

1     **Semi-Analytic Functions to Calculate the Deposition Coefficients for Ice**  
2             **Crystal Vapor Growth in Bin and Bulk Microphysical Models.**

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## ABSTRACT

13 Numerical cloud models require estimates of the vapor growth rate for ice  
14 crystals. Current bulk and bin microphysical parameterizations generally as-  
15 sume that vapor growth is diffusion limited, though some parameterizations  
16 include the influence of surface attachment kinetics through a constant depo-  
17 sition coefficient. A parameterization for variable deposition coefficients is  
18 provided herein. The parameterization is an explicit function of the ambient  
19 ice supersaturation and temperature, and an implicit function of crystal dimen-  
20 sions and pressure. The parameterization is valid for variable surface types  
21 including growth by dislocations and growth by step nucleation. Deposition  
22 coefficients are predicted for the two primary growth directions of crystals, al-  
23 lowing for the evolution of the primary habits. Comparisons with benchmark  
24 calculations of instantaneous mass growth indicate that the parameterization  
25 is accurate to within a relative error of 1%. Parcel model simulations using  
26 Lagrangian microphysics as a benchmark indicate that the bulk parameteriza-  
27 tion captures the evolution of mass mixing ratio and fall speed with typical  
28 relative errors of less than 10%, whereas the average axis lengths can have  
29 errors of up to 20%. The bin model produces greater accuracy with relative  
30 errors often less than 10%. The deposition coefficient parameterization can  
31 be used in any bulk and bin scheme, with low error, if an equivalent volume  
32 spherical radius is provided.

## 33 **1. Introduction**

34 Numerical models of ice-containing clouds require estimates of the ice crystal vapor growth  
35 rate. However, the vapor growth rate is complex, involving the diffusion of water vapor and  
36 thermal energy through the background gas. Gas-phase diffusion, in turn, depends on the size and  
37 shape of the crystal along with the surface processes that determine the incorporation of water  
38 molecules into the crystalline lattice. It is these surface processes that control the development  
39 of crystal habits (Hallett 1965; Lamb and Scott 1972; Nelson 2001). The challenge in modeling  
40 the ice growth lies in taking simultaneous account of crystal shape effects on gas-phase diffusion  
41 along with the surface kinetic processes that influence the mass uptake of the crystal.

42 The most common method for parameterizing the growth and ablation of ice crystals in numer-  
43 ical cloud models follows the work of Houghton (1950) in using capacitance theory. Capacitance  
44 theory assumes that the vapor density is constant along the crystal surface, which occurs when the  
45 surface is rough on the nanometer scale. Surface processes are ignored in this model: facets cannot  
46 remain flat (Saito 1996, Ch. 27), and aspect ratio cannot evolve (Ham 1959) without supplemen-  
47 tary theories (Chen and Lamb 1994). Though it was historically understood that surface processes  
48 were the drivers of the variations in habit forms, it was not clear how to include these processes  
49 in cloud models. For instance, Koenig (1971) included surface processes through a reduction fac-  
50 tor that acts in a similar mathematical fashion to a ventilation coefficient, but this kinetic factor  
51 was not included in most subsequent models. The work of Todd (1964) and Hindman and John-  
52 son (1972) avoided capacitance theory entirely by using laboratory-measured axis growth rates  
53 to drive habit development. Since their rate equations were taken directly from laboratory data,  
54 both surface and gas phase diffusion processes were empirically woven into the parameterization.  
55 While this line of modeling died out, it did presage current particle property approaches (Chen and

56 Lamb 1999; Hashino and Tripoli 2007; Chen and Tsai 2016). Most cloud model parameterizations  
57 do not include the effects of surface processes on mass uptake during vapor growth, but those that  
58 do commonly use deposition coefficients ( $\alpha$ ). Deposition coefficients account, in aggregate, for  
59 all of the surface processes occurring on the crystal surface that ultimately control the growth  
60 rates. Though all numerical models that include  $\alpha$  treat it as a constant, this approximation is only  
61 valid over a very narrow range of conditions (Nelson 2005). In this paper, we develop a parame-  
62 terization of supersaturation- and temperature-dependent  $\alpha$  that is consistent with faceted growth  
63 and is suitable for bulk and bin microphysical models. The parameterization is developed to be  
64 flexible in that it can be used with traditional and particle property schemes. The parameterization  
65 is tested against benchmark simulations using a parcel model framework with Lagrangian bin ice  
66 microphysics, and the accuracy and limitations of the method are discussed. We first review the  
67 theory of faceted growth, and the need for a closed-form approximation for  $\alpha$ .

## 68 **2. Mass and Dimensional Growth of Faceted Ice**

69 Deposition coefficients ( $\alpha$ ) have long been used to model the influences of surface attachment  
70 kinetic (hereafter *surface-kinetic*) processes on vapor growth (Strickland-Constable 1968). For  
71 faceted crystals,  $\alpha$  varies explicitly with the ambient ice supersaturation ( $s_i$ , hereafter “supersatu-  
72 ration”) and implicitly with the temperature, crystal size and shape (Nelson and Baker 1996; Wood  
73 et al. 2001). The classical theory of faceted growth posits that crystals grow primarily by the prop-  
74 agation of steps across their surface. In order for growth to proceed, adsorbed water molecules  
75 must attach to a step before they desorb from the surface. The fraction of molecules that adsorb,  
76 migrate to a step, and incorporate into the crystalline lattice defines the deposition coefficient.

77 The growth of faceted ice requires the formation of surface steps, and there are at least two mech-  
78 anisms that produce them. The first mechanism is associated with natural dislocations that occur

79 in the crystal lattice and can outcrop on the surface. Dislocations provide permanent step sources,  
 80 the theory of which originated with Burton et al. (1951). This mechanism appears to control the  
 81 growth of newly formed crystals (Harrington and Pokrifka 2021) and crystals grown at low super-  
 82 saturation (Nelson 2001). The second mechanism is the nucleation of two-dimensional steps on  
 83 the crystal surface (step nucleation). This mechanism occurs on facets that have large defect-free  
 84 areas, and appears to control the growth of larger crystals with distinct habits (Nelson and Knight  
 85 1998; Harrington et al. 2019). Indeed, Frank (1982) points out that thin crystals are only possible  
 86 if steps nucleate at the crystal edge. Step nucleation is strongly dependent on the supersaturation  
 87 immediately above the surface (surface supersaturation,  $s_{surf}$ ), with very weak growth at  $s_{surf}$  val-  
 88 ues below some critical supersaturation, and faster growth once the critical supersaturation has  
 89 been exceeded. While both theories have been developed in detail, an approximation for  $\alpha$  that  
 90 encapsulates both growth mechanisms was provided by Nelson and Baker (1996),

$$91 \quad \alpha(s_{surf}, T) = \alpha_s \left[ \frac{s_{surf}}{s_{char}(T)} \right]^M \tanh \left[ \frac{s_{char}(T)}{s_{surf}} \right]^M \quad (1)$$

92 where  $s_{char}(T)$  is a temperature-dependent “characteristic” supersaturation that describes the  
 93 supersaturation-dependence of surface-kinetic mediated growth, and  $M$  is a parameter that de-  
 94 scribes the surface growth mode. The adsorption efficiency ( $\alpha_s$ ) is thought to be near unity (Nel-  
 95 son 2001), which we will assume. Convenient polynomial fits to values of  $s_{char}$  derived from data  
 96 (Harrington et al. 2019) are used in this study and are available from a data archive (see our data  
 97 statement). A value of  $M = 1$  is consistent with the theory of dislocation growth, whereas a value  
 98 of  $M \geq 10$  is suitable for step nucleation. In general,  $\alpha$  rises commensurately with  $s_{surf}$ , and the  
 99 rate of rise is controlled by  $M$  (Zhang and Harrington 2015, see their Fig. 1). The evidence above  
 100 suggests that  $M = 1$  may be appropriate for the growth of smaller crystals in numerical cloud mod-

101 els, whereas  $M = 10$  may be more applicable to the growth of larger crystals with well-defined  
 102 habits.

103 The above form of  $\alpha$  has been most often used in models of faceted crystal growth requiring  
 104 complex numerical solution methods (Nelson and Baker 1996; Wood et al. 2001). However, it is  
 105 possible to include the above model for  $\alpha$  in theories suitable for use in Eulerian cloud models  
 106 (MacKenzie and Haynes 1992; Zhang and Harrington 2014). The theory of Zhang and Harrington  
 107 (2014) combines the surface boundary conditions for faceted ice with the diffusive fluxes from  
 108 the capacitance model, thus allowing for the calculation of the deposition coefficients using Eq. 1.  
 109 The resulting growth equation has the same general form as the capacitance model,

$$110 \quad \frac{dm}{dt} = 4\pi C(c, a) \rho_{eq} s_i D_{eff}(T, P, a, c, \alpha_a, \alpha_c), \quad (2)$$

111 where  $\rho_{eq}$  is the ice equilibrium vapor density,  $s_i$  is the supersaturation,  $C(c, a)$  is the capacitance,  
 112 and  $c$  and  $a$  are the crystal semi-dimensions that are referenced to the prism and basal faces of  
 113 hexagonal ice, respectively. The combined effects of vapor and thermal energy diffusion along  
 114 with surface kinetic effects ( $\alpha_a$  and  $\alpha_c$ ) enter into the growth equation through an effective diffu-  
 115 sivity ( $D_{eff}$ ) that also depends on size and shape (see Zhang and Harrington 2014, their Eq. 15).  
 116 The a- and c-axis lengths define a spheroid that is used as a surrogate for crystal shape. Spheroids  
 117 are not meant to exactly represent crystal shapes, but rather to provide equations for two crystal  
 118 dimensions instead of one dimension (see below).

119 Predicting the change in the crystal semi-dimensions ( $a$  and  $c$ ) requires equations for the evolu-  
 120 tion of the axis lengths. Faceted crystals often have steps that form near crystal edges where  $s_{surf}$   
 121 is greatest, in this case the ratio of the  $c$  and  $a$  axis growth rates is (Nelson and Baker 1996),

$$122 \quad \frac{dc}{da} = \frac{\alpha_c}{\alpha_a} = \Gamma \quad \text{or} \quad \frac{d \ln \phi}{d \ln V} = \frac{\Gamma / \phi - 1}{\Gamma / \phi - 2}, \quad (3)$$

123 where the right-most form can be derived using the volume ( $4/3\pi a^2 c$ ) and aspect ratio ( $\phi = c/a$ )  
 124 of a spheroid. Current habit-evolving cloud models (Hashino and Tripoli 2007; Harrington et al.  
 125 2013) use a different form of  $dc/da$  rooted in the work of Chen and Lamb (1994), however this  
 126 equation produces incorrect growth when variable deposition coefficients are used (Harrington  
 127 et al. 2019). The Chen and Lamb (1994) expression is replaced with Eq. 3 in the parameterizations  
 128 developed below.

129 Secondary habit features that appear at high supersaturations, such as dendritic branching and  
 130 hollowing, cannot be modeled explicitly. These features are frequently treated through an “ef-  
 131 fective” particle density ( $\rho_p$ ) that is lower than the bulk density of ice (Miller and Young 1979;  
 132 Thompson et al. 2008). Chen and Lamb (1994) hypothesized that one could treat the volumetric  
 133 increase in ice crystals with a deposition density ( $\rho_{dep}$ ) that mimics the spatial gaps caused by  
 134 branching and hollowing,

$$135 \frac{dV}{dt} = \frac{1}{\rho_{dep}} \frac{dm}{dt}. \quad (4)$$

136 The above equation, when used in combination with Eqs. 1, 2, and 3 produces crystal axis lengths,  
 137 effective densities, and fall speeds that compare well to wind tunnel measurements of columnar  
 138 and dendritic ice crystals grown at liquid saturation. The theory also compares well to hexagonal  
 139 model solutions for crystals grown at low ice supersaturations, and to measurements of crystals  
 140 grown at low pressures (Harrington et al. 2019).

141 While the above model provides a good approximation for faceted growth, care should be ex-  
 142 ercised when applying these theories in general. It is important to bear in mind that the surface  
 143 growth mechanism can change in time. Evidence suggests that ice crystals grow by dislocations  
 144 ( $M = 1$ ) when they are relatively small and at low supersaturations. However, at higher supersatu-  
 145 rations step nucleation ( $M = 10$ ) is thought to control the growth since it is otherwise not possible  
 146 to produce thin crystals (Frank 1982; Nelson and Knight 1998; Harrington et al. 2019), though

147 quasi-liquid layers (QLL) are also important (Neshyba et al. 2016; Sibley et al. 2021). Ice crystals  
148 are known to have stacking faults which reduce the nucleation barrier for surface steps (Ming et al.  
149 1988), and Nelson and Baker (1996) have suggested modeling this growth with  $M \simeq 3$  in Eq. 1.  
150 Crystals can have both slower and faster growing regions (Gonda and Yamazaki 1984), and facets  
151 can grow along the surface instead of outward (Gonda and Yamazaki 1984; Nelson and Swanson  
152 2019). Faster growing (rough) regions can starve slower growing facets of water vapor, leading to  
153 stagnated growth rates (Harrington and Pokrifka 2021). The grain boundaries in polycrystalline  
154 ice are sources of dislocations that may cause rapid growth (Pedersen et al. 2011). Mesoscopic  
155 surface roughness has been measured on many crystals (Neshyba et al. 2013; Magee et al. 2014),  
156 but the scale of these features is generally larger than the steps that influence growth, and some of  
157 these measured crystals stop growing entirely (Magee et al. 2014). Unfortunately, measurements  
158 of many of the above growth modes are scant and theoretical models are generally lacking.

159 It is also important to keep in mind that spheroidal shapes are an approximation for two crys-  
160 tal dimensions only. It is not clear how complex crystal morphologies should be treated. For  
161 instance, it has been shown that ellipsoids are more accurate than spheroids as a representation  
162 of aggregate shapes (Jiang et al. 2019; Dunnavan et al. 2019). Complex growth morphologies,  
163 such as capped columns and the polycrystalline forms that occur at low temperatures (e.g. planar  
164 polycrystals, tetragons with side planes, scrolls, and rosettes) provide other compelling examples.  
165 These growth forms suggest that multiple axes may be needed to characterize the crystal shape,  
166 and since these crystals are faceted they can be described by faceted growth kinetics. Though  
167 predicting the precise shape of these crystals is beyond the capabilities of any current theory, it  
168 may be possible to treat the overall influence of surface kinetics on mass growth. Zhang and Har-  
169 rington (2015) and Harrington et al. (2019) have shown that the overall influence of attachment  
170 kinetics on the growth of columnar and planar crystals can be treated with an equivalent volume



171 sphere and a particle averaged deposition coefficient. Since columnar and planar crystals have  
172 very different deposition coefficients for each crystal facet, more complex crystals may also be  
173 amenable to treatment with an average deposition coefficient. Indeed, Pokrifka et al. (2020) found  
174 that particle-average deposition coefficients characterized most of the growth of small ice crystals  
175 at temperatures below  $-40^{\circ}\text{C}$ .

#### 176 *a. Closed-Form Approximation of the Deposition Coefficient*

177 Calculating the deposition coefficients requires the surface supersaturation ( $s_{surf}$ ) for each crys-  
178 tal axis (Eq. 1), however  $s_{surf}$  also depends on the gas-phase vapor diffusion rate. Consequently,  
179  $s_{surf}$  for each crystal axis depends strongly on  $\alpha$  (see Zhang and Harrington 2014, their Eq. 9).  
180 The problem is transcendental, requiring numerical solutions that are too costly for use in model  
181 parameterizations (Zhang 2012). It is therefore imperative to develop an approximate, yet accurate  
182 method to solve for  $s_{surf}$  in closed-form.

183 The strong sensitivity of  $\alpha$  to  $s_{surf}$  is demonstrated in Fig. 1 by solving Eq. 9 of Zhang and  
184 Harrington (2014) for a planar crystal with an aspect ratio of five, and an  $a$ -axis semi-length of  
185  $86\ \mu\text{m}$  that is growing by step nucleation ( $M = 10$ ) at a temperature of  $-15^{\circ}\text{C}$  and a pressure of  
186  $500\ \text{hPa}$ . When the ambient supersaturation ( $s_i$ ) is low, step nucleation is inhibited and the surface  
187 supersaturation is nearly identical to the ambient value. As the ambient supersaturation rises,  
188 growth by step nucleation commences thus keeping  $s_{surf}$  near  $s_{char}$ . The surface supersaturation  
189 rises slowly with further increases in  $s_i$  because increasing growth, through substantially rising  
190 deposition coefficients, keeps  $s_{surf}$  low. The rise in  $s_{surf}$  again becomes commensurate with  $s_i$  once  
191  $\alpha$  reaches unity, however, this occurs at supersaturations that are not realized in the atmosphere.  
192 The strong sensitivity of  $\alpha$  to changes in  $s_{surf}$  indicates why a closed-form parameterization of  
193  $\alpha$  is difficult to achieve: Calculating the deposition coefficient requires a quantitative method to

194 relate  $s_{surf}$  to the ambient supersaturation for particles of any shape and size, though the equations  
 195 for  $\alpha$  are extremely sensitive to any change in  $s_{surf}$ . On the other hand, the results shown in Fig. 1  
 196 provide a hint for developing a closed-form parametrization: The variation of  $s_{surf}$  with  $s_i$  has a  
 197 similar functional form for both the a- and c-axes, suggesting that a scaling law may exist that  
 198 relates the two quantities. Moreover, the form of the equation for  $\alpha$  itself (Eq. 1) suggests seeking  
 199 scaling laws that exploit ratios of a measure of supersaturation with  $s_{char}$ .

200 Since our approach is empirical, we tested a number of different scaling relationships to calculate  
 201  $s_{surf}$ . Since  $s_{surf}$  for each axis depends on  $\alpha$  itself, one possibility is to simply set  $\alpha$  to unity in the  
 202 equations for  $s_{surf}$  for each axis, and to scale the resulting equation with  $s_{char}$ . Rearranging Eq. 9  
 203 of Zhang and Harrington (2014) and setting  $\alpha$  to unity for the a and c axes gives,

$$\begin{aligned}
 204 \quad s_{diff,a} &= s_i \frac{1}{1+L_a} & \text{where} & \quad L_a = \frac{ac}{C_{\Delta}(c,a)} \frac{\bar{v}_v}{4D_v}, \\
 205 \quad s_{diff,c} &= s_i \frac{1}{1+L_c} & \text{where} & \quad L_c = \frac{a^2}{C_{\Delta}(c,a)} \frac{\bar{v}_v}{4D_v}, \tag{5}
 \end{aligned}$$

206 In the above equation,  $s_i$  is the ambient supersaturation,  $D_v$  is the vapor diffusivity in air,  $\bar{v}_v$  is the  
 207 mean speed of a vapor molecule,  $L_a$  and  $L_c$  are unitless quantities that depend on the crystal geom-  
 208 etry, and  $C_{\Delta}(c,a)$  is the capacitance evaluated one mean free path from the surface. The quantities  
 209  $s_{diff,a}$  and  $s_{diff,c}$  are the surface supersaturations over the  $a$  and  $c$  axes when  $\alpha_a$  and  $\alpha_c$  are unity,  
 210 and we therefore define these as *diffusion-limited* surface supersaturations. Our empirical testing  
 211 showed that, over a relatively large range of ambient supersaturations, the surface supersaturation  
 212 scales with  $s_{char}/s_{diff}$  for a given axis. The form of that dependence can be well approximated  
 213 with a power-law,

$$214 \quad s_{surf} \sim s_{pwr} \equiv s_{diff} \left( \frac{s_{char}}{s_{diff}} \right)^{\beta} = s_{diff}^{1-\beta} \cdot s_{char}^{\beta}, \tag{6}$$

215 where the exponent,  $\beta$ , can be found by fitting to the exact calculation (Fig. 2). Simulations that  
 216 we conducted indicate that the value of  $\beta$  is relatively insensitive to the size and aspect ratio of the

217 crystal. This result may be due to the inclusion of length and aspect ratio information through the  
 218 variables  $L_a$  and  $L_c$ . This makes the above equations ideal for parameterization development.

219 The above approximation increasingly deviates from the actual surface supersaturation when  
 220 approaching the low and high  $s_i$  limits, and therefore must be corrected. As  $s_i$  rises  $\alpha$  eventually  
 221 reaches unity and the surface supersaturation begins to climb away from the approximate value  
 222 ( $a$ -axis in Fig. 2). As the supersaturation declines and  $s_{char}$  is approached, surface kinetics begin  
 223 to dominate the growth process and  $s_{surf}$  declines rapidly, eventually becoming the same as the  
 224 ambient supersaturation (blue dashed lines on Fig. 2). In order to correct the approximation for  
 225 these limits, we first correct for the low supersaturation limit by taking the minimum between  $s_{pwr}$   
 226 and  $s_i$ ,

$$227 \quad s_{lim} = \min(s_{pwr}, s_i). \quad (7)$$

228 This limited form of the power-law approximation deviates from the actual surface supersaturation  
 229 only in the vicinity of  $s_{char}$  and at high supersaturations; these deviations are indicated by dashed  
 230 circles on Fig. 2. The deviation of  $s_{lim}$  from  $s_{char}$  in these regions, which we call residuals, have  
 231 consistent behavior that depends fundamentally on the ratio of  $s_{diff}/s_{char}$ , as is shown by the black  
 232 lines in Fig. 3. The size and aspect ratio dependence of the residuals occurs because of the length-  
 233 scales,  $L_a$  and  $L_c$ , that define  $s_{diff}/s_{char}$ . The maximum value reached by the residuals does not  
 234 vary with the size or aspect ratio of the crystal (not shown). We fit the residuals as a function of  
 235 the  $s_{diff}/s_{surf}$ , so that the parameterization becomes,

$$236 \quad \frac{s_{diff}}{s_{surf}} \approx \frac{s_{diff}}{s_{lim}} + R_l - R_u, \quad (8)$$

237 where  $R_l$  and  $R_u$  are the residuals shown in Fig. 3. Note that the sign of  $R_l$  and  $R_u$  differ because  
 238 the absolute value of the residual is plotted in the figure. Both residuals can be well approximated

239 with a similar power-law form that convolves rising and decaying functions,

$$\begin{aligned}
 240 \quad R_l &= R_{max,l} \left( \frac{s_{diff}}{s_{pwr}} \right) \left( \frac{s_i}{s_{pwr}} \right)^{p1} \min \left[ \left( \frac{s_i}{s_{pwr}} \right)^{p2}, 1 \right], \\
 241 \quad R_u &= R_{max,u} \left( \frac{s_{diff}}{s_{pwr}} \right) \left( \frac{s_{diff}}{s_{lim}} \right)^{n1} \left( \max \left[ 0, \frac{s_{diff}}{s_{lim}} - 1 \right] + 1 \right)^{n2}. \quad (9)
 \end{aligned}$$

242 The results shown in Fig. 3 indicate that the maximum in each residual curve,  $R_{max,l}$  and  $R_{max,u}$ , is  
 243 nearly constant, which we assume. The power-law exponents,  $p1$ ,  $p2$ ,  $n1$ , and  $n2$ , are determined  
 244 by least-squares fitting. Examples of the residual fits for the  $a$ -axis of a planar crystal with an  
 245 aspect ratio of 0.1 are shown by the blue dashed lines in Fig. 3. While the fit is not perfect, the  
 246 small deviation from the actual curves produces very low errors in the modeled growth rates (see  
 247 below). The surface supersaturation for a given axis can now be calculated approximately by  
 248 rearranging Eq. 8,

$$249 \quad s_{surf} \approx \frac{s_{diff}}{s_{diff}/s_{lim} + R_l - R_u}. \quad (10)$$

250 Each term in the above equation can be calculated based on the ambient temperature, pressure, su-  
 251 persaturation, and crystal axis length since the crystal geometry enters into the calculation through  
 252  $s_{diff}$ . This equation provides an approximate closed-form solution to the calculation of  $s_{surf}$  and,  
 253 therefore, the deposition coefficients (Eq. 1), for each crystal axis.

254 An advantage of the above approach for calculating  $s_{surf}$  is that the main fitting coefficients  
 255 ( $\beta$ ,  $R_{max,l}$ ,  $R_{max,u}$ ,  $p1$ ,  $p2$ ,  $n1$ , and  $n2$ ) do not depend on crystal size or geometry. However, the  
 256 approximation does depend on the growth mechanism through the parameter  $M$  in Eq. 1. We  
 257 therefore repeated the above fitting procedure using integer values of  $M$  ranging between unity  
 258 (dislocation growth) and 15. Naturally, the fitting coefficients change substantially with different  
 259 values of  $M$ , however the behavior of the coefficients themselves is regular and can be fit with up  
 260 to a tenth-order polynomial in  $M$  (Fig. 4). The coefficient values for Eqs. 6 and 9, along with the

261 polynomial fits to the coefficients, and code to compute  $s_{surf}$  are available from a data archive (see  
262 our data statement).

### 263 *b. Single-Particle Tests of the Deposition Coefficient Approximation*

264 In order to test the accuracy of the  $\alpha$  approximation described above, a large number of simula-  
265 tions were conducted against accurate benchmark calculations with the iterative solution method  
266 used by Zhang and Harrington (2014). Simulations were done for individual crystals covering a  
267 wide range of temperatures (0 to  $-40^{\circ}\text{C}$ ), pressures (1000 to 100 hPa), and supersaturations (near  
268 0% to liquid saturation). We conducted simulations using initially spherical crystals with a ra-  
269 dius of  $10\ \mu\text{m}$ , and the crystals grew for a time ranging from 5 to 30 minutes. In general, the  
270 approximate calculation of  $\alpha$  produces accurate solutions to the mass and axis ratio evolution. For  
271 example, it is not possible to visually distinguish between the approximate and accurate solutions  
272 for the  $a$  and  $c$  axes of crystals grown for 10 minutes over a range of ambient supersaturations at  
273 a temperature of  $-15^{\circ}\text{C}$  and a pressure of 500 hPa in Fig. 5. The level of accuracy is high regard-  
274 less of whether the crystals grow by step nucleation ( $M = 10$ ), which has a strong supersaturation  
275 dependence to the deposition coefficient, or a more efficient mechanism with  $M = 3$  or  $M = 1$   
276 (dislocations). This accuracy is due entirely to the prediction of the deposition coefficients, as  
277 shown in Fig. 6. Relative errors of around 10% can occur for the minor crystal axis as  $\alpha$  decreases  
278 with supersaturation (yellow and red curves, Fig. 6a), however these errors have only a small influ-  
279 ence on the minor axis growth rate. The accuracy in the estimates of the deposition coefficients is  
280 due, primarily, to the accuracy in the calculation of  $s_{surf}$ , as is clearly shown in Fig. 6b using step  
281 nucleation as an example: The surface supersaturation calculated with the approximation remains  
282 near the ambient value until  $s_i$  approaches the characteristic value. At this stage, step nucleation  
283 begins and  $s_{surf}$  decreases due to vapor uptake at the crystal surface. Further increases in  $s_i$  cause

284 a slow rise in  $s_{surf}$  since step nucleation increases, thus increasing the vapor uptake rate and the  
285 deposition coefficient.

286 The aspect ratios of single crystals are strongly dependent on temperature, and the approximate  
287 model of the deposition coefficients captures this dependence (Fig. 7). These simulations show  
288 the  $a$ - and  $c$ -axis lengths and deposition coefficients after 10 minutes of growth using dislocations  
289 ( $M = 1$ ) and step nucleation ( $M=10$ ). Each simulation was conducted at a constant temperature (-2  
290 to -40°C), a pressure of 500 hPa, and a relatively low supersaturation (5% of liquid saturation).  
291 A low supersaturation was used because errors are largest when the supersaturation is low. The  
292 simulations show that the crystal  $a$  and  $c$  axes after 10 minutes of growth are well captured by  
293 the approximate model for both dislocation and step nucleation growth. Small deviations (relative  
294 errors less than 6%) appear in the axis lengths after 10 minutes of growth when step nucleation  
295 growth is assumed. The approximate model also captures the cessation of axis growth when  $s_{surf}$   
296 falls substantially below  $s_{char}$  for a given axis length (at temperatures below -12.5°C for the  $c$ -axis  
297 and below -19°C for the  $a$ -axis). Indeed, at temperatures below -20°C crystal growth is effectively  
298 suppressed at the supersaturations used in these calculations, since the  $s_{char}$  are substantially larger  
299 than  $s_{surf}$  (not shown). Note that the cessation of dimensional growth has been observed in the  
300 laboratory (Nelson and Knight 1998; Magee et al. 2014) and may be responsible for extremely thin  
301 crystals that are sometimes observed (Jensen et al. 2008). The errors shown in these calculations  
302 are representative of the approximate form of  $s_{surf}$  across a wide range of temperatures, pressures,  
303 and supersaturations. In order to illustrate the degree to which attachment kinetics affect the  
304 growth rates, calculations using the Chen and Lamb (1994) adaptive-habit method are also shown.  
305 The adaptive habit method assumes that growth is diffusion-limited, leading to much stronger  
306 growth of the  $a$ - and  $c$ -axes, and to generally thinner crystals.

### 307 **3. Deposition Coefficient Parameterization**

308 Given the accuracy of the approximate form of  $\alpha$ , we next develop parameterizations for bin and  
309 bulk microphysical models. Eulerian bin microphysical parameterization is relatively straightfor-  
310 ward given that bin widths are narrow enough to perform deposition coefficient calculations using  
311 the bin-average crystal dimensions. Bulk parameterization requires a different approach since the  
312 growth rates are integrated analytically across a wide range of crystal dimensions. We discuss each  
313 parameterization in turn and then describe tests of the parameterizations against a Lagrangian bin  
314 microphysical model.

#### 315 *a. Bin Microphysical Model Parameterization*

316 Eulerian bin microphysical modeling is computationally costly, but has the advantage that no  
317 assumptions are made about the shape of the size distribution. However, Eulerian bin models do  
318 suffer from numerical problems such as artificial distribution broadening caused by numerical dif-  
319 fusion on the Eulerian mass grid, and on the spatial grid in Eulerian cloud models (Morrison et al.  
320 2018) though this latter effect appears to be small in some cases (Pardo et al. 2020). The Eulerian  
321 bin microphysical framework from our prior work (e.g. Harrington et al. 1999) is expanded here to  
322 use variable deposition coefficients, and to predict two axis lengths and an effective density con-  
323 sistent with the approach of Harrington et al. (2013). The bin model uses the method-of-moments  
324 approach for mixed-phase microphysics (Reisin et al. 1996) and predicts the number and mass  
325 mixing ratio for each of 35 Eulerian size bins, with bin edges defined by mass doubling. The 35  
326 bins span an equivalent volume diameter range of 3 to 4030  $\mu\text{m}$ , which is sufficient for the growth  
327 processes modeled here.

328 The transport of number and mass mixing ratio among bins is treated in a semi-Lagrangian  
329 sense following the “top-hat” method advocated by Stevens et al. (1996). The top-hat method

330 for growth and the remapping of the particle properties among bins assumes that the distribution  
 331 is flat within a bin (Fig. 8). The lower and upper mass edges ( $m_l(t)$  and  $m_u(t)$ , respectively)  
 332 of the top-hat are defined following the procedure in Stevens et al. (1996), and the new mass  
 333 edges at the end of a time-step ( $m_l(t + \Delta t)$  and  $m_u(t + \Delta t)$ ) are determined from the solution to  
 334 the growth equation. Though the capacitance and the deposition coefficients vary with the crystal  
 335 dimensions, the growth equation can be integrated forward in time with relatively low error using  
 336 some simplifying approximations (Chen 1992; Harrington et al. 2019): If the time-step is less than  
 337 about 20 seconds, Eq. 2 can be integrated assuming an equivalent volume sphere (radius  $r_{eq}$ ) with  
 338 the shape factor ( $q_{eq} = C(a, c)/r_{eq}$ ), particle effective density ( $\rho_p$ ), and the effective diffusivity  
 339 ( $D_{eff}$ ) assumed constant over the time-step ( $\Delta t$ ),

$$340 \quad m(t + \Delta t) = \left[ m(t)^{2/3} + \frac{8 \pi \alpha_v q_{eq} D_{eff} \rho_{eq} \bar{s}_i \Delta t}{3 \rho_p^{1/3}} \right]^{3/2}, \quad (11)$$

341 where  $\alpha_v = [3/(4\pi)]^{1/3}$  originates from the definition of the equivalent volume spherical mass  
 342 ( $m = 4/3\pi r_{eq}^3 \rho_p$ ). The deposition coefficients are computed using the average  $a$ - and  $c$ -axes for  
 343 a given bin. This equation (Eq. 11) is similar to Eq. A2 in Stevens et al. (1996) except that  
 344 the integral forcing term  $\tau$  is written as the time-step averaged supersaturation,  $\bar{s}_i$ . The time-step  
 345 averaged supersaturation is computed from the supersaturation forcing equation following Wu  
 346 (1999). The method is the same as that of Stevens et al. (1996) and mass closure is enforced  
 347 (Tzivion et al. 1989), thus ensuring mass conservation.

348 Equation 11 is used to evolve the top-hat mass edges in time, and remap distribution properties  
 349 among the bins. In the example shown in Fig. 8, the resulting growth causes the top-hat distribu-  
 350 tion to straddle two bins. The number concentration within bin- $k$  ( $N_k$ ) is redistributed based on the  
 351 fractional area of the top-hat that resides within a given bin while preserving the total concentra-



352 tion,

$$353 \quad N_k = \frac{1}{\Delta m} \int_{m_l}^{m_u} N_k dm = \frac{1}{\Delta m} \int_{m_l}^{m_{k+1}} N_k dm + \frac{1}{\Delta m} \int_{m_{k+1}}^{m_u} N_k dm = N_k \frac{m_{k+1} - m_l}{\Delta m} + N_k \frac{m_u - m_{k+1}}{\Delta m}, \quad (12)$$

354 where  $\Delta m = m_u - m_l$  and  $m_u$  and  $m_l$  are the values at the end of the time-step. The right-most  
 355 term in the equation above represents the concentration that is remapped to the next bin (shown  
 356 as the blue shaded region in Fig. 8) whereas the left-most term represents the concentration that  
 357 remains in the original bin (unshaded region). This approach is also applied to the mass moment,  
 358 thus conserving mass during vapor growth.

359 Predicting a second axis length and effective density requires transporting information on aspect  
 360 ratio and volume as well as number and mass. Jensen et al. (2017) showed that aspect ratio and  
 361 effective density can be tracked accurately on the spatial grid of an Eulerian cloud model if mixing  
 362 ratios of total volume and total volume times aspect ratio are conserved. We follow this approach  
 363 here and conserve the moments,

$$364 \quad \begin{aligned} V_k &= \frac{1}{\Delta m} \int_{m_l}^{m_u} N_k V dm \simeq \frac{1}{\bar{\rho}_p \Delta m} \int_{m_l}^{m_u} N_k m dm \\ \Phi_k &= \frac{1}{\Delta m} \int_{m_l}^{m_u} N_k V \phi dm \simeq \frac{\bar{\phi}}{\bar{\rho}_p \Delta m} \int_{m_l}^{m_u} N_k m dm \end{aligned} \quad (13)$$

366 where  $V_k$  and  $\Phi_k$  are the total volume and total volume times aspect ratio in bin- $k$ . General analyt-  
 367 ical expressions for the co-variation of the effective density and aspect ratio with size do not exist,  
 368 and we therefore use bin-averaged quantities ( $\bar{\rho}_p$  and  $\bar{\phi}$ ). This approximation allows us to write  
 369 the volume as  $V = m/\bar{\rho}_p$ , and therefore the above moment equations reduce to variations of the  
 370 mass-moment, which are shown as the right-most equations (Eq. 13). This approach is attractive  
 371 because the mass-moment remapping can be used for  $V_k$  and  $\Phi_k$ , however it requires estimates of  
 372  $\bar{\rho}_p$  and  $\bar{\phi}$  at the end of a time-step.

373 There are several procedures that could be invoked to estimate  $\bar{\rho}_p$  and  $\bar{\phi}$ , and each approach  
 374 has its limitations. However, testing shows that the following approach is most accurate. Since

375 the change in mass is known, we calculate the volume of the upper ( $V_u$ ) and lower ( $V_l$ ) top-hat  
 376 mass edges at the end of a time-step using Eq. 4. We then estimate the new particle density by  
 377 preserving the zeroth moment,  $\int_{m_l}^{m_u} N_k dm = \int_{V_l}^{V_u} N_k \bar{\rho}_p dV$  which implies that

$$378 \quad \bar{\rho}_p = \frac{m_u - m_l}{V_u - V_l}. \quad (14)$$

379 This method produces average effective densities that are higher than Lagrangian bin microphys-  
 380 ical calculations (see §4 below). However, it provides a better overall match with the ice water  
 381 content, axis lengths, and fall-speed, quantities that are arguably more critical to capture accu-  
 382 rately. Finally, we can use the change in the average volume to estimate the change in the average  
 383 aspect ratio directly from Eq. 3 by assuming that the ratio  $\Gamma/\phi$  is constant over a typical time-step  
 384 (less than 20 s), which is usually a good approximation.

### 385 *b. Bulk Microphysical Model Parameterization*

386 Treating variable deposition coefficients in a bulk microphysical model is less straightforward,  
 387 since the deposition coefficients vary considerably across the size distribution. Nevertheless, our  
 388 prior work shows that it is possible to accurately parameterize the influences of constant deposition  
 389 coefficients (Harrington et al. 2009). In this section, we use this approach to extend the adaptive  
 390 habit parameterization of Harrington et al. (2013) and Jensen et al. (2017) so that it is consistent  
 391 with variable deposition coefficients. We also provide an approach for the general use of variable  
 392 deposition coefficients in any bulk model.

393 Including variable deposition coefficients in a bulk model ultimately involves approximating the  
 394 integrated mass growth rate, which gives the change in the ice mixing ratio ( $q_i$ ) in time,

$$395 \quad \frac{dq_i}{dt} = \frac{1}{\rho_a} \int_0^\infty \frac{dm(a)}{dt} n(a) da \quad (15)$$

396 where  $\rho_a$  is the air density, the mass is a function of a length-scale ( $a$ ), and  $n(a)$  is the gamma  
397 distribution. The length scale we use here is the a-axis length of a spheroid as defined in Harring-  
398 ton et al. (2013). This integral cannot be solved analytically for variable deposition coefficients  
399 because the effective diffusivity ( $D_{eff}$ ) varies with size. Harrington et al. (2009) showed that when  
400 the deposition coefficient is constant, the above integral can be approximated accurately if  $D_{eff}$  is  
401 calculated at an appropriate “kinetic” length-scale. Zhang (2012) showed that this approach can  
402 be extended to variable deposition coefficients if the ratio of the second and first moments of the  
403 distribution are used to define the kinetic length scales for the a- and c-axes,

$$404 \quad a_{kin} \equiv \frac{\int_0^\infty a^2 n(a) da}{\int_0^\infty a n(a) da} = a_n \frac{\Gamma(\nu + 2)}{\Gamma(\nu + 1)} \quad \text{and} \quad c_{kin} \equiv c_n \frac{\Gamma(\nu + 2)}{\Gamma(\nu + 1)}. \quad (16)$$

405 In the above equation,  $\nu$  is the distribution shape and the characteristic length scale  $a_n$  is used  
406 in the gamma distribution definition. Both  $a_n$  and  $c_n$  are directly related to the number-weighted  
407 mean a- and c-axis lengths (for details see Harrington et al. 2013). The kinetic length-scales  
408 are used to calculate representative values of the deposition coefficients ( $\overline{\alpha_a}$  and  $\overline{\alpha_c}$ ), which are  
409 then used to calculate a representative value of  $\overline{D_{eff}} \equiv D_{eff}(\overline{\alpha_a}, \overline{\alpha_c}, a_{kin}, c_{kin}, T, P)$ . When these  
410 approximations are used in Eq. 2 they allow us to write Eq. 15 as,

$$411 \quad \frac{dq_i}{dt} \simeq \frac{N_i}{\rho_a} 4\pi \overline{C} \overline{D_{eff}} \rho_{eq} s_i, \quad (17)$$

412 where  $N_i$  is the ice concentration and  $\overline{C}$  is the distribution-averaged capacitance. The above equa-  
413 tion allows us to calculate changes in ice mass mixing ratio subject to the influences of variable  
414 deposition coefficients, and it should be generally applicable since the form is nearly identical to  
415 that used in most bulk microphysical schemes. In addition to using  $\overline{\alpha_a}$  and  $\overline{\alpha_c}$  in  $D_{eff}$  to estimate  
416 the overall effects of surface kinetics on mass growth, we also use these values in Eq. 3 to evolve  
417 the average a- and c-axis lengths following the procedure in Harrington et al. (2013). These mod-  
418 ifications make the bulk adaptive habit microphysical model (Harrington et al. 2013; Jensen et al.

419 2017) consistent with faceted growth and variable deposition coefficients. In the next section, both  
420 the Eulerian bin and bulk habit models are tested against Lagrangian bin microphysics.

#### 421 **4. Parcel Model Testing against Lagrangian Microphysics**

422 The parameterizations are implemented into a parcel model framework (Sulia and Harrington  
423 2011) and are tested against a Lagrangian bin microphysical model that includes variable depo-  
424 sition coefficients (Zhang and Harrington 2015). Parcel models are idealized in that only parcel  
425 lifting at either a constant or sinusoidally varying updraft speed is used to provide the supersatu-  
426 ration forcing. No mixing with the environment occurs, and all of the hydrometeors move with  
427 the parcel. However, the idealized nature of parcel models makes them useful for testing micro-  
428 physical schemes since complicating processes (such as mixing and sedimentation) are ignored.  
429 The influence of growth processes alone can therefore be isolated, and biases and errors are easier  
430 to detect. The parcel model used here (described fully in Zhang and Harrington 2015) solves dif-  
431 ferential equations for the temperature, pressure, height, and total water mixing ratio, along with  
432 the microphysical equations. The Lagrangian bin microphysics is configured with 100 ice crystal  
433 bins for which the a- and c-axes, mass, and effective density are tracked. Since the growth of  
434 each bin is followed explicitly, the Lagrangian model results are used as the benchmark against  
435 which the Eulerian bin and bulk solutions are tested. The parcel model in each case is run for 4000  
436 seconds and initialized with a constant updraft speed, initial temperature, and initial pressure that  
437 varies for each simulation (described below). The initial relative humidity with respect to liquid  
438 for all simulations is 0.95, and this allows us to explore diffusion and kinetics-limited growth in  
439 a single simulation: High supersaturations and  $\alpha$  are produced early in the simulations, whereas  
440 low supersaturations and  $\alpha$  occur later in the simulations. Liquid water is not included in the sim-  
441 ulations and ice is nucleated instantaneously at the first time-step, which removes complications

442 that mixed-phase processes and nucleation feedbacks introduce. The instantaneously nucleated  
443 ice is spherical with an average initial radius of  $10 \mu\text{m}$  for all the models. This initial ice spectrum  
444 is distributed over the the bins of the Lagrangian and Eulerian models during the first time-step  
445 using a gamma distribution with a shape of  $\nu = 4$ . Note that the results are not highly sensitive  
446 to the assumed shape of the initial ice spectrum. A distribution shape of  $\nu = 5$  is prescribed for  
447 the bulk model because this value produces the best match with the Lagrangian simulations, and  
448 therefore provides an estimate of the minimum error associated with the parameterization. Depo-  
449 sition coefficients in all models are predicted with the parameterization described above using step  
450 nucleation ( $M = 10$ ) for two reasons: First, the development of crystal habits is thought to be due  
451 to step-nucleation mediated growth (Frank 1982). Second, step nucleation is the most error-prone  
452 growth process to model due to the strong supersaturation dependence of  $\alpha$ .

453 Parcel model simulations were conducted for a range of constant vertical motions (from 0.1 to  
454  $1 \text{ m s}^{-1}$ ), a range of initial temperatures from  $-4$  to  $-45 \text{ }^\circ\text{C}$ , and a range of ice concentrations from  
455 10 to  $500 \text{ L}^{-1}$ . Vertical motion primarily alters the supersaturation forcing term, and since errors  
456 tended to be somewhat larger at lower vertical motions we only show results for a fixed vertical  
457 motion of  $0.25 \text{ m s}^{-1}$ . In the analyses presented below, we first provide time-series results from  
458 a selected set of simulations that are representative of the ensemble of simulations. These results  
459 are followed by analyses of simulation-averaged results over a range of initial temperatures, which  
460 provide a broader picture of the parameterization accuracy.

#### 461 *a. Time-series Results*

462 Time-series results for two sets of simulations conducted at high ( $-15^\circ\text{C}$  and 850 hPa) and low  
463 ( $-45^\circ\text{C}$  and 300 hPa) respective initial temperatures and pressures are shown in Fig. 9. For these  
464 simulations,  $s_{char}$  and  $\rho_{dep}$  were held constant at their initial values so that temperature feedbacks

465 to the growth through  $\alpha$  and the density do not occur. Consequently, any errors that appear should  
466 be due primarily to the evolution of the particle axis lengths. The constancy of  $s_{char}$  and  $\rho_{dep}$  is  
467 relaxed in the next subsection.

468 For all of the simulations (Fig. 9a), the supersaturation rises and then declines depending on  
469 when ice crystal growth dominates over the supersaturation production caused by vertical lifting.  
470 At  $-15^{\circ}\text{C}$  and a concentration of  $10\text{ L}^{-1}$  the supersaturation rises above that of liquid, but as  
471 noted above we have neglected liquid-phase microphysics. Note that both the Eulerian bin and the  
472 bulk microphysical schemes capture the supersaturation evolution, though it is over-estimated in  
473 the bulk model, and under-estimated in the Eulerian bin model. This result illustrates the reason  
474 we ignored liquid-phase microphysics for these simulations: Not only does liquid-phase micro-  
475 physics introduce another complicating process, but liquid-phase microphysics would limit the  
476 supersaturation rise and therefore may not expose differences in model performance. Note that the  
477 supersaturation predicted by the Eulerian bin model is nearly identical to the Lagrangian solution  
478 at the higher ice concentration, however the bulk model prediction remains slightly high.

479 The ice water content (Fig. 9b) rises continuously with time, but begins to asymptote as the  
480 supersaturation approaches steady-state. This is well predicted by both the Eulerian bin and the  
481 bulk models, though there are small differences that are difficult to discern in the figure: Since  
482 the bulk model over-predicts the supersaturation, it tends to slightly under-predict the ice water  
483 content (since total mass is conserved). The semi-axis lengths averaged over the size distribu-  
484 tions (Fig. 9c and d) are consistent with the behavior expected at each temperature. At  $-15^{\circ}\text{C}$  the  
485 average major semi-axis length (a-axis) increases rapidly reaching nearly  $800\ \mu\text{m}$  when the con-  
486 centration is low ( $10\text{ L}^{-1}$ ) whereas the minor semi-axis (c-axis) remains small. This growth is  
487 consistent with planar dendrites, and it is dependent on the ice concentration. The reason for the  
488 concentration dependence is the lack of a liquid phase: Including a liquid-phase would keep the

489 supersaturation near that of liquid saturation, thus constraining the growth and limiting the ice  
490 concentration dependence. At  $-45^{\circ}\text{C}$  columnar crystals are produced with much smaller major  
491 semi-axis dimensions (up to  $150\ \mu\text{m}$ ) than crystals grown at the higher temperature. The Eulerian  
492 bin and bulk models capture the evolution of the average major semi-axis length with relatively  
493 high accuracy. The average minor semi-axis, in contrast, is only well-predicted by the Eulerian  
494 bin model. The bulk microphysical model either over- or under-predicts this axis length by 14%  
495 at  $-15^{\circ}\text{C}$  and 30% at  $-45^{\circ}\text{C}$ .

496 While the distribution shape is fixed in the bulk microphysical model, it varies with time in the  
497 Eulerian and Lagrangian bin models. The Lagrangian bin model produces a rapid narrowing of  
498 the crystal size spectrum (Fig. 10), an expected result that Sheridan et al. (2009) showed is due  
499 to the faster habit development and growth of initially smaller particles. The Eulerian bin model  
500 captures the evolution of the distributions for both axis lengths in that the distribution mode is  
501 relatively well predicted. The a-axis distribution appreciably narrows similarly to the Lagrangian  
502 model, however the c-axis distribution width remains broader and is skewed towards the lower  
503 end. This result is due to the use of an average aspect ratio for each bin.

504 The Eulerian bin and bulk microphysical models approximate the manner in which the deposi-  
505 tion coefficients, the effective density, and the aspect ratio are treated during growth, and some  
506 variables will thus be predicted with lower precision, a consequence that is clearly shown in  
507 Fig. 11. The effective density is relatively well predicted by the bulk microphysical model at -  
508  $15^{\circ}\text{C}$ , however it is slightly under-predicted at  $-45^{\circ}\text{C}$ . It is possible to produce a better prediction  
509 of the density at lower temperature, but doing so causes the fall speed error to become greater than  
510 the 28% relative error shown in Fig. 11c. In contrast, the average effective density predicted by the  
511 Eulerian bin model is generally too high, though the fall speeds are predicted with a relative error  
512 of less than 10%. It is possible to predict the density more accurately by using mass moment con-

513 servation instead of the zeroth moment (Eq. 14). However, doing so leads to particles with smaller  
514 a- and c-axis lengths, and fall speeds that are much lower and with larger error (over 20%). The  
515 key point is that improving the prediction of one variable will necessarily introduce errors in other  
516 variables, and we choose to minimize the error in the ice water content and fall speed. It is also  
517 worth noting that the accuracy of the Eulerian bin parameterization is not strongly dependent on  
518 bin resolution. Tests with bin spacing reduced by half and one quarter produced nearly indistin-  
519 guishable results, and so they are not included on the figures. The insensitivity to bin resolution is  
520 due to a few factors. First of all, mass doubling is used to define the bin edges, and this leads to  
521 increasing bin widths for larger crystals. Therefore, reducing the bin width has less of an effect at  
522 larger sizes. Larger crystals also have the lowest densities, and accurate predictions of both aspect  
523 ratio and density are difficult to achieve when an average density is estimated for each bin. The  
524 relative insensitivity of the parameterization to bin width is a disadvantage, in that higher accuracy  
525 cannot be attained by reasonable refinements to the bin width. However, it is also an advantage in  
526 that using smaller numbers of bins will not strongly decrease the accuracy of the scheme.

527 In contrast to the effective density and the fall speed, the distribution-averaged deposition co-  
528 efficients are relatively well predicted by each model. The deposition coefficient for the major  
529 semi-axis is always greatest, and this is expected: The surface supersaturation maximizes near  
530 regions of high curvature, such as at narrow end of a plate or a column, thus leading to larger  $\alpha$ .  
531 Note that  $\alpha$  for the major semi-axis begins above 0.1 when the supersaturation is high. Values of  
532  $\alpha$  above about 0.1 do not cause strong reductions in mass growth (Gierens et al. 2003). Growth of  
533 the major axis is therefore not strongly inhibited by surface kinetics early in the simulations, and is  
534 driven primarily by gas-phase diffusion. In contrast, the deposition coefficient for the minor axis is  
535 always below 0.1. The minor axis is therefore strongly inhibited by surface kinetics, and this is the  
536 reason that the modeled crystals develop planar and columnar shapes over time. As the simulations



537 progress, the supersaturation in each case declines and  $\alpha$  for the major axis even decreases below  
538 0.1 indicating that growth is increasingly inhibited by surface processes. The bulk and Eulerian  
539 bin models capture these transitions remarkably well, especially given the strong supersaturation  
540 dependence of step nucleation.

#### 541 *b. Simulation-Averaged Results*

542 The above time-series results are illuminating, but a broader picture of the parameterization  
543 results can be painted if we examine the various microphysical quantities, both averaged over the  
544 course of the simulations and as a function of the initial temperature. In the simulations presented  
545 below, we relax the assumption that the deposition density and the characteristic supersaturations  
546 are fixed at their initial value. Simulations are shown for initial temperatures between -4 and -  
547 40°C, a pressure of 850 hPa, and for three initial ice concentrations of 10, 50, and 500 L<sup>-1</sup>, which  
548 produces a wide range of average particle sizes and aspect ratios.

549 The simulation results show that both the Eulerian bin and bulk models predict the average ice  
550 water content trend with temperature, and with small relative errors (less than 5%) at all con-  
551 centrations and at initial temperatures below -10°C (Fig. 12a). The ice water content decreases  
552 commensurately with temperature, as expected. Note that all the models predict a local minimum  
553 in the predicted ice water content near -9°C at lower ice concentrations ( $N_i = 10 \text{ L}^{-1}$ ). The mini-  
554 mum in ice water content is due to the isometric growth of the crystals near -9°C, which is much  
555 slower than the columnar and planar growth that occur near -6 and -15°C, respectively (Sulia and  
556 Harrington 2011). This result indicates that the Eulerian bin and bulk parameterizations can cap-  
557 ture an important feature of habit-dependent growth, even though the relative error in the ice water  
558 content is larger at higher temperatures: At initial temperatures above -10°C the relative error  
559 reaches values of up to 14%.

560 The Eulerian bin and the bulk models also capture the general temperature dependence of the a-  
561 and c-axes of the crystals (Fig. 12c and d), with planar dendritic crystals that have low effective  
562 density (Fig. 12b) predicted between temperatures of -10 and -20°C, and columnar crystals pre-  
563 dicted at temperatures above -10°C. The effective density is well predicted by the bulk model at  
564 temperatures above -20°C, however the Eulerian bin model tends to over-predict the effective den-  
565 sity. These results are consistent with those of the last section, and while we could alter the model  
566 to improve the effective density, the accuracy of the ice water content and the fall speed prediction  
567 (Fig.13b) would then suffer. Though it is difficult to discern from the figure, the simulated crystals  
568 are isometric at temperatures below -30°C with relatively high effective density. As pointed out  
569 in Harrington et al. (2019), little data on  $s_{char}$  exist at temperatures below -30°C, and crystals at  
570 these temperatures are often polycrystalline. Given our limited knowledge we used a single  $s_{char}$   
571 for growth at low temperatures, leading to isometric crystals. Modeling either planar or columnar  
572 growth at low temperatures, as was done in the subsection above, requires reducing  $s_{char}$  for the  
573 major axis, though little data is available to guide such a choice.

574 The Eulerian bin model predicts the average axis evolution with a high degree of accuracy in that  
575 relative errors are less than 2%. In contrast, the bulk microphysical model tends to under-predict  
576 both average axis lengths by up to 20%. The larger error in the axis lengths is due primarily  
577 to the constant distribution shape,  $\nu$ , which fixes the spectrum with a greater breadth than that  
578 simulated by the Lagrangian and Eulerian bin models. It is possible to improve upon the accuracy  
579 with which the bulk average axis lengths are predicted by changing the distribution shape. For  
580 instance, Fig. 13a shows that distribution shapes ranging between 3 and 6 produce average axis  
581 lengths that encompass the Lagrangian model solutions. However, using much smaller or larger  
582 values of  $\nu$  then increase errors in other quantities including the ice water content (not shown) and  
583 fall speed (Fig. 13b). For instance, a value of  $\nu = 6$  produces larger average axis lengths, which

584 causes much larger fall speeds. However, at  $T < -20^\circ\text{C}$ , a smaller value of  $\nu=3$  also produces  
585 larger fall speeds even though the crystal sizes are smaller. This result is due to the increase in the  
586 effective density that occurs as  $\nu$  is reduced (not shown). A  $\nu$  value of 5 appears to produce the  
587 best prediction of both the ice water content and the fall speed as compared to the Lagrangian bin  
588 model. However, it is worth keeping in mind that these benchmark comparisons do not include  
589 processes that will naturally broaden the size spectrum, such as differential vertical advection due  
590 to sedimentation, mixing, aggregation, and ice nucleation. One could therefore argue that a smaller  
591 value of  $\nu$  may be more appropriate for simulations in Eulerian cloud models.

592 The deposition coefficient parameterization developed above is general enough for use in any  
593 bulk microphysical scheme. Harrington et al. (2019) have shown that accurate mass growth rate  
594 calculations are possible if the growth rate is evaluated using the equivalent volume spherical  
595 radius ( $r_{eq}$ ) and an average characteristic supersaturation ( $\bar{s}_{char}$ ),

$$596 \quad \frac{dq_i}{dt} \simeq \frac{N_i}{\rho_a} 4\pi \bar{r}_{eq} q_{eq} \overline{D_{eff}}[\alpha(\bar{s}_{char}), r_{eq}] \rho_{eq} s_i, \quad (18)$$

597 where  $q_{eq} = \bar{C}/r_{eq}$  is an effective shape factor, and  $\overline{D_{eff}}[\alpha(\bar{s}_{char}), r_{eq}]$  is the effective diffusivity  
598 evaluated at  $r_{eq}$  using a single  $\alpha$  calculated with the average value of  $s_{char}$ . In order to test the ac-  
599 curacy of this approximation for bulk models, the simulations shown in Fig. 12 were recomputed  
600 using Eq. 18 to calculate the mass growth only. Crystal shapes were still allowed to develop in  
601 time using the  $\bar{\alpha}_a$  and  $\bar{\alpha}_c$  values for each axis. Since the evolution of the crystal a- and c-axes  
602 is tied to changes in volume through the mass growth rate (see Eq. B26, Harrington et al. 2013),  
603 the change in crystal mass evolution will be consistent with Eq. 18. Consequently, any errors in  
604 the approximate mass growth rate should appear in the evolution of the crystal shapes and the ice  
605 water content, however, the relative errors in those quantities was always below 1%. To illustrate  
606 the low relative errors, Fig. 14 shows the simulation-averaged ice water content growth rate as a

607 function of the initial temperature. The overall mass uptake rate from the bulk model that uses a  
608 single  $\alpha$  (Eq. 18) is nearly identical to the model that predicts both  $\alpha_a$  and  $\alpha_c$ . Note that the  $\alpha$   
609 value calculated with the above approach falls between  $\alpha_a$  and  $\alpha_c$ . The value of  $\alpha$  tends to reside  
610 nearest the value for the fastest growing axis, and this makes physical sense: During either planar  
611 or columnar growth the major axis dominates the overall mass uptake by the crystals, and thus  $\alpha$   
612 for this axis will control most of the growth. These results indicate that Eq. 18 provides a use-  
613 ful approximation of the supersaturation-dependent deposition coefficient for bulk microphysical  
614 schemes.

## 615 **5. Summary and Concluding Remarks**

616 Surface attachment kinetics are often treated in numerical cloud models with a constant depo-  
617 sition coefficient. Such an approximation is only valid for a small range of conditions, and it is  
618 inappropriate for faceted crystals, including crystals with small faceted structures such as dendrites  
619 and the lacunae that occur with hollowed columns and plates. While theories for supersaturation-  
620 dependent deposition coefficients consistent with the growth of faceted ice have been available for  
621 many years, methods to connect those theories to the growth equations used in cloud models have  
622 been lacking. Moreover, the numerical procedures needed to calculate the deposition coefficients  
623 consistently with the equations for vapor growth are cumbersome and computationally costly. In  
624 this work, we provide an efficient method for calculating the deposition coefficient. This approxi-  
625 mate method produces small errors (less than 1%) relative to benchmark numerical solutions and  
626 allows for the specification of different surface growth modes, therefore providing flexibility in  
627 calculating  $\alpha$ .

628 The approximate method for calculating the deposition coefficient was parameterized for Eu-  
629 lerian bin and bulk microphysical models by making use of prior modeling methods. Parcel

630 tests of the Eulerian bin and bulk schemes indicate that both models are capable of reproducing  
631 temperature-dependent habit growth at low and high supersaturations, including the development  
632 of low density planar crystals consistent with dendrites, and narrow columnar crystals consistent  
633 with needles and hollow columns. Moreover, temperature-dependent features of the ice water con-  
634 tent, such as a minimum near a temperature of  $-9^{\circ}\text{C}$ , are reproduced by both bin and bulk models.  
635 The ice water content is generally simulated with relatively low error by both models, though  
636 errors can reach 14% at higher temperatures (above  $-6^{\circ}\text{C}$ ). Fall speeds and average axis lengths  
637 are well predicted by the Eulerian bin model (relative errors  $< 10\%$ ), however effective density is  
638 over-predicted. In contrast, the bulk model predicts the effective density with lower relative error,  
639 but produces larger errors in the average axis lengths (up to 20%). Better axis length prediction  
640 by the bulk model is possible by changing the distribution shape parameter ( $\nu$ ), however doing so  
641 can produce larger errors in the fall speed (over 20%). Using an equivalent volume radius sphere  
642 and a single deposition coefficient can reproduce the growth rates of highly anisotropic crystals,  
643 and therefore provides a method for including variable deposition coefficients in any bulk scheme.  
644 It is worth noting that the present parameterization is perhaps most easily adapted to Lagrangian  
645 super-particle schemes, where the properties of particles are tracked in a Lagrangian sense within  
646 an Eulerian spatial framework (e.g. Shima et al. 2020)

647 Even though our focus is on ice crystal growth, for completeness we point out that sublimating  
648 crystals can also be treated with the framework described in this manuscript, though with mod-  
649 ifications. Sublimation causes the crystal surface to roughen rapidly (Magee et al. 2014), and  
650 the sublimation coefficient appears to be near unity (Magee et al. 2011). Moreover, single crys-  
651 tals become spheroidal during sublimation, and their aspect ratios remain approximately constant  
652 (Nelson 1998).

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659 *Data Statement:* Data tables for the fits to the surface supersaturation, and output from from the  
660 calculations used to produce the figures are available from The Pennsylvania State University Data  
661 Commons at <https://doi.org/10.26208/f6q0-8p03>. Fortran codes to calculate the characteristic and  
662 surface supersaturation, and the deposition coefficients is also available through Data Commons  
663 at <https://doi.org/10.26208/s7de-et44>.

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## LIST OF FIGURES

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799 ambient supersaturation line is shown on the figure in blue and is labeled. The surface  
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829 three values of the growth mechanism parameter,  $M$ , of  $1$  (dislocation growth),  $3$ , and  $10$   
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832 using the approximate form of the deposition coefficient are indicated by the dashed blue  
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836 shown for three values of the growth mechanism parameter,  $M$ , of  $1$  (dislocation growth),  
837  $3$ , and  $10$  (ledge formation), which are indicated by the curves. Benchmark calculations  
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 847 a constant ambient supersaturation that is 5% of liquid saturation,  $s_i = 0.05 \times [e_s - e_i]/e_i$   
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 856 original top-hat construction in bin- $k$  is shown in red, with the lower and upper mass edges  
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 858 is used to calculate the change in the top-hat edges indicated by the black arrows ( $m_l(t + \Delta t)$   
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 860 this example, the number mixing ratio ( $N_k$ ) is then remapped to the next bin ( $k + 1$ ) using  
 861 the fraction shown by the blue shade, while the remainder (shown in white) is mapped to  
 862 the original bin. The total concentration (zeroth-moment) is conserved in this process. This  
 863 procedure is used to remap the mass, volume, and aspect ratio. . . . . 47

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 866 two different initial temperatures ( $-15^{\circ}\text{C}$ , red and black, and  $-45^{\circ}\text{C}$ , blue) and two difference  
 867 ice concentrations for the  $-15^{\circ}\text{C}$  simulation (labeled on panel a). Both simulations used a  
 868 constant updraft speed of  $0.25 \text{ m s}^{-1}$ . An initial pressure of 850 hPa (300 hPa) was assumed  
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 871 bin (solid), Eulerian bin (dashed), and bulk (circle-dashed) models are shown. . . . . 48

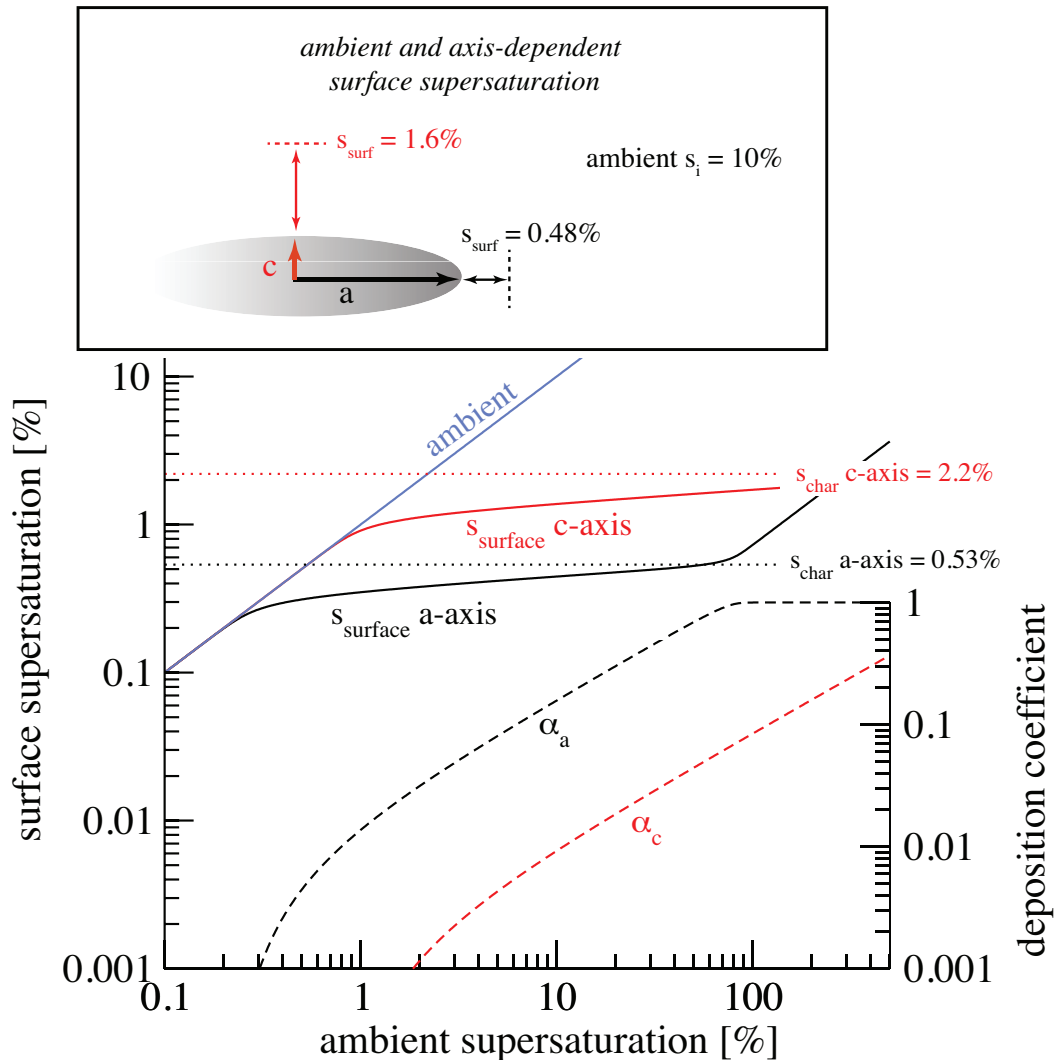
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 882 tions were conducted for two different initial temperatures ( $-15^{\circ}\text{C}$ , red and black, and  $-45^{\circ}\text{C}$ ,  
 883 blue) and two difference ice concentrations for the  $-15^{\circ}\text{C}$  simulation (labeled on panel a).  
 884 Both simulations used a constant updraft speed of  $0.25 \text{ m s}^{-1}$ . An initial pressure of 850  
 885 hPa (300 hPa) was assumed for the  $-15^{\circ}\text{C}$  ( $-45^{\circ}\text{C}$ ) simulation. Note that the major axis at  
 886  $-15^{\circ}\text{C}$  ( $-45^{\circ}\text{C}$ ) is the  $a$ -axis ( $c$ -axis). Ice crystal growth assumed step nucleation ( $M = 10$ ).  
 887 Results using the Lagrangian bin (solid), Eulerian bin (dashed), and bulk (circle-dashed)  
 888 models are shown. . . . . 50

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 893 850 hPa were used. Ice crystal growth assumed step nucleation ( $M = 10$ ). Results from the  
 894 Lagrangian bin (solid), Eulerian bin (dashed), and bulk (circle-dashed) models are shown. . . . 51

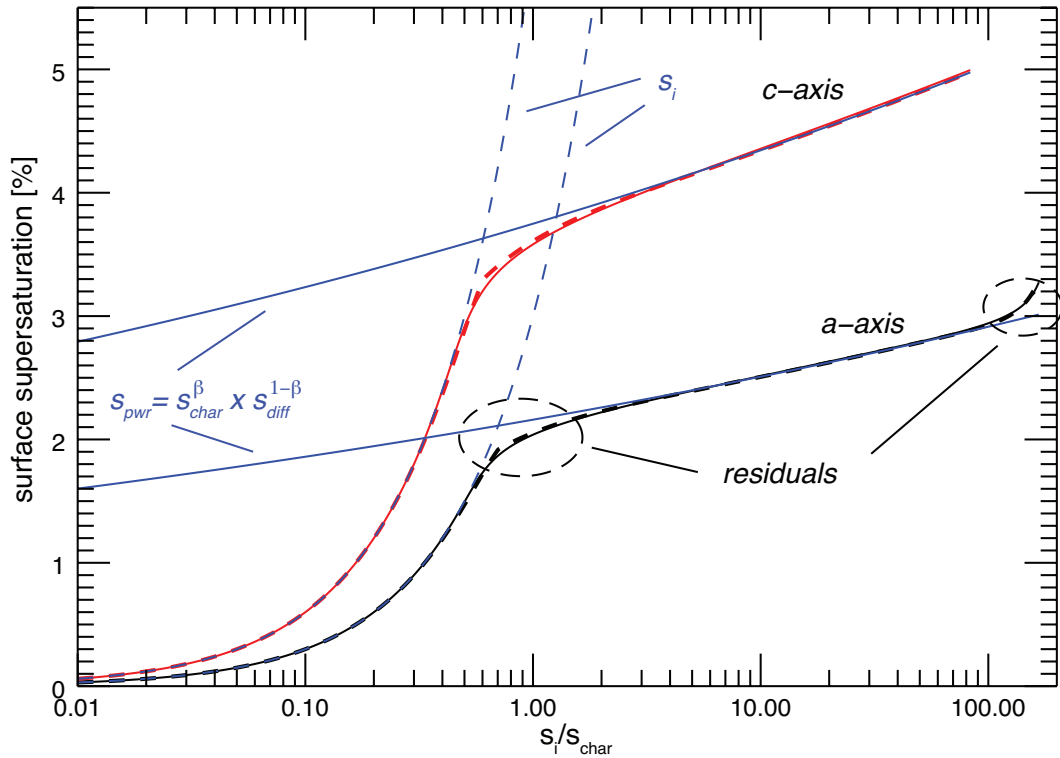
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 898 initial pressure of 850 hPa were used. Ice crystal growth assumed step nucleation ( $M = 10$ ).  
 899 Lagrangian and bulk model results are shown by the solid line and the dashed-dotted lines,  
 900 respectively. Eulerian bin model results are shown by the red dashed line for the fall speed  
 901 only. The influence of the assumed distribution shape on the axis lengths is indicated by  
 902 the long-dashed and short-dashed lines bounding the shaded regions. The bounding long-  
 903 dashed and short dashed lines used a distribution shape of  $\nu = 3$  and  $\nu = 6$ , respectively. For  
 904 reference, this is indicated for the c-axis in (a). . . . . 52

905 **Fig. 14.** Simulation and distribution average of the (a) ice water content growth rate and (b) the  
 906 deposition coefficients as a function of the initial temperature. Results are shown for bulk  
 907 model simulations using both deposition coefficients ( $\bar{\alpha}_a$  and  $\bar{\alpha}_c$ , solid lines) and bulk model  
 908 simulations using a single deposition coefficient as could be used in classical bulk models  
 909 (dashed-dotted lines). The ice water content growth rate is shown three initial ice concen-  
 910 trations of 10 (black lines), 50 (red lines), and 500 (blue lines)  $L^{-1}$ , along with a constant  
 911 updraft speed of  $0.25 \text{ m s}^{-1}$  and an initial pressure of 850 hPa. The deposition coefficients  
 912 are shown only for the simulation with an ice concentrations of  $10 L^{-1}$ . . . . . 53

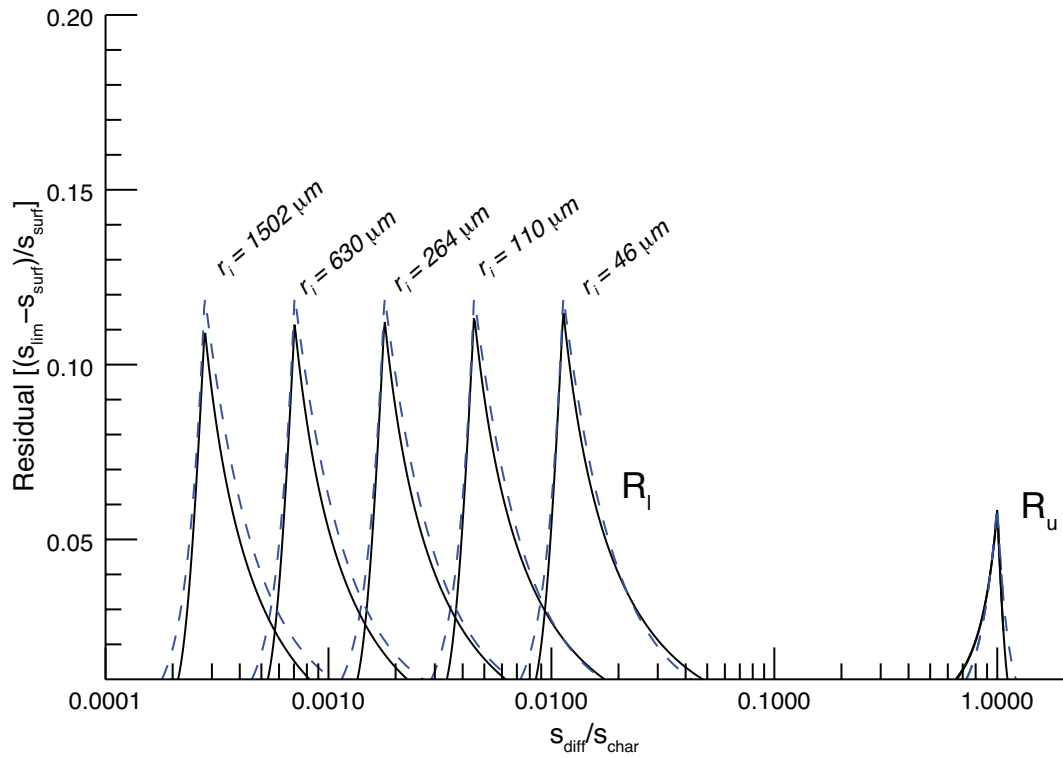


913 FIG. 1. Variation of the surface supersaturations (left axis, solid lines) and the deposition coefficients (right  
 914 axis, dashed lines) as a function of the ambient supersaturation for a crystal with an  $a$ -axis of  $86 \mu\text{m}$ , a  $c$ -axis of  
 915  $17 \mu\text{m}$ , and at  $T = -15^\circ\text{C}$ ,  $P = 500 \text{ hPa}$ . The one-to-one ambient supersaturation line is shown on the figure in  
 916 blue and is labeled. The surface supersaturation and deposition coefficient for the  $a$  and  $c$  axes are given by the  
 917 black and red curves (respectively) and are labeled on the figure. The characteristic supersaturation for each axis  
 918 is indicated by the dotted lines with  $c$ -axis  $s_{char} = 2.2\%$  (red) and  $a$ -axis  $s_{char} = 0.53\%$  (black). The cartoon at  
 919 the top illustrates the surface supersaturation for each axis (dashed line) at an ambient supersaturation of  $10\%$ .  
 920 The proximity of the dashed line to the surface indicates the degree of supersaturation ( $s_{surf}$ ).

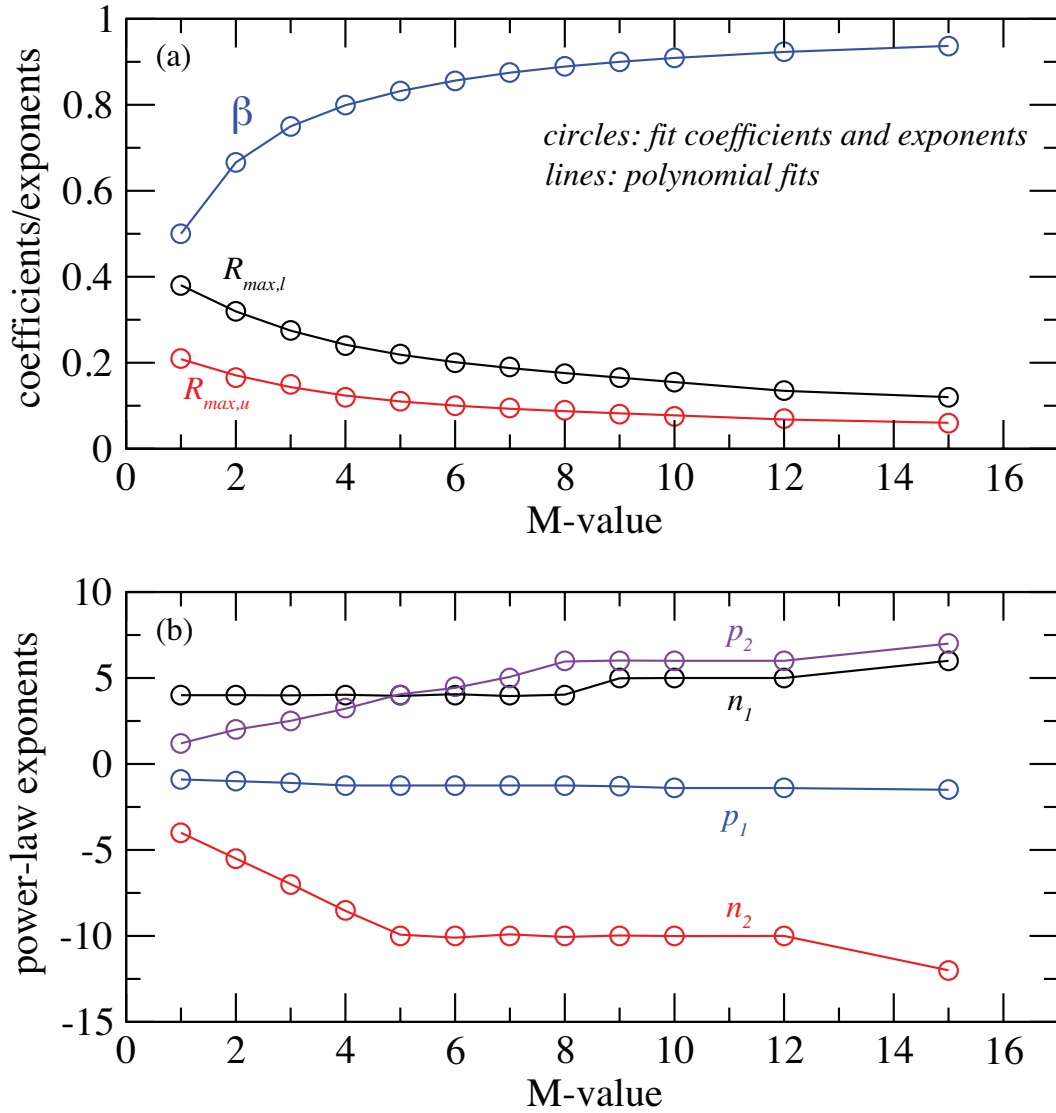




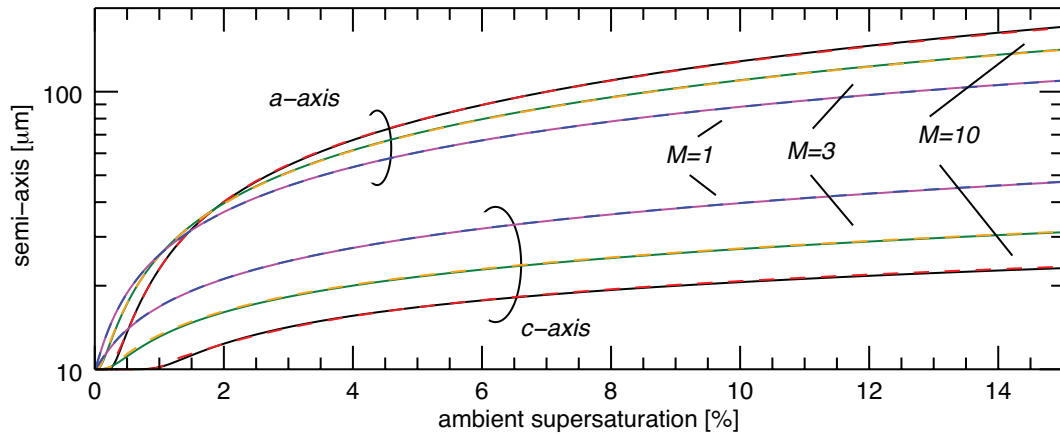
921 FIG. 2. Surface supersaturation as a function of the ratio of the ambient supersaturation to the characteristic  
 922 value ( $s_i/s_{char}$ ) for a planar crystal with an a-axis length of  $240 \mu\text{m}$ , an aspect ratio of 0.1, a temperature of  
 923  $-35^\circ\text{C}$ , and a pressure of 500 hPa. Ledge nucleation ( $M = 10$ ) was assumed with characteristic supersaturations  
 924 for the a- and c-axes of  $s_a = 3\%$  and  $s_c = 6\%$ , respectively. Exact calculation of  $s_{sfc}$  for the a- and c-axes are  
 925 shown with the solid black and red lines, respectively whereas the parameterization is shown with the dashed  
 926 lines. The ambient supersaturation is indicated by the blue dashed lines, and the power-law fit ( $s_{pwr}$ ) is given by  
 927 the solid blue lines for each axis. Deviations from the power-law fit are indicated by the black circles and labeled  
 928 residuals, using the a-axis as an example.



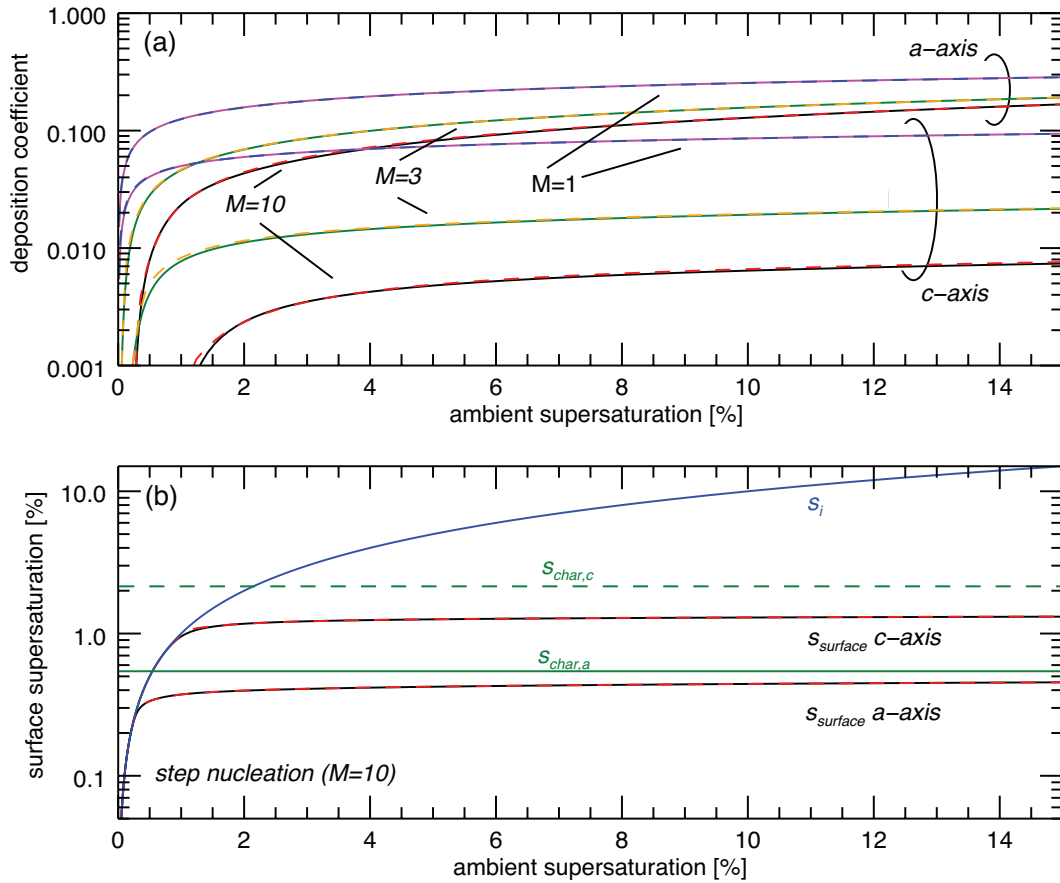
929 FIG. 3. Residuals (black lines) as a function of  $s_{diff}/s_{char}$  computed from the difference between the limited  
 930 power-law value ( $s_{lim}$ ) and the actual surface supersaturation ( $s_{surf}$ ). The residuals are given as a fractional  
 931 quantity. The temperature, pressure, growth mechanism, and aspect ratio were the same as Fig. 2. The particle  
 932 size was varied by keeping the aspect ratio constant and changing the radius of an equivalent volume sphere  
 933 ( $r_{eq}$ ). The dashed blue lines show the parameterized residuals:  $R_l$  varies implicitly with size whereas  $R_u$  is fixed  
 934 near unity.



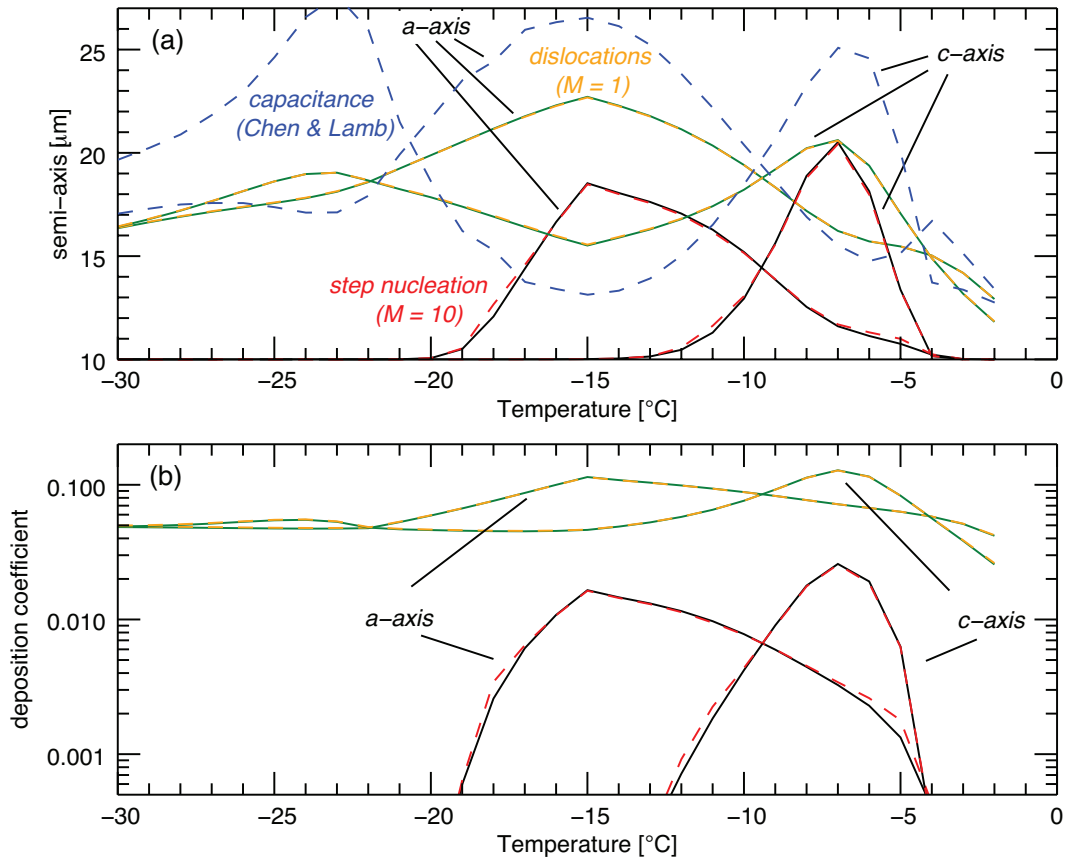
935 FIG. 4. Deposition coefficient growth mechanism parameter  $M$ -dependence of, (a) power-law exponent used  
 936 in Eq. 6 and coefficients used in Eq. 9, and (b) power-law exponents used in Eq. 9. Circles represent the actual  
 937 values used to fit Eqs. 6 and 9 to accurate calculations of the surface supersaturation (values are given in Table  
 938 1). Lines are polynomial fits to the circles, and the fit coefficients are given in Table 2.



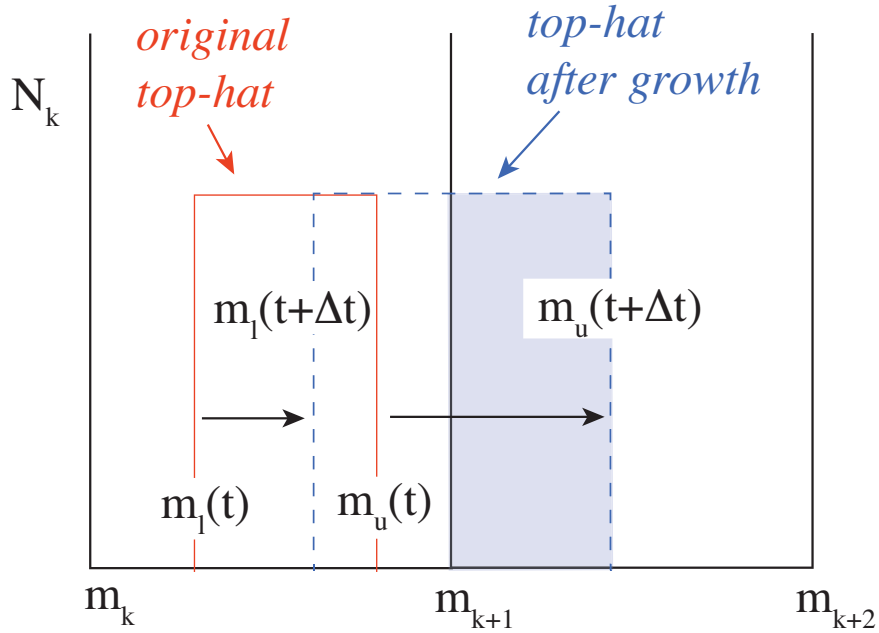
939 FIG. 5. Semi-axis lengths ( $a$  and  $c$ ) after 10 minutes of growth at a pressure of 500 hPa and a temperature of  
 940  $-15^{\circ}\text{C}$  and a constant ambient supersaturation. Calculations are shown for three values of the growth mechanism  
 941 parameter,  $M$ , of 1 (dislocation growth), 3, and 10 (ledge formation), which are indicated by the lines. Bench-  
 942 mark calculations for three values  $M$ , are indicated by the magenta ( $M=1$ ), green ( $M=3$ ), and black ( $M=10$ ) lines.  
 943 Simulations using the approximate form of the deposition coefficient are indicated by the dashed blue ( $M=1$ ),  
 944 orange ( $M=3$ ), and red ( $M=10$ ) lines.



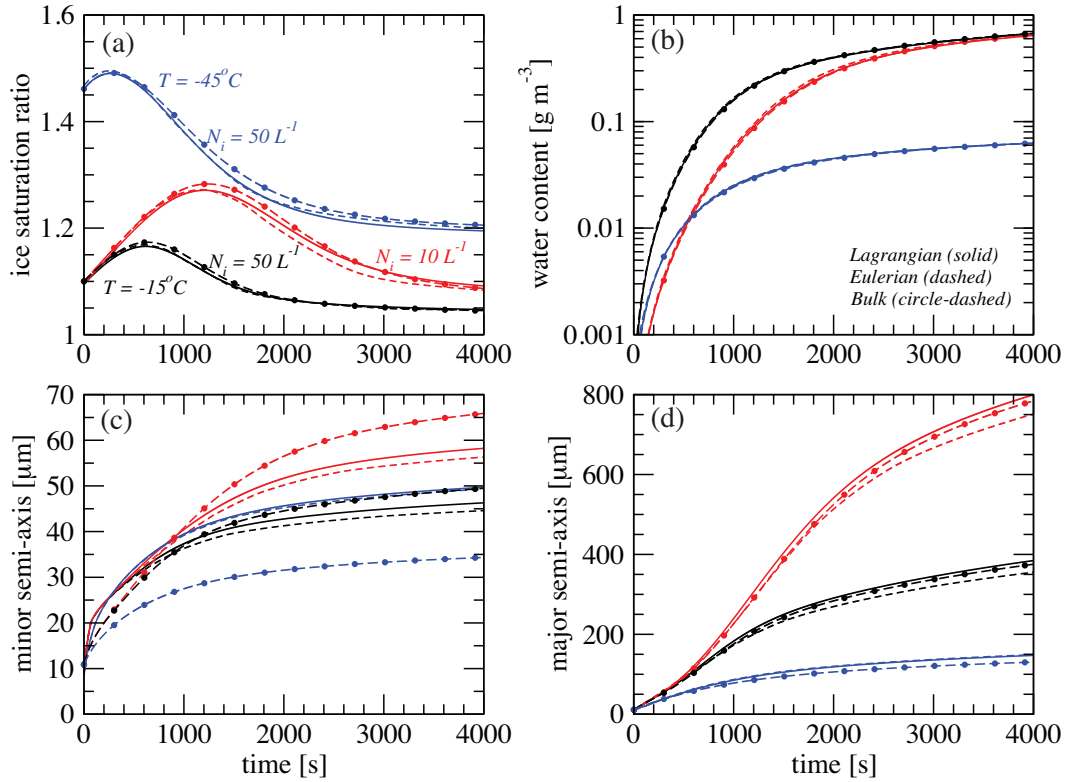
945 FIG. 6. (a) Deposition coefficients ( $a$  and  $c$ ) after 10 minutes of growth at a pressure of 500 hPa, a temperature  
 946 of  $-15^\circ\text{C}$  as a function of the ambient supersaturation ( $s_i$ ). Calculations are shown for three values of the growth  
 947 mechanism parameter,  $M$ , of 1 (dislocation growth), 3, and 10 (ledge formation), which are indicated by the  
 948 curves. Benchmark calculations for three values  $M$ , are indicated by the magenta ( $M=1$ ), green ( $M=3$ ), and  
 949 black ( $M=10$ ) curves. Simulations using the approximate form of  $\alpha$  are indicated by the dashed blue ( $M=1$ ),  
 950 orange ( $M=3$ ), and red ( $M=10$ ) curves. (b) Surface supersaturation for the  $a$ - and  $c$ -axes as a function of  $s_i$  for  
 951 step nucleation ( $M = 10$ ). Benchmark calculations are shown with the black curve, whereas the approximate  
 952 form is given by the red-dashed curve. The one-to-one ambient supersaturation is given by the blue curve, and  
 953 the values of  $s_{char}$  for the  $a$ - and  $c$ -axes are given by the green solid and dashed lines, respectively.



954 FIG. 7. (a) Semi-axis lengths (*a* and *c*) and, (b) deposition coefficients after 10 minutes of growth at a pressure  
 955 of 500 hPa, a temperature of  $-15^{\circ}\text{C}$ , an initial crystal radius of  $10\mu\text{m}$ , and a constant ambient supersaturation  
 956 that is 5% of liquid saturation,  $s_i = 0.05 \times [e_s - e_i]/e_i$  where  $e_s$  and  $e_i$  are the equilibrium vapor pressures of  
 957 liquid and ice, respectively. Accurate benchmark calculations are indicated by the green (*M*=1, dislocations),  
 958 and black (*M*=10, step nucleation) lines. Simulations using the approximate form of the deposition coefficient  
 959 are indicated by the dashed orange (*M*=1) and dashed red (*M*=10) lines. Simulations using the capacitance  
 960 model with the Chen and Lamb (1994) habit parameterization is shown by the blue dashed lines.

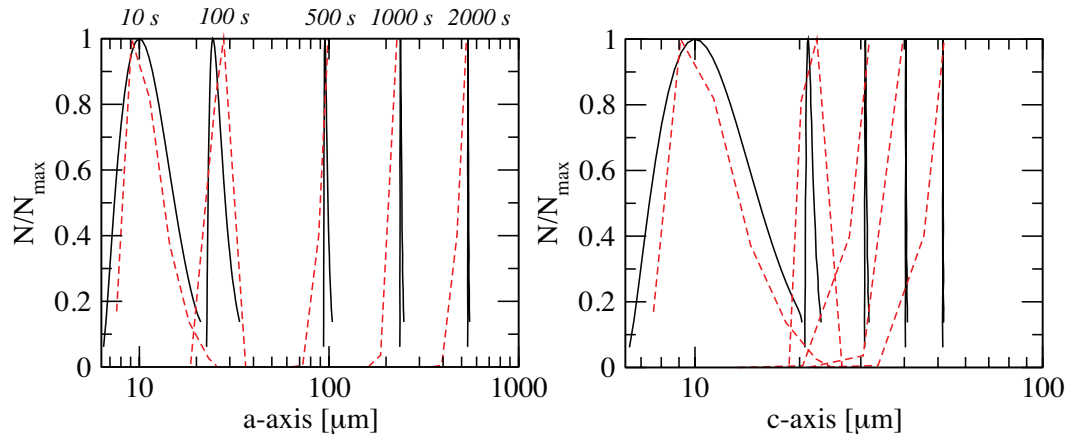


961 FIG. 8. Cartoon example of top-hat semi-Lagrangian depositional growth (Stevens et al. 1996). Bin mass  
 962 edges are given along the x-axis as  $m_k$  and  $m_{k+1}$  defining bin- $k$ . The edges of the original top-hat construction in  
 963 bin- $k$  is shown in red, with the lower and upper mass edges shown ( $m_l(t)$  and  $m_u(t)$ , respectively). The analytical  
 964 solution to the vapor growth equation is used to calculate the change in the top-hat edges indicated by the black  
 965 arrows ( $m_l(t + \Delta t)$  and  $m_u(t + \Delta)$ ), resulting in a new top-hat distribution shown by the dashed blue lines. In  
 966 this example, the number mixing ratio ( $N_k$ ) is then remapped to the next bin ( $k + 1$ ) using the fraction shown  
 967 by the blue shade, while the remainder (shown in white) is mapped to the original bin. The total concentration  
 968 (zeroth-moment) is conserved in this process. This procedure is used to remap the mass, volume, and aspect  
 969 ratio.

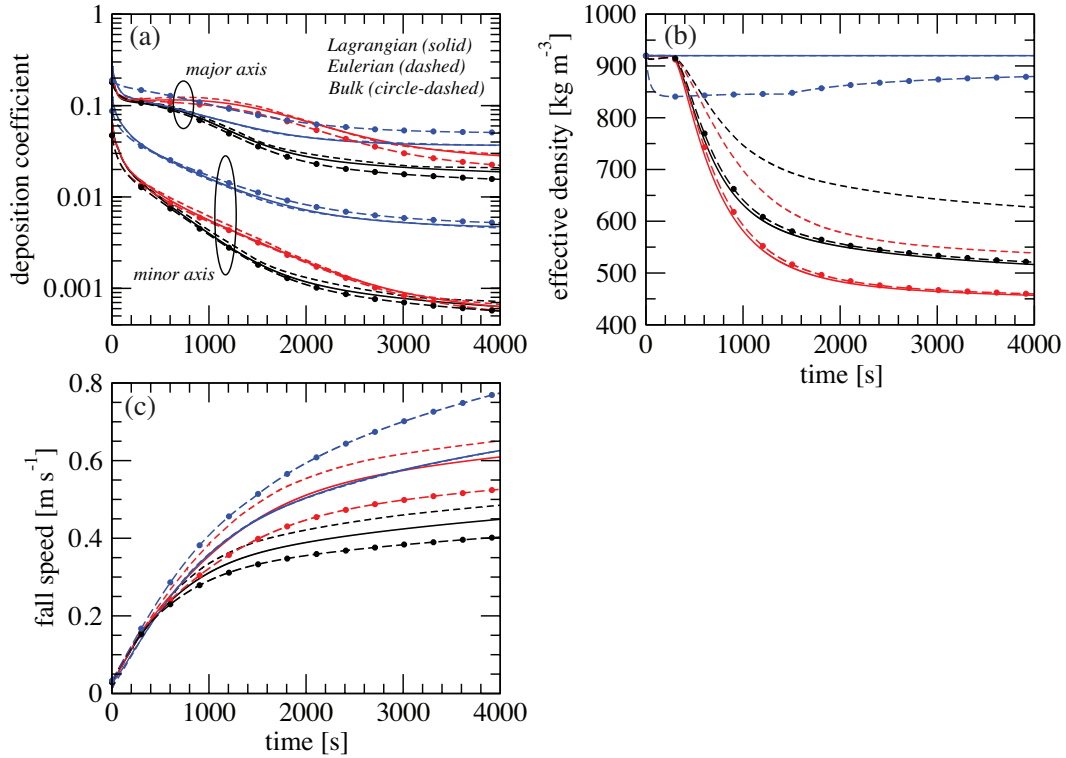


970 FIG. 9. Parcel model simulation time-series of (a) ice saturation ratio ( $e/e_i$ ), (b) ice water content, (c) minor  
 971 semi-axis length, and (d) major semi-axis length. The simulations were conducted for two different initial tem-  
 972 peratures ( $-15^\circ\text{C}$ , red and black, and  $-45^\circ\text{C}$ , blue) and two different ice concentrations for the  $-15^\circ\text{C}$  simulation  
 973 (labeled on panel a). Both simulations used a constant updraft speed of  $0.25\text{ m s}^{-1}$ . An initial pressure of 850  
 974 hPa (300 hPa) was assumed for the  $-15^\circ\text{C}$  ( $-45^\circ\text{C}$ ) simulation. Note that the major axis at  $-15^\circ\text{C}$  ( $-45^\circ\text{C}$ ) is the  
 975 a-axis (c-axis). Ice crystal growth assumed step nucleation ( $M = 10$ ). Results using the Lagrangian bin (solid),  
 976 Eulerian bin (dashed), and bulk (circle-dashed) models are shown.

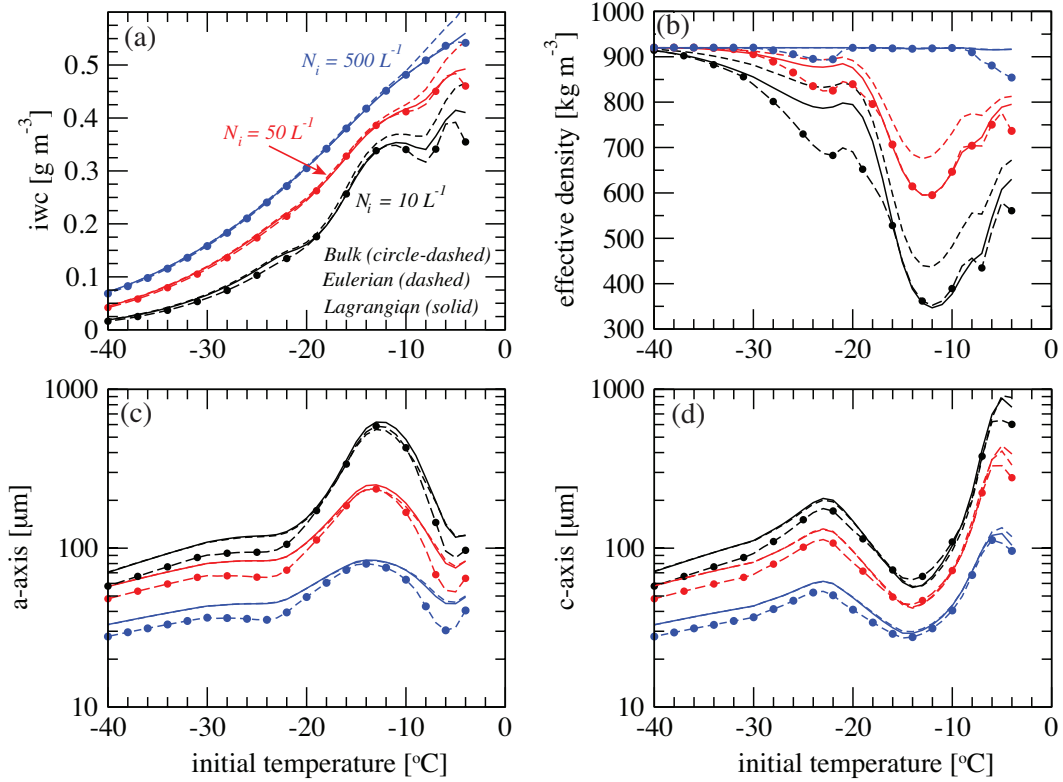




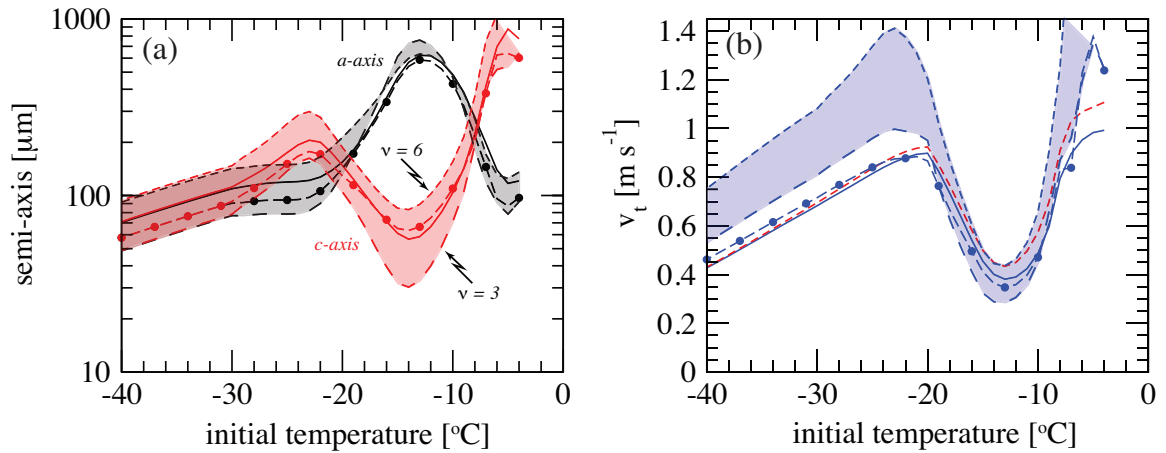
977 FIG. 10. Distributions of fractional ice concentration ( $N/N_{max}$ ) as a function of the a-axis (left panel) and  
 978 c-axis (right panel) semi-lengths.  $N$  is the ice crystal concentration and  $N_{max}$  is the concentration at the distri-  
 979 bution peak (mode). Lagrangian microphysical model distributions are given by the solid lines, Eulerian bin  
 980 microphysical distributions by the dashed red lines. Distributions are plotted at the simulation times indicated  
 981 above the distributions shown in the left panel. Distributions are plotted for the simulation with an initial tem-  
 982 perature of  $-15^{\circ}\text{C}$ , an initial pressure of 850 hPa, an ice concentration of  $10\text{ L}^{-1}$ , and a constant updraft speed of  
 983  $0.25\text{ m s}^{-1}$ .



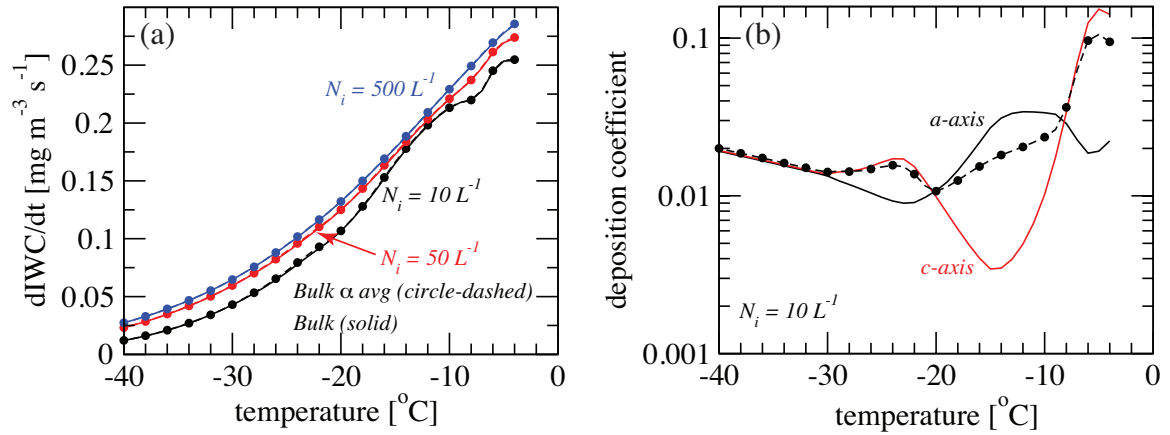
984 FIG. 11. Parcel model simulation time-series of average (a) deposition coefficients for the minor and major  
 985 semi-axes (b) effective particle density, and (c) mass-weighted fall speed. The simulations were conducted for  
 986 two different initial temperatures ( $-15^{\circ}\text{C}$ , red and black, and  $-45^{\circ}\text{C}$ , blue) and two difference ice concentrations  
 987 for the  $-15^{\circ}\text{C}$  simulation (labeled on panel a). Both simulations used a constant updraft speed of  $0.25\text{ m s}^{-1}$ .  
 988 An initial pressure of 850 hPa (300 hPa) was assumed for the  $-15^{\circ}\text{C}$  ( $-45^{\circ}\text{C}$ ) simulation. Note that the major  
 989 axis at  $-15^{\circ}\text{C}$  ( $-45^{\circ}\text{C}$ ) is the a-axis (c-axis). Ice crystal growth assumed step nucleation ( $M = 10$ ). Results using  
 990 the Lagrangian bin (solid), Eulerian bin (dashed), and bulk (circle-dashed) models are shown.



991 FIG. 12. Simulation and distribution averages of (a) the ice water content, (b) the effective density, (c) the a-  
 992 axis semi-length and, (d) the c-axis semi-length as a function of the initial temperature of the simulation. Initial  
 993 ice crystal concentrations of 10 (black lines), 50 (red lines), and 500 (blue lines)  $L^{-1}$ , along with a constant  
 994 updraft speed of  $0.25 \text{ m s}^{-1}$  and an initial pressure of 850 hPa were used. Ice crystal growth assumed step  
 995 nucleation ( $M = 10$ ). Results from the Lagrangian bin (solid), Eulerian bin (dashed), and bulk (circle-dashed)  
 996 models are shown.



997 FIG. 13. Simulation and distribution average of (a) the a-axis (black) and c-axis (red) semi-lengths, and (b)  
 998 the mass-weighted fall speed as a function of the initial temperature. An initial ice concentration of  $10 \text{ L}^{-1}$ ,  
 999 along with a constant updraft speed of  $0.25 \text{ m s}^{-1}$  and an initial pressure of  $850 \text{ hPa}$  were used. Ice crystal  
 1000 growth assumed step nucleation ( $M = 10$ ). Lagrangian and bulk model results are shown by the solid line and  
 1001 the dashed-dotted lines, respectively. Eulerian bin model results are shown by the red dashed line for the fall  
 1002 speed only. The influence of the assumed distribution shape on the axis lengths is indicated by the long-dashed  
 1003 and short-dashed lines bounding the shaded regions. The bounding long-dashed and short dashed lines used a  
 1004 distribution shape of  $v = 3$  and  $v = 6$ , respectively. For reference, this is indicated for the c-axis in (a).



1005 FIG. 14. Simulation and distribution average of the (a) ice water content growth rate and (b) the deposition  
 1006 coefficients as a function of the initial temperature. Results are shown for bulk model simulations using both  
 1007 deposition coefficients ( $\bar{\alpha}_a$  and  $\bar{\alpha}_c$ , solid lines) and bulk model simulations using a single deposition coefficient  
 1008 as could be used in classical bulk models (dashed-dotted lines). The ice water content growth rate is shown  
 1009 three initial ice concentrations of 10 (black lines), 50 (red lines), and 500 ( $L^{-1}$ , along with a constant  
 1010 updraft speed of  $0.25 \text{ m s}^{-1}$  and an initial pressure of 850 hPa. The deposition coefficients are shown only for  
 1011 the simulation with an ice concentrations of  $10 L^{-1}$ .