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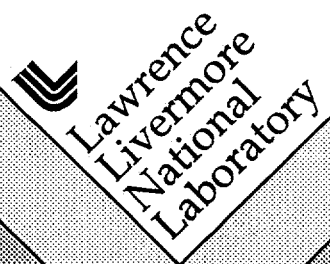
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Ethylene Oxidation Chemistry in a Well-Stirred Reactor

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ETHYLENE OXIDATION CHEMISTRY IN A WELL-STIRRED REACTOR

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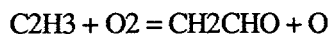
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ETHYLENE OXIDATION CHEMISTRY IN A WELL-STIRRED REACTOR

ABSTRACT

Detailed fuel-lean C₂H₄/H₂O/AIR well-stirred reactor data by Thornton [1] were used to analyze reported combustion chemistry mechanisms and the development of this study's ethylene oxidation mechanism. The data set had been obtained for the temperature range 1003 to 1253K and ethylene-oxygen equivalence ratio range 0.086 to 0.103, at atmospheric pressure. Mechanisms were derived from reaction sets of Westbrook and Pitz [2], and Dagaut, Cathonnet and Boettner [3]. Examination of each reported mechanism indicated unusually large kinetic rates for the vinyl decomposition reaction were used in order to obtain agreement with the Thornton data set.

An ethylene oxidation model was developed in order to address the mechanistic problems of the previous models. This study's mechanism well simulated the overall rate of ethylene oxidation and concentration profiles of CO, CO₂, H₂, CH₂O, C₂H₂, CH₃OH, CH₄, and C₂H₆. Successful predictions by the model were dependent on a new high temperature vinyl oxidation reaction route,



with a $k_{\text{C}_2\text{H}_3+\text{O}_2=\text{CH}_2\text{CHO}+\text{O}}/k_{\text{C}_2\text{H}_3+\text{O}_2=\text{CH}_2\text{O}+\text{HCO}}$ branching ratio of 1.19 - 1.21 at 1053K to 1.63 - 2.47 at 1253K. The branching ratio values were *dependent* upon the extent of fall-off for the $\text{C}_2\text{H}_3 + \text{O}_2 = \text{CH}_2\text{O} + \text{HCO}$ reaction.

INTRODUCTION

Ethylene is an important intermediate in the combustion of methane [4,5], larger aliphatic hydrocarbons [6,7], and aromatics [8]. Consequently, its oxidation is considered to be one of the principal submechanisms for the development of kinetic models for complex fuels. We have identified nine studies devoted to the modeling of ethylene oxidation [2,9-16]. Experimental data used to validate these models were obtained from flow, static and jet-stirred reactors and from shock tubes and flames. The experimental results used in this study to test existing C₂ mechanisms and the presently compiled model were obtained by Thornton [1] using a well-stirred reactor operated at atmospheric pressure, for the temperature range 1003 to 1253 K and ethylene-oxygen equivalence ratio of 0.086 to 0.103. Initial modeling of these results was undertaken and reported by Westbrook et al. [2] and includes Thornton's complete data set.

That work reported that H-atom abstraction from ethylene by OH attack dominated fuel consumption. The rate expression due to Tully [17] represented this primary oxidation pathway and reproduced the well-stirred reactor experimental observations for the loss of ethylene in the 1150 to 1200K range. However, the experimental results at other temperatures were not well simulated by the model, nor were the measured intermediate species well simulated.

In the present study, reported chemical kinetic mechanisms of Westbrook/Pitz (WP) [2], and Dagaut/Cathonnet/Boettner (DCB) [3] were examined by comparing predicted species concentration profiles against experimental measurements of Thornton. These mechanisms were previously tested against the Thornton data set and served as a starting point in the present investigation. Sensitivity and reaction pathway analysis were used to identify of the important reactions controlling the ethylene oxidation process and intermediate concentrations. Differences in the predictions amongst the

mechanisms were determined and discussed in terms of reaction pathways and/or rate expressions used. After a detailed examination of each reported mechanism was conducted an ethylene oxidation model was developed to address the inadequacies represented by the existing mechanisms.

EXPERIMENTAL - DATA SOURCE

The data of Thornton [1] were obtained in a well-stirred reactor using gas chromatography. The details of the well-stirred reactor have been published previously [18,19], including verification of the well-stirred behavior. The stirred reactor was operated at one atmosphere, temperature range of 1003 to 1253K, nominal residence time of 2msec, and ethylene-oxygen equivalence ratio range of 0.086 to 0.103. The inlet composition consisted of complete products of very fuel-lean hydrogen combustion of approximately 11% O₂, 14% H₂O, and 75% N₂ together with the amount of ethylene (0.36%) seeded into the flow. All values are molar.

Detailed multipoint calibration curves were generated for H₂, CO, CO₂, O₂, and C₂H₄, where there was concern about qualitative accuracy over the range of concentrations seen in these experiments. Only in rare cases was the accuracy in the concentration measurements poorer than that of the calibration standards of 2%. Thornton determined the uncertainties to the measured species concentration to be approximately 2% for CH₄ and C₂H₆; 10% for C₂H₂; and 20% for CH₂O and CH₃OH. No measurements were undertaken for free radicals. Errors introduced by jet-stirred reactor inhomogeneity were considered to apply only to components derived from the introduction of the ethylene additive. Measurement uncertainties due to reactor inhomogeneity are estimated to be 40% for CH₂O and CH₃OH, and an estimated uncertainty of 20% for all other species. An elemental carbon and oxygen balance was checked at all temperatures and was found good to 101±1.0% and 102±1.6% respectively.

Non-catalytic coated type R platinum-rhodium thermocouples were used to measure the reactor temperature. Uncertainties from radiation and conduction losses are estimated to be less than 20K.

COMPUTATIONAL MODEL AND MECHANISMS

The computational model used for this study is the Sandia micromixed perfectly stirred reactor (PSR) code [20]. The model considers the 15.8cc reactor volume in which the experiments took place. Input parameters are the measured reactor temperature, inlet mass flow rate, and inlet composition.

The reported mechanisms considered in this study are summarized below:

1. The mechanism of Westbrook and Pitz (WP) was initially developed to analyze the experimental results of ethylene oxidation by Thornton. The detailed numerical modeling analyses has been reported, however, a reexamination of their mechanism was conducted for the purposes of identifying which reaction or interacting set of reactions cause agreement or disagreement between the full data set and predictions. Both forward and reverse rates are given in the mechanism, thus insuring use of their thermochemistry.
2. The Dagaut, Cathonnet and Boettner (DCB) mechanism is an improved version of their previous ethylene reaction sets [15,16]. This particular mechanism had been validated for ethylene, methane and ethane combustion for the conditions of 1-10 atmospheres, 900-1200K temperature range and fuel-air equivalence ratio range 0.1-1.5. Sixteen unimolecular and bimolecular chemically activated reactions have been pressure corrected to one atmosphere and are included in the mechanism. Only the forward rate expressions were cited and thermodynamics were taken from the Chemkin Thermodynamics Database [21] and Burcat thermochemical data (i.e. C₂H₄O) [22].

While these kinetic schemes may not represent the current mechanisms of these authors, the aim of the present analysis is to elucidate the important reactions controlling the ethylene oxidation process and reaction intermediates formed from therein.

RESULTS OF THE REPORTED MECHANISMS

Concentration profiles for the measured stable species (C_2H_4 , CO , CO_2 , H_2 , CH_2O , C_2H_2 , CH_3OH , CH_4 , and C_2H_6) as computed using the WP and DCB mechanisms have been compared with the Thornton data set. The full presentation of the numerical computations and discussion are found in Marinov [23]. Only a summary of the important findings are presented here.

The two mechanisms showed good agreement for the loss of ethylene in only a limited temperature range. The WP mechanism well represented the loss of ethylene for only the 1150-1200K temperature range. The DCB mechanism showed a better representation for the loss of ethylene over the 1050 - 1200K temperature range. Reaction pathway analysis indicated that approximately 40 - 50% of the ethylene is consumed by OH radicals followed by a substantial secondary amount of consumption by O-atom. In contrast, alkyne flame modeling studies [24] found oxidation by O-atom to be critical in fuel-lean to fuel-rich lightly sooting flame; while in alkane flames, oxidation by OH and H-atom at fuel-lean to stoichiometric conditions are considered to be important.

Intermediates, in general, were not well simulated by the WP mechanism while DCB simulated all stable species, except for acetylene and methanol, fairly well for temperatures up to 1200K. Acetylene was overpredicted by a factor of 20 to 30 for both mechanisms and methanol was underpredicted by approximately a factor of 10 by DCB. DCB overpredicted ethane by a factor of two to three for the 1050 - 1200K temperature range, while in WP, ethane was underpredicted by roughly

one order of magnitude. The two mechanisms predicted formaldehyde to within a factor of two for all temperatures. Methane, hydrogen, carbon monoxide and carbon dioxide species were well-simulated by DCB for temperatures to 1200K, while WP simulated these species well only around 1178K. Figures 1 and 2 show the measured and predicted profiles by WP and DCB for ethylene, acetylene and methanol.

Temperatures greater than 1200K, the loss of ethylene is overpredicted by both mechanisms. Poor mixing of the gases at the microscale was suggested by WP and DCB as the reason for the observed disagreement between model and experimental measurement.

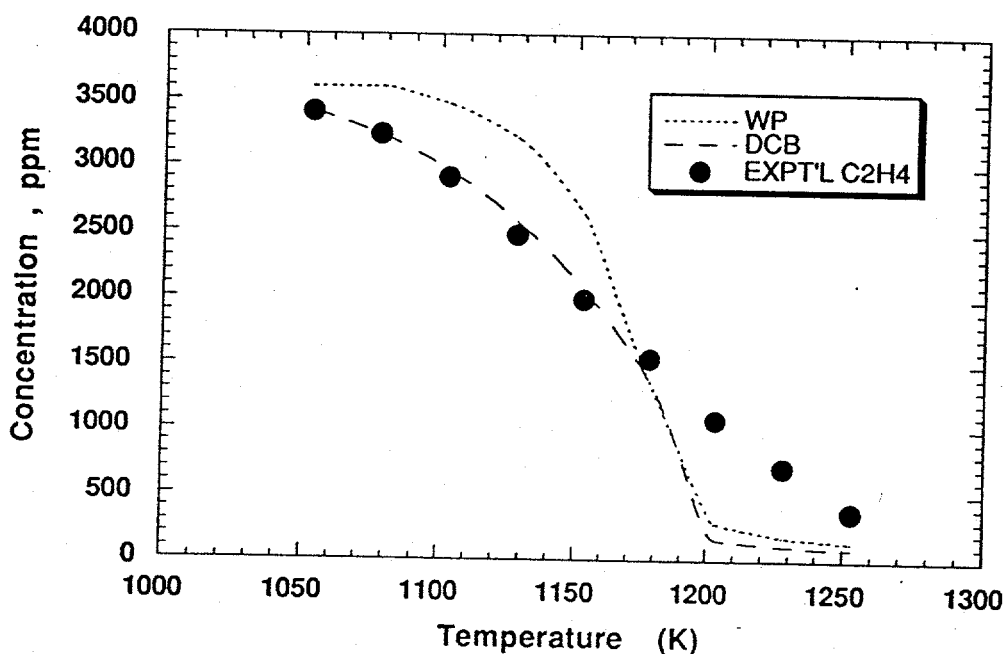


Figure 1 : Comparison of predicted and experimental concentration profile of ethylene in the well-stirred reactor for ethylene oxidation: Experimental (solid symbols), from Thornton; predicted curves, from the mechanisms of Westbrook and Pitz (WP); and Dagaut, Cathonnet, and Boettner (DCB).

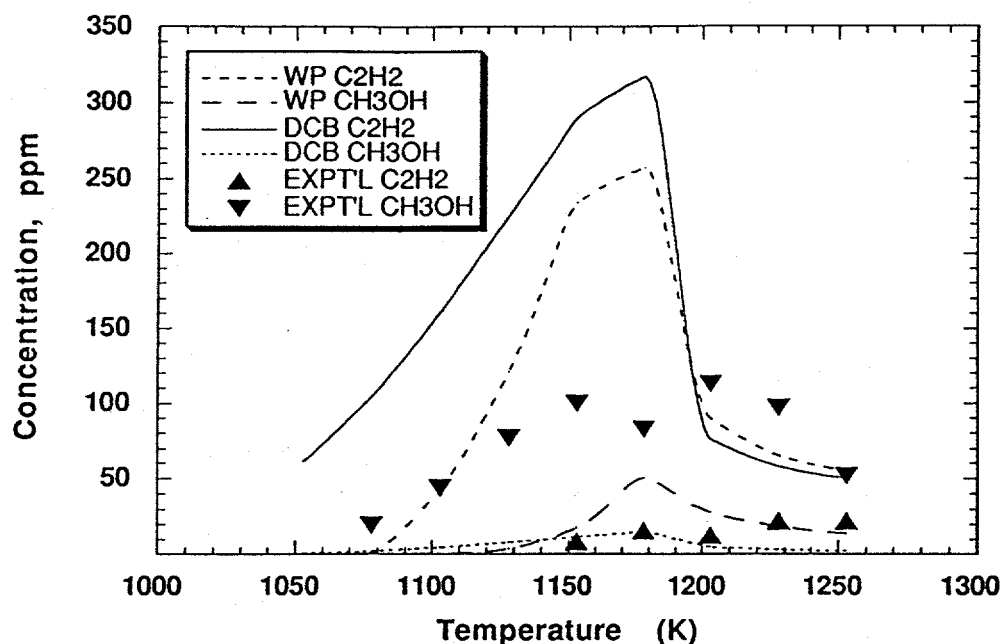


Figure 2: Comparison of predicted and experimental concentration profiles of acetylene and methanol in the well-stirred reactor for ethylene oxidation: Experimental (solid symbols), from Thornton; predicted curves, from the mechanisms of Westbrook and Pitz (WP); and Dagaut, Cathonnet, and Boettner (DCB).

The principal difference in the model predictions between the DCB and WP mechanisms lies in the kinetic rate choice for the vinyl decomposition reaction. DCB used a two orders of magnitude faster vinyl decomposition rate than WP which allowed vinyl decomposition to predominate over vinyl oxidation by O_2 . The early production of H-atom from $C_2H_3 = C_2H_2 + H$ allows for rapid chain branching through $H + O_2 = OH + O$. The formed O-atom will preferentially react with C_2H_4 producing $CH_3 + HCO$ and $CH_2 + HCO + H$ in DCB or $CH_3CO + H$ in WP. The H-atom produced from $C_2H_4 + O$ allows for additional chain branching which further consumes the ethylene. DCB attained better agreement at the lower temperatures than WP primarily due to the usage of a higher vinyl decomposition rate.

Minor differences were exhibited by both mechanisms with regards to the predicted methanol and ethane profiles. These predicted profiles did not compare well with the experimental data and indicates a problem symptomatic to both mechanisms. The problem either lies in a lack of methyl radical production (which leads to methanol and ethane formation) or inconsistencies within the methyl radical removal kinetic rates and/or kinetics.

VINYL RADICAL KINETICS AND THERMOCHEMISTRY

The vinyl radical intermediate plays an integral role in ethylene oxidation due to the importance of $\text{C}_2\text{H}_4 + \text{OH} = \text{C}_2\text{H}_3 + \text{H}_2\text{O}$. Unfortunately, the kinetics and product formation involving the vinyl destruction process is not well understood. Furthermore, the uncertainty of the vinyl radical heat of formation affects calculated thermodynamic equilibrium rates with considerable sensitivity. The important vinyl removal kinetics were assessed by comparing DCB and WP's choices to known evaluations and reviews. This would determine the relative importance each model placed on vinyl decomposition with respect to the ethylene oxidation modeling.

Table 1 represents a listing of typically assigned products and rate expressions involving the important vinyl oxidation and decomposition reactions used in the current literature and modeling studies. A wide range of values are exhibited for the $\text{C}_2\text{H}_3 + \text{O}_2$ pathway to $\text{C}_2\text{H}_2 + \text{HO}_2$ and vinyl decomposition rates. The former is due to the uncertainty in product domination for vinyl oxidation at typical combustion temperatures (i.e. $T > 900\text{K}$) and the later is due to a poor understanding of the vinyl decomposition process.

The vinyl radical heat of formation has been measured or reviewed for a considerable range of values as exhibited in Table 1. The choice of

Table 1
The Main Vinyl Oxidation and Decomposition Reaction Rate Expressions and
Vinyl Heat of Formation as used by Modellers or cited in the Kinetics Literature
Rate Data in cm³-mole-sec-kcal units
 $k = A \cdot T^n \cdot \exp(-E_A/RT)$

Source	log A	n	E _A	log k(1153K)	Ref.
C2H3 + O2 = CH2O + HCO^ae)					
Slagle et al.	12.60	0.0	-0.248	12.647	29
DCB	12.48	0.0	-0.25	12.527	3
WP	12.176	0.0	0.0	12.176	2
Westmoreland ^{b)}	26.651	-4.55	5.48	11.681	30
Bozzelli/Dean ^{b)}	23.037	-3.29	3.892	12.226	31
C2H3 + O2 = C2H2 + HO2^{c)}					
Tsang/Hampson	11.08	0.0	0.0	11.08	4
Glarborg	12.73	0.0	0.0	12.73	32
Warnatz	12.0	0.0	0.0	12.0	5
Westmoreland ^{b)} addition rxn.	21.708	-3.24	5.66	10.72	30
Westmoreland metathesis rxn.	11.6	0.0	0.0	11.6	30
Bozzelli/Dean ^{b)}	15.715	-1.26	3.31	11.23	31
DCB and WP did not include this reaction pathway					
C2H3 (+M) = C2H2 + H (+M) a)c)f)					
DCB	44.323	-8.447	51.106	8.77	3
WP	28.58	-4.4	44.29	6.71	2
Tsang/Hampson	44.715	-9.8	52.24	4.81	4
Baulch	42.352	-9.2	49.14	4.87	25
Warnatz	13.567	-1.0	32.06	4.43	5
Miller / Bowman	25.639	-4.4	42.52	4.11	26
KWKW ^{d)}	36.79 ± 0.4	-8.17	45.59	3.13	28
Rao/Skinners ^{g)}	13.73	-1.3	33.97	3.31	27,5
Source	$\Delta H_f(298K, C_2H_3)$		Ref.		
Ayranci / Back	63.4	kcal/mol	32		
Shiromaru	77		33		
Golden	66		27		
McMillian / Golden	70.4		35		
Ervin	71.7		36		
Kee et al.	68.4		21		

a) Corrected for fall-off at 1.0 atm. b) Based on $\Delta H_f(C_2H_3, 298K) = 70.4$ kcal/mol
c) Based on $\Delta H_f(C_2H_3, 298K) = 68.4$ kcal/mol

d) KWKW performed RRKM calculations based on $\Delta H_f(C_2H_3, 298K) = 63.4$ kcal/mol. This study has adjusted the activation energy downward from 50.59kcal/mol to 45.59kcal/mol to obtain a comparison to other rate expression evaluations performed at $\Delta H_f(C_2H_3, 298K) = 68.4$ kcal/mol.

e) Rate expression units: cm³/mol-sec f) Rate expression units: sec⁻¹

g) Used $k_{\infty, C_2H_2+H = C_2H_3}$ from Warnatz [5] for Lindemann-Hinshelwood pressure correction. Equilibrium constants calculated from Kee et al. thermochemistry [21].

heat of formation value used may have an impact on the modeling calculations. Thermodynamic considerations aptly point out that the higher heat of formation value implies less stability of the vinyl radical which in turn favors higher rate expressions for vinyl decomposition or oxidation reactions and vice-versa. In this current study, no sensitivity analysis was conducted to assess which is the better heat of formation value.

Vinyl Decomposition

A compiled list of $C_2H_3 (+M) = C_2H_2 + H (+M)$ rate expressions corrected for fall-off have been derived and are presented in Table 1. Curved Arrhenius plots of these expressions are presented in figure 3. The list includes the reviews by Baulch et al. [25], Tsang and Hampson [4], and Warnatz [5] plus the recommendation from Miller and Bowman [26]. Recent shock tube studies of Rao and Skinner [27], and Kiefer, Wei, Kern and Wu (KWKW) [28] have been included in the assessment of the vinyl decomposition reaction at high temperatures.

Pressure correction was performed according to the information presented by the various evaluations, and are based on a 68.4 kcal/mol heat of formation value. The referenced sources of these evaluations and applied pressure corrections have been conducted in the following manner. Tsang and Hampson obtained a RRKM calculated low pressure rate expression based on the forward rate expression determined by Benson and Haugen [37] plus the measured low temperature and high pressure reverse rates of Payne and Stief [38] and Sugarawa et al. [39]. The Tsang and Hampson low pressure rate expression was corrected for weak collisions by using the recommended collisional deactivation step size of 450 cm^{-1} for a N_2 collider at one atmosphere. Table 1 lists the Tsang and Hampson pressure corrected rate evaluation. Baulch et al. [25] recommended the use of the Tsang and Hampson vinyl decomposition low pressure rate expression but advised the use of the Troe Method for fall-off corrections. The high pressure forward rate

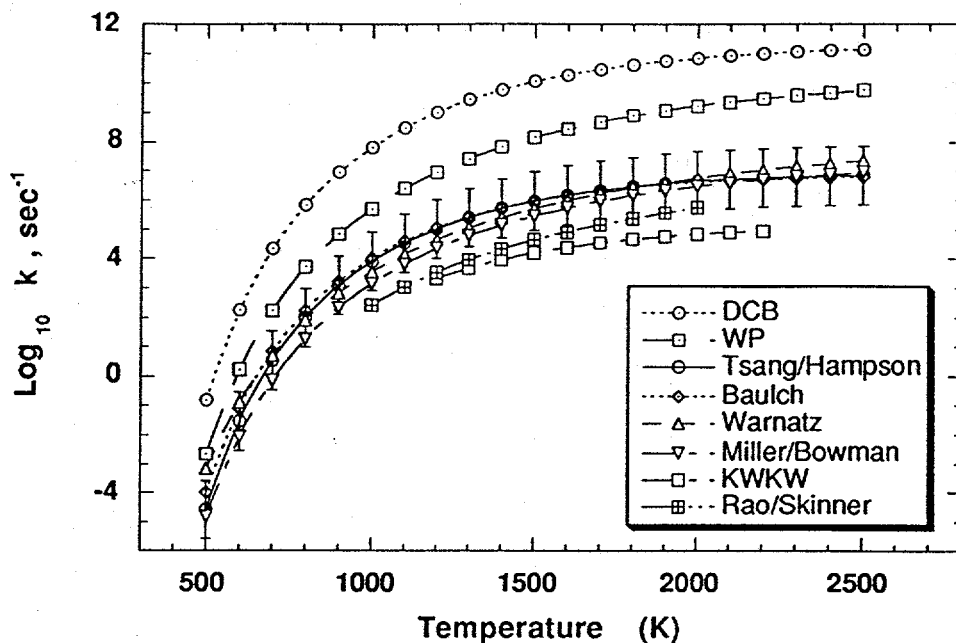


Figure 3: Evaluated kinetic rate data at one atmosphere for vinyl decomposition based on $\Delta H_f(C_2H_3, 298K) = 68.4 \text{ kcal/mol}$. See Table 1 for the numerical representation of the fall-off corrected kinetic rates.

expression was taken from the Warnatz review and a center-broadening parameter value of 0.35 as recommended by Baulch et al. was then used to derive the Table 1 expression. The Warnatz [5] recommended low and high pressure forward rate expressions were based on literature data taken from the 1960's and 1970's. The Lindemann-Hinshelwood method was then applied to derive the rate expression ascribed to Warnatz in Table 1. All reviews have an associated uncertainty factor of 10 and, along with the Miller and Bowman recommendation, lie within this measure of uncertainty. This is noted by the uncertainty factor bars placed about the Tsang and Hampson rate expression shown in the figure. Clearly, all reviews are in accordance with one another.

A comparison of the reviewed vinyl decomposition kinetics with recent shock tube measurements indicates slower vinyl decomposition kinetics occurs than suggested by the recent reviews. The high temperature vinyl-bromide and vinyl-iodide pyrolysis shock tube measurements of Rao and Skinner indicate the vinyl decomposition rate occurs a factor of 10 lower than the recent reviews. Their vinyl decomposition results were determined independently of the vinyl radical heat of formation and support the revised rate expression of KWKW as determined by this study. The high temperature 1,3-butadiene pyrolysis shock tube measurements and RRKM analysis of KWKW suggest a relatively stable vinyl radical and a slow vinyl decomposition kinetic rate in direct contradiction to WP and DCB.

The WP and DCB mechanisms utilize vinyl decomposition kinetic rates which exceed the upper uncertainty factor limit for the reviewed evaluations by approximately one and three orders of magnitude. Furthermore, WP and DCB usage of fast vinyl decomposition rates are not supported by the Rao/Skinner and KWKW shock tube studies. The analysis of the vinyl decomposition process coupled with the poor acetylene modeling predictions of DCB and WP clearly suggest that a lower vinyl decomposition kinetic rate must be used than those supported by DCB and WP.

Vinyl Oxidation by Molecular Oxygen

The dearth of high temperature studies concerning the reaction kinetics of $C_2H_3 + O_2$ is the primary cause of uncertainty in product formation and kinetic rates at typical combustion conditions. However, the kinetics concerning $C_2H_3 + O_2$ is well-defined at low temperatures. Experiments by Baldwin and Walker [40] and Gutman et al. [29, 41] indicated that the addition channel leading to $CH_2O + HCO$ is the primary products for $C_2H_3 + O_2$ at low temperatures. Gutman et al. measured rate constants and conclusively established that $C_2H_3 + O_2$ formed $CH_2O + HCO$

at 297-599K and 0.48-3.6 torr He. No C₂H₂ and HO₂ were detected, so any C₂H₂ + HO₂ product pathway contribution is considered to be less than 10%.

No direct high temperature chemical kinetic studies have been conducted to examine the C₂H₃ + O₂ reaction. However, Cooke and Williams [42] studied ignition delays in shock-heated ethane-oxygen-argon mixtures at 1400-1800K and 200-300 torr. Their measured induction times were modelled with a 34-step mechanism that included the C₂H₃ + O₂ = C₂H₂ + HO₂ reaction.

Reviews by Tsang and Hampson [4] and Warnatz [5] assumed the C₂H₃ + O₂ reaction proceeded to C₂H₂ + HO₂ in an analogous fashion as the C₂H₅ + O₂ reaction which was thought to proceed by simple H-atom abstraction by O₂ under typical combustion conditions. However, the recent study by Wagner et al. [43] postulated that the ethyl radical plus oxygen reaction is complex. The reaction involves O₂ addition followed by stabilization of the adduct (only for temperatures below approximately 650K) or isomerization of the adduct followed by decomposition to C₂H₄ + HO₂. The postulated reaction scheme effectively rules out the direct H-atom metathesis route for C₂H₅ + O₂ and therefore suggests that H-atom abstraction from C₂H₃ by O₂ is unlikely to occur. Unfortunately, the viability of the simple H-atom abstraction by O₂ reaction mechanism is not known for the C₂H₃ + O₂ reaction. Interestingly, Westmoreland [30] suggested the possibility that C₂H₃ + O₂ metathesis reaction leading to C₂H₂ + HO₂ could dominate at temperatures above 1500 K depending on the prescribed nature of the fall-off for the C₂H₃ + O₂ = CH₂O + HCO reaction.

If the primary oxidation channel is CH₂O + HCO at high temperatures, then the early source of reactive free radicals must come from formyl radical dissociation. The H-atom produced from formyl decomposition would be sufficient to sustain chain branching and further ethylene oxidation. The other possibility, C₂H₂ + HO₂, is ruled out due to poor

predictions of the acetylene profile that would result if this reaction were to be favored and the production of an unreactive HO₂ radical.

Lastly, vinyl plus a radical reaction is unlikely to provide the necessary impetus for substantial reactive free radical production as the C₂H₃ + O₂ reaction dominates at these temperatures.

THIS STUDY'S ETHYLENE OXIDATION MODEL

The inadequacies represented by the poorly predicted acetylene, methanol and other reaction intermediate profiles, and the disagreement at the higher temperatures of the data set by the WP and DCB mechanisms warranted the development of this studies ethylene oxidation model. A review of kinetics literature was conducted for the development and compilation of this mechanism [23].

The presently developed model was used to reproduce the ethylene oxidation experimental measurements of Thornton and the lean, atmospheric pressure, methane and ethane data sets for the 900 - 1200K temperature range of Dagaut et al. [3,44]. Discussion will pertain only to the ethylene oxidation chemistry, further discussion on the methane and ethane modeling is presented in Marinov [23]. The ethylene mechanism is listed in Table 2 and consists of 206 reactions and 40 species. The inclusion of third body efficiencies and pressure corrections were applied as necessary to the model. Table 3 shows the species thermochemistry used in this study.

Discussion

Ethylene Kinetics:

For the temperature range 1053 to 1253K of this study, the major loss of ethylene occurs by reaction (50) of Table 2:

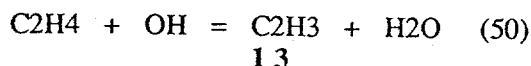


Table 2
Ethylene oxidation mechanism. Rate data in cm³-mole-sec-kcal units,
 $k = A \cdot T^n \cdot \exp(-E_A/RT)$

No.	Reaction						log A	n	E _A	Ref.
1.	H	H	M	=	H ₂	M	18.0	-1.0	0.0	[45]
2.	H	H	H ₂	=	H ₂	H ₂	16.964	-0.6	0.0	[45]
3.	H	H	H ₂ O	=	H ₂	H ₂ O	19.778	-1.25	0.0	[45]
4.	H	H	CO ₂	=	H ₂	CO ₂	20.74	-2.0	0.0	[45]
5.	O	H	M*	=	OH	M*	18.673	-1.0	0.0	[4]
6.	OH	H	M*	=	H ₂ O	M*	22.345	-2.0	0.0	[4]
7.	O	O	M*	=	O ₂	M*	13.275	0.0	-1.788	[4]
8.	H	O ₂	M#	=	HO ₂	M#	17.903	-0.8	0.0	[25]
9.	OH	OH	(M)	=	H ₂ O ₂	(M)†	14.092	-0.37	0.0	[46,4, a]
10.	H ₂ O	O		=	OH	OH	5.171	2.6	15.175	[47]
11.	H ₂	OH		=	H ₂ O	H	8.0	1.6	3.298	[25]
12.	O ₂	H		=	OH	O	16.546	-0.7	17.07	[48]
13.	H	HO ₂		=	H ₂	O ₂	13.63	0.0	1.41	[25]
14.	H	HO ₂		=	OH	OH	14.22	0.0	0.87	[25]
15.	H	HO ₂		=	H ₂ O	O	13.48	0.0	1.72	[25]
16.	O	HO ₂		=	OH	O ₂	13.26	0.0	-0.397	[4]
17.	OH	HO ₂		=	H ₂ O	O ₂	13.46	0.0	-0.497	[25]
18.	H ₂ O ₂	OH		=	HO ₂	H ₂ O	0.381	4.042	-2.126	(b)
19.	H ₂ O ₂	O		=	OH	HO ₂	6.984	2.0	3.974	[4]
20.	H ₂ O ₂	H		=	HO ₂	H ₂	12.23	0.0	3.775	[25]
21.	H ₂ O ₂	H		=	H ₂ O	OH	13.382	0.0	3.974	[4]
22.	HO ₂	HO ₂		=	H ₂ O ₂	O ₂	-14.06	8.1	-8.68	[49]
23.	H ₂	O ₂		=	OH	OH	13.23	0.0	47.78	[25]
24.	O	H ₂		=	OH	H	4.705	2.67	6.29	[50]
25.	CO	OH		=	CO ₂	H	6.643	1.5	-0.741	[5]
26.	CO	O	M*	=	CO ₂	M*	14.79	0.0	3.00	[4]
27.	CO	HO ₂		=	CO ₂	OH	14.18	0.0	23.64	[5]
28.	CO	O ₂		=	CO ₂	O	12.4	0.0	47.7	[5]
29.	CH ₃	CH ₃	(M)	=	C ₂ H ₆	(M)	16.964	-1.174	0.636	[51,a]
30.	C ₂ H ₆	OH		=	C ₂ H ₅	H ₂ O	6.859	2.0	0.864	[25]
31.	C ₂ H ₆	O		=	C ₂ H ₅	OH	10.941	0.957	6.637	[52]
32.	C ₂ H ₆	H		=	C ₂ H ₅	H ₂	2.73	3.5	5.21	[4]
33.	C ₂ H ₆	HO ₂		=	C ₂ H ₅	H ₂ O ₂	11.47	0.0	14.94	[4]
34.	C ₂ H ₆	CH ₃		=	C ₂ H ₅	CH ₄	-6.822	6.0	6.046	[25]
35.	C ₂ H ₆		(M)	=	C ₂ H ₅	H	20.947	-1.22	102.2	[53,c]
36.	C ₂ H ₆	O ₂		=	C ₂ H ₅	HO ₂	13.6	0.0	50.87	[4]
37.	C ₂ H ₅	OH		=	C ₂ H ₄	H ₂ O	13.38	0.0	0.0	[4]
38.	C ₂ H ₅	OH		=	CH ₃	CH ₂ O	13.38	0.0	0.0	[4]
39.	C ₂ H ₅	O		=	CH ₃	CH ₂ O	13.645	0.0	0.0	[54]
40.	C ₂ H ₅	O		=	CH ₃ CHO	H	13.727	0.0	0.0	[54]
41.	C ₂ H ₅	O		=	C ₂ H ₄	OH	13.512	0.0	0.0	[54]
42.	C ₂ H ₅	HO ₂		=	CH ₃	CH ₂ O	13.2	0.0	0.0	[4,d]
43.	C ₂ H ₅	C ₂ H ₅		=	C ₂ H ₄	C ₂ H ₆	12.14	0.0	0.0	[4]
44.	C ₂ H ₅	CH ₃		=	C ₂ H ₄	CH ₄	-3.36	5.0	8.3	[3]
45.	C ₂ H ₅	H		=	C ₂ H ₄	H ₂	14.1	0.0	8.0	[3]
46.	C ₂ H ₅	HCO		=	C ₂ H ₆	CO	14.0	0.0	0.0	[4]
47.	C ₂ H ₅	O ₂		=	C ₂ H ₄	HO ₂	20.48	-2.86	6.76	[55]
48.	C ₂ H ₅	O ₂		=	C ₂ H ₄ O ₂ H		40.11	-9.41	11.03	[55]
49.	C ₂ H ₅	O ₂		=	CH ₃ CHO	OH	14.20	-1.17	10.39	[55]
50.	C ₂ H ₄	OH		=	C ₂ H ₃	H ₂ O	6.47	2.0	2.235	[56]
51.	C ₂ H ₄	O		=	CH ₃	HCO	13.74	0.0	5.5	[57,e]
52.	C ₂ H ₄	O		=	CH ₂	HCO	13.37	0.0	5.5	[57,e]
53.	C ₂ H ₄	H		=	C ₂ H ₃	H ₂	7.18	2.0	6.0	[9]
54.	C ₂ H ₄	CH ₃		=	C ₂ H ₃	CH ₄	0.821	3.7	9.5	[4]
55.	C ₂ H ₄	HO ₂		=	C ₂ H ₃	H ₂ O ₂	13.05	0.0	30.43	[12]
56.	C ₂ H ₄	HO ₂		=	C ₂ H ₄ O ₂ H		11.3	0.0	8.0	[12]
57.	C ₂ H ₄	H	(M)	=	C ₂ H ₅	(M)	13.42	0.0	2.16	[58,a]
58.	C ₂ H ₄	O ₂		=	C ₂ H ₃	HO ₂	13.63	0.0	57.6	[4]
59.	C ₂ H ₄		(M)	=	C ₂ H ₂	H ₂	12.90	0.44	88.76	[4,i]
60.	C ₂ H ₄		(M)	=	C ₂ H ₃	H	12.90	0.44	88.76	[4,i]
61.	C ₂ H ₄ O ₂ H			=	C ₂ H ₄ O	OH	11.5	0.0	19.5	[12]
62.	C ₂ H ₄ O	OH		=	C ₂ H ₃ O	H ₂ O	13.68	0.0	5.955	[12]
63.	C ₂ H ₃ O			=	CH ₃ CO		14.93	0.0	14.0	[12]
64.	CH ₂ CHO			=	CH ₂ CO	H	37.02	-7.189	44.32	[9]
65.	CH ₂ CHO	O ₂		=	CH ₂ CO	HO ₂	10.2	0.0	0.0	[k98]
66.	CH ₂ CHO	O ₂		=	CH ₂ O	CO	10.4	0.0	0.0	[25]
67.	CH ₂ CHO	O ₂		=	CHOCHO	OH	11.4	0.0	14.64	[k160]
68.	CH ₂ CHO	O		=	CH ₂ O	HCO	13.6	0.0	0.0	(h)
69.	CH ₂ CHO	HO ₂		=	CH ₂ O	HCO	13.0	0.0	0.0	(k157)

70.	CHOCHO		(M*)	=	CH2O	CO	(M*)	12.63	0.0	50.6	[59, 60,i]
71.	CHOCHO		(M*)	→	CO	CO	(M*)	14.03	0.0	55.1	[60,i]
72.	CHOCHO	OH		=	CHOCO	H2O		13.0	0.0	0.0	(61,h)
73.	CHOCHO	O		=	CHOCO	OH		12.86	0.0	1.97	(i)
74.	CHOCHO	H		=	CH2O	HCO		12.0	0.0	0.0	[60]
75.	CHOCHO	HO2		=	CHOCO	H2O2		12.23	0.0	10.7	(i)
76.	CHOCHO	CH3		=	CHOCO	CH4		12.24	0.0	8.44	(i)
77.	CHOCHO	O2		=	HCO	CO	HO2	13.8	0.0	30.0	(i)
78.	CHOCO			=	HCO	CO		7.3	0.0	0.0	[62]
79.	CHOCO	O2		=	CO	CO	HO2	12.6	0.0	0.0	[h]
80.	CH3CHO	OH		=	CH3CO	H2O		10.73	0.73	-1.11	[25]
81.	CH3CHO	H		=	CH3CO	H2		9.612	1.16	2.4	[25]
82.	CH3CHO	O		=	CH3CO	OH		12.77	0.0	1.81	[25]
83.	CH3CHO	O2		=	CH3CO	HO2		13.3	0.5	42.2	[63]
84.	CH3CHO	CH3		=	CH3CO	CH4		-5.7	5.64	2.464	[25]
85.	CH3CO		(M)	=	CH3	CO	(M)	13.3	0.0	17.625	[25,i]
86.	CH2CO	OH		=	CH2OH	CO		13.45	0.0	0.0	[64]
87.	CH2CO	OH		=	HCCO	H2O		13.0	0.0	2.0	[26,d]
88.	CH2CO	O		=	CH2	CO2		12.251	0.0	1.3	[65]
89.	CH2CO	O		=	HCCO	OH		13.7	0.0	8.0	[66]
90.	CH2CO	H		=	CH3	CO		13.05	0.0	3.428	[26]
91.	CH2CO	H		=	HCCO	H2		13.88	0.0	8.0	[26]
92.	CH2CO	HO2		=	CH2O	CO	OH	11.78	0.0	12.74	[67]
93.	CH2CO		(M)	=	CH2	CO	(M)	14.48	0.0	70.98	[5,i]
94.	C2H3	O2		=	C2H3O2			46.663	-10.69	12.338	[29]
95.	C2H3	O2		=	CH2O	HCO		29.23	-5.312	6.500	[29]
96.	C2H3	O2		=	CH2CHO	O		14.835	-0.611	5.260	[30,68,e]
97.	C2H3	O2		=	CHOCHO	H		23.847	-4.069	4.465	[29]
98.	C2H3	O2		=	C2H2	HO2		10.544	0.0	0.0	(e)
99.	C2H3		(M)	=	C2H2	H	(M)	9.805	1.0	37.609	(e,f)
100.	C2H3	HO2		=	CH3	CO	OH	13.60	0.0	0.0	[4,d]
101.	C2H3	OH		=	C2H2	H2O		13.48	0.0	0.0	[4]
102.	C2H3	O		=	CH3	CO		13.48	0.0	0.0	[69]
103.	C2H3	H		=	C2H2	H2		13.08	0.0	0.0	[25]
104.	C2H3	CH3		=	C2H2	CH4		-3.36	5.0	8.3	[3]
105.	C2H3	CH2O		=	C2H4	HCO		3.73	2.81	5.86	[4]
106.	C2H2	O		=	CH2	CO		6.338	2.09	1.562	[70]
107.	C2H2	O		=	HCCO	H		6.706	2.09	1.562	[70]
108.	C2H2	OH		=	C2H	H2O		7.53	2.0	14.0	[71]
109.	C2H2	OH		=	HCCOH	H		5.702	2.3	13.5	[71]
110.	C2H2	OH		=	CH2CO	H		-3.659	4.5	-1.0	[71]
111.	C2H2	OH		=	CH3	CO		-3.314	4.0	-2.0	[71]
112.	C2H2	O2		=	HCCO	OH		8.3	1.5	30.1	[66]
113.	HCCOH	H		=	CH2CO	H		13.0	0.0	0.0	(h)
114.	HCCO	OH		=	HCO	CO	H	13.0	0.0	0.0	[66]
115.	HCCO	H		=	CH2(S)	CO		14.18	0.0	0.0	[72]
116.	HCCO	O		=	CO	CO	H	14.04	0.0	0.0	[73]
117.	HCCO	O2		=	CO2	CO	H	12.204	0.0	0.854	[73]
118.	C2H	H2		=	C2H2	H		5.618	2.39	0.864	[74]
119.	C2H	O2		=	CO	CO	H	13.4	0.0	0.0	[75]
120.	C2H	O2		=	CH	CO2		15.65	0.0	25.1	[76]
121.	C2H	OH		=	CH2	CO		13.26	0.0	0.0	[4]
122.	C2H	O		=	CH	CO		13.0	0.0	0.0	[25]
123.	CH2O	OH		=	HCO	H2O		9.64	1.18	-0.447	[4]
124.	CH2O	H		=	HCO	H2		8.341	1.77	3.00	[4]
125.	CH2O	O		=	HCO	OH		7.519	1.94	1.037	[77]
126.	CH2O	HO2		=	HCO	H2O2		12.3	0.0	11.665	[78]
127.	CH2O	CH3		=	HCO	CH4		-12.05	7.4	-0.96	[79]
128.	CH2O		M	=	HCO	H	M	41.08	-6.9	96.55	[4]
129.	HCO		M*	=	H	CO	M*	17.27	-1.0	17.0	[80]
130.	HCO	O2		=	CO	HO2		8.217	1.36	-1.24	(k)
131.	HCO	OH		=	CO	H2O		13.48	0.0	0.0	[5]
132.	HCO	H		=	CO	H2		13.96	0.0	0.0	[25]
133.	HCO	HO2		=	CO2	OH	H	13.48	0.0	0.0	[4]
134.	HCO	O		=	CO	OH		13.48	0.0	0.0	[5]
135.	HCO	O		=	CO2	H		13.48	0.0	0.0	[5]
136.	CH3O		(M)	=	CH2O	H	(M)	13.30	0.0	27.42	[81,4,h]
137.	CH3O	O2		=	CH2O	HO2		-12.37	7.6	-3.527	[82,83]
138.	CH3O	CO		=	CH3	CO2		2.67	3.16	5.38	[84]
139.	CH3O	CH2O		=	CH3OH	HCO		11.01	0.0	2.98	[4]

140.	CH3O	H	=	CH2O	H2	13.3	0.0	0.0	[4]
141.	CH3O	OH	=	CH2O	H2O	13.26	0.0	0.0	[4]
142.	CH3O	O	=	CH2O	OH	13.18	0.0	0.0	[25]
143.	CH3O	HO2	=	CH2O	H2O2	13.08	0.0	0.0	(h)
144.	CH2OH		(M) =	CH2O	H	(M) 14.8	0.0	29.6	[85,l]
145.	CH2OH	O2	=	CH2O	HO2	(M) 14.34	0.0	4.71	[86]
146.	CH2OH	H	=	CH2O	H2	13.48	0.0	0.0	[4]
147.	CH2OH	OH	=	CH2O	H2O	13.38	0.0	0.0	[87]
148.	CH2OH	O	=	CH2O	OH	13.7	0.0	0.0	[87]
149.	CH2OH	HO2	=	CH2O	H2O2	13.08	0.0	0.0	[87]
150.	CH4	OH	=	CH3	H2O	6.622	2.0	2.547	[56]
151.	CH4	H	=	CH3	H2	4.984	2.57	6.637	[88]
152.	CH4	O	=	CH3	OH	8.84	1.56	8.485	[25]
153.	CH4	HO2	=	CH3	H2O2	13.05	0.0	24.64	[89]
154.	CH4		(M') =	CH3	H	(M') 16.38	0.0	104.9	[90,a]
155.	CH3	O	=	CH2O	H	13.9	0.0	0.0	(h)
156.	CH3	HO2	=	CH4	O2	12.43	0.0	0.0	[l]
157.	CH3	HO2	=	CH3O	OH	13.0	0.0	0.0	[l]
158.	CH3	O2	=	CH3O	O	18.3	-1.57	29.23	[4]
159.	CH3	O2	=	CH2O	OH	11.4	0.0	14.64	(m)
160.	CH3	OH	=	CH2(S)	H2O	13.6	0.0	2.50	[91]
161.	CH3	OH	=	CH2O	H2	12.503	-0.53	10.81	[92]
162.	CH3	OH	=	CH3O	H	12.759	-0.23	13.931	[92]
163.	CH3	OH	=	CH2OH	H	19.422	-1.8	8.068	[92]
164.	CH3	OH	=	CH2	H2O	6.875	2.0	5.0	[26]
165.	CH3	HCO	=	CH4	CO	14.08	0.0	0.0	[4]
166.	CH3	CH3	=	C2H5	H	-6.42	4.838	7.71	[53,c]
167.	CH3	CH3	=	C2H4	H2	14.0	0.0	32.0	[93]
168.	CH3	H	=	CH2	H2	13.85	0.0	15.1	[26]
169.	CH3		M =	CH2	H	M 16.3	0.0	91.6	[25]
170.	CH2	O	=	CO	H	H 13.70	0.0	0.0	[26]
171.	CH2	O	=	CO	H2	13.48	0.0	0.0	[26]
172.	CH2	O	=	CH	OH	13.70	0.0	12.0	[94]
173.	CH2	O2	=	CO	H2O	14.377	-1.0	0.0	[95,l]
174.	CH2	O2	=	CO2	H2	14.252	-1.0	0.0	[95,l]
175.	CH2	O2	=	CH2O	O	13.775	-1.0	0.0	[95,l]
176.	CH2	O2	=	CO2	H	H 13.775	-1.0	0.0	[95,l]
177.	CH2	O2	=	CO	OH	H 13.775	-1.0	0.0	[95,l]
178.	CH2	OH	=	CH	H2O	7.053	2.0	3.0	[26]
179.	CH2	OH	=	CH2O	H	13.48	0.0	0.0	[4]
180.	CH2	H	=	CH	H2	26.6	-4.0	3.46	(n)
181.	CH2(S)	N2	=	CH2	N2	12.825	0.0	0.0	[4]
182.	CH2(S)	AR	=	CH2	AR	12.54	0.0	0.0	[4]
183.	CH2(S)	O2	=	CO	OH	H 13.3	0.0	0.0	[4,h]
184.	CH2(S)	O2	=	CO2	H	H 13.0	0.0	0.0	[4,h]
185.	CH2(S)	O	=	CO	H	H 13.178	0.0	0.0	[4]
186.	CH2(S)	O	=	CO	H2	13.178	0.0	0.0	[4]
187.	CH2(S)	H	=	CH2	H	14.3	0.0	0.0	[26]
188.	CH2(S)	H2O	=	CH2	H2O	13.6	0.0	0.0	[4]
189.	CH2(S)	CO2	=	CH2O	CO	12.48	0.0	0.0	[4]
190.	CH2(S)	H2	=	CH3	H	13.86	0.0	0.0	[4]
191.	CH	O	=	CO	H	13.78	0.0	0.0	[76]
192.	CH	O2	=	HCO	O	13.52	0.0	0.0	[25]
193.	CH	CO2	=	HCO	CO	12.53	0.0	0.69	[96]
194.	CH	H2O	=	CH2O	H	12.756	0.0	-0.755	[97]
195.	CH	OH	=	HCO	H	13.7	0.0	0.0	[94]
196.	CH	CH2O	=	CH2CO	H	13.975	0.0	-0.515	[97]
197.	CH3OH	OH	=	CH3O	H2O	4.52	2.53	0.96	[87]
198.	CH3OH	OH	=	CH2OH	H2O	4.52	2.53	0.96	[87]

199.	CH3OH	H	=	CH2OH	H2	8.505	1.49	4.25	[98]
200.	CH3OH	H	=	CH3O	H2	6.623	2.11	4.868	[87]
201.	CH3OH	O	=	CH2OH	OH	5.589	2.5	3.08	[87]
202.	CH3OH	CH3	=	CH2OH	CH4	1.5	3.17	7.17	[87]
203.	CH3OH	CH3	=	CH3O	CH4	1.16	3.1	6.93	[87]
204.	CH3OH	HO2	=	CH2OH	H2O2	13.6	0.0	19.4	[99]
205.	CH3OH	(M)	=	CH3	OH	16.3	0.0	89.87	[100,f,l]
206.	CH3OH	O2	=	CH2OH	HO2	13.31	0.0	44.91	[87]

No.	Fall- Off Correction Parameters	log A	n	E _A	Ref.
9.	a = 0.47, T*** = 100., T* = 2000., T** = 1.0e10	30.483	-4.63	2.046	[46,4]
29.	a = 0.405, T*** = 1120., T* = 1120., T** = 1.0e10	36.06	-5.246	1.71	[51]
35.	a = 47.61, b = 16182., c = 3371., <ΔE> _{all} = 600 cm ⁻¹	42.84	-6.431	107.2	[53,o]
57.	a = 1., T*** = 1., T* = 786., T** = 3250.	18.6	0.0	1.12	[58]
59.	---	17.42	0.0	79.35	[5]
60.	---	17.42	0.0	96.56	[5]
70.	---	16.95	0.0	49.2	[60]
71.	---	16.41	0.0	38.4	[60]
85.	---	27.73	-3.37	18.88	[25]
93.	---	15.56	0.0	59.27	[5]
99.	---	14.18	0.1	32.67	[27,c]
136.	---	25.37	-2.7	30.6	[4,d,l]
144.	---	14.88	0.0	20.0	[85]
154.	a = 0.638, T*** = 1.0e-10, T* = 3230., T** = 1.0e10	17.66	0.0	90.81	[90]
166.	a = 1.641, b = 4334., c = 2725., <ΔE> _{all} = 600 cm ⁻¹	12.7	0.099	10.6	[53,o]
205.	---	17.3	0.0	68.36	[100]

$$[M^{\#}] = 21.0 [H_2O] + 3.8 [CO_2] + 16.0 [CH_4] + 2.5 [H_2] + 1.9 [CO]$$

$$[M^*] = 16.0 [H_2O] + 3.8 [CO_2] + 16.0 [CH_4] + 2.5 [H_2] + 1.9 [CO]$$

$$[M^{**}] = 10.0 [H_2O] + 2.0 [O_2] + 2.0 [N_2] + 2.0 [H_2]$$

† All pressure corrected reactions have the high pressure rate expression listed in the full mechanism. The low pressure rate expression is listed below along with its associated fall - off correction parameters.

(a) Fall - off reaction in the Troe form:

$$F_{cent} = (1 - a) \exp(-T / T^{***}) + a \exp(-T / T^*) + \exp(-T^{**} / T)$$

(b) Fitted expression based on Ref. [101-108]

(c) Fall - off reaction in the SRI form: $F^{sc} = a \exp(-b / T) + \exp(-T / c)$

(d) Adjusted

(e) See Text

(f) Fall - off reaction in the Lindemann - Hinshelwood form.

(g) QRRK calculated rate expression at one atmosphere, M = N₂.

(h) Estimate

(i) Estimate based on CH₃CHO + X (X = OH, O, HO₂, CH₃) reaction.

(j) The pre-exponential frequency factor is estimated by analogy to CH₂O + O₂ reaction. Activation energy based on CHOCHO/O₂/N₂ study of Ref. [109].

(k) Fitted expression based on Ref. [110 - 116].

(l) This Study [23].

(m) Fitted expression based on Ref. [117 - 119]

(n) Fitted expression based on Ref. [96, 120 - 122].

(o) Used Troe relation [123], $\beta_c / (1 - \beta_c^{0.5}) = -\langle \Delta E \rangle_{all} / F E k_B T$, to obtain β_c from $\langle \Delta E \rangle_{all}$.

Transition state frequencies obtained from [53]. Fitted expressions at one atmosphere are $k_{35} = 10^{51.319} T^{-10.60} \exp(-115.575 \text{ kcal}/RT) \text{ sec}^{-1}$ and

$k_{166} = 10^{14.919} T^{-0.50} \exp(-13.045 \text{ kcal/mol}) \text{ cm}^3/\text{mol-sec}$ with M_s = N₂.

Table 3
Thermodynamic Properties
at 1 Atmosphere Standard State

Species	DH _f (298K) (kcal/mol)	S°(298K) (cal/mol)	C _p (T) Calculation
HO2	3.8 [124]	54.7 [21]	Kee et al. [21]
C2H4O2H CH2CH2OOH	7.3 [55]	77.5 [55]	Bozzelli/Dean [55]
C2H4O	-12.6 [22]	58.0 [22]	Burcat [22]
C2H3O [125] ^b	36.0	59.8	THERM: Primary CH bond option applied to C2H4O (Ethylene oxide) parent: BDE = 100.6kcal/mol
C2H3	70.4 [34]	55.5 [21]	Kee et al. [21]
CHOCHO	-50.7 [126]	66.5 [29]	2 - CO(H)(C) ^a , 1-OI Int. Rot. , [127,128]
CHOCO	-16.8	68.9	Parent: C H O C H O BD group CCJ*O [125] ^b
CH2 (S)	103.9 [85]	45.08 [21]	Kee et al. [21]
All other species	Chemkin Thermodynamic Database [21]		

^aAssumed CO(H)(C)=CO(H)(CO) for C_p(T) calculation ; ^bEstimate ; BD = Bond Dissociation ; OI = Optical Isomer, Int. Rot. = Internal Rotation , rd = radical

Chemical kinetic modeling analysis favors the use of the Tully kinetic rate expression over the recent study by Bott and Cohen [129] for this reaction. The non-Arrhenius kinetic expression of Atkinson [56] was used in this study and is based on the experimental results of Tully [17] and Smith [130].

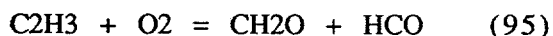
The O-atom reaction with ethylene produces the most prevalent organic intermediates as determined by this study. The Thornton measurements for formaldehyde, methane and methanol exhibited about 1% maximum yield from the initial ethylene concentration in the 1153 to 1203K temperature range. Eventhough formaldehyde is primarily formed from the vinyl reaction with O₂, the C₂H₄ + O-atom reaction does lead to formaldehyde production via methyl radical oxidation. Methane and methanol are formed from the methyl radical produced from C₂H₄ + O-atom.

The kinetic rate expression used in this study for the reaction $\text{C}_2\text{H}_4 + \text{O} \rightarrow \text{Products}$ was taken from Klemm et al. [57]. Their results are represented by an Arrhenius expression for the 1052 - 2000K temperature range. This study used the product channels for the $\text{C}_2\text{H}_4 + \text{O}$ reaction as suggested by Dagaut et al. [16] and are represented by equations (51) and (52). This study applied a branching ratio value of $k_{51}/k_{52} = 2.3$ to the two product channels in accord with Schmoltner et al. [131].

The H-atom abstraction reaction by H-atom, $\text{C}_2\text{H}_4 + \text{H} = \text{C}_2\text{H}_3 + \text{H}_2$ (53), consumes only a small fraction of the ethylene, though it is one of the primary hydrocarbon reactions for the formation of H_2 . The rate expression used was based on the fitted expression of Westbrook et al. [9].

Vinyl Radical Kinetics:

The kinetics of the $\text{C}_2\text{H}_3 + \text{O}_2$ reactions were initially taken from the theoretical analysis work of Westmoreland. Westmoreland [30] proposed that the reaction structure of vinyl and O_2 undergoes multiple isomerizations of chemically activated isomers resulting in several reaction paths and thermal products. The resulting major product channels from the Westmoreland Bimolecular Quantum-RRK study are the reactions shown below for the 300-2000K temperature range.



This study has examined these product channels and their influence on the combustion intermediates. Formaldehyde is the primary intermediate produced by way of Baldwin and Walkers' [40] proposed mechanism of C_2H_3 and O_2 addition, cyclization and beta-scissions to

make CH₂O and HCO. This reaction channel has the lowest energy barrier to products and subsequently it is favored over internal H-atom abstraction followed by decomposition to C₂H₂ plus HO₂ and the channel leading to CHOCHO and H-atom. The association reaction, C₂H₃ + O₂ = C₂H₃O₂, reverts back to reactants for the conditions examined in this study and is not a major vinyl consuming route.

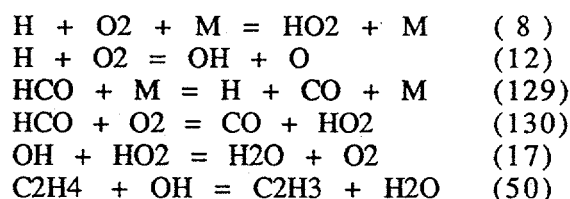
The rate expressions for the major vinyl radical plus molecular oxygen reaction channels were calculated by Westmoreland with a vinyl radical heat of formation value of 70.4 kcal/mol. The Westmoreland C₂H₃ + O₂ product sets, rate expressions and the C₂H₃ heat of formation value were implemented into the model.

The Rao and Skinner rate expression [27] for vinyl decomposition to acetylene plus H-atom was pressure corrected using the high pressure rate expression for the reverse reaction by Organ (as cited by Mackie [132]) and the thermodynamic equilibrium rate based on the 70.4 kcal/mol vinyl radical heat of formation value. Pressure correction was performed by using the Lindemann-Hinshelwood method.

Modeling efforts with the Westmoreland C₂H₃ + O₂ products and rate expressions proved to be unsuccessful. The ethylene consumption and CH₄, CH₃OH, C₂H₆, CO and CO₂ profiles were well underpredicted. The CH₂O and H₂ profiles were well predicted and acetylene profile showed a five fold overprediction for all temperatures. The acetylene predicted profile was very sensitive to the rate constant choice for C₂H₃ + O₂ = C₂H₂ + HO₂ and the pronounced nature of fall-off for the C₂H₃ + O₂ = CH₂O + HCO reaction, while insensitive to vinyl decomposition. A factor of four reduction to the Westmoreland rate expression for the C₂H₃ + O₂ = C₂H₂ + HO₂ product channel was tried while keeping all other reactions fixed and acetylene predictions improved to within a factor two for the temperature range studied. If the Westmoreland fall-off correction to C₂H₃ + O₂ = CH₂O + HCO was not taken into consideration, e.g. chemical kinetic modeling were to implement the Slagle et al. measured rate expression of $4.0 \times 10^{12} \exp(125/T) \text{ cm}^3/\text{mol-sec}$ for the

$C_2H_3 + O_2 = CH_2O + HCO$ reaction, then a rate constant value of approximately $1.25 \times 10^{11} \text{ cm}^3/\text{mol-sec}$ for $C_2H_3 + O_2 = C_2H_2 + HO_2$ would be required for accurate acetylene profiling. This latter value concurs with the Tsang and Hampson recommendation and agrees to within a factor of two with the Westmoreland predicted rate expression. Thus, if matching the recommendation of Tsang/Hampson or Westmoreland for the $C_2H_3 + O_2 = C_2H_2 + HO_2$ reaction is considered desirable then chemical kinetic modeling analysis indicates that fall-off for the overall $C_2H_3 + O_2 \rightarrow \text{Products}$ reaction should be less pronounced than indicated by Westmoreland.

Careful chemical kinetic rate adjustment was then made to those reactions exhibiting rate controlling behavior as determined from reaction-pathway analysis or show significant sensitivity to the ethylene oxidation calculations as determined from the sensitivity analysis. These adjustments were performed while retaining the Westmoreland $C_2H_3 + O_2$ product channels and rate expressions in the chemical kinetic model. The reactions listed below had its respective rate expression altered for the purpose of achieving reasonable agreement with the Thornton data set.



No satisfactory result was achieved in adjusting these rate expressions. The typical problem encountered was poor profiling of the ethylene, CO, CO₂ and the aggregate concentration of methane plus methanol for the full temperature range. Also, simultaneous agreement with the ethylene data set of Thornton and for the methane and ethane data sets of Dagaut to within a factor of two for all measured species could not be achieved by careful chemical kinetic rate adjustments of the aforementioned reactions in the presently compiled model.

Chemical kinetic rate adjustment consideration was then applied to $C_2H_3 (+M) = C_2H_2 + H (+M)$. The vinyl decomposition reaction rate adjustment to the levels prescribed in the WP and DCB reaction sets allowed good agreement to be achieved against the Thornton data set for all measured species but acetylene at temperatures less than 1200K. No agreement could be achieved for temperatures in excess of 1200K. Furthermore, simultaneous modeling of the Dagaut methane and ethane data sets showed reasonable agreement with the measured profiles for the parent hydrocarbon, the intermediates and by-product CO_2 formed. Computer modeling studies determined that altering the vinyl decomposition or oxidation kinetic rates does not have a significant impact on the methane and ethane oxidation kinetics.

If a high vinyl decomposition chemical kinetic rate, on the order of the DCB prescribed rate, is considered acceptable then a reevaluation of the vinyl decomposition process is in order. The high production rate of acetylene resulting from the vinyl decomposition pathway would rule out the $C_2H_3 + O_2 \rightarrow C_2H_2 + HO_2$ as a contributing route to acetylene production for the conditions of this study. The alternative consideration of implementing the revised KWKW vinyl decomposition kinetic rate expression lowers the acetylene and H-atom production rate. The vinyl radical then becomes exclusively consumed by O_2 , and the production loss of H-atom (from $C_2H_3 \rightarrow C_2H_2 + H$) seriously compromises any modeling agreement with the Thornton data set.

This study increased the chemical kinetic rate to $C_2H_3 + O_2 \rightarrow CHOCHO + H$ than previously prescribed by Westmoreland . No reasonable agreement could be achieved toward obtaining an adequate match to the Thornton data set based on this adjusted reaction rate. The kinetic rate limitations imposed by the Gutman et al. experimental studies involving the reaction $C_2H_3 + O_2 \rightarrow$ Products hampered the extent of rate enhancement to this reaction.

Modeling efforts indicate that the $C_2H_3 + O_2$ product channel must produce a reactive free radical in order to attain agreement with the

Thornton data set. Bozzelli and Dean [30], using the Bimolecular-QuantumRRK treatment to the $C_2H_3 + O_2$ reaction, suggested a potential vinyl oxidation sequence of O_2 addition to the vinyl followed by an O-atom splitting off



or simply,



They believe that the vinoxy and O-atom product channel is enhanced by the resonance stabilization of the vinoxy which makes this channel more accessible than the analogous channel (ethoxy plus O-atom) in the ethyl plus O_2 reaction system. Their analysis of the $C_2H_3 + O_2$ reaction favors the vinoxy and O-atom product channel for temperatures greater than 900K. This study initially used the Bimolecular-QRRK predicted $C_2H_3 + O_2 = CH_2CHO + O$ rate expression of $1.191E14 T^{-0.611} \exp(-2646/T)$ $cm^3/mol\text{-}sec$ [67] based on the arguments presented by Bozzelli and Dean for the viability of this reaction. This kinetic rate was subsequently adjusted upward to $7.0E14 T^{-0.611} \exp(-2646/T)$ $cm^3/mol\text{-}sec$ for complete agreement with the Thornton measured speciation profiles. This rate expression differs by more than two orders of magnitude higher than the Westmoreland prediction [30] and lies a factor of three lower than the Bozzelli and Dean prediction [31] for the conditions of this study.

An explanation for the large difference between the Westmoreland and the Bozzelli/Dean predictions for the vinoxy and O-atom product channel lies in the suitable choice for the high pressure pre-exponential frequency factor, $A_{\infty, fwd}$, and activation energy barrier, $E_{act, \infty, fwd}$, for the reaction $C_2H_3OO \cdot \rightarrow \cdot CH_2CHO + O$. Westmoreland assumed a tight transition state structure for the O-atom addition to the oxygen of the $C=O$ bond in $\cdot CH_2CHO$. He calculated a $A_{\infty, rev}$ of $2 \times 10^{10} cm^3 mol^{-1} sec^{-1}$ with microscopic reversibility yielding $A_{\infty, fwd} = 2.1 \times 10^{12} cm^3 mol^{-1} sec^{-1}$. Bozzelli and Dean used the analogy of O-atom

addition to ethylene to obtain the reverse A-factor for O-atom addition to the oxygen of the carbonyl bond in CH_2CHO . Their analogy yielded a $A_{\infty,\text{rev}}$ value of $7.8 \times 10^{12} \text{ cm}^3 \text{ mol}^{-1} \text{ sec}^{-1}$ with microscopic reversibility yielding $A_{\infty,\text{fwd}} = 3.3 \times 10^{14} \text{ cm}^3 \text{ mol}^{-1} \text{ sec}^{-1}$. The three orders of magnitude difference (at this study's conditions) between the Westmoreland and Bozzelli/Dean QRRK predicted kinetics for $\text{C}_2\text{H}_3 + \text{O}_2 = \text{CH}_2\text{CHO} + \text{O}$ is primarily due to the $A_{\infty,\text{rev}}$ determination. The large difference in $A_{\infty,\text{fwd}}$ (or $A_{\infty,\text{rev}}$) indicates a problem of interpreting the structure of the chemically activated and resonantly stabilized 2-oxo-ethyl - O atom/ethenyloxy - O atom ($\text{C}_2\text{H}_3\text{O}-\text{O}$) complex. There is also a ~ 8.0 kcal/mol energy barrier difference between the two studies regarding the choice of the $E_{\text{act},\infty,\text{fwd}}$ for the $\text{C}_2\text{H}_3\text{OO} \rightarrow \text{CH}_2\text{CHO} + \text{O}$ reaction or $E_{\text{act},\infty,\text{rev}}$ for the addition of O-atom to the oxygen of the carbonyl bond in CH_2CHO . This energy barrier difference accounts for the remaining disagreement in the predicted kinetics for $\text{C}_2\text{H}_3 + \text{O}_2 = \text{CH}_2\text{CHO} + \text{O}$ between Westmoreland and Bozzelli/Dean. The difference in barrier heights between the two studies is critical for the predicted $\text{C}_2\text{H}_3 + \text{O}_2 = \text{CH}_2\text{CHO} + \text{O}$ kinetics at low temperatures, whereupon we refer the reader to Bozzelli/Dean's work. The most important difference that can be concluded for high temperature combustion is the choice of the high pressure A-factor for the $\text{C}_2\text{H}_3\text{OO} \leftrightarrow \text{CH}_2\text{CHO} + \text{O}$ reaction.

Modeling efforts readily support the $\text{C}_2\text{H}_3 + \text{O}_2$ channel leading to $\text{CH}_2\text{CHO} + \text{O}$ -atom as an extremely important reaction in the ethylene oxidation process. This result indicates that the Bozzelli/Dean interpretation of the $\text{C}_2\text{H}_3 + \text{O}_2 = \text{CH}_2\text{CHO} + \text{O}$ reaction proceeding through a looser transition state than perceived by Westmoreland is correct as determined by this modeling study. The $\text{C}_2\text{H}_3 + \text{O}_2 = \text{CH}_2\text{CHO} + \text{O}$ -atom reaction followed by $\text{CH}_2\text{CHO} = \text{CH}_2\text{CO} + \text{H}$ is a very potent chain branching process involved in ethylene oxidation. The additional O-atom source other than from $\text{H} + \text{O}_2 = \text{OH} + \text{O}$ allows for rapid ethylene oxidation by O-atom. The reactive H-atom produced from vinoxy decomposition and from $\text{C}_2\text{H}_4 + \text{O}$ -atom reactions can also further the oxidation of the ethylene. The subsequent $\text{C}_2\text{H}_4 + \text{O}$ -atom reactions have

the ability to produce methyl radical which eventually forms methane, methanol, and ethane. Figures 4 and 5 illustrate the agreement between the modelled and experimental measurements for the loss of ethylene and the reaction intermediates' formed due to the inclusion of reaction (96).

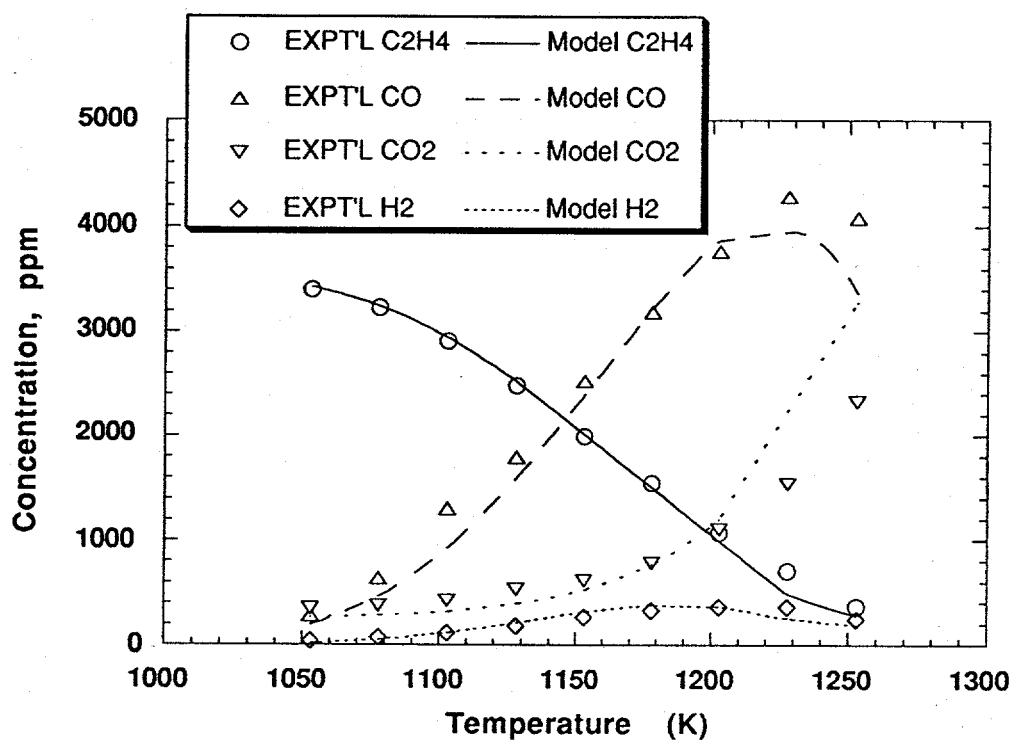


Figure 4: Comparison of predicted and experimental concentration profiles of C2H4, CO, CO2 and H2 in the well-stirred reactor for ethylene oxidation: experimental (open symbols), from Thornton; predicted curves from the compiled ethylene oxidation model.

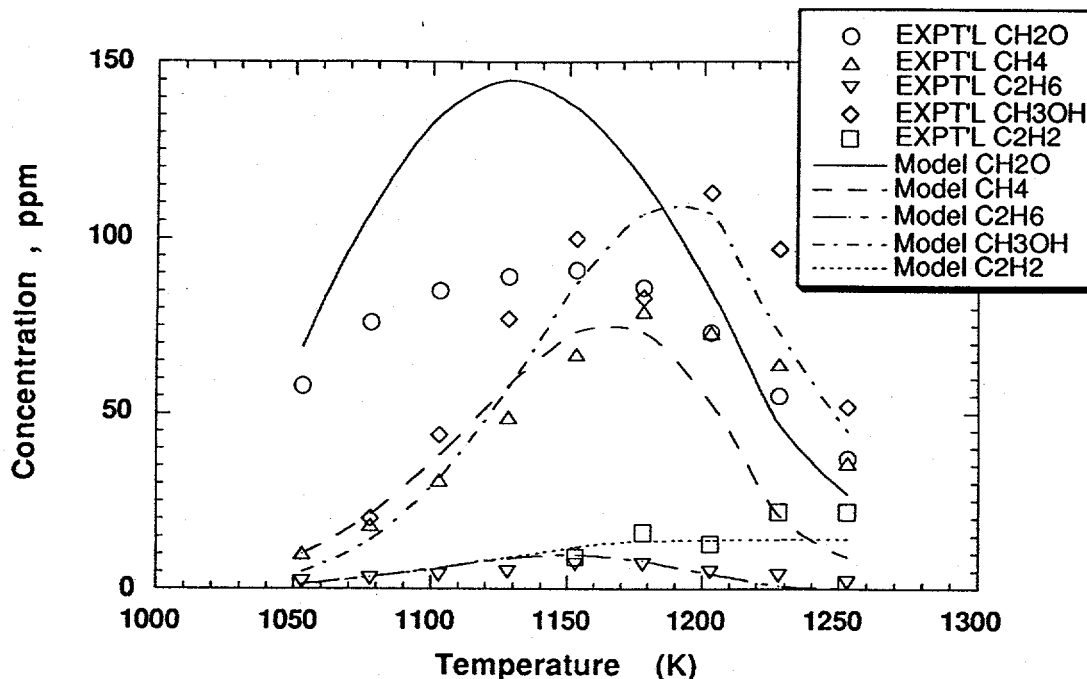


Figure 5: Comparison of predicted and experimental concentration profiles of CH₂O, CH₄, CH₃OH, C₂H₆ and C₂H₂ in the well-stirred reactor for ethylene oxidation: experimental (open symbols), from Thornton; predicted curves from the compiled ethylene oxidation model.

Modeling analysis is indeterminate toward obtaining the proper individual kinetic rates for the various C₂H₃ + O₂ product pathways since vinyl radical is consumed principally by O₂. However, sensitivity to the modeled predictions is strongly exhibited by the branching ratios selected. If the C₂H₃ + O₂ = CH₂O + HCO reaction exhibits fall-off at high temperatures similar to the predicted kinetics of Westmoreland, then the branching ratios for the product sets, CH₂O+HCO : CH₂CHO+O : C₂H₂ + HO₂, are 1.0 : 1.21 : 0.052 at 1053K and 1.0 : 2.47 : 0.080 at 1253K [Table 2 kinetics]. If the Slagle et al. [29] measured kinetic rate were used for the C₂H₃ + O₂ = CH₂O + HCO reaction, hence no fall-off is exhibited for this reaction, then the branching ratios for the aforementioned product sets would be 1.0 : 1.19 : 0.067 at 1053K and 1.0 : 1.63 : 0.068 at 1253K (where the

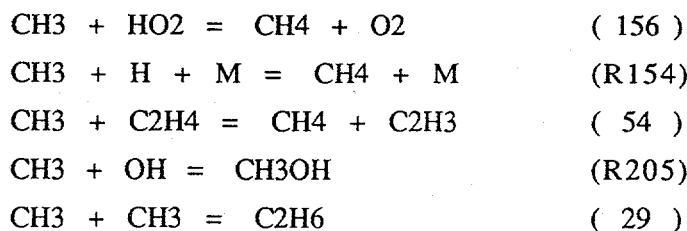
kinetic rate of $C_2H_3 + O_2 \rightarrow CH_2CHO + O$ would be $4.62E15 T^{-0.611} \exp(-2646/T) \text{ cm}^3/\text{mol-sec}$ and $C_2H_3 + O_2 \rightarrow C_2H_2 + HO_2$ would be $3.00E11 \text{ cm}^3/\text{mol-sec}$. The domination of the $C_2H_3 + O_2 \rightarrow CH_2CHO + O$ pathway is expected to occur around 1000K for one atmosphere pressure.

Remaining Reaction Intermediates Kinetics:

Acetylene primarily reacts with O-atom to form $CH_2 + CO$, reaction (106), and $HCCO + H$, reaction (107). The product channels, rate expression and branching ratio of $K_{106}/K_{107} = 0.7$ involving $C_2H_2 + O \rightarrow$ Products were taken from Michael and Wagner [69]. The product channels and rate expressions for $C_2H_2 + OH \rightarrow$ Products, i.e. reactions (108), (109), (110) and (111), were taken from Miller and Melius [70].

Formaldehyde primarily produced by $C_2H_3 + O_2 \rightarrow CH_2O + HCO$ is consumed by OH, O, H radicals to make HCO. Formyl radicals do not reach large concentrations relative to formaldehyde and are quickly oxidized or decomposed to produce carbon monoxide.

The primary route to methyl radical formation is from O-atom attack on the ethylene. The methyl radical produced is the precursor species to methane, methanol, and ethane formation as observed by Thornton. The reactions leading to methane, methanol and ethane formation are:



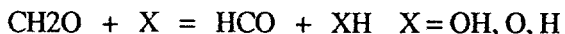
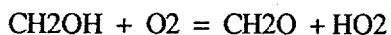
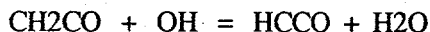
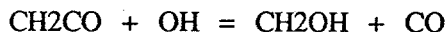
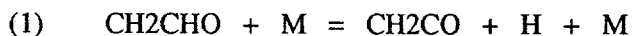
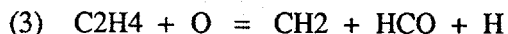
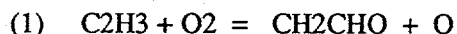
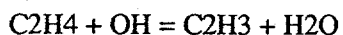
Carbon monoxide is primarily formed from the destruction reactions involving the formyl radical. Carbon monoxide is then principally converted to carbon dioxide by $\text{CO} + \text{OH} \rightarrow \text{CO}_2 + \text{H}$. Carbon dioxide is primarily formed from carbon monoxide oxidization and minor production from $\text{CH}_2 + \text{O}_2 \rightarrow \text{CO}_2 + \text{H}_2$ and $\text{HCCO} + \text{O}_2 \rightarrow \text{CO}_2 + \text{CO} + \text{H}$.

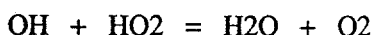
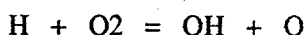
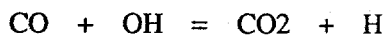
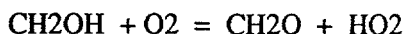
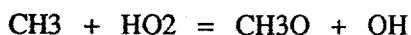
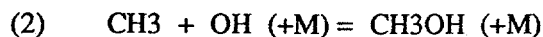
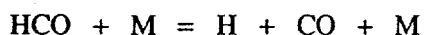
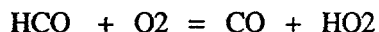
CHEMICAL KINETIC MODEL ANALYSIS AND VALIDATION

The 1050K - 1200K Temperature Range

The computational analysis performed with the compiled ethylene oxidation model supports the earlier conclusion of WP and DCB that for the 1050K - 1200K temperature range the reactor behaves in a well-stirred mode. Furthermore, very good agreement is found between the model's predictions and the experimental measurements for the loss of ethylene and the reaction intermediate concentrations formed as indicated in figures 3 and 4. Reaction pathway analysis was performed at 1153K using the presently compiled model in order to identify the principal and secondary ethylene oxidation pathways.

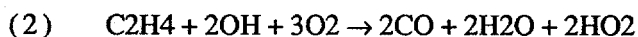
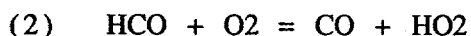
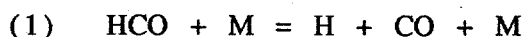
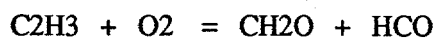
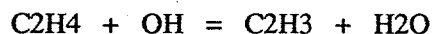
The principal oxidation pathway was determined to be the following:





The $\text{C}_2\text{H}_3 + \text{O}_2 = \text{CH}_2\text{CHO} + \text{O}$ reaction followed by $\text{CH}_2\text{CHO} = \text{CH}_2\text{CO} + \text{H}$ is a very potent chain branching process for ethylene oxidation. This pathway allows for the formation of O-atom, H-atom, and ketene species. It is essential for promoting the O-atom attack on the ethylene in steps (2) and (3) and providing a source of free radicals for the further ethylene consumption. The O-atom formed from step (1) will preferentially react with the ethylene to form methyl and formyl radicals or methylene, formyl radical and H-atom. The methyl radical is principally consumed by reactions involving HO_2 and OH radicals. These reactions are $\text{CH}_3 + \text{HO}_2 = \text{CH}_3\text{O} + \text{OH}$ and $\text{CH}_3 + \text{OH} (+\text{M}) = \text{CH}_3\text{OH} + (+\text{M})$. The methylene primarily reacts with O_2 to form CO_2 , CO , H_2O , and H_2 products. The oxidized ethylene contribution from steps (1 - 3) creates formyl radicals which either decompose to produce H-atoms or oxidize to form HO_2 radicals. The formed H-atom will add to O_2 to make HO_2 radical, but for the experimental conditions of this study, the important HO_2 producing pathway is $\text{HCO} + \text{O}_2 = \text{CO} + \text{HO}_2$. The HO_2 radical is primarily removed by $\text{HO}_2 + \text{HO}_2 = \text{H}_2\text{O}_2 + \text{O}_2$, $\text{HO}_2 + \text{OH} = \text{H}_2\text{O} + \text{O}_2$, and $\text{H} + \text{HO}_2 = \text{OH} + \text{OH}$.

The secondary oxidation pathway was determined to be the following:



The net overall reaction indicates that the secondary oxidation pathway can produce either reactive H-atoms or unreactive HO₂ radicals. The formed H-atoms is primarily consumed by O₂ (25% at 1053K to 52% at 1253K) to make OH and O-atom which futhers ethylene oxidation. The HO₂ radical is not active in consuming ethylene at these conditions and prefers to self react or react with OH and H-atom thereby consuming free radicals and inhibiting ethylene oxidation. The dominance of either the H-atom or HO₂ production pathway is strictly determined by the nature of the formyl radical destruction. For the lower temperatures of this study, formyl radical is primarily removed by step (2). Temperatures greater than 1200K, formyl radical is consumed equally by steps (1) and (2).

Temperatures Greater Than 1200K

The good agreement represented by the ethylene oxidation model predictions against the Thornton measurements in the 1200 - 1250K temperature range differs substantially from the WP and DCB reaction set predictions. The underlying difference in the numerical predictions is due to the kinetics and product pathways involving the vinyl radical and the fundamental role the reaction intermediates play in moderating the OH concentration within the well-stirred reactor.

Previously, Westbrook and Pitz explained the observed disagreement between their computed results and the Thornton measurements in the 1200 - 1250K temperature range as being caused by the presence of turbulent species fluctuations within the reactor and ruled out the possibility that a mechanistic change could explain the Thornton measurements in this temperature regime. This explanation was later supported by the chemical kinetic computational investigation of Dagaut/Cathonnet/Boettner.

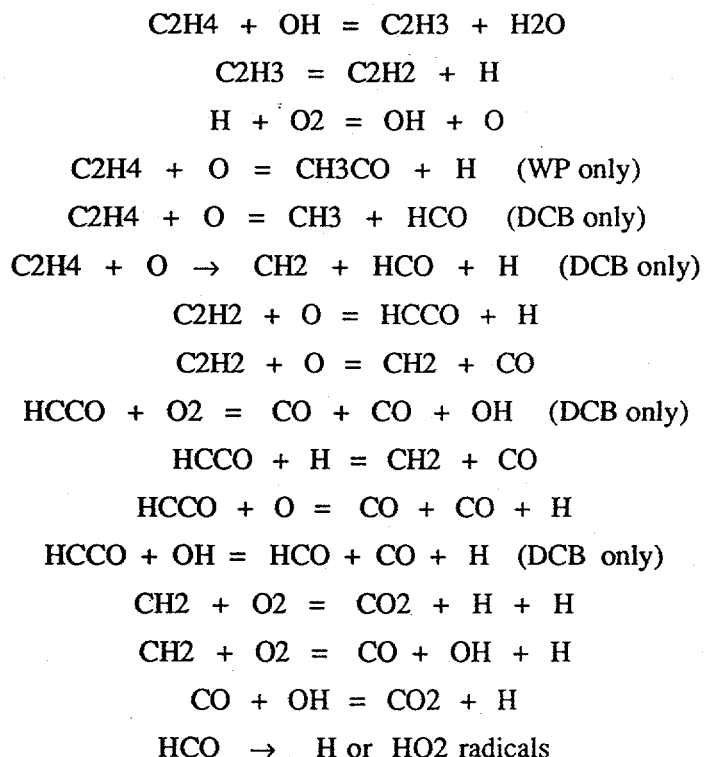
The presently compiled ethylene oxidation model supports the theory that abundant formation of HO₂, CH₂O, CO, and CH₃ competes with C₂H₄ for OH at the highest temperatures of the data set. This results in reaction (50) experiencing a reduced share of OH concentration needed for further ethylene consumption as exhibited in Table 4. The competition for OH at the higher temperatures would explain why significant amounts of ethylene remain and why it is possible to maintain reasonable spatial homogeneity within the reactor for as high as 1253K.

Table 4
Computed OH Normalized Rate of Production
Percent Contribution at 1153K and 1228K

Reaction	1153K	1228K
HO ₂ + OH = H ₂ O + O ₂	21%	27%
H ₂ + OH = H ₂ O + H	2	4
H ₂ O ₂ + OH = HO ₂ + H ₂ O	4	-
CO + OH = CO ₂ + H	4	15
C ₂ H ₄ + OH = C ₂ H ₃ + H ₂ O	23	14
CH ₂ CO + OH = CH ₂ OH + CO	12	8
CH ₂ O + OH = HCO + H ₂ O	23	18
CH ₃ + OH = CH ₃ OH	6	6
CH ₃ OH + OH = CH ₃ O + H ₂ O	-	2
CH ₃ OH + OH = CH ₂ OH + H ₂ O	-	2

This study can not refute the likelihood that poor mixing at the microscale level may exist at temperatures greater than 1200K. However, the WP and DCB poor mixing conclusion is based on their usage of fairly high rates of vinyl dissociation which promotes excessive chain branching at the higher temperatures. In particular, the coupling of acetylene

production and the build-up of O-atom to sufficient concentrations at the high temperature end of the data set unleashes a potent chain branching process. This is exemplified by the following reaction sequence,



which produces a plethora of reactive free radicals that eventually consumes all the ethylene at the higher temperatures of the dataset as indicated earlier by WP and DCB.

In conclusion, the principal difference between this study's ethylene oxidation model and the WP and DCB mechanisms is the importance of vinyl oxidation kinetics, in particular, the $\text{C}_2\text{H}_3 + \text{O}_2 = \text{CH}_2\text{CHO} + \text{O}$ reaction. The resulting reaction sequence from vinyl oxidation allows for rapid chain branching and favors the formation of stable products such as formaldehyde, methane and methanol. Acetylene kinetics does not play a significant role in the ethylene oxidation process as noted in the Thornton data set and supported by the

presently compiled ethylene oxidation mechanism. This finding differs from the proposed ethylene oxidation mechanism of Westbrook/Pitz and Dagaut/Cathonnet/Boettner which favors considerable participation of acetylene kinetics in the ethylene oxidation process.

This study supports the viability of the $C_2H_3 + O_2 = CH_2CHO + O$ reaction. Implementation of this reaction should be considered for future high temperature combustion chemistry modeling studies.

SUMMARY

The reported mechanisms of WP and DCB were used to understand the important features of the ethylene oxidation chemistry. The DCB mechanism showed agreement to the ethylene profile at the lower temperatures of the data set and for an extended temperature range than WP. This was due to the heavy reliance by DCB on the vinyl decomposition to $C_2H_2 + H$ as the predominant vinyl consumption reaction.

The reaction intermediates predicted by the WP and DCB showed limited agreement in temperature range and for certain measured species. In particular, the predicted versus measured acetylene profile showed gross disagreement, and thereby ruling out vinyl dissociation as the prominent vinyl destruction process.

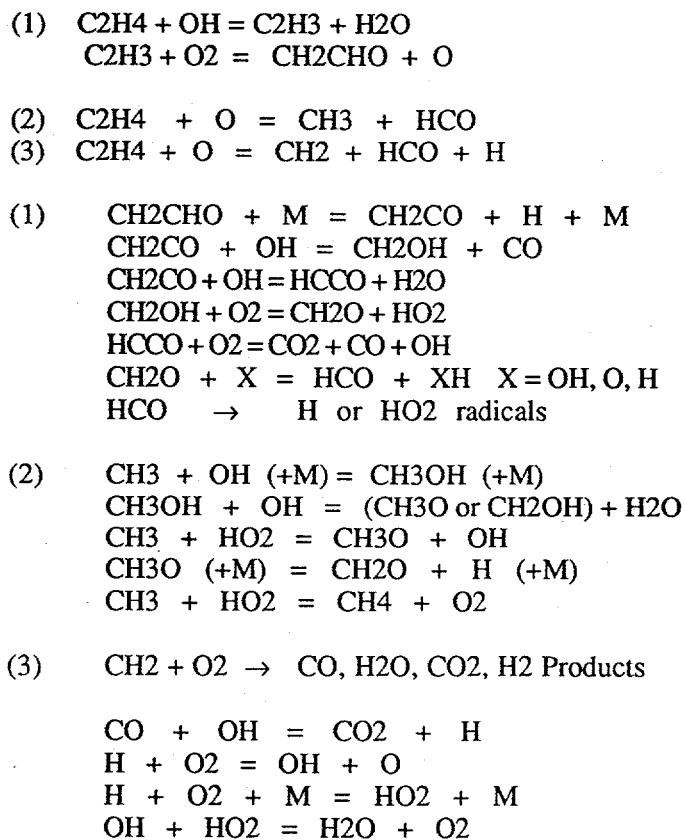
The inadequacies represented by these mechanisms was the motivation for developing the current ethylene oxidation model.

The ethylene oxidation model developed in the present study addressed the issue of whether or not the vinyl oxidation pathway produces a reactive free radical early in the ethylene oxidation process or if careful chemical kinetic rate adjustment must be made to the most sensitive rate controlling reactions in order to obtain agreement with the ethylene oxidation measurements of Thornton.

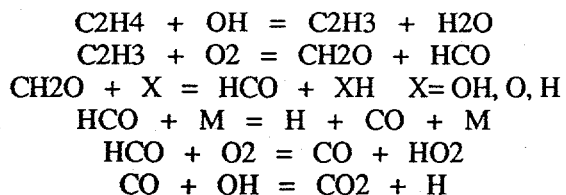
The model made use of the Westmoreland rate parameters for the important product sets involving the $C_2H_3 + O_2$ reaction. The modeling results involving the ethylene and the reaction intermediates formed proved unsuccessful with the Westmoreland $C_2H_3 + O_2$ predictions. Careful chemical kinetic rate adjustment made to the most sensitive rate controlling reactions proved unsuccessful when trying to achieve agreement with the ethylene, methane and ethane oxidation data sets.

The $C_2H_3 + O_2$ pathway to $CH_2CHO + O\text{-atom}$ proved to be a very important reaction in the ethylene oxidative pyrolysis. The very potent chain branching sequence of $C_2H_3 + O_2 \rightarrow CH_2CHO + O\text{-atom}$ followed by $CH_2CHO (+M) \rightarrow CH_2CO + H (+M)$ is needed to accurately model the Thornton ethylene data set.

Reaction pathway analysis was utilized to determine the principal and secondary ethylene oxidation routes. The principal oxidation pathway was determined to be the following:



The secondary oxidation pathway was determined to be the following:



Good agreement between the compiled model's predictions and the experimental measurements were attained for the 1053 to 1253K temperature range. The favorable chemical kinetic modeling results for temperatures greater than 1200K suggested that the rate of mixing was sufficiently rapid to maintain reasonable spatial homogeneity within the reactor for temperatures as high as 1253K.

The $\text{C}_2\text{H}_3 + \text{O}_2$ reaction to form $\text{CH}_2\text{CHO} + \text{O}$ proved to play an integral part in the ethylene oxidation process and should be used in future high temperature combustion chemistry modeling studies.

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