, r , θ , and z , is employed for the study with the origin defined at the center of the tank base, e.g., $z = 0$, at the tank base and $\theta = 0$ taken parallel to the direction of the seismic excitation. The lateral excitation considered herein is denoted by $\ddot{x}(t)$. The temporal variation of $\ddot{x}(t)$ can be arbitrary.

APPROACH AND SOLUTIONS

The liquid field is first divided into n layers as shown in Fig. 2. The thickness of the Layer j ($j = 1, 2, 3 \dots n$) is denoted by H_j . The thicknesses of the different layers may not be the same. The liquid density for layer H_j is taken to be the value of the original liquid density at mid-height of the layer, and it is denoted by ρ_j . It is assumed that the liquid is uniform in each layer. Thus, the mathematical model that represents the physical system depicted in Fig. 1 is a system which has n layers of liquids with different thicknesses and liquid densities. For the convenience of derivations, a local cylindrical coordinate system, r , θ , z_j , is introduced for the Layer j where z_j is related to z by the equation

$$z = z_j + \sum_{k=1}^{j-1} H_k \text{ for } 0 \leq z_j \leq H_j \quad (1)$$

Given the conditions that the liquids are incompressible and inviscid, the hydrodynamic pressure induced at Layer j , denoted by p_j , must satisfy the Laplace equation

$$\nabla^2 p_j = 0 \text{ for } j = 1, 2, 3 \dots n \quad (2)$$

in the region $0 \leq r \leq R$, $0 \leq \theta \leq 2\pi$, and $0 \leq z_j \leq H_j$. The liquid acceleration at an arbitrary point in Layer j along s -direction is given by

$$a_s = - \frac{1}{\rho_j} \frac{\partial p_j}{\partial s} \quad (3)$$

The boundary conditions are:

1. The vertical acceleration of liquid at the tank base must be zero; i.e.,

$$\left. \frac{\partial p_1}{\partial z_1} \right|_{z_1=0} = 0 \quad (4)$$

2. The radial acceleration of liquid adjacent to the tank wall must equal the acceleration of the tank wall, i.e.,

$$-\frac{1}{\rho_j} \left. \frac{\partial p_j}{\partial r} \right|_{r=R} = \ddot{x}(t) \cos \theta, \quad j = 1, 2 \dots n \quad (5)$$

3. At the free surface, the linearized boundary condition is

$$\left(\frac{\partial^2 p_n}{\partial t^2} + g \left. \frac{\partial p_n}{\partial z_n} \right| \right)_{z_n=H_n} = 0 \quad (6)$$

where g is the gravitational acceleration.

At the interface of Layers j and $j+1$, the boundary conditions are:

4. Continuity of the vertical acceleration, i.e.,

$$-\frac{1}{\rho_j} \left. \frac{\partial p_j}{\partial z_j} \right|_{z_j=H_j} = -\frac{1}{\rho_{j+1}} \left. \frac{\partial p_{j+1}}{\partial z_{j+1}} \right|_{z_j=0} \quad (7)$$

and

5. Continuity of the hydrodynamic pressure, i.e.,

$$p_j \Big|_{z_j=H_j} = p_{j+1} \Big|_{z_{j+1}=0} \quad (8)$$

Note that, strictly speaking, if the densities of the liquids in Layers j and $j+1$ were indeed different, the hydrodynamic pressure would have a jump at the interface, and Eq. 8 would have to be replaced by (Tang 1993b)

$$\left(\frac{\partial^2 p_j}{\partial t^2} + g \left. \frac{\partial p_j}{\partial t_j} \right| \right) \Big|_{z_j=H_j} = \left(\frac{\partial^2 p_{j+1}}{\partial t^2} + g \left. \frac{\partial p_{j+1}}{\partial z_{j+1}} \right| \right) \Big|_{z_{j+1}=0} \quad (9)$$

However, the reason that ρ_j is not equal to ρ_{j+1} is derived from the mathematical modeling not from the original physical system. It should be noted in the physical system the density of liquid is continuous at the interface. Also, if one uses Eq. 9 instead of Eq. 8 to solve the problem, one will obtain n distinct natural frequencies for each horizontal sloshing mode (Tang 1993b) which

is believed to be unrealistic for the physical system considered. Therefore, Eq. 8 instead of Eq. 9 is used in this study.

The solutions for p_j is expressed as the sum of the impulsive component and the convective component, i.e.,

$$p_j = p_j^i + p_j^c \quad (10)$$

where the superscript i stands for the impulsive component and the superscript c stands for the convective component.

Impulsive Component

The function p_j^i must satisfy

$$\nabla^2 p_j^i = 0 \quad \text{for } j = 1, 2 \dots n \quad (11)$$

and the following boundary conditions:

$$\left. \frac{\partial p_1^i}{\partial z_1} \right|_{z_1=0} = 0 \quad (12a)$$

$$\left. \frac{\partial p_j^i}{\partial r} \right|_{r=R} = -\rho_j \ddot{x}(t) \cos \theta, \quad j = 1, 2 \dots n \quad (12b)$$

$$p_n^i \Big|_{z_n=H_n} = 0 \quad (12c)$$

$$-\frac{1}{\rho_j} \left. \frac{\partial p_j^i}{\partial z_j} \right|_{z_j=H_j} = -\frac{1}{\rho_{j+1}} \left. \frac{\partial p_{j+1}^i}{\partial z_{j+1}} \right|_{z_{j+1}=0} \quad (12d)$$

$$p_j^i \Big|_{z_j=H_j} = p_{j+1}^i \Big|_{z_{j+1}=0} \quad (12e)$$

The method of separation of variables is employed to solve Eq. 11, and the integration constants are determined from the boundary conditions. Satisfying Eqs. 11 and 12b, the function p_j^i takes the form

$$\begin{aligned}
p_j^i &= \left[-\frac{r}{R} + \sum_{k=1}^{\infty} \left(A_{jk} \cosh\left(\lambda_k \frac{z_j}{R}\right) + B_{jk} \sinh\left(\lambda_k \frac{z_j}{R}\right) \right) \right. \\
&\quad \left. \frac{J_1\left(\lambda_k \frac{r}{R}\right)}{J_1'(\lambda_k)} \right] \rho_j R \ddot{x}(t) \cos \theta, \quad \text{for } j = 1, 2, \dots, n
\end{aligned} \tag{13}$$

where J_1 is the Bessel function of the first kind of order 1, λ_k = the k th zero of J'_1 , the first derivative of J_1 , and A_{jk} and B_{jk} are the constants of integration that may be determined from the boundary conditions. From Eq. 12a, one obtains

$$B_{1k} = 0 \quad \text{for all } k \tag{14}$$

and from Eqs. 12d and 12e, one obtains

$$B_{(j+1)k} = \sinh \beta_{jk} A_{jk} + \cosh \beta_{jk} B_{jk}, \quad \text{for } j = 1, 2, \dots, n \tag{15a}$$

and

$$\begin{aligned}
A_{(j+1)k} &= \frac{\rho_j}{\rho_{j+1}} \cosh \beta_{jk} A_{jk} + \frac{\rho_j}{\rho_{j+1}} \sinh \beta_{jk} B_{jk} \\
&+ \left(1 + \frac{\rho_j}{\rho_{j+1}} \right) \chi_k, \quad \text{for } j = 1, 2, \dots, n
\end{aligned} \tag{15b}$$

respectively. Equations (15a) and (15b) can be cast into the matrix form given by

$$\begin{aligned}
\begin{Bmatrix} A_{(j+1)k} \\ B_{(j+1)k} \end{Bmatrix} &= \begin{bmatrix} \frac{\rho_j}{\rho_{j+1}} \cosh \beta_{jk} & \frac{\rho_j}{\rho_{j+1}} \sinh \beta_{jk} \\ \sinh \beta_{jk} & \cosh \beta_{jk} \end{bmatrix} \begin{Bmatrix} A_{jk} \\ B_{jk} \end{Bmatrix} \\
&+ \begin{Bmatrix} 1 - \frac{\rho_j}{\rho_{j+1}} \\ 0 \end{Bmatrix} \chi_k
\end{aligned} \tag{15c}$$

where $\beta_{jk} = \lambda_k H_j / R$ and

$$\chi_k = \frac{2}{\lambda_k^2 - 1} \quad (16)$$

To arrive at Eq. 15b, the following series expansion for r/R is utilized.

$$\frac{r}{R} = \sum_{k=1}^{\infty} \chi_k \frac{J_1\left(\lambda_k \frac{r}{R}\right)}{J_1(\lambda_k)} \quad (17)$$

With the aid of the recursive relation defined by Eq. 15c and the fact that $B_{1k} = 0$, the constants, A_{nk} and B_{nk} , can be expressed in terms of the constant, A_{1k} ; then, A_{1k} can be determined from the following equation which is obtained from Eq. 12c.

$$A_{nk} \cosh \beta_{nk} + B_{nk} \sinh \beta_{nk} = \chi_k \quad (18)$$

After A_{1k} is obtained, the constants A_{jk} and B_{jk} for $j = 2 \dots n$ can be determined repeatedly by making use of Eq. 15c.

Convective Component

The convective component of the hydrodynamic pressure, p_j^c , must satisfy

$$\nabla^2 p_j^c = 0 \quad \text{for } j = 1, 2 \dots n \quad (19)$$

and the following boundary conditions:

$$\left. \frac{\partial p_1^c}{\partial z_1} \right|_{z_1=0} = 0 \quad (20a)$$

$$\left. \frac{\partial p_j^c}{\partial r} \right|_{r=R} = 0 \quad (20b)$$

$$\left. \left(\frac{\partial^2 p_n^c}{\partial t^2} + g \frac{\partial p_n^c}{\partial z_n} \right) \right|_{z_n=H_n} = -g \left. \frac{\partial p_n^c}{\partial z_n} \right|_{z_n=H_n} \quad (20c)$$

$$-\frac{1}{\rho_j} \frac{\partial p_j^c}{\partial z_j} \Big|_{z_j=H_j} = -\frac{1}{\rho_{j+1}} \frac{\partial p_{j+1}^c}{\partial z_{j+1}} \Big|_{z_{j+1}=0} \quad (20d)$$

and

$$p_j^c \Big|_{z_j=H_j} = p_{j+1}^c \Big|_{z_{j+1}=0} \quad (20e)$$

Following the same procedure used in solving Eq. 11, the function p_j^c that satisfies Eqs. 19 and 20b takes the form

$$p_j^c = \sum_{k=1}^{\infty} \left[C_{jk}(t) \cosh\left(\lambda_k \frac{z_j}{k}\right) + D_{jk}(t) \sinh\left(\lambda_k \frac{z_j}{k}\right) \right] \frac{J_1\left(\lambda_k \frac{r}{R}\right)}{J_1(\lambda_k)} \rho_j R \cos\theta \quad (21)$$

in which $C_{jk}(t)$ and $D_{jk}(t)$ are the integration functions that may be determined by satisfying the boundary conditions. From Eq. 20a, one obtains

$$D_{1k} = 0 \quad \text{for all } k \quad (22)$$

and from Eqs. 20d and 20e, one obtains

$$\begin{Bmatrix} C_{(j+1)k} \\ D_{(j+1)k} \end{Bmatrix} = \begin{bmatrix} \frac{\rho_j}{\rho_{j+1}} \cosh \beta_{jk} & \frac{\rho_j}{\rho_{j+1}} \sinh \beta_{jk} \\ \sinh \beta_{jk} & \cosh \beta_{jk} \end{bmatrix} \begin{Bmatrix} C_{jk} \\ D_{jk} \end{Bmatrix} \quad (23)$$

Similar to Eq. 15c, Eq. 23 defines a relation between the integration functions of j th layer and those of the $(j+1)$ th layer. By repeating application of Eq. 23 from $j=1$ to $j=n$ and making use of Eq. 22, one obtains the equation that links the C_{1k} with C_{nk} and D_{nk} . Symbolically, this equation can be written as

$$\begin{Bmatrix} C_{nk} \\ D_{nk} \end{Bmatrix} = \begin{bmatrix} T_{11} & T_{12} \\ T_{21} & T_{22} \end{bmatrix} \begin{Bmatrix} C_{1k} \\ 0 \end{Bmatrix} \quad (24)$$

where the 2×2 matrix in Eq. 24 is the transfer matrix, and T_{11} , T_{12} , T_{21} and T_{22} are its elements. Introducing a coefficient, η_{nk} that represents the ratio of D_{nk} to C_{nk} , i.e.,

$$D_{nk} = \eta_{nk} C_{nk} \quad (25)$$

from Eq. 24 η_{nk} is given by

$$\eta_{nk} = \frac{T_{21}}{T_{11}} \quad (26)$$

Finally, C_{nk} may be determined by the following equation which is obtained from boundary condition Eq. 20c

$$\begin{aligned} & (\cosh \beta_{nk} + \eta_{nk} \sinh \beta_{nk}) \ddot{C}_{nk}(t) \\ & + \frac{g \lambda_k}{R} (\sinh \beta_{nk} + \eta_{nk} \cosh \beta_{nk}) C_{nk}(t) \\ & = -\frac{g \lambda_k}{R} (A_{nk} \sinh \beta_{nk} + B_{nk} \cosh \beta_{nk}) \ddot{x}(t) \end{aligned} \quad (27)$$

The natural circular frequency for the k th vibration mode of the sloshing motion, denoted by ω_k , can be obtained from the free vibration equation associated with Eq. 27, and the result is given by

$$\omega_k^2 = \frac{g \lambda_k}{R} \left(\frac{\eta_{nk} + \tanh \beta_{nk}}{1 + \eta_{nk} \tanh \beta_{nk}} \right) \quad (28)$$

where the coefficients A_{nk} and B_{nk} are obtained from the preceding section for the impulsive component. The solution to Eq. 28 is given by

$$C_{nk}(t) = - \left(\frac{A_{nk} \tanh \beta_{nk} + B_{nk}}{\eta_{nk} + \tanh \beta_{nk}} \right) A_k(t) \quad (29)$$

where $A_k(t)$ is the pseudoacceleration function for the k th vibration mode of the sloshing motion and is defined by

$$A_k(t) = \omega_k \int_0^t \ddot{x}(\tau) \sin(\omega_k(t-\tau)) d\tau \quad (30)$$

The convective component of the hydrodynamic pressure for the n th layer, p_n^c , is then obtained from Eq. 21 by setting $j = n$ and substituting Eqs. 25 and 30 into the resulting equation. The result is given by

$$p_n^c = - \sum_{k=1}^{\infty} \left(\frac{A_{nk} \tanh \beta_{nk} + B_{nk}}{\eta_{nk} + \tanh \beta_{nk}} \right) \left(\cosh \lambda_k \frac{z_n}{R} + \eta_{nk} \sinh \lambda_k \frac{z_n}{R} \right) \frac{J_1 \left(\lambda_k \frac{r}{R} \right)}{J_1(\lambda_k)} A_k(t) \rho_n R \cos \theta \quad (31)$$

The sloshing wave height, $d(r, \theta, t)$, of an arbitrary point at the liquid surface is determined from

$$p_n^c \Big|_{z_n = H_n} = \rho_n g d(r, \theta, t) \quad (32)$$

and the result is expressed as

$$d(r, \theta, t) = \left[\sum_{k=1}^{\infty} r_k \left(\frac{2}{\lambda_k^2 - 1} \right) \frac{A_k(t)}{g} \frac{J_1 \left(\lambda_k \frac{r}{R} \right)}{J_1(\lambda_k)} \right] R \cos \theta \quad (33)$$

in which r_k is a dimensionless coefficient which is equal to one if the liquid has uniform density; therefore, r_k represents the effect of the nonuniform liquid density on the k th mode of sloshing wave height. Also, another dimensionless coefficient, α_k , is introduced to assess the effect of nonuniform liquid density on the sloshing frequencies; α_k is defined by rewriting Eq. 28 as

$$\omega_k^2 = \alpha_k \left(\frac{g \lambda_k}{R} \tanh \left(\lambda_k \frac{H}{R} \right) \right) \quad (34)$$

Again, α_k has a value of one if the liquid has uniform density. Note that for the case of $n=2$ the closed form solutions for r_k and α_k are available in Tang (1993a). After C_{nk} is obtained from Eq. 24, the coefficient C_{1k} may be computed by the equation given by

$$C_{1k} = \frac{1}{T_{11}} C_{nk} \quad (35)$$

which is derived from Eq. 24. With the information for D_{1k} given in Eq. 22, the coefficients C_{jk} and D_{jk} for $j = 2, 3, \dots, n$ can be calculated from Eq. 23 recursively, and the convective hydrodynamic pressure given by Eq. 21 can be computed as well. The maximum convective hydrodynamic pressure exerted on the tank wall is obtained by evaluating Eq. 21 at $r = R$, and $\theta = 0$; the result can be cast into the following equation

$$p^c(z, t) = \sum_{k=1}^{\infty} c_k(z) A_k(t) \rho_b R \quad (36)$$

Note that in Eq. 36, the magnitude of the pressure is normalized by ρ_b which is the maximum value of the liquid density.

NUMERICAL RESULTS

Unlike the case of a tank containing uniform liquid where H/R is the only parameter that controls the response, for tanks filled with nonuniform liquid, the parameters that control the response are H/R , ρ_t/ρ_b , and the density variation along the liquid depth. For the numerical study presented herein, the variation of the liquid density between ρ_t and ρ_b is assumed to be either a linear or a cosine function. More precisely, if $\rho(z)$ represents the density at liquid depth of z , the linear function is given by

$$\rho(t) = \rho_t + \left(\frac{H - z}{H} \right) (\rho_b - \rho_t) \quad (37)$$

and the cosine function is given by

$$\rho(z) = \rho_t + (\rho_b - \rho_t) \cos \left(\frac{\pi z}{2H} \right) \quad (38)$$

It is important to determine the number of layers needed to approximate the liquid field in order to get accurate results. Therefore, the study for the convergence of the natural frequency and sloshing displacement is performed first. Since the major contribution to the sloshing response comes from the fundamental mode of vibration, the convergence study for the frequency coefficient α_k and r_k for $k = 1$ is presented in Tables 1 and 2, respectively, assuming either linear or cosine variation for the liquid density. In these tables, values of α_1 and r_1 for tanks with $H/R = 0.5$ and 3 filled with liquid with $\rho_t/\rho_b = 0.25, 0.5$ and 0.75 were obtained by using different numbers of layers, and for simplicity the thicknesses of these layers are taken to be the same.

As one can see from these tables that for larger value of ρ_v/ρ_b and linear variation of density the convergence for α_1 and r_1 is faster. Also, from the tables one may conclude that with $n = 300$, the results are quite accurate. Thus all solutions presented hereinafter are obtained by using $n = 300$. It should be mentioned herein that the approach presented in this paper is implemented into a FORTRAN computer program that runs on PC 486 machine, and for $n = 600$ the CPU time spent is less than 5 seconds.

The frequency coefficient α_k and sloshing displacement coefficient r_k for $k = 1$ are plotted in Figs. 3 and 4, respectively, for linear and cosine variations of density as a function of ρ_v/ρ_b . Four different values of H/R , 0.5, 1, 2 and 3, are considered. Examining the information presented in Figs. 3 and 4, one notices that the effects of nonuniform liquid density on the sloshing response are: (1) it decreases the fundamental natural frequency of the sloshing motion; and (2) it may increase the sloshing wave height. This effect is more pronounced for broad tanks with low value of ρ_v/ρ_b , and these effects are not particularly sensitive to the detailed variation of the density value between ρ_t and ρ_b . The increase of the wave height may be significant; for example, the value of r_1 is more than double for $H/R = 0.5$ and $\rho_v/\rho_b < 0.25$ compared with that for $H/R = 0.5$ and $\rho_v/\rho_b = 1$, the uniform density. To further confirm this finding, the maximum sloshing wave height of a liquid with $\rho_v/\rho_b = 0.25$ in a tank of radius $R = 25$ ft (7.63 m) and liquid height $H = 12.5$ ft (3.81 m) subjected to the 29-second horizontal component of the September 16, 1978 Tabas earthquake of Iran is computed. The peak acceleration of the Tabas recorded is denoted by \ddot{x}_g . The maximum sloshing wave height, denoted by d_{max} , may be obtained by evaluating Eq. 33 at $r = R$ and $\theta = 0$. For the first three modes of vibration, d_{max} may be expressed as

$$d_{max} = d_1 \frac{A_1(t)}{g} + d_2 \frac{A_2(t)}{g} + d_3 \frac{A_3(t)}{g} \quad (39)$$

in which the subscripts 1, 2 and 3 represent the first, second and third mode, respectively, and the coefficient d_i , $i=1,2$ and 3 has the unit of length. The first three natural frequencies, denoted by f_i , the value of d_i and the maximum values of $A_i(t)$, denoted by SA_i , for $i = 1,2$ and 3 are tabulated in Table 3 for the cases of linear, cosine and uniform liquid density variations. Also, listed in the Table 3 are the d_{max} obtained from Eq. 39 by the square root of the sum of the squares (SRSS) of the three components. One, again, can see clearly that the sloshing wave

height increases from the uniform density case to the linear variation case by 67%, and for the cosine variation case the increase is 46%.

The distribution function of the convective hydrodynamic pressure exerted on the tank wall, $c_k(z)$, $k = 1$, is plotted in Figs. 5 and 6 for $H/R = 0.5$ and 3, respectively, for the values of $\rho/\rho_b = 0.25$ and 0.75 for the linear and cosine variations of liquid density. Plotted in the same figures and shown by the dotted lines are the corresponding information for the case of uniform liquid density of ρ_b . It is clearly shown in these two figures that the convective hydrodynamic pressure may be far off the true solution if uniform liquid density is assumed. It is noted herein that the accuracy of the pressure computed has been checked against those presented in Tang (1993a) for the case of $n = 2$.

CONCLUSIONS

A study on the effect of nonuniform liquid density on the sloshing response of an upright circular cylindrical tank is presented. The response quantities examined include the natural sloshing frequencies and surface sloshing displacement. It shows that nonuniform liquid density has two main effects on the sloshing response: (1) it increases the sloshing wave height; and (2) it decreases the sloshing frequencies, and the magnitude of the convective hydrodynamic pressure induced may be quite different from that of uniform liquid. Also, it is shown in the numerical example that if the effect of the nonuniform liquid density is considered, the maximum sloshing wave height may be increased by more than 50 percent when compared with that of the identical tank filled with uniform liquid.

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Appendix-Reference

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Table 1. Convergence Table of Sloshing Frequency Coefficient, α_1

No. of Layers	$\rho_v/\rho_b = 0.75$		$\rho_v/\rho_b = 0.50$		$\rho_v/\rho_b = 0.25$	
	Linear	Cosine	Linear	Cosine	Linear	Cosine
$H/R = 0.5$						
2	0.976	0.975	0.947	0.948	0.911	0.917
5	0.957	0.949	0.899	0.884	0.813	0.797
10	0.950	0.938	0.880	0.856	0.769	0.738
50	0.944	0.928	0.864	0.832	0.729	0.682
100	0.943	0.927	0.862	0.829	0.724	0.674
150	0.943	0.927	0.861	0.827	0.722	0.672
200	0.943	0.927	0.861	0.827	0.721	0.670
250	0.943	0.927	0.861	0.827	0.721	0.670
300	0.943	0.926	0.860	0.826	0.720	0.669
600	0.943	0.926	0.860	0.826	0.720	0.668
$H/R = 3.0$						
2	1.000	1.000	0.999	0.999	0.999	0.999
5	0.996	0.995	0.990	0.987	0.978	0.973
10	0.992	0.988	0.979	0.970	0.947	0.933
50	0.987	0.980	0.964	0.957	0.909	0.874
100	0.986	0.979	0.962	0.944	0.902	0.864
150	0.986	0.979	0.961	0.942	0.900	0.862
200	0.986	0.979	0.960	0.942	0.899	0.860
250	0.986	0.978	0.960	0.941	0.898	0.859
300	0.986	0.978	0.960	0.941	0.898	0.858
600	0.986	0.978	0.960	0.940	0.897	0.857

Table 2. Convergence Table of Sloshing Displacement Coefficient, α_1

No. of Layers	Displacement					
	$\rho_s/\rho_b = 0.75$		$\rho_s/\rho_b = 0.50$		$\rho_s/\rho_b = 0.25$	
	Linear	Cosine	Linear	Cosine	Linear	Cosine
$H/R = 0.5$						
2	1.064	1.067	1.150	1.148	1.271	1.248
5	1.112	1.134	1.290	1.337	1.628	1.689
10	1.130	1.162	1.348	1.428	1.825	1.979
50	1.145	1.185	1.401	1.514	2.031	2.322
100	1.147	1.188	1.408	1.526	2.061	2.375
150	1.147	1.190	1.410	1.530	2.071	2.393
200	1.147	1.190	1.411	1.532	2.076	2.402
250	1.148	1.190	1.412	1.533	2.079	2.408
300	1.148	1.911	1.413	1.534	2.081	2.411
600	1.148	1.191	1.414	1.536	2.087	2.421
$H/R = 3.0$						
2	1.009	1.009	1.021	1.021	1.038	1.035
5	1.030	1.040	1.079	1.101	1.174	1.203
10	1.042	1.060	1.116	1.158	1.282	1.360
50	1.055	1.079	1.156	1.222	1.415	1.576
100	1.057	1.082	1.161	1.231	1.435	1.611
150	1.057	1.083	1.163	1.235	1.442	1.623
200	1.057	1.083	1.164	1.236	1.446	1.629
250	1.058	1.084	1.165	1.237	1.448	1.633
300	1.058	1.084	1.165	1.238	1.449	1.636
600	1.058	1.084	1.166	1.239	1.453	1.642

Table 3. Comparison of Response Quantities of the Tank-Liquid Systems Considered in Numerical Example

	Linear	Cosine	Uniform
f_1 (Hz)	0.151	0.140	0.209
f_2 (Hz)	0.343	0.322	0.415
f_3 (Hz)	0.462	0.438	0.528
d_1/R	1.742	2.018	0.837
d_2/R	0.09	0.148	0.07
d_3/R	0.04	0.05	0.03
$\frac{SA_1}{g}$	0.212	0.157	0.265
$\frac{SA_2}{g}$	0.523	0.534	0.442
$\frac{SA_3}{g}$	0.574	0.471	0.769
$\frac{d_{\max}}{R} \cdot \left(\frac{g}{\ddot{x}_g} \right)$	0.376	0.331	0.225

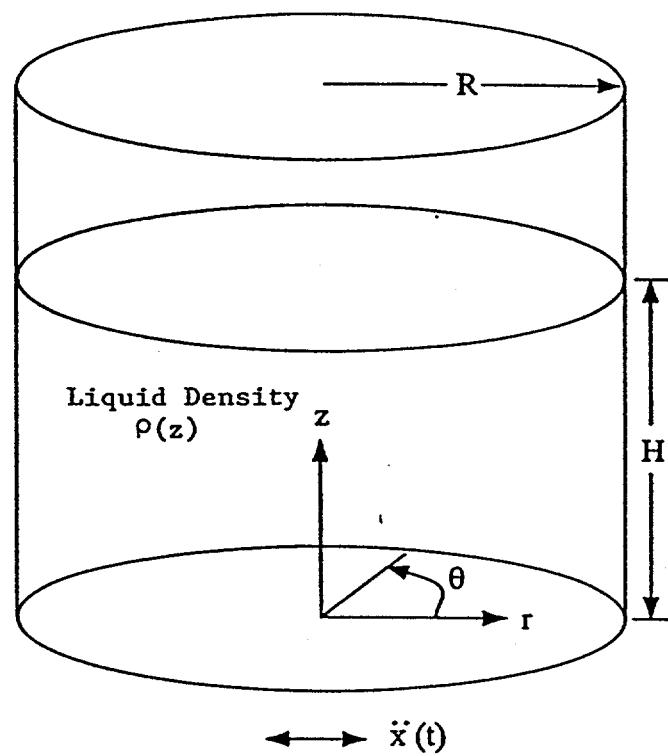


Fig. 1. System Considered

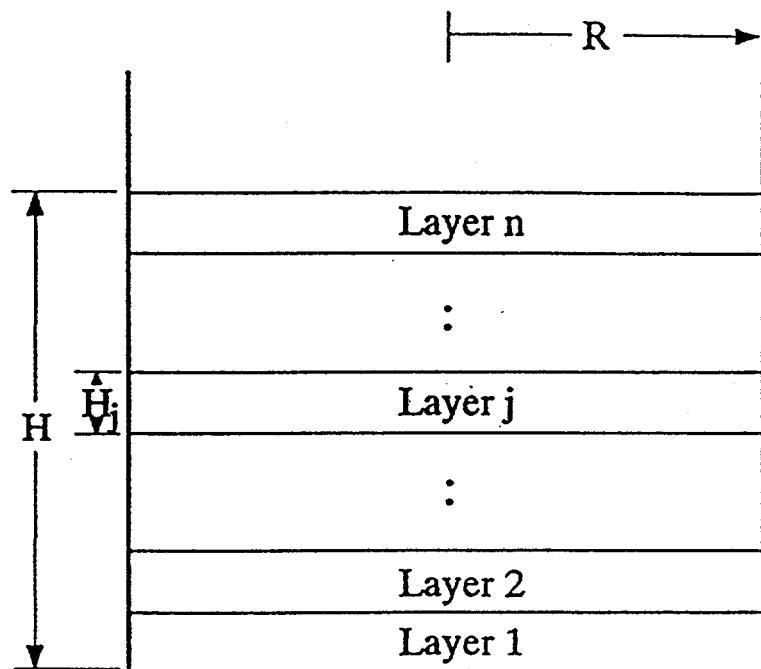


Fig. 2. Mathematical Model for the Liquid Field

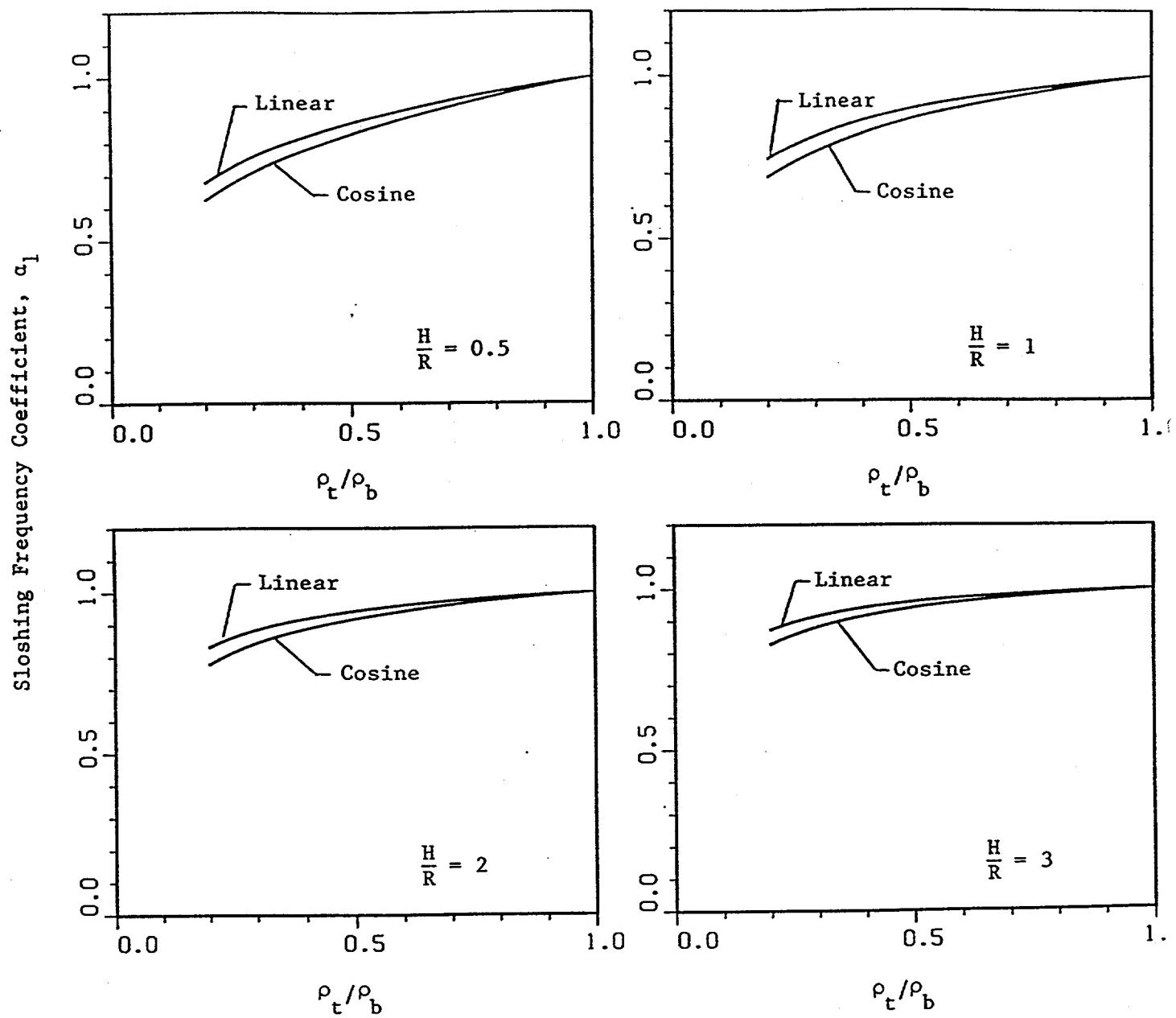


Fig. 3. Effect of Liquid Density on the Sloshing Frequency

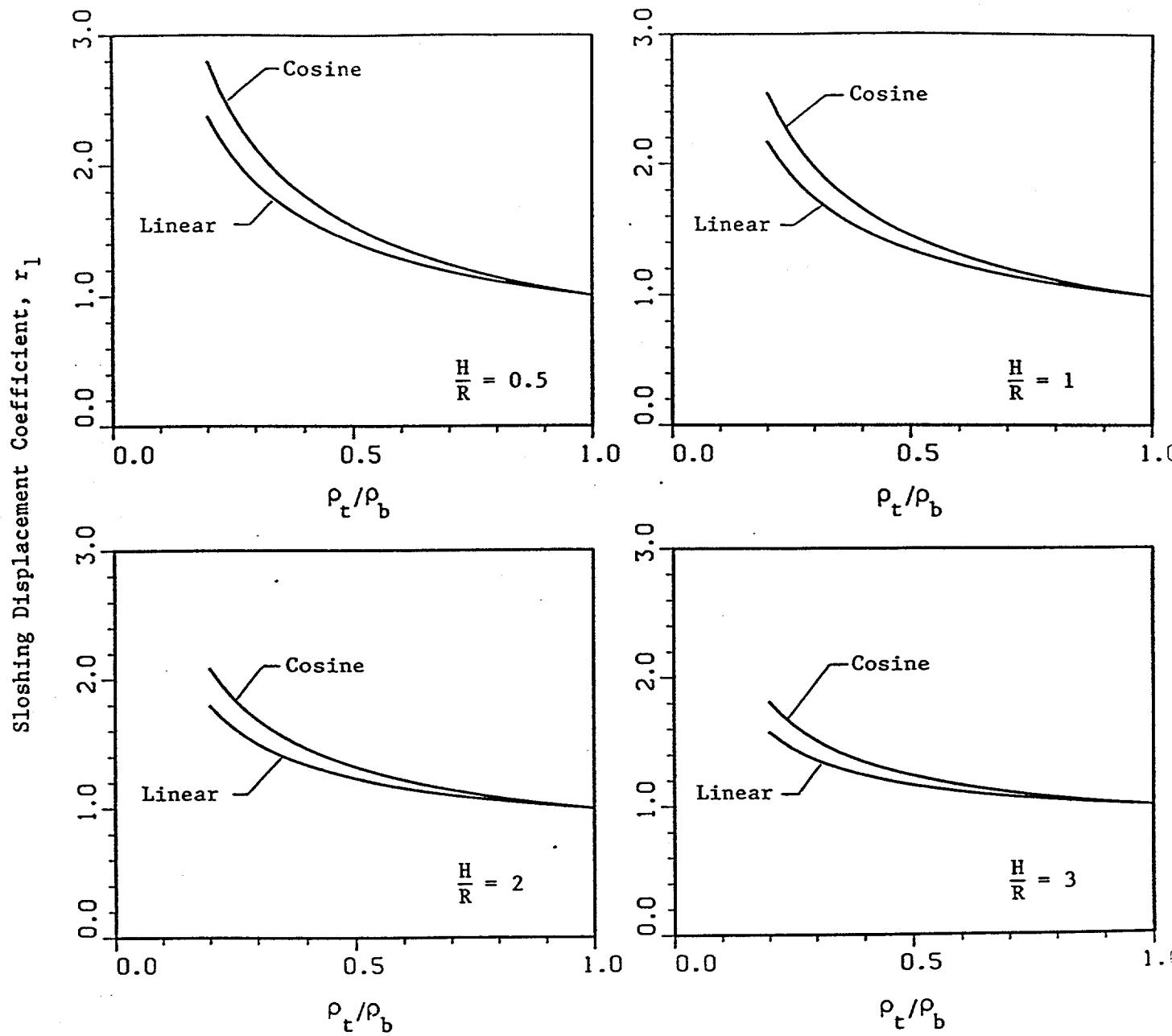


Fig. 4. Effect of Liquid Density on the Sloshing Displacement

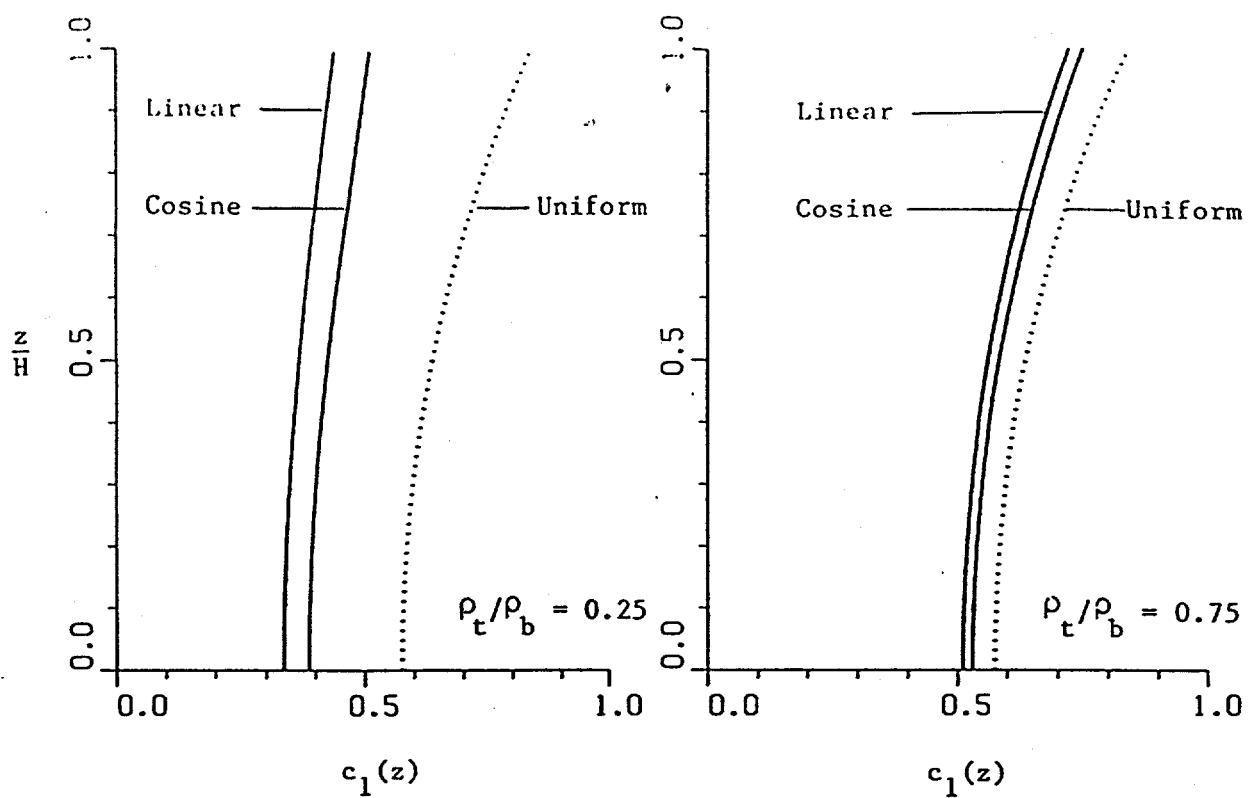


Fig. 5. Convective Pressure Exerted on Wall of Rigid Tanks with $H/R = 0.5$

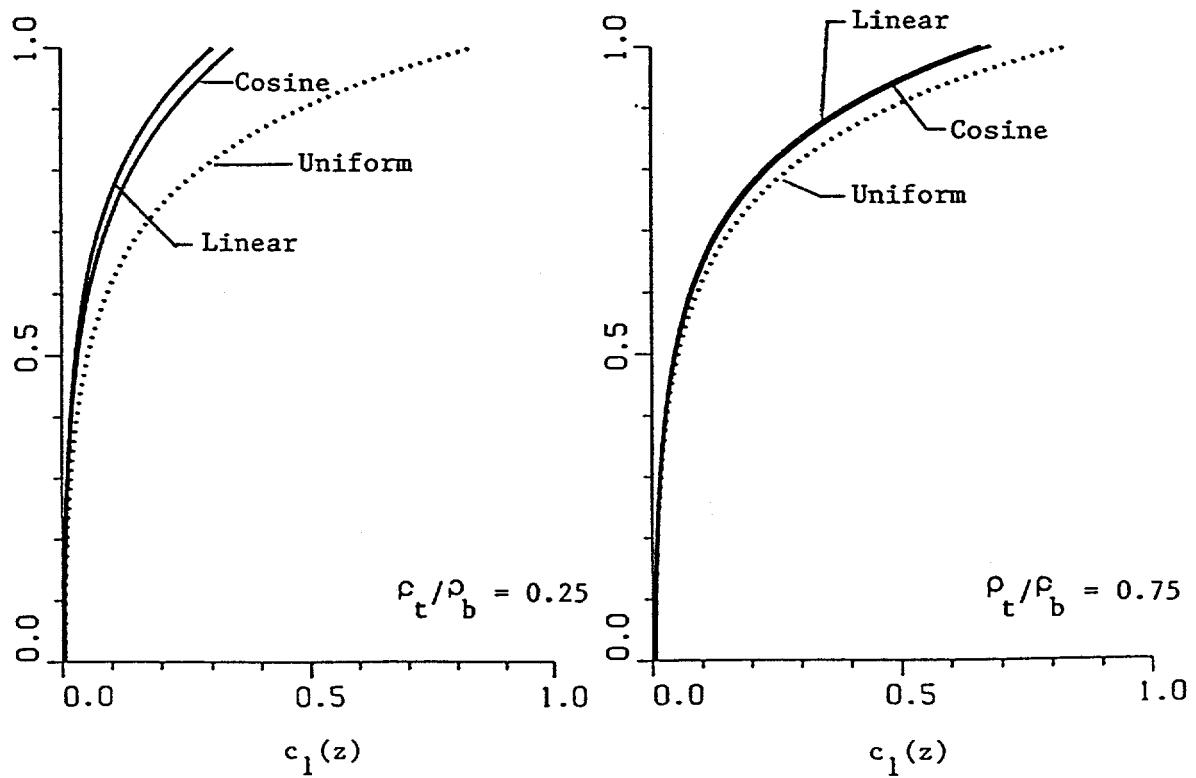


Fig. 6. Convective Pressure Exerted on Wall of Rigid Tanks with $H/R = 3$