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# RF MODELING AND DESIGN OF A FOLDED WAVEGUIDE LAUNCHER FOR THE ALCATOR C-MOD TOKAMAK

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## ABSTRACT

The folded waveguide (FWG) launcher is being investigated as an improved antenna configuration for plasma heating in the ion cyclotron range of frequencies (ICRF). A development FWG launcher was successfully tested at Oak Ridge National Laboratory (ORNL) with a low-density plasma load and found to have significantly greater power density capability than current strap-type antennas operating in similar plasmas. To further test the concept on a high density tokamak plasma, a collaboration has been set up between ORNL and Massachusetts Institute of Technology (MIT) to develop and test an 80-MHz, 2-MW FWG on the Alcator C-Mod tokamak at MIT. The radio frequency (rf) electromagnetic modeling techniques and laboratory measurements used in the design of this antenna are described in this paper. A companion paper [1] describes the mechanical design of the FWG.

## INTRODUCTION

The standard FWG launcher [2] is a resonant cavity formed with a half wavelength section of thin rectangular waveguide folded in one dimension and completely enclosed on the back end as shown in Fig. 1. Folding allows a large, low frequency waveguide to fit into the available port dimensions on tokamak devices. The folding process is implemented by stacking flat vanes with rounded tips on alternate sides of a rectangular box. On the plasma facing end, the FWG is partially shorted with a polarizing plate that has openings between alternate vanes to allow in-phase polarized magnetic fields to couple to the plasma. The magnetic fields penetrate into the plasma edge and couple to plasma fast waves when the waveguide is oriented with the rf magnetic fields in the toroidal direction. There is a small ripple component in the magnetic field pattern caused by the spaces between polarizing plate openings. This ripple is not expected to adversely affect the plasma coupling since its amplitude dies out quickly away from the FWG. Antenna patterns for the FWG resemble those of current strap antennas outside the ripple region. Transverse electromagnetic fields inside the FWG vary

sinusoidally along its length. The electric field is maximum at the center, zero at the back wall, and very low at the plasma end. The magnetic field is maximum at the back wall and polarizing plate. The low electric field and high magnetic field at the polarizing plate is optimum for plasma coupling.

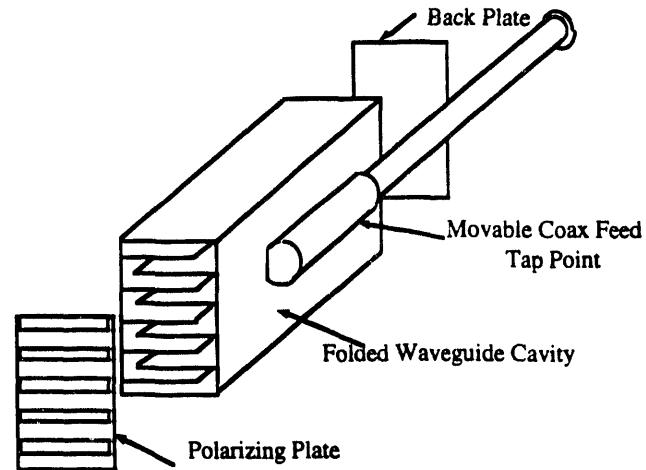


Fig. 1 Folded waveguide launcher configuration

The FWG launcher is under development as an ICRF antenna because of several features that may be particularly advantageous in a fusion reactor environment: (1) tests of a development FWG at ORNL have demonstrated a factor of ~5 increase in power density capability for essentially identical plasma loads [3]; (2) since the FWG has no center conductor, ceramic insulating supports are not required close to the plasma; (3) the FWG does not require a Faraday shield and is inherently robust against plasma disruption induced forces; (4) the input impedance can be internally matched eliminating the need for external tuning equipment; (5) there is very little mutual coupling between adjacent FWG apertures which simplifies phasing arrays; and (6) the FWG can be designed to provide radial position adjustment capability.

The main disadvantage of the standard FWG launcher is its narrow bandwidth. It is necessary to vary the cavity length or width to change resonant frequency. This requires that additional mechanical hardware be incorporated inside the FWG which is not desirable in a reactor antenna. Reliability of frequency tuning and matching hardware mounted inside a FWG needs to be established. For some reactor scenarios, narrow band operation may be acceptable. Other configurations of the FWG have been devised such as the quarter-wavelength FWG cavity version, a folded stripline, and

a stacked stripline [4] may offer the potential for wider bandwidth operation using either external matching or less complex internal tuning hardware.

Although the FWG has many potential advantages, it has not yet been tested with a high-density tokamak plasma. Therefore, a collaborative development and testing program has been established between ORNL and MIT to test a FWG on the Alcator C-Mod tokamak. An 80-MHz, 2-MW FWG launcher is currently being designed at ORNL and is scheduled to be tested on C-Mod beginning in late 1995. The C-Mod FWG will have a movable feed point for impedance matching and will have radial position adjustment capability. A vacuum tank will enclose the FWG and rf power will be coupled through a 9-in.,  $50\Omega$  vacuum feedthrough. Design of the FWG is being based on techniques derived from previous FWG design projects and an 80-MHz development FWG that was tested to 1 MW. Objectives of the C-Mod FWG testing program will be to measure the plasma loading, power density, plasma impurity generation, reliability, and heating capabilities of the folded waveguide with a high density divertor-type plasma.

### FWG RF DESIGN PROCEDURE

The parameters required for the design and analysis of the FWG cavity are the resonant frequency, the electric and magnetic fields in the cavity, the rf losses (or cavity Q), and ultimately the fields around the polarizing plate openings and the feed structure. From the cavity field values, estimates can be generated for the plasma loading, the power launch spectrum, and the power handling capability.

The FWG launcher is a complicated three-dimensional device, which makes modeling difficult especially when the plasma-antenna interaction is being considered. Fortunately, the behavior of the FWG cavity is only slightly perturbed by the plasma load, which allows the FWG cavity to be designed independent of plasma conditions by using modified unfolded waveguide cavity models or commercially available numerical codes. More accurate calculation of the cavity resonant frequency and electric fields and currents around the FWG internal vane tips is best handled by using a 2-D modeling technique for an infinite length waveguide such as the finite element or the finite-difference time-domain method (FDTD). Nonuniform grids with higher point density near the vane tips are desirable for greater accuracy. Since the numerical techniques can require hours of computing time for each case, a simpler approximate analytical technique is useful for the initial FWG design and has been implemented in a spreadsheet. Accurate modeling of the plasma loading, launch spectrum, and currents on the antenna front facing the plasma requires more complicated plasma-antenna interaction codes that are under development at ORNL [5] and elsewhere.

On the Alcator C-Mod tokamak, a transmitter operating frequency of 80 MHz and port dimensions of 203 mm horizontal by 438 mm vertical are available. The waveguide cutoff frequency is set by the effective width of the folded cavity and must be sufficiently below the operating frequency

to allow a reasonably short waveguide box. If too many vanes are required, the vane-to-vane spacing will provide insufficient clearance for the input power feed "vane toucher." Uneven vane spacing can be used to allow more room for the feed at the central vane. For the C-Mod case, 13 evenly spaced vanes of 6.35 mm thickness and 12.7-mm walls have been chosen, which produces a cutoff frequency of 69 MHz. This size allows 6 mm clearance between the outside of the FWG box and the C-Mod port sidewalls.

The cutoff frequency of the FWG is set by the effective width of the cavity, which to first order, is simply the centerline length of the meandering waveguide path. The sharp 180° hairpin turns at each vane tip combined with the square corners on the opposite walls act as capacitive discontinuities in the line that shorten its effective length. A simple but fairly accurate analytical model of the effective length has been developed based on an electrostatic approximation of the fields near a rounded vane tip, which is elevated in potential above the nearby rectangular corner. The half-potential surface is pulled closer to the vane, effectively shortening the path length over the original centerline as shown in Fig 2. A spreadsheet program to calculate the effective waveguide width has been implemented, which allows quick estimates of the FWG resonant frequency. This spreadsheet predicts a resonant frequency of 386.35 MHz for a 9-vane scale model test FWG, which is very close to the measured value of 386.37 MHz.

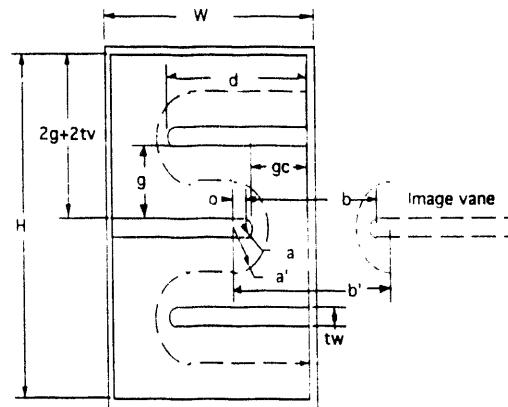


Fig. 2 GEOMETRY USED IN FWG DESIGN CALCULATOR

### FWG ANALYSIS TECHNIQUES

Several analysis tools have been applied to the FWG without a plasma load. Two commercially available numerical codes, EMAS [6] and VARGUS [7], have been used to solve for the eigenmodes of a basic FWG cavity that is closed on both ends and has square-ended vanes. Both codes have successfully converged for several of the lowest order modes of scale model FWG's. The resonant frequencies agree closely with values measured on a test unit (which actually has rounded vane tips).

The VARGUS code uses a frequency-domain eigenmode solver for the finite difference form of Maxwell's equations. A

$77 \times 26 \times 21$  (42,042 point) grid was used to model the test FWG, and a resonant frequency of 386.2 MHz was predicted, which agrees well with the measured resonant frequency of 386.37 MHz. This code and grid configuration will also be used to model the C-Mod FWG unit. A surface plot of VARGUS output for the electric field component parallel to the vanes in a cross section slightly above the vanes and on the midplane of the 386-MHz model is shown in Fig. 3. The electric field is peaked near the vane tips and maximum along its length at the center point of the FWG. The electric fields near the corners of the square vane tips appear as spikes in the output data.

The EMAS code uses finite elements to solve the vector potential form of Maxwell's equations. A grid that is tailored to match the geometry of the problem can be set up to improve the accuracy. A simple FWG box case has been successfully solved with this code. This code has a large number of features and advanced graphical output plotting capabilities.

## FWG-PLASMA INTERACTION

The VARGUS and EMAS numerical electromagnetic codes are capable of analyzing the FWG box, and both codes can probably be extended to include the open polarizing plate by adding an additional box around the face of the antenna. Plasma loading can be simulated by adding absorbing material or absorbing boundary conditions near the polarizing plate. The modeling of a realistic tokamak plasma is very difficult with this type of code due to the complicated nature of the rapidly varying plasma dielectric and the large relative size of the plasma. Although the plasma and FWG internal structure are almost decoupled, the small coupling that does exist represents the antenna loading. Ultimately, a model that includes both FWG and plasma regions with high accuracy is desirable.

The MANTIS code developed at ORNL by Carter [5] for analyzing the interaction between current strap antennas and plasma has been adapted to the FWG case. This code uses a slab plasma model with toroidal and poloidal periodicity to estimate the plasma surface impedance for a realistic density profile and edge plasma. A grid of current elements is set up to approximate the current distribution flowing on the polarizing plate and back into the FWG on each vane surface. The power coupled to the plasma and the launch spectrum is calculated by enforcing continuity of the fields at the plasma edge in Fourier space. The power coupled to the plasma vs. rf magnetic field at the polarizing plate for the C-Mod FWG is estimated to be  $140 \times 10^9$  W/Tesla<sup>2</sup> using the modified MANTIS code. A relationship between the polarizing plate magnetic field and internal electric fields can be estimated using the MANTIS code and also the numerical codes. Laboratory measurements of the FWG fields can be used to check these results [8].

A FWG code based on waveguide modal analysis using unfolded waveguide modes was written by Owens [2]. This code models the plasma region in front of the polarizing plate

as a lossy dielectric and is quite useful in studying the field distribution inside and outside the FWG cavity. Further accuracy may be possible by using this code or the MANTIS code with numerical solutions for the actual modal fields inside the FWG calculated by the EMAS or VARGUS codes.

## CONCLUSION

The rf design and analysis techniques for FWG launchers that are being applied to develop a FWG for the C-Mod tokamak have been quite successful in the preliminary design stage. Numerical techniques have yielded accurate results for the FWG cavity fields. Improved simulations using finer grids and a polarizing plate are expected to be performed soon. A plasma-FWG interaction model is being developed and will be used for predicting loading and launch spectrum. Detailed measurements of resonant frequency and magnetic field patterns for a 386-MHz test unit have been performed and are available for code verification.

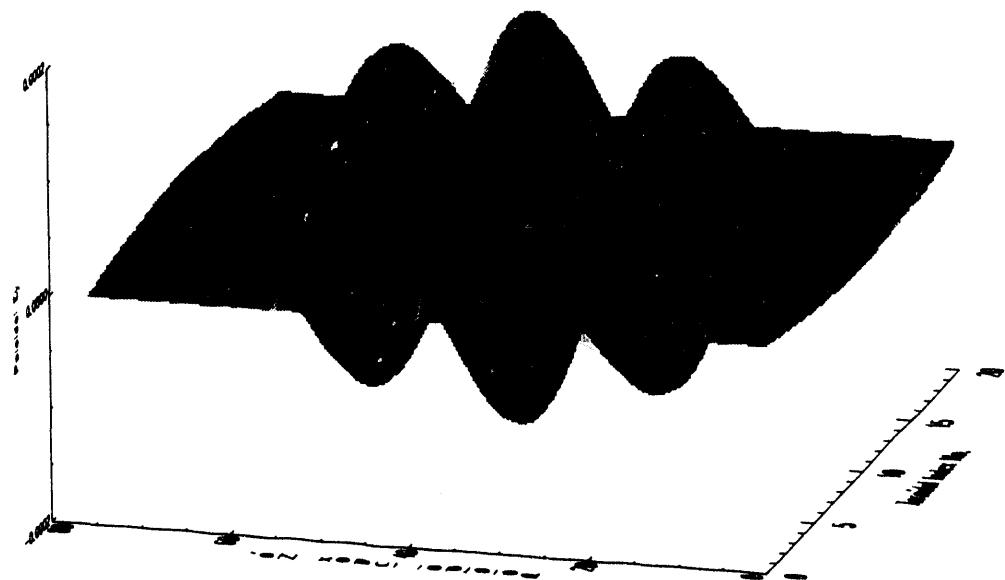
## REFERENCES

- [1] C. H. Fogelman et al., paper this proceedings.
- [2] T. L. Owens, *IEEE Trans. Plasma Sci.*, Vol. PS-14 (6), pp. 934-46, 1986.
- [3] F.W. Baity et al., "Radio-Frequency Power in Plasmas," AIP Conf. Proc. 244, pp. 298-301, 1991.
- [4] W. L. Gardner et al., "Radio-Frequency Power in Plasmas," AIP Conf. Proc., 1993 (unpublished)
- [5] M.D. Carter et al., "Multiple Antenna Implementation System," ORNL/TM-12264, 1993.
- [6] EMAS - a proprietary product available from the McNeil-Schwindler Corp., Milwaukee, Wisconsin.
- [7] VARGUS - a proprietary product available from SAIC, McLean, Virginia.
- [8] G. R. Haste, et al., "The folded waveguide - a high frequency rf launcher," Fus. Engr. & Des. (unpublished).

**NINE VANE FOLDED WAVEGUIDE (5:1 Scale)**  
**First Eigenmode at 386.2 MHz**

**Dimensions:  $60.7 \times 13.5 \times 5.5$  cm Grid:  $23 \times 79 \times 28$**

**Poloidal Field Component  $E_y$  at Toroidal Location  $z = 1.12$  cm (vane tips)**



**Poloidal Field Component  $E_y$  at Toroidal Location  $z = 2.7$  cm (midplane)**

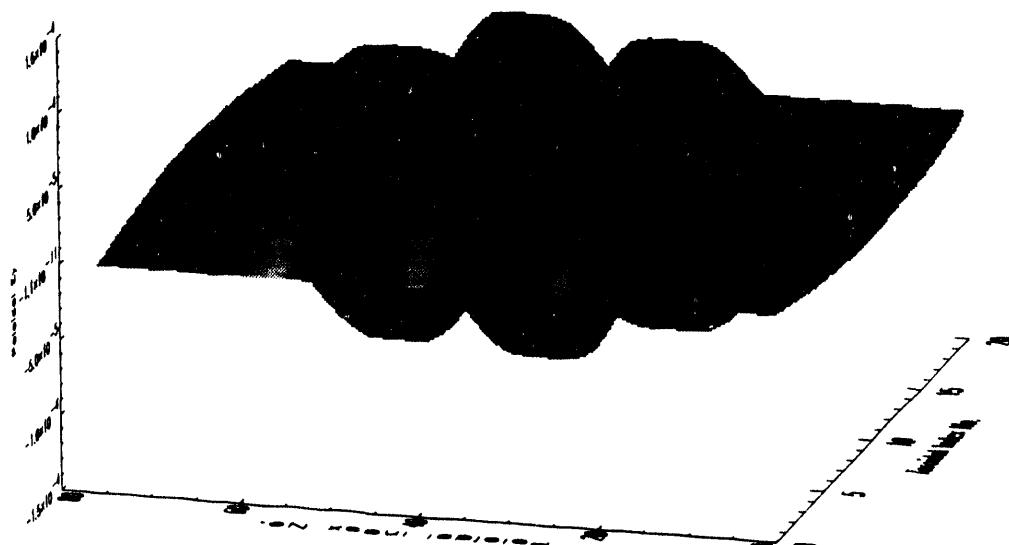


Fig. 3 Calculations of the poloidal electric field component,  $E_y$  for the 386 MHz FWG using VARGUS

A vertical stack of three abstract graphic elements. The top element is a horizontal row of four vertical bars of varying widths, with the central two being the widest. The middle element is a thick, dark L-shaped block, with its vertical leg on the left and its horizontal leg extending to the right. The bottom element is a large, dark, irregular shape with a white, rounded rectangular cutout in the center, resembling a stylized letter 'U' or a shield.

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