



A Review of Remote Welding and Nondestructive Examination Technologies for the DOE Standard Canister

October 2024

Changing the World's Energy Future

Devin D Imholte, Nilay Atul Kulkarni, Nathan Levine Hofmeister, Samuel Jackson Trost, Cody Michael Bennett



DISCLAIMER

This information was prepared as an account of work sponsored by an agency of the U.S. Government. Neither the U.S. Government nor any agency thereof, nor any of their employees, makes any warranty, expressed or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness, of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. References herein to any specific commercial product, process, or service by trade name, trade mark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the U.S. Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the U.S. Government or any agency thereof.

A Review of Remote Welding and Nondestructive Examination Technologies for the DOE Standard Canister

**Devin D Imholte, Nilay Atul Kulkarni, Nathan Levine Hofmeister, Samuel Jackson
Trost, Cody Michael Bennett**

October 2024

**Idaho National Laboratory
Idaho Falls, Idaho 83415**

<http://www.inl.gov>

**Prepared for the
U.S. Department of Energy
Under DOE Idaho Operations Office
Contract DE-AC07-05ID14517**

1 **A Review of Remote Welding & Non-destructive Examination**
2 **Technologies for the DOE Standard Canister**

3 D. Devin Imholte^{a,*}, Nilay A. Kulkarni^a, Nathan L. Hofmeister^a, Sam J. Trost^a,
4 Cody M. Bennett^a

5 *^aIdaho National Laboratory, 2525 N. Freemont Ave, Idaho Falls, Idaho 83415*

6 **Corresponding author, devin.imholte@inl.gov*

7

8 **A Review of Remote Welding & Non-destructive Examination**
9 **Technologies for the DOE Standard Canister**

10 The U.S. Department of Energy (DOE) manages a wide variety of spent nuclear
11 fuel that poses a unique management challenge. To help address this challenge,
12 the DOE Standard Canister (DOESC)—designed to remain sealed during
13 handling, storage, transportation, and disposal—was conceptualized as a
14 standardized containment vessel to accommodate DOE-managed spent nuclear
15 fuel. Since 1999, several welding and examination processes have yet been
16 independently developed for the DOESC’s closure welds. However, neither the
17 DOESC nor these processes have been realized in an operational capacity. This
18 review paper seeks to present and compare previously developed DOESC
19 closure weld, non-destructive examination, and repair processes and
20 technologies. Specific processes developed for the Idaho Spent Fuel Facility, in
21 preparation for the Yucca Mountain geological repository, and the recent Road-
22 Ready Demonstration Project will be discussed. Specific focus will be given to
23 how different operating constraints and the American Society of Mechanical
24 Engineers Boiler and Pressure Vessel Code drove certain welding and non-
25 destructive examination requirements. Historical DOESC welding and
26 examination strategies will be assessed against current regulatory and Boiler
27 and Pressure Vessel Code requirements. The comparison of welding processes,
28 technologies, and DOESC designs presented in this review paper will inform
29 further construction efforts for other commercial and DOE-managed spent
30 nuclear fuel containments, including the DOESC.

31 Keywords: remote, welding, spent nuclear fuel, non-destructive examination,
32 DOE Standard Canister, storage, transportation, disposal

33 **I. INTRODUCTION**

34 The United States (U.S.) Department of Energy (DOE) Standard Canister (DOESC) was
35 conceptualized as a group of standardized spent nuclear fuel (SNF) containments for DOE-
36 managed SNF (Figure 1)^{1,2}. The DOESC was meant to remain sealed during handling (i.e.,
37 after SNF loading and closure), storage, transportation, and disposal—without the need to

38 repackage its contents.

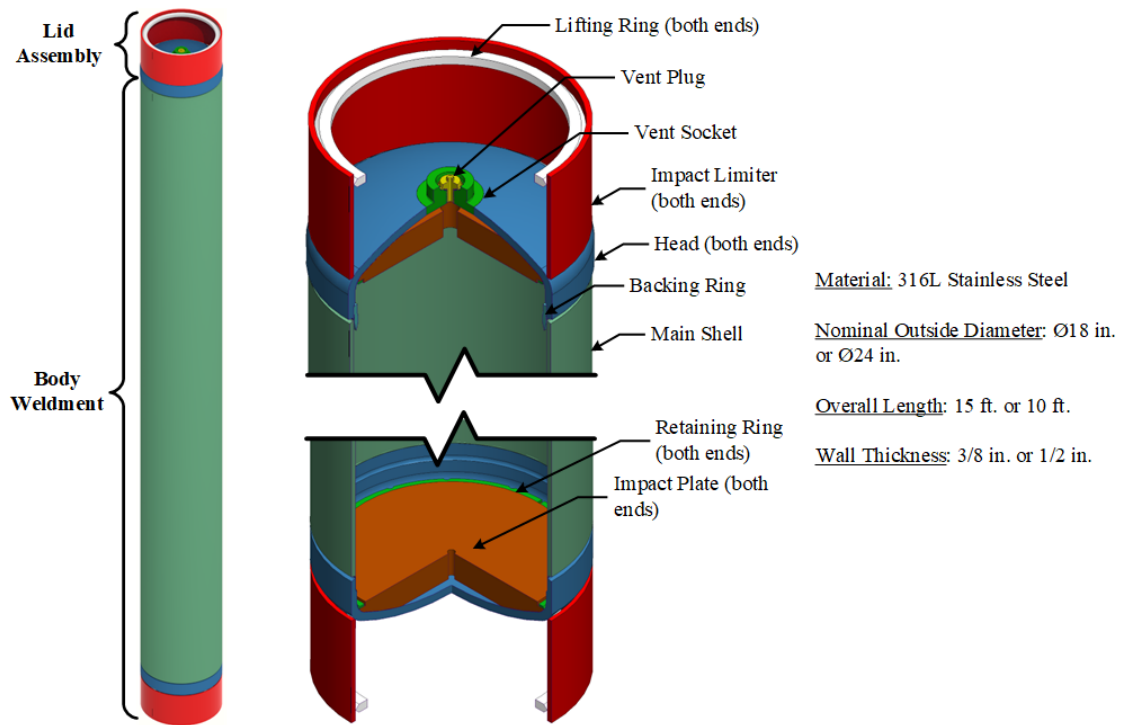
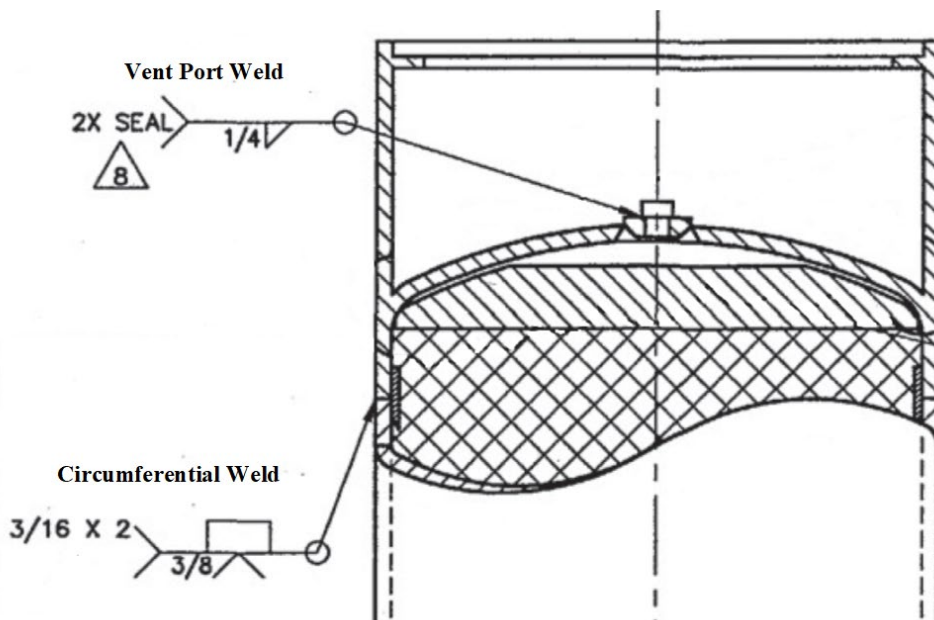


Figure 1: The Department of Energy Standard Canister (DOESC).

39 Similar to commercial SNF storage and transport canisters, the DOESC design includes two
40 closure welds that are performed after the contents are loaded³. These closure welds are
41 referred to as the circumferential weld and the vent port weld (Figure 2).



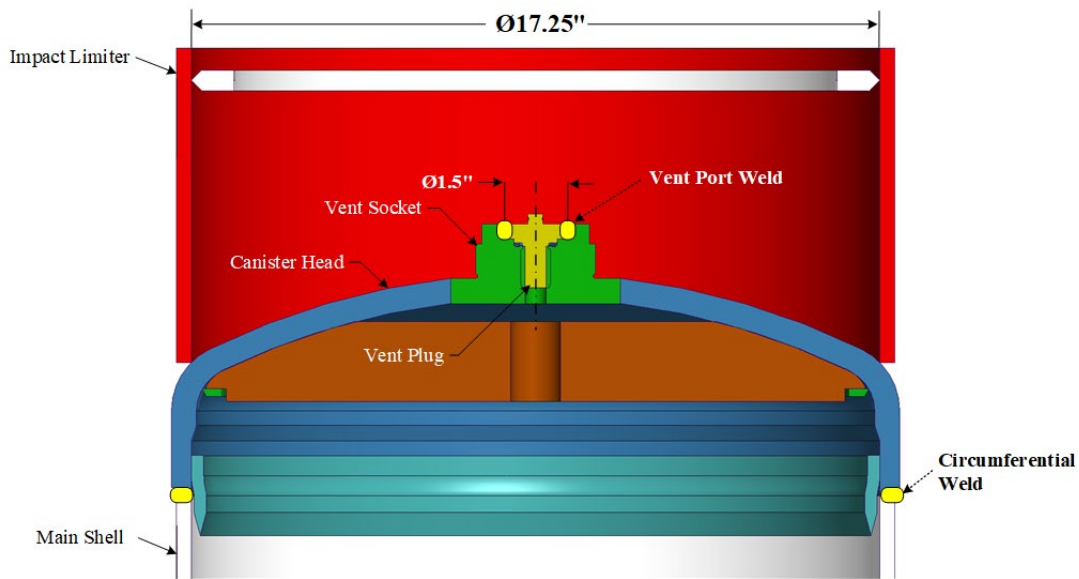


Figure 2: DOESC closure welds from NSNFP 1 design² (top) and RRDP design (bottom).

42 Since the DOESC was originally conceptualized, different welding, repair, and non-
 43 destructive examination (NDE) processes have been developed for the Idaho Spent Fuel
 44 Facility (ISFF), National Spent Nuclear Fuel Program (NSNFP), and recent Road-Ready
 45 Demonstration Project (RRDP)⁴⁻⁶ (Figure 3).

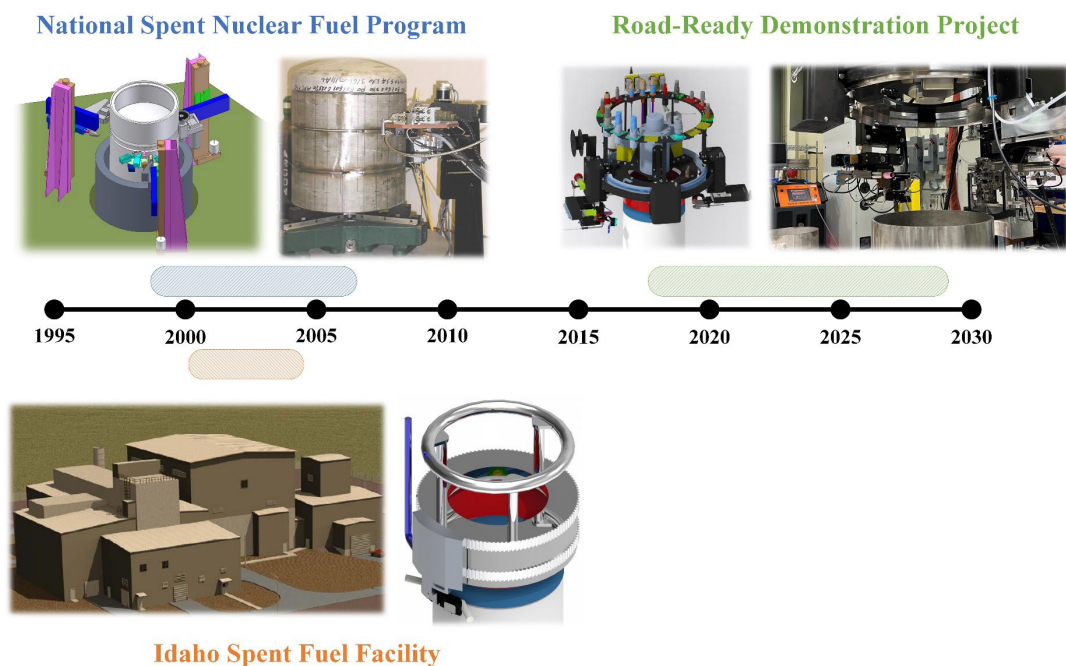


Figure 3: DOESC weld and NDE development timeline^{5, 7}.

46 Although commercial SNF canister construction has been reviewed elsewhere³, the
 47 differences across these DOESC closure weld technologies and processes have not been

48 documented. This review paper will compare these technologies and processes and discuss
49 ongoing challenges to inform further construction efforts for other commercial and DOE-
50 managed SNF containments.

51 Section I will provide a brief background on DOE SNF management, canister fabrication,
52 and the recent efforts to package DOE-managed SNF for road-ready dry storage. Section II
53 will describe the fabrication and inspection technologies for the DOESC used in the ISFF.
54 Section III will review the DOESC canister closure system developed under the NSNFP.
55 Section IV will present the canister closure system developed for the recent RRDP. Section V
56 will compare these different closure weld technologies and discuss relevant design attributes
57 and contemporary challenges. Section VI will conclude with a summary of the work, along
58 with the path forward for DOE SNF canister welding and inspection technologies.

59 *I.A. Background*

60 Throughout the 20th century, the research, development, and commercialization of nuclear
61 energy technology by the U.S. Atomic Energy Commission and DOE lead to the generation
62 of SNF. This so-called ‘DOE-managed SNF’ is different from conventional light water
63 reactor nuclear fuels in the U.S., often having different fuel geometries, fuel materials, and
64 cladding materials⁸. The Idaho National Laboratory (INL) site manages 250+ types of DOE-
65 managed SNF⁹. In pursuit of an integrated and long-term SNF management program for
66 DOE-managed SNF, and for meeting the 1995 Idaho Settlement agreement, the DOE Office
67 of Environmental Management (DOE-EM) created the NSNFP for research, development,
68 and testing of treatment, shipment, and disposal technologies^{10, 11}. One of the first challenges
69 the NSNFP faced was the “aging” of DOE-managed SNF in containers originally designed
70 for interim storage prior to reprocessing—not for shipment to a geological repository.

71 A significant portion of DOE-managed SNF lacked the rigor and pedigree of characterization
72 that is typical of commercial SNF¹². Retroactive characterization of DOE-managed SNF was
73 determined to be unviable¹³. The DOE-managed SNF could therefore not be credited for
74 performing a nuclear safety function. To address this challenge, the NSNFP conceptualized
75 the DOESC as a sealed containment that could be credited for a containment safety function
76 during handling, storage, transportation, and disposal (Figure 1)^{1, 2}.

77 The DOESC was rigorously tested and analyzed, including 30 ft. full-scale drop tests with

78 surrogate fuel assemblies, baskets, and other internals¹⁴. These testing campaigns
79 successfully demonstrated a robust design. However, the DOESC's fabrication and NDE
80 strategy were outside the scope of these drop-testing campaigns. Shortly after these testing
81 campaigns, the welding and NDE processes for the closure welds (Figure 2) were designed
82 and developed for the ISFF (Section II) and NSNFP (Section III)^{4, 5}.

83 There have been many developments in SNF canister welding and examination since the
84 DOESC closure weld systems were developed for the ISFF and NSNFP. Process
85 development efforts have been made by Oak Ridge National Laboratory to carry out remote
86 repair of welds for dry SNF storage systems^{15, 16}. Recent advancements in quality assessment
87 include integrating robust machine learning capabilities for in-situ quality and construction
88 code compliance^{17, 18}. Separate from the DOESC, DOE-EM developed the multi-canister
89 overpack (MCO) as a containment for Hanford's N-reactor SNF. The MCO containment was
90 constructed and certified (i.e., N-stamped) in accordance with the rules of Section III,
91 Division 1 of the American Society of Engineers (ASME) Boiler and Pressure Vessel Code
92 (BPVC), including the first application of BPVC Code Case N-595 for its closure welds. The
93 BPVC is a standardized construction code for pressure vessels, including SNF storage and
94 transportation containments. A Gas Tungsten Arc Welding (GTAW) machine process was
95 used for the MCO closure weld¹⁹. The MCO closure weld examination included liquid dye
96 penetrant examination (PT) of the root, intermediate and cover weld passes. While the
97 DOESC closure process has been developed to different degrees, none have been executed in
98 an operational capacity similar to the MCO.

99 The current DOESC design has a circumferential and vent port closure weld that would be
100 performed after the contents (i.e., SNF, basket(s), and shielding device(s)) are loaded (Figure
101 2). Similar to other SNF containments, these closure welds are primarily performed
102 remotely²⁰. The circumferential weld is performed first, which attaches the Ø18" Schedule
103 40S or Ø24" Schedule 80S pipe to the DOESC head, followed by a vacuum drying process of
104 the DOESC's contents. The vent port weld is performed after backfilling the loaded DOESC
105 with helium. These closure welds are critical to the DOESC's containment safety function.
106 Special attention to the design, fabrication, examination, and failure mechanisms of these
107 closure welds is required to assure adequate performance of this safety function²¹.

108 The first generation of the DOESC design was completed by the NSNFP, which established
109 Section III, Divisions 1 and 3 of the BPVC as the construction code of record for the DOESC

110 (including N-stamping)^{2, 22, 23}. The ASME BPVC contains rules for materials, design,
111 fabrication, examination, and testing of welds of SNF storage and transportation
112 containments, such as the DOESC's closure welds. Under the BPVC, both closure welds
113 required volumetric and surface NDE. For volumetric NDE, ultrasonic examination (UT) was
114 preferred over radiographic examination (RT) due to the possibility of high radiation fields
115 during SNF loading¹. No surface NDE technique was originally specified, although the
116 ASME BPVC only permitted PT²³. The DOESC closure welding, examination, and repair
117 processes have been previously and independently developed, to different degrees, for
118 ISFF²⁴, under the direction of the NSNFP⁵, and most recently, for the INL's RRDP⁶. This
119 paper seeks to comprehensively compare these different DOESC closure welding
120 technologies and processes.

121 ***I.B. DOE SNF Road-Ready Demonstration Project***

122 Given the wide variety of DOE-managed SNF at the INL site, one SNF management concept
123 is to package the DOE-managed SNF at the INL site into dry, sealed canisters, which are then
124 placed in onsite storage for later removal. The canisters and associated packaging are
125 designed to facilitate SNF removal from the intermediate SNF storage facility and allow
126 long-term dry storage before shipment to alternative storage or eventual disposal when an
127 appropriate facility becomes available. This management concept is known as "road-ready
128 dry storage" (RRDS)²⁵. The RRDP is the most recent effort to use DOESCs, which aims to
129 develop and demonstrate the designs, technology, processes, and regulatory framework for
130 packaging DOE-managed SNF into a RRDS system²⁶ (Figure 4).

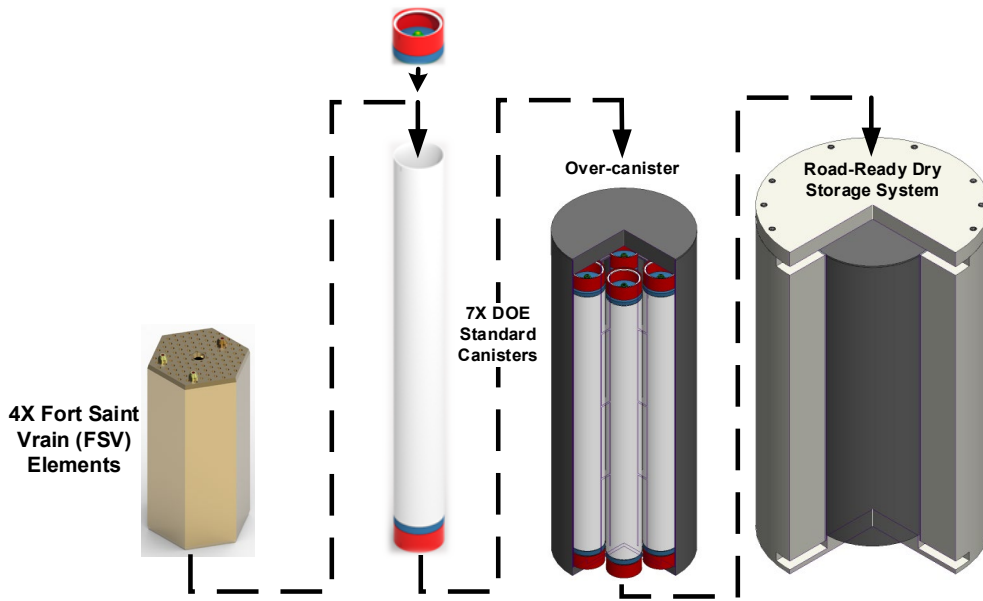


Figure 4: RRDP objectives schematic.

131 The specific type of SNF chosen for the RRDP is Fort Saint Vrain high-temperature gas-
 132 cooled reactor SNF currently stored at the INL’s Idaho Nuclear Engineering Technology and
 133 Engineering Center (INTEC). This SNF will be loaded at INTEC into an Ø18” × 15 ft.
 134 DOESC^{27, 28}. Multiple DOESCs will be loaded into a commercial welded over-canister³ and
 135 transportable overpack for interim storage (Figure 4).

136 The RRDP’s canister closure system, which includes welding and NDE equipment for the
 137 DOESC’s circumferential closure weld, has recently been designed and developed⁶, moving
 138 beyond the previous ISFF and NSNFP efforts. Vent port welding and NDE equipment design
 139 and development is still ongoing.

140 II. IDAHO SPENT FUEL FACILITY’S WELDING AND NDE SYSTEM

141 The ISFF was designed and licensed by the Nuclear Regulatory Commission (NRC) as a dry
 142 SNF interim storage facility at the INL²⁴. Although never realized as an operational facility,
 143 the ISFF was intended to repackage DOE-managed SNF into DOESCs for interim storage
 144 prior to shipment to a repository. These DOESCs were to be loaded, welded, and inspected
 145 using a combination of automated and manual equipment and techniques.

146 Because construction rules for storage containments had not yet been defined in Division 3 of
 147 the BPVC during design of the ISFF, the ISFF established the DOESC’s code of record as
 148 Section III, Division 1, Subsection NB of the ASME BPVC (1998 ed. With 2001 addenda),

149 with Code Case N-595²⁹. Because Subsection NB is a construction code for nuclear reactor
150 pressure vessels, Code Case N-595 was required to modify requirements typical for reactor
151 pressure vessels, such as replacing the hydrostatic pressure test of the closure welds with a
152 helium leak test. The circumferential weld was classified as a structural weld subject to the
153 ASME BPVC's fabrication and examination (UT and PT) requirements. The vent port weld
154 was considered a seal weld and only subject to PT examination.

155 Each closure weld would have been performed via a manual or automated GTAW process.
156 The circumferential weld was a full penetration butt weld formed by a single j-groove, while
157 the vent port weld was an autogenous (i.e., a weld without filler) single pass weld³⁰. The
158 circumferential weld and vent port weld would be performed manually using a standard hand
159 torch if the automated techniques were unable to perform the welds, or if repairs had to be
160 made. Nominally, the circumferential weld was performed using a commercial orbital weld
161 head equipped with a water-cooled 300A torch, remote-controlled wire feed nozzle
162 manipulators, and live video feed of the weld zone^{4,31} (Figure 5). The wire feed manipulator
163 mechanism would adjust the weld wire height relative to the electrode, moving the wire
164 across the weld seam, and adjusting the wire's entry angle. The vent port weld was performed
165 using a commercial orbital tube welder designed for joining tubes to tubesheet in high
166 production applications⁴ (Figure 5).

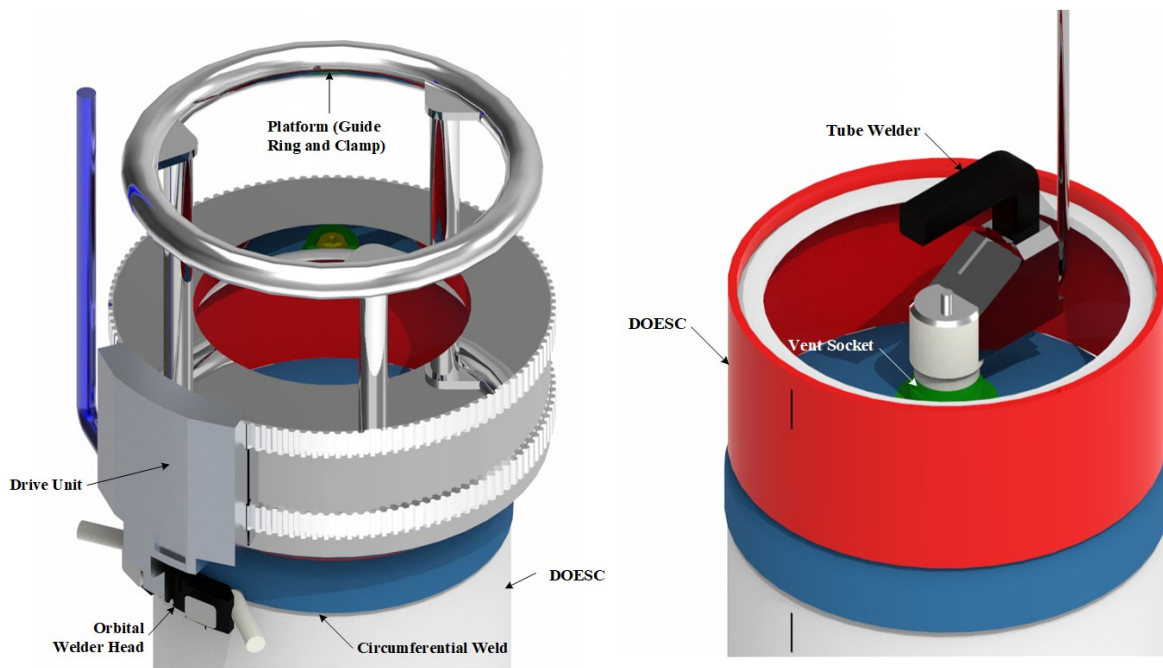


Figure 5: ISF circumferential orbital welder (left) and vent port tube welder (right). Adapted from³¹.

167 This tube welder was equipped with a 150 Amps-DC torch, completely enclosed purge

168 chamber, and pneumatic mandrel. The pneumatic mandrel engaged a centerhole drilled
169 within the DOESC's vent plug. The tube welder then performed a single pass autogenous
170 weld to join the vent plug to the vent socket.

171 PT of both the circumferential and vent port welds was performed manually using standard
172 equipment (e.g., light meter, penetrant and developer sprays, cleaning materials). UT was
173 performed for the circumferential weld either manually or with the drive unit from the orbital
174 welder.

175 There is little information available on the development of the ISFF welding and examination
176 processes for the DOESC. Development testing was planned for the UT equipment, with
177 particular attention given to the distinct UT response from where the DOESC pipe's
178 longitudinal seam weld intersects the circumferential weld.

179 The concept of the ISFF utilized commercial hardware, which likely would have been
180 developed had the ISFF been constructed and operated. The phased array UT sensors,
181 scanning technique, defect repair, or couplant recovery, were not designed in detail.

182 **III. NATIONAL SPENT NUCLEAR FUEL PROGRAM'S CANISTER** 183 **CLOSURE SYSTEM**

184 After the ISFF received its NRC license, researchers from INL completed the detailed design
185 and development of a canister closure system for remote and semi-automated welding, NDE
186 (visual, eddy current (ET), and UT), and repair of the DOESC's circumferential weld within
187 a hot cell environment⁵. This canister closure system was not designed to perform, examine,
188 or repair the DOESC's vent port weld. Each of these circumferential weld subsystems were
189 mounted on a rotating carousel that surrounded the DOESC (Figure 6). A stationary shield
190 tube surrounded all but a small portion around the DOESC's circumferential weld. This
191 shield tube provided a barrier for all subsystems to be safely stowed when not in use.

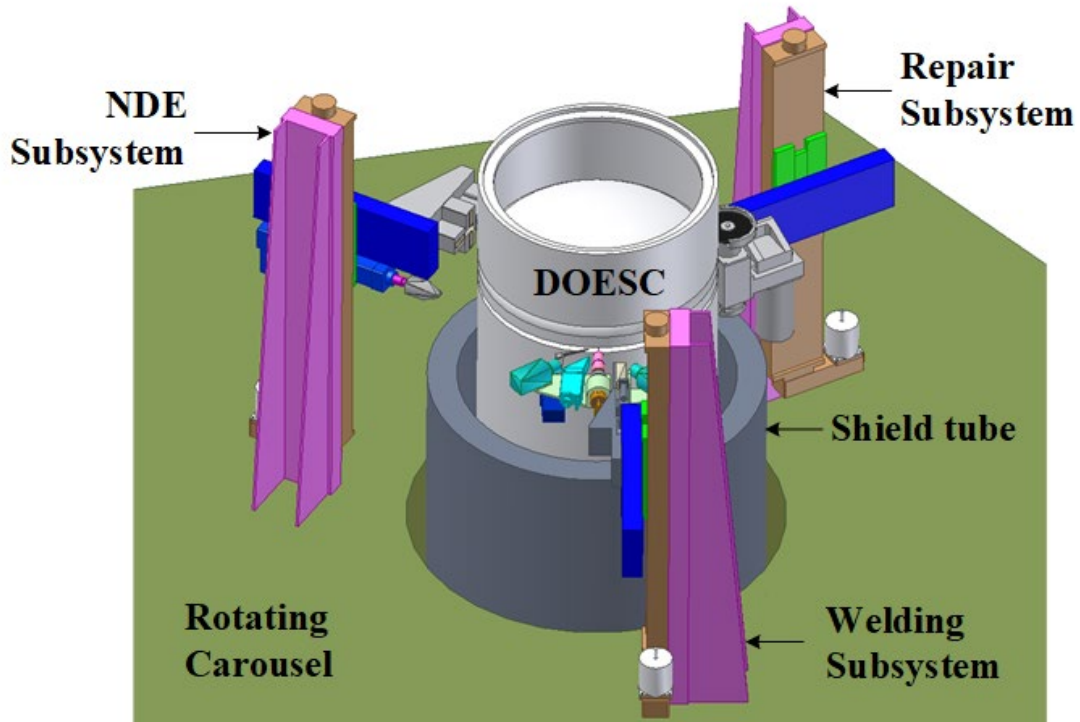


Figure 6: NSNFP canister closure system. Adapted from⁵.

192 The custom weld head was equipped with a 300A, air-cooled GTAW torch, arc viewing
 193 cameras, laser seam tracker, wire feed positioner, and arc voltage control (Figure 7). Two arc
 194 viewing cameras were placed forward and aft of the torch that could observe both the joint
 195 while in low light and the weld pool during welding. The weld head's laser seam tracker was
 196 used for tracking the electrode with the seam and for visual examinations of the weld before
 197 initiating the ET and UT examinations.

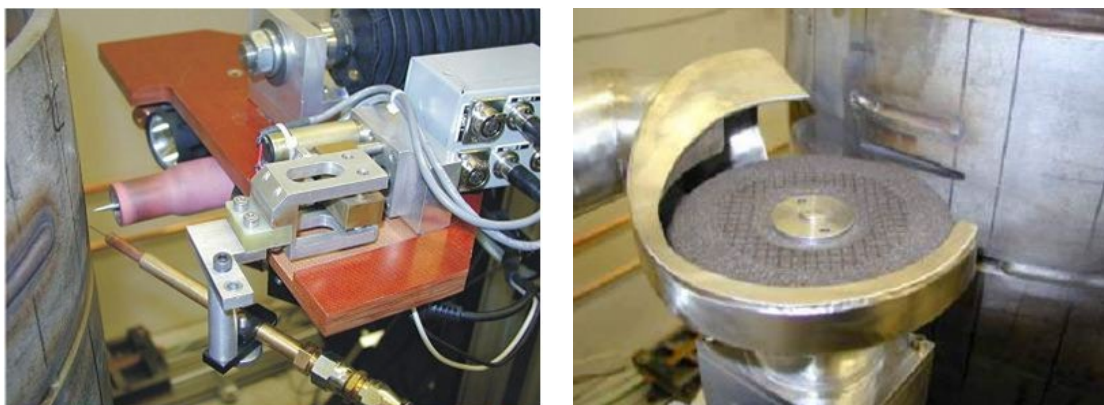


Figure 7: NSNFP weld head (left) and repair grinding wheel (right)⁵.

198 The repair subsystem removed defects in the closure welds created during welding and
 199 subsequently identified by the NDE subsystem. The restriction of cutting fluid in a hot cell

200 environment and imprecision of arc-gouging led to grinding with a conventional grinding
201 disc as the selected technique for making these repairs (Figure 7). Following a weld, the
202 repair subsystem wire brushed the weld and heat affected zone to remove oxides produced
203 during welding. If defects were discovered during examination, the repair subsystem would
204 grind out the previous pass. The repair subsystem developed a cutting toolpath based on the
205 NDE's determination of the defect's size and location within the weld.

206 The NDE subsystem included surface and volumetric examination according to the ASME
207 BPVC. Given the requirement of remote operation in a hot cell environment, ET was selected
208 as the technique for performing the surface examination. INL researchers acknowledged an
209 ASME BPVC case was needed to permit ET in lieu of the PT that is required by the ASME
210 BPVC. The ET subsystem used an array of probes that would contour over the weld and a
211 separate array for the narrower repair cavity. Remote volumetric NDE was performed using
212 two pairs of phased array ultrasonic transducer (PAUT) sensors. To identify the size and
213 orientation of defects required by the ASME BPVC, one pair of sensors was oriented
214 longitudinally (i.e., across from the weld seam), and the other pair was oriented
215 circumferentially (i.e., in line with weld seam). An expert panel review was performed of the
216 canister closure system, with a recommendation to move forward with development,
217 especially regarding performance under the harsh radiological environment³².

218 **IV. ROAD-READY DEMONSTRATION REMOTE CLOSURE SYSTEM**

219 As part of the RRDP, a new effort to design, develop, and construct a DOESC remote
220 canister closure system was initiated. This canister closure system would specifically be
221 operated at INTEC. The remote closure system is comprised of five platforms that interface
222 with the top of the DOESC (Table 1). These platforms include modules capable of remotely
223 performing, examining, and repairing the DOESC's circumferential and vent port welds. The
224 design and development efforts for this canister closure system have been reported in detail
225 elsewhere^{6, 33, 34}. These platforms are compared against the ISFF and NSNFP technologies
226 below.

Table 1: RRDP remote canister closure system weld platforms.

Platform Number	DOESC Closure Weld	Weld Equipment	NDE Equipment	Repair Equipment
1	Circumferential	Air-Cooled GTAW Torch	ET, PAUT	—
2		—	ET	Side Milling Cutter
3	Vent Port	Air-Cooled GTAW Torch	ET	—
4		—	PAUT	—
5		—	—	Annular Cutting Wheel

227 **IV.A. Circumferential Weld Platforms**

228 Two circumferential weld platforms have been designed and developed by INL and Liburdi
 229 Dimetrics® for use in the RRDP⁶. Platform number 1 (Figure 8) is designed to perform the
 230 circumferential closure weld and weld NDE. Platform number 1 is equipped with a semi-
 231 autonomously controlled, 600A, air-cooled GTAW torch, which can run a pre-programmed
 232 weld routine, or welding using manual user input. The circumferential welds are formed by a
 233 single u-groove butt joint and created by a series of four or six weld passes for Ø18” and
 234 Ø24” canisters respectively. A pair of ET and PAUT sensors are mounted to the platform to
 235 perform the surface and volumetric NDE. Platform number 2 (Figure 9) is designed to
 236 remove any potential weld defects in the circumferential weld using a pneumatically driven
 237 high-speed steel cutting wheel. A cutting wheel was selected because the finer debris could
 238 be collected easier than coarser debris from a grinding disc. A vacuum module is located
 239 adjacent to the cutting wheel to collect debris during the repair process. An ET sensor is also
 240 mounted to platform number 2 to perform ET after a weld repair.

241 These platforms are based around a frame and module architecture⁶. The center frame allows
 242 the platform to be pneumatically clamped to the DOESC lid assembly and has a rigging
 243 attachment point. The center frame is fixed. A rotating frame is attached to the center frame
 244 via a track and bearing system and is rotated around the track by a pinion gear. The welding
 245 torch, NDE sensors, and repair head are attached to the rotating frame on modules. The weld,
 246 ET, PAUT, and repair modules are equipped with servo motors that allow each end effector

247 to be positioned around the weld groove, as well as high-definition cameras and lights to
248 view the operations.

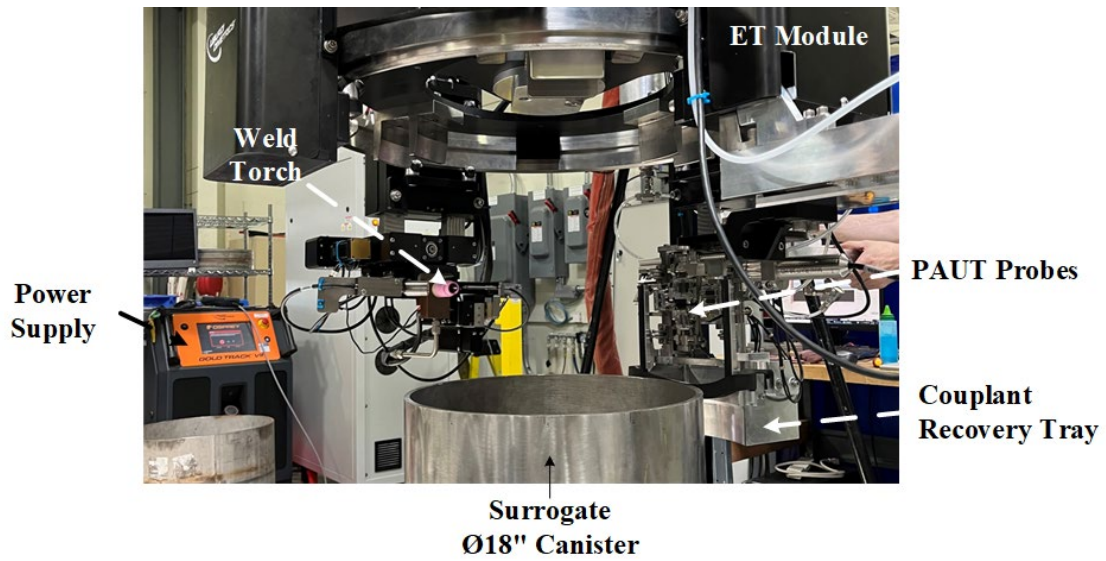


Figure 8: RRDP remote canister closure system platform number 1 (circumferential weld & NDE platform) being lowered onto a surrogate Ø18" DOESC.

249

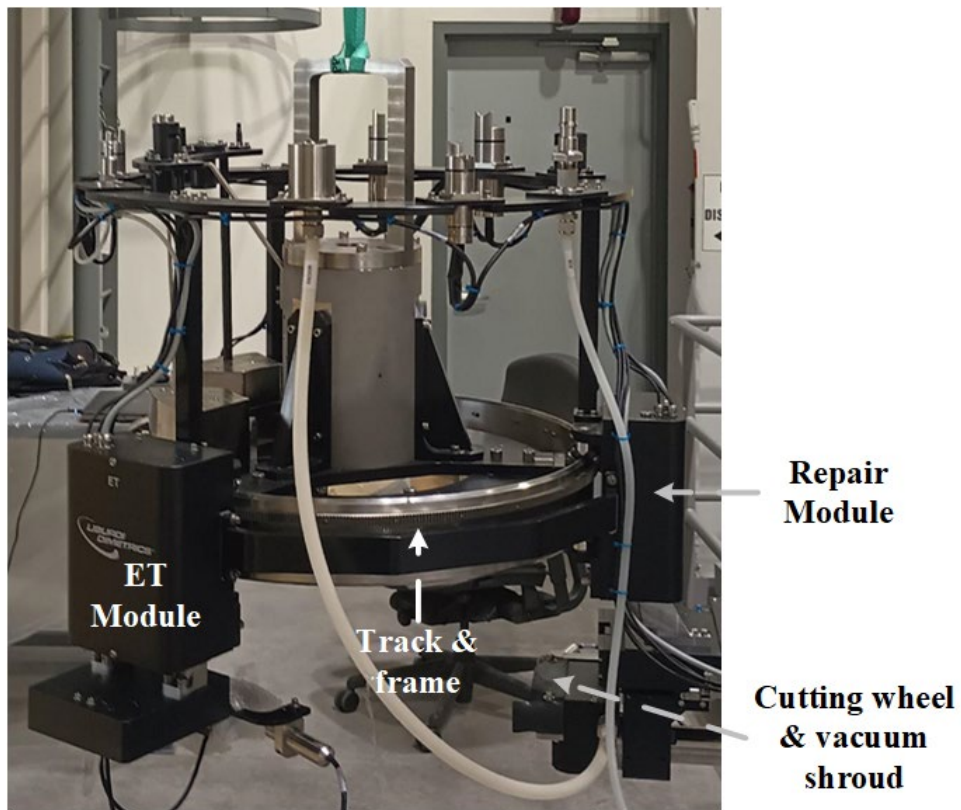


Figure 9: RRDP remote canister closure system platform number 2 (circumferential weld repair platform) suspended from rigging attachment point.

250 The weld platforms are powered and operated by a GoldTrack VII power supply, Liburdi
251 Canister Closure Console (LCCC) cabinet, and Fireview user interface all developed by
252 Liburdi Dimetrics®. This is the same power supply used for the MCO's closure weld¹⁹. The
253 control console is equipped with screens that can display selected camera views, allowing the
254 operator to observe and control platform operations in real-time. During the semi-automated
255 welding process, the control console executes a pre-programmed welding routine with
256 buttons for manual adjustments to critical welding parameters such as amperage, voltage,
257 wire feed rate, and travel speed. For NDE and repair tasks, the operator directly controls the
258 platform through the console, pausing and continuing NDE as needed.

259 ***IV.B. Vent Port Weld Platforms***

260 The RRDP has also designed three platforms (numbers 3, 4, and 5) for the vent port weld
261 (Table 1, Figure 10). Although detailed design and development is still underway, the
262 platforms will clamp to the DOESC the same way and use the same Gold Track VII power
263 supply, LCCC cabinet, and the Fireview user interface as platforms 1 and 2. In addition, the
264 same weld torch, wire feed mechanism, cameras, PAUT probes, and eddy current probe array
265 will be used. The vent port weld uses the same u-groove butt joint as the circumferential
266 weld, but on a Ø1.5" seam within the confined space of the Ø17.25" impact limiter (Figure
267 2). This enclosed space reduces the available space for equipment, which is why the vent port
268 weld requires three platforms.

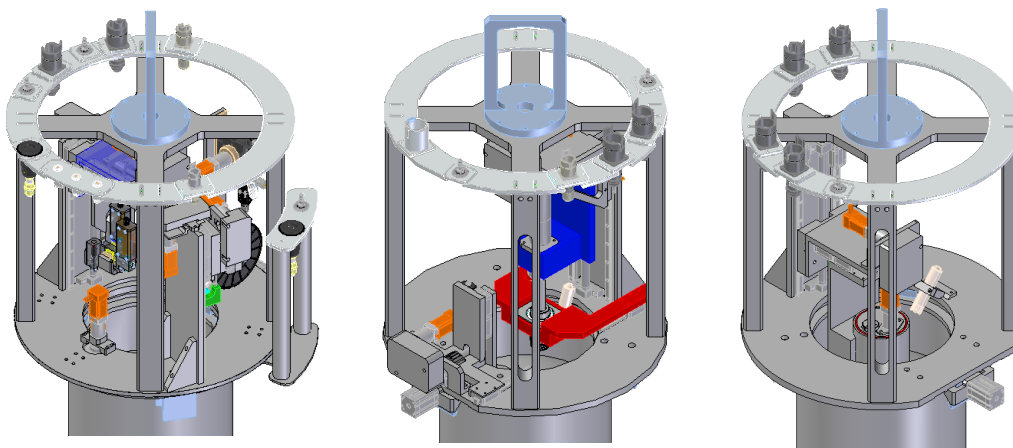


Figure 10: RRDP canister closure system platform number 3 (left), number 4 (middle), and number 5 (right)

269 Although generally the same equipment as platform number 1 and 2 will be used for the vent
270 port weld, the vent port weld's geometry requires customized brackets and linkages for
271 welding, NDE, and repair. Platform number 3's weld torch and eddy current probe array will

272 be vertically oriented and include motorized vertical plunge and cross-seam motion relative
273 to the weld. Platform number 4 will solely be for performing PAUT of the vent port weld.
274 This PAUT module will require a customized couplant delivery and recovery system. The
275 PAUT module design is of particular interest given the challenges with compression wave
276 scanning and dry couplant previously reported for the circumferential weld⁶.

277 Platform number 5 will utilize a custom annular cutting wheel sized to the vent port's u-
278 groove. Unlike platform number 2, platform number 5 will only be capable of vacuuming
279 debris as a separate step after the repair cut is made.

280 **V. DISCUSSION**

281 The circumstances under which the abovementioned welding and NDE technologies were
282 developed somewhat influenced their design. The ISFF welding and NDE systems and
283 NSNFP canister closure system were each developed when the Yucca Mountain geological
284 repository was due to receive DOE-managed SNF packaged within DOESCs³⁵. Given the
285 decision to suspend Yucca Mountain construction, the recent RRDP focuses more on near-
286 term storage, with suitability for eventual off-site transportation and disposal²⁶. In addition,
287 the only function of the DOESC in the ISFF license was for interim storage. The NSNFP
288 considered storage and transportation requirements from the ASME BPVC³². Finally,
289 although transportability of the DOESCs was an objective for the ISFF³⁶, no NRC
290 certification of a transportation package was required for the ISFF. Similarly, no
291 transportation package certification is currently required for the RRDP³⁷.

292 *V.A. Differences*

293 The abovementioned welding and NDE technologies utilize different processes and
294 techniques to fabricate and examine the DOESC's closure welds (Table 2). These
295 technologies are also designed to varying constraints, stemming from their operating
296 environments and construction code.

Table 2: Comparison of DOESC welding and NDE techniques.

DOESC Program	DOESC Closure Weld	Volumetric NDE	Surface NDE	Weld Technique	Repair Technique	Code of Record
ISFF	Circumferential	UT	PT	GTAW (Manual & Automated)	Machining, Grinding, or Thermal Gouging	Section III, Division 1 ²⁹
	Vent Port	None				N/A
NSNFP	Circumferential	PAUT	ET	GTAW (Semi-Automated)	Grinding Disk	Section III, Divisions 1&3 ^{29, 38}
RRDP	Circumferential & Vent Port	PAUT	ET	GTAW (Semi-Automated)	Cutting Wheel	Section III, Division 3 ³⁹

297 The ISFF was built and designed to specifically allow collocated personnel during DOESC
 298 closure in its canister closure area, which permitted manual operations. The NSNFP did not
 299 have a specific operating environment defined for its welding and NDE processes. When
 300 design of the RRDP’s remote canister closure system began, a facility at INTEC had been
 301 identified, but operating constraints had not been defined in significant detail. Conservative
 302 constraints were given to moderator control and remote operation for the NSNFP and RRDP
 303 systems. One specific way these differences were manifested in the design is in the weld
 304 torch. While the ISF orbital weld torch is water-cooled, both the NSNFP canister closure
 305 system and RRDP weld platforms use air-cooled torches for compatibility in moderator-
 306 controlled environments. While the RRDP system did originally consider a ‘dry couplant’
 307 PAUT wheel probe, the RRDP platforms now ultimately uses limited couplant (i.e., water)
 308 between the PAUT sensors and DOESC’s closure welds to achieve the coverage required by
 309 the BPVC⁶. The PAUT module includes a couplant delivery and recovery system.

310 In addition to different technologies, the weld joint geometry of the circumferential and vent
 311 port welds differs across the ISFF, NSNFP, and RRDP DOESC designs (Figure 11). The
 312 original NSNFP DOESC used a v-groove circumferential pipe weld with an optional
 313 threaded plug for the vent port. Per the original DOESC design, the NSNFP assumed a

314 threaded plug would be added, removed, and welded (if required) in a hot cell to form a
 315 containment to meet BPVC requirements^{2, 32}. This design was adapted by the ISFF program,
 316 which utilized a single-sided j-groove circumferential weld—likely driven by its suitability to
 317 semi-automated welding. Additionally, the ISFF modified the vent port weld by inserting a
 318 metallic mechanical seal beneath the vent plug to temporarily seal it until the final vent port
 319 seal weld was completed (Figure 11). The RRDP has further modified both weld joints. The
 320 RRDP circumferential weld groove has a single-sided u-groove with a steeper angle than
 321 previous iterations to limit each weld pass thickness to 3 mm (0.12”). This weld pass
 322 thickness was selected to maximize coverage provided by ET, while the steep angle
 323 precludes the need for multiple weld stringers in each layer. The vent port weld utilizes an
 324 identical weld joint to the circumferential joint. Furthermore, the RRDP has modified the
 325 backing ring, which does not contact the root of the weld for more consistent PAUT
 326 inspection. This backing ring is only used as a barrier to protect the SNF from any slag
 327 potentially produced while performing the circumferential closure weld (Figure 11).

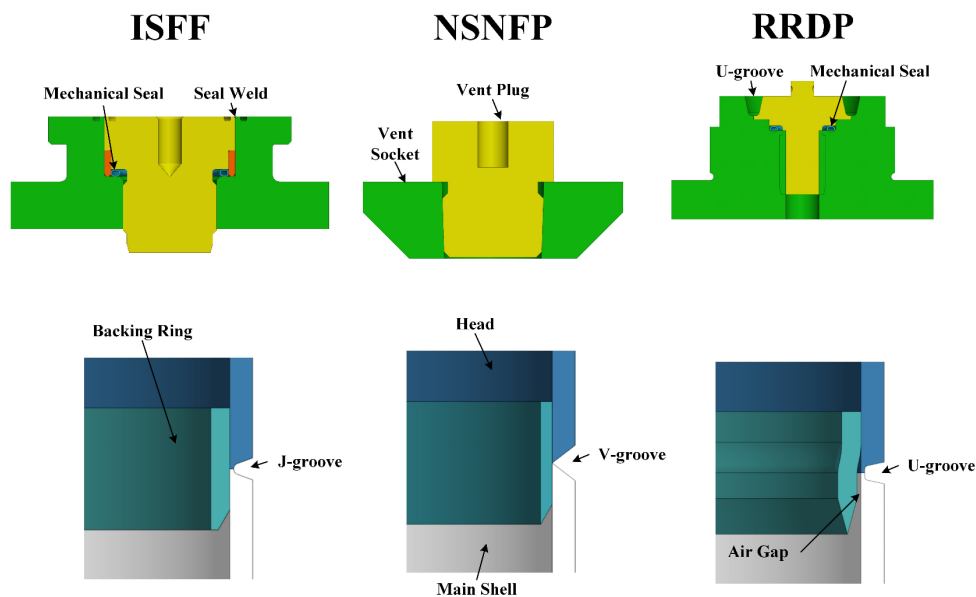


Figure 11: Weld joint geometry of ISFF⁴⁰, NSNFP¹, and RRDP DOESC vent port welds joining the vent plug to the vent socket (top) and circumferential closure weld joining the head to the main shell (bottom).

328 Construction code requirements are another driver for the technology and process
 329 differences. The ISFF classified the vent port weld as a seal weld. This placed it outside the
 330 scope of the ASME BPVC and removed the volumetric NDE requirement. PT was suitable
 331 for the ISFF because of the operating environment and its common application in weld NDE
 332 of commercial SNF containments⁴¹. As mentioned above, the optional threaded vent plug in
 333 the NSNFP DOES design required welding of its exposed threads to meet ASME BPVC

334 requirements. The RRDP has classified the circumferential and vent port closure welds as
335 structural welds⁴², meaning both require volumetric (PAUT) and surface (ET) examination
336 are required. The NSNFP welding equipment did not include equipment for performing or
337 examining the DOESC's vent port weld.

338 *V.B. Alternative DOESC Closure Weld Techniques*

339 Although the ISFF, NSNFP, and RRDP design efforts selected GTAW as the closure weld
340 process, other weld processes were considered during the RRDP design effort. In the
341 category of arc welding, shielded metal arc welding (SMAW), gas metal arc welding
342 (GMAW), and submerged arc welding (SAW) were potential candidates⁴³. Friction welding
343 (FRW) and friction stir welding (FSW) were two solid state welding processes that were also
344 considered during the RRDP design effort⁴⁴.

345 Based on the radiation dose rates expected, the quantity of canisters expected during the
346 RRDP, and the length of the circumferential weld, manual welding was considered
347 unacceptable and automated, semi-automated, or at least mechanized weld application was
348 required. SMAW does not generally accommodate these application methods, and available
349 mechanized applications for SMAW such as gravity welding would not be usable in the
350 DOESC orientation⁴³. SMAW was thus quickly eliminated from consideration. GMAW has
351 better applicability to automated application methods and can produce clean, repeatable
352 welds and thus could be an acceptable weld process for the DOESC. However, the GMAW
353 modes appropriate for structural welds, spray transfer and pulsed spray, produce excessive
354 heat in the welding torch and require water cooling. Due to restrictions on neutron
355 moderating materials in the work area requiring the use of a gas cooled torch, and with no
356 other clear benefit versus GTAW, GMAW was removed from consideration. SAW was not
357 given much consideration due to the weld positions, as implementing the flux bed around the
358 circumferential weld and removing excess flux from the impact limiter around the vent port
359 would be difficult, without any clear benefit versus GTAW.

360 Both FRW and FSW offered some advantages over arc welding processes. The heat and
361 resulting stresses in the base metal can be less than that of arc welding, improving resistance
362 to stress corrosion cracking. The welds are applied quickly in a single pass, resulting in
363 reduced process time compared to a long, multi-layered GTAW weld. However, several
364 requirements currently prevent implementing either of these processes for the DOESC. FRW

365 for the DOESC lid would require very large holding and turning machinery, which would be
366 difficult to incorporate in the designated INTEC workspace. Using FSW for the
367 circumferential weld requires very high tool force against the wall of the DOESC with no
368 internal support in that area, which would likely deform the canister. Although there is
369 ongoing research to reduce these tool forces, FSW is currently not feasible⁴⁴. For these
370 reasons, both FRW and FSW were eliminated.

371 *V.C. DOESC Closure Weld Code and Regulatory Compliance*

372 The RRDS's storage function, which is its most near-term application, will be regulated by
373 DOE³⁷. The RRDS's specific transportation and disposal regulatory requirements for the
374 RRDP are not yet defined. However, compatibility with the NRC's 10 CFR 71, "Packaging
375 and Transportation of Radioactive Material" is expected⁴⁵. The DOESC will only be a
376 subsystem of the broader RRDS system for storage, transportation, and disposal. For the
377 RRDP, the construction code of record for the DOESC has been established as Section III,
378 Division 3⁴². Division 3 has not yet been endorsed by the NRC for storage or transportation
379 containments^{46, 47}. Commercial storage and transportation containments are typically
380 constructed according to Section III, Division 1⁴⁸, while documenting alternative
381 requirements in their system-specific safety documentation. Full compliance with the ASME
382 BPVC is not a necessary condition to obtain a certificate or license for an NRC transportation
383 or storage system. The development of the regulatory framework for RRDS is as notable a
384 challenge as the engineering and development efforts associated with the RRDP. Defining the
385 degree of DOE and NRC regulatory compliance is ongoing.

386 *1. UT in lieu of RT in NRC transportation and storage containments*

387 While compliance with the BPVC is not required, the NRC has identified certain BPVC
388 Cases that are, and are not, approved for use in nuclear reactor, SNF storage, and SNF
389 transportation applications^{49, 50}. For the RRDP, DOESC construction applies UT in lieu of
390 RT, as permitted by Division 3 of the BPVC³⁹. However, the NRC does not approve of this
391 substitution citing the UT technique's inability to examine the full thickness of the weld
392 volume in austenitic stainless steels⁴⁹.

393 Austenitic stainless steel weld NDE is a unique challenge for the UT technique. The grain
394 structure of austenitic stainless steel is coarse, particularly in the weld zone. This creates

395 difficulty for ultrasonic beams to penetrate and focus in the as-welded state. This difficulty
396 arises from increased attenuation and beam spread on the transmission path as well as the
397 return path. The ultrasonic inspection industry has made progress tuning systems for these
398 inspections using PAUT focusing techniques and software filtering to reduce the external
399 noise displayed during inspection⁵¹. While the challenge is not eliminated, the resultant
400 output is significantly improved over conventional UT technology and techniques.

401 For PAUT of the DOESC closure welds, acceptance is dependent on satisfying the specified
402 ASME BPVC acceptance criteria³⁹. The threshold for investigation of discontinuities in the
403 weld zone is 20% of the full screen height reference level. For indications with amplitude
404 greater than the investigative threshold, the inspector maximizes the response and measures
405 the length of the indication to determine if the acceptance criteria have been met. Indications
406 exceeding the reference level and maximum length, inclusive, are rejected. During
407 evaluation, indications dispositioned by showing characteristics of cracks, lack of fusion, or
408 incomplete penetration shall be rejected—regardless of length.

409 Although the RRDP is developing the DOESC's PAUT procedure according to the
410 requirements of the ASME BPVC to address these issues, its acceptability in lieu of RT in an
411 NRC-regulated transportation package needs to be addressed further.

412 2. *ET in lieu of PT in NRC transportation and storage containments*

413 The BPVC Code typically requires RT and PT for welds on austenitic stainless steel welds³⁹.
414 PT is commonly used in NRC and DOE applications^{19, 41}. However, the anticipated high
415 radiation fields and high volume of DOESCs anticipated for SNF packaging make a remote
416 technique, such as ET, more attractive. For the RRDP, DOESC construction applies ET in
417 lieu of PT, as permitted by BPVC Code Case N-748 under Division 3 of the BPVC³⁹. The
418 acceptability of code case N-748 has not been established by the NRC^{49, 50}.

419 VI. CONCLUSION

420 The closure welding and NDE processes of the DOESC have been designed and developed
421 three separate times, to varying degrees. The DOESC design has also evolved along with the
422 closure welding technology. Development activities were based on different operating
423 environments and construction codes. The ISFF had defined constraints as a dry SNF storage

424 packaging facility that permitted collocated personnel during closure, and its certification to
425 the ASME BPVC. While licensed by the NRC as a dry SNF storage facility, certain details
426 regarding the development and qualification of its welding, repair and NDE processes were
427 not available. The NSNFP documented its development efforts of its canister closure system
428 for the circumferential weld, particularly of the PAUT process. Even though the original
429 DOESC design required the vent port weld to be performed after loading SNF, the NSNFP
430 did not develop a weld or NDE process for it. The RRDP is currently developing and
431 qualifying its weld processes for the circumferential and vent port closure welds.

432 While the design of the ISFF and NSNFP closure weld systems have concluded for the time
433 being, the RRDP remote canister closure system is still being developed at the INL. The
434 RRDP remote canister closure system platforms, especially for the vent port weld, need
435 further development before deployment at INTEC. The repair and NDE functions of the
436 circumferential weld platforms will continue on coupons and full-length DOESC mock-up(s)
437 to qualify personnel and processes. The vent port weld platforms are still being designed but
438 will also be subject to the same development and testing. These development activities will
439 also include verification of their welding, NDE, and repair functions in a radiological
440 environment. The circumferential and vent port closure weld platforms must reliably
441 perform, examine, and repair (if necessary) the closure welds to the requirements of the
442 ASME BPVC.

443 Separate from the development activities, confirmation is also needed on the acceptability of
444 PAUT and ET NDE for any DOESC functions regulated by the NRC (e.g., transportation
445 and/or disposal). The DOESC includes closure welds whose design and examination differ
446 from typical commercial SNF storage confinements welds. The RRDP is currently applying a
447 surface and volumetric NDE scheme that meets the requirements of the ASME BPVC, but
448 further development may be necessary to address potential NRC concerns regarding use of
449 PAUT and/or ET in nuclear reactor construction.

450 **VII. ACKNOWLEDGEMENTS**

451 This work was supported through the U.S. Department of Energy Office of Environmental
452 Management under DOE Idaho Operations Office Contract DE-AC07-05ID14517.
453 Accordingly, the U.S. Government retains and the publisher, by accepting the article for
454 publication, acknowledges that the U.S. Government retains a nonexclusive, paid-up,

455 irrevocable, world-wide license to publish or reproduce the published form of this
456 manuscript, or allow others to do so, for U.S. Government purposes. The authors would like
457 to thank Liburdi Dimetrics® and INL engineers and technicians that have enabled and
458 supported this work.

459 **VIII. DECLARATION OF INTEREST**

460 This information was prepared as an account of work sponsored by an agency of the U.S.
461 Government. Neither the U.S. Government nor any agency thereof, nor any of their
462 employees, makes any warranty, express or implied, or assumes any legal liability or
463 responsibility for the accuracy, completeness, or usefulness of any information, apparatus,
464 product, or process disclosed, or represents that its use would not infringe privately owned
465 rights. References herein to any specific commercial product, process, or service by trade
466 name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its
467 endorsement, recommendation, or favoring by the U.S. Government or any agency thereof.
468 The views and opinions of authors expressed herein do not necessarily state or reflect those
469 of the U.S. Government or any agency thereof.

470 **IX. REFERENCES**

- 471 1. U.S. DEPARTMENT OF ENERGY, "Preliminary Design Specification for
472 Department of Energy Standardized Spent Nuclear Fuel Canisters, Volume II -
473 Rationale Document," DOE/SNF/REP-011, Rev. 3, Idaho Falls, ID, (1999).

- 474 2. U.S. DEPARTMENT OF ENERGY, "Preliminary Design Specification for
475 Department of Energy Standardized Spent Nuclear Fuel Canisters, Volume I - Design
476 Specification," DOE/SNF/REP-011, Rev. 3, Idaho Falls, ID, (1999).

- 477 3. M. G. EL-SAMRAH, A. F. TAWFIC, S. E. CHIDIAC, "Spent nuclear fuel interim
478 dry storage; Design requirements, most common methods, and evolution: A review,"
479 *Annals of Nuclear Energy* **160**, 108408 (2021)
480 <https://doi.org/10.1016/j.anucene.2021.108408>.

- 481 4. FOSTER-WHEELER ENVIRONMENTAL CORPORATION, "ISF Project Design
482 Criteria Document - Canister Weld NDE System (ISF-FW-RPT-0082)," ISF-FW-
483 RPT-0082, (2003).

- 484 5. E. D. LARSEN et al., "Remote Welding, NDE, and Repair of DOE Standardized
485 Canisters,presented at "5th International Conference on NDE in Relation to Structural
486 Integrity for Nuclear & Pressurized Components", San Diego, CA, 2006.
- 487 6. N. HOFMEISTER et al., "Acceptance Testing of Remote Closure Platforms for
488 Closure of DOE Standard Canisters – 24557,"*2024 Waste Management Symposia*,
489 Phoenix, AZ, 2024, (2024).
- 490 7. FOSTER-WHEELER ENVIRONMENTAL CORPORATION, "License Application:
491 Idaho Spent Fuel Facility (Docket No. 72-27) (ISF-FW-RPT-0127)," ISF-FW-RPT-
492 0127, (2003).
- 493 8. U.S. NUCLEAR WASTE TECHNICAL REVIEW BOARD, "Management and
494 Disposal of U.S. Department of Energy Spent Nuclear Fuel: A Report to the United
495 States Congress and the Secretary of Energy," (2017).
- 496 9. T. J. HILL, D. L. FILLMORE, "Managing Spent Nuclear Fuel at the Idaho National
497 Laboratory,presented at "NATO Advanced Research Workshop, Safety-Related
498 Issues of Spent Nuclear Fuel Storage", 2005.
- 499 10. U.S. DEPARTMENT OF ENERGY OFFICE OF ENVIRONMENTAL
500 MANAGEMENT, "National Spent Nuclear Fuel Program Program Management
501 Plan," DOE/SNF/PP-033, Rev. 0, (2000).
- 502 11. IDAHO DEPARTMENT OF ENVIRONMENTAL QUALITY, 1995. 1995
503 Settlement Agreement, in: State of Idaho (Ed.).
- 504 12. U.S. NUCLEAR REGULATORY COMMISSION, "Standard Review Plan for Dry
505 Storage and Transportation of High Burnup Spent Nuclear Fuel," NUREG-2224,
506 (2020).
- 507 13. A. J. LUPTAK, K. D. BULMAHN, "Evaluation of Nondestructive
508 Assay/Nondestructive Examination Capabilities for Department of Energy Spent
509 Nuclear Fuel," DOE/SNF/REP-030, Rev. 0, (1998).
- 510 14. IDAHO NATIONAL LABORATORY, "FY1999 Drop Testing Report for the 18-
511 inch Standardized DOE SNF Canister," EDF-NSNF-007, Rev. 2, (1999).
- 512 15. W. TANG et al., "Welding Process Development for Spent Nuclear Fuel Canister
513 Repair,"*ASME 2019 Pressure Vessels & Piping Conference*", 2019, Volume 1: Codes
514 and Standards, (2019).

- 515 16. S. CHATZIDAKIS et al., "A Versatile Remediation Module for Remote Repair of
516 Spent Nuclear Fuel and High-Level Waste Storage Containers," *Nuclear Technology*
517 **207**, 750-760 (2021) 10.1080/00295450.2020.1800309.
- 518 17. J. STAVRIDIS, A. PAPACHARALAMPOPOULOS, P. STAVROPOULOS, "A
519 cognitive approach for quality assessment in laser welding," *Procedia CIRP* **72**, 1542-
520 1547 (2018) <https://doi.org/10.1016/j.procir.2018.03.119>.
- 521 18. P. STAVROPOULOS, A. PAPACHARALAMPOPOULOS, K. SABATAKAKIS,
522 "Online Quality Inspection Approach for Submerged Arc Welding (SAW) by
523 Utilizing IR-RGB Multimodal Monitoring and Deep Learning," *Flexible Automation*
524 *and Intelligent Manufacturing: The Human-Data-Technology Nexus*, Cham, 2023//,
525 2023, 160-169, Springer International Publishing (2023).
- 526 19. G. CANNELL, L. GOLDMANN, "Design of the Hanford Multi-Canister Overpack
527 (MCO) and Development and Qualification of the Closure Welding Process," *2004*
528 *ASME International Mechanical Engineering Congree and Exposition*", Anaheim,
529 California, 2004, (2004).
- 530 20. H. J. LEE et al., "Status of Closure Welding Technology of Canister for
531 Transportation and Storage of High Level Radioactive Material and Waste,"
532 KAERI/AR-863/2010, (2010).
- 533 21. R. M. MEYER et al., "Review of NDE Methods for Detection and Monitoring of
534 Atmospheric SCC in Welded Canisters for the Storage of Used Nuclear Fuel," PNNL-
535 22158, (2013).
- 536 22. AMERICAN SOCIETY OF MECHANICAL ENGINEERS, 1997. Boiler and
537 Pressure Vessel Code - Division 3, Containment Systems and Transport Packagings
538 for Spent Nuclear Fuel and High Level Radioactive Waste. American Society of
539 Mechanical Engineers, New York, NY.
- 540 23. AMERICAN SOCIETY OF MECHANICAL ENGINEERS, 1989. Boiler and
541 Pressure Vessel Code - Division 1, Rules for Construction of Nuclear Power Plant
542 Components Class 1 Components. American Society of Mechanical Engineers, New
543 York, NY.
- 544 24. U.S. NUCLEAR REGULATORY COMMISSION, 2004. Notice of Issuance of
545 Materials License SNM-2512 for the Idaho Spent Fuel Facility, in: U.S. Nuclear
546 Regulatory Commission (Ed.). Federal Register.
- 547 25. U.S. DEPARTMENT OF ENERGY, "Strategic Framework for DOE-Managed Spent
548 Nuclear Fuel," (2021).

- 549 26. S. J. TROST et al., "INL SNF Road-Ready Demonstration - Updates and Progress -
550 24071,"*2024 Waste Management Symposia*", Phoenix, AZ, 2024, (2024).
- 551 27. W. ANDERNTON, K. MORTENSEN, K. OLTMANNNS, "Adapting Legacy DOE
552 Dry Storage Facility for New "Road Ready" Packaging Process– 24592,"*2024 Waste*
553 *Management Symposia*", Phoenix, AZ, 2024, (2024).
- 554 28. D. A. THOMAS, "Preliminary Evaluation of Loading DOE Standardized Canisters in
555 the CPP-603 Irradiated Fuel Storage Facility," INL/EXT-19-55389, Revision 1,
556 (2019).
- 557 29. AMERICAN SOCIETY OF MECHANICAL ENGINEERS, 2000. Boiler and
558 Pressure Vessel Code - Division 1, Code Case N-595-2, Requirements for Spent Fuel
559 Storage Canisters, Section III, Division 1. American Society of Mechanical
560 Engineers, New York, NY.
- 561 30. FOSTER-WHEELER ENVIRONMENTAL CORPORATION, "ISF Project Design
562 Criteria Document - Canister Design Criteria (ISF-FW-RPT-0053)," ISF-FW-RPT-
563 0053, (2004).
- 564 31. FOSTER-WHEELER ENVIRONMENTAL CORPORATION, "Canister Closure
565 Area Canister Welding & NDE System Layout (ISF-ME-T-11119)," ISF-ME-T-
566 11119, (2001).
- 567 32. ASME INTERNATIONAL, INSTITUTE FOR REGULATORY SCIENCE, "Spent
568 Nuclear Fuel Canister Welding Concept," CRTD-Vol. 76, (2004).
- 569 33. J. BIALACH et al., "Process and Tooling Selection for Remote Closure of DOE
570 Standard Canisters – 22078,"*2022 Waste Management Symposia*", Phoenix, AZ,
571 2022, (2022).
- 572 34. D. A. THOMAS, "DOE SNF Packaging Demonstration Overview and 2022
573 Activities – 23162,"*2023 Waste Management Symposia*", Phoenix, AZ, 2023, (2023).
- 574 35. U.S. DEPARTMENT OF ENERGY, "Yucca Mountain Repository Safety Analysis
575 Report, Chapter 1: Repository Safety Before Permanent Closure," DOE/RW-0573,
576 Rev. 2, (2008).
- 577 36. FOSTER-WHEELER ENVIRONMENTAL CORPORATION, "ISF Project Design
578 Criteria Document - Transport System Concept Design Report (ISF-FW-RPT-0059),"
579 ISF-FW-RPT-0059, (2001).

- 580 37. IDAHO CLEANUP PROJECT, "Regulatory Authority for the Road Ready
581 Demonstration Project Activities and Idaho Spent Nuclear Fuel Staging Facility,"
582 RPT-2175, Rev. 0, (2024).
- 583 38. AMERICAN SOCIETY OF MECHANICAL ENGINEERS, 2000. Boiler and
584 Pressure Vessel Code - Division 3, Containment Systems and Transport Packagings
585 for Spent Nuclear Fuel and High Level Radioactive Waste. American Society of
586 Mechanical Engineers, New York, NY.
- 587 39. AMERICAN SOCIETY OF MECHANICAL ENGINEERS, 2015. Boiler and
588 Pressure Vessel Code - Division 3, Rules for Construction of Nuclear Facility
589 Components, Class TC and SC Containments. American Society of Mechanical
590 Engineers, New York, NY.
- 591 40. FOSTER-WHEELER ENVIRONMENTAL CORPORATION, "18" O.D. SNF
592 Canister Fabrication (Long Canister)," ISF-ME-S-16001, (2002).
- 593 41. U.S. NUCLEAR REGULATORY COMMISSION, 2008. ISG-18, The Design and
594 Testing of Lid Welds on Austenitic Stainless Steel Canisters as the Confinement
595 Boundary for Spent Fuel Storage, in: Division of Spent Fuel Storage and
596 Transportation (Ed.).
- 597 42. IDAHO NATIONAL LABORATORY, "Code of Record: Department of Energy
598 Standard Canister," COR-0009, Rev. 0, (2024).
- 599 43. HOWARD B. CARY, S. C. HELZER, "Modern Welding Technology," p. Pearson,
600 (2011).
- 601 44. T. WANG et al., "Force reduction of friction stir welding and processing of steel,"
602 *Materialia* **33**, 102050 (2024) <https://doi.org/10.1016/j.mtla.2024.102050>.
- 603 45. NUCLEAR REGULATORY COMMISSION, 2001. Packaging and Transportation of
604 Radioactive Material, in: National Archives (Ed.), 10 CFR 71.
- 605 46. U.S. NUCLEAR REGULATORY COMMISSION, "Standard Review Plan for Spent
606 Fuel Dry Storage Systems and Facilities," NUREG-2215, (2020).
- 607 47. U.S. NUCLEAR REGULATORY COMMISSION, "Standard Review Plan for
608 Transportation Packages for Spent Fuel and Radioactive Material," NUREG-2216,
609 (2020).

- 610 48. U.S. NUCLEAR REGULATORY COMMISSION, "Fabrication Criteria for Shipping
611 Containers," NUREG/CR-3854, (1985).
- 612 49. U.S. NUCLEAR REGULATORY COMMISSION, "ASME Code Case Not
613 Approved for Use," RG 1.193, Rev. 7, (2021).
- 614 50. U.S. NUCLEAR REGULATORY COMMISSION, 2021. Design, Fabrication, and
615 Materials Code Case Acceptability, ASME Section III. Nuclear Regulatory
616 Commission, Washington D.C.
- 617 51. J. BERLANGER et al., "Efficient PA UT Inspection of Austenitic Welds "in Lieu of
618 RT", presented at "12th International Conference on NDE in Relation to Structural
619 Integrity for Nuclear and Pressurized Components", Dubrovnik, Croatia, 2016.
- 620