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Using *in operando* diffraction to relate lattice strain with degradation mechanism in a NMC battery

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Key words: NMC, battery, in situ, in operando, diffraction, strain, degradation, EDXRD

Abstract

Crystallographic structural changes in a commercial 5 Ah prismatic graphite-NMC battery were investigated during its operation using energy dispersive X-ray diffraction (EDXRD). The characteristic diffraction peaks for the anode and cathode were identified, and their peak positions were linked to the charge-discharge cycle of the battery. The edge of the negative terminal of battery was shown to undergo irregular cycling behavior. Stresses developed at the battery layer interfaces were proposed to be the source for this deterioration, which limits the lifetime of the battery. The effect of pulse discharge on strain in cathode has also been studied.

1. Introduction

Development of hybrid and fully electric vehicles reduces the consumption of nonrenewable energy sources, but requires the development of high capacity, light weight batteries with high reliability and long lifetimes. The materials used for these batteries have evolved over time from lead acid (General Motors EV1, 1996-1999) to Nickel-Cadmium to Nickel metal

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4 hydride and currently to Li-ion batteries (Tesla Model S and Nissan Leaf)[1]. Li-ion batteries have
5 a number of advantages over the aforementioned types: highest energy density (100-265 Wh/kg),
6 higher voltage to deliver the current needed for high power applications, low current leakage rates,
7 and the absence of the ‘memory effect’ as found in Nickel-Cadmium batteries, wherein repeated
8 partial charge-discharge cycles result in lower battery capacity. The absence of ‘memory effects’
9 provides flexibility in operation by allowing partial charge-discharge of the battery rather than
10 requiring a full discharge before recharging. All of these factors make Li-ion batteries a desirable
11 choice for electric vehicles.
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19 While Li-ion batteries are used ubiquitously in consumer applications, such as laptops and
20 mobile phones, their successful adoption by the automotive industry has been difficult due to
21 expectations of 2000 cycles over 5 years of operation [2] in order to be economically viable at the
22 current cost of battery manufacturing. There exists a gap between the expectations of battery
23 performance and the reality, as batteries tend to fail prematurely due to the complexity of the
24 design required for scaling up energy storage capacity [3-7]. Current Li-ion batteries are intricately
25 designed, multi-layered, multi-material devices that rely on concurrent electronic and mass transfer
26 during operating cycles. High capacity and energy density requirements make assembly of the
27 battery complicated. Many factors have been identified for the early end-of-life of a Li-ion battery,
28 such as: dendritic growth of lithium, oxidation of the electrolyte at the cathode leading to capacity
29 loss, aging mechanisms [4, 8, 9], growth of solid electrolyte interphase (SEI) [8], which blocks the
30 graphitic anode, formation of dead zones in the battery, porosity and thickness of the electrodes,
31 mechanical design parameters, delamination of layers, permanent deformation, thermal exposure
32 [10, 11] and other unknown mechanisms active during the operation of the battery. Considering
33 all these factors, batteries are often built to overcapacity to meet minimum expectations of
34 performance over extended periods of time. Reducing these performance losses offers an
35 opportunity to reduce the overcapacity requirements so it becomes crucial to identify the
36 mechanism(s) responsible for early degradation.
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52 One challenge to improving battery efficiency is that the electrode materials are
53 inaccessible once they are packaged, thus limiting the ability to determine battery failure
54 mechanisms. Impedance spectroscopy or voltage-current cycle data can be obtained [11] but they
55 do not reveal the effect of localized structural changes during the cycle. Another option is the use
56 of destructive testing, but it is not always suitable since the same battery cannot be used for further
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4 testing and *ex situ* measurements of the electrodes do not capture the actual electrochemical
5 dynamics present during its operation. Once the battery is brought to its rest state the
6 microstructure relaxes due to the fast diffusion kinetics of lithium. Additionally, removing the
7 components from the device itself may alter the material state that is provided by the casing.
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11 X-ray diffraction is commonly used to identify and quantify crystalline materials.
12 Mechanical and electrochemical strain in materials can be determined by comparing the measured
13 lattice parameters against a reference state. Recently *in situ* x-ray and neutron diffraction has been
14 successfully used to study the structural changes in electrodes during battery operation [2, 12-18].
15 Energy dispersive x-ray diffraction (EDXRD) is among these *in situ* methods, previously used as
16 a nondestructive method to understand the state of stress and strain of engineered components [19-
17 22]. The EDXRD measurements are made using a transmission geometry and provide spatial and
18 temporal mapping capabilities. High-energy x-rays can penetrate through tens of centimeters of
19 material and isolate a discrete volume within the battery to quantify the local strain. A collimated
20 x-ray beam with a broad spectrum of wavelengths impinges on the sample and scatters into a solid-
21 state detector [23]. The detector simultaneously collects the intensity of different wavelengths to
22 capture a range of diffraction peaks corresponding to different energies. Upon rearranging Bragg's
23 Law and substituting wavelength λ with energy, E , equation 1 is obtained, which converts energy
24 of radiation with constructive diffraction peak into the corresponding interplanar spacing.
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$$E = \frac{hc}{2\sin\theta} \left(\frac{1}{d_{hkl}} \right) \quad (1)$$

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41 Paxton *et al.* [23, 24] demonstrated the use of this method for the spatial distribution of
42 electrochemical materials in the battery. However, it is worth noting that while EDXRD provides
43 advantages over monochromatic diffraction in terms of isolating the measured data to a small
44 gauge volume, it also has shortcomings, such as non-uniform absorption for different wavelengths
45 which makes this method unsuitable for Rietveld analysis [25]. Rietveld refinement uses the least
46 squares fitting method and refines the theoretical line profile to match with the experimentally
47 obtained pattern. This analysis helps to determine the peak broadening because of strain in the
48 lattice and changes in grain-size as well as possible texture in the material. In the case of EDXRD,
49 unlike monochromatic radiation, a spectrum of white light X ray radiation is used and the intensity
50 of certain wavelengths matches the diffraction condition. However, there are two problems with
51 this configuration: (a) the intensity of incident X rays are not the same for all wavelengths and (b)
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4 the absorption of X rays by the material is wavelength dependent. It is important to note that for a
5 small energy range, such as for a single diffraction peak, these factors have minimal effect on the
6 individual peak's shape, allowing accurate estimation of the interplanar spacing.
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10 In the current study, the EDXRD technique is used to understand the deterioration
11 mechanisms operating in different parts of a graphite-NMC ($\text{Li}_x\text{Ni}_{1/3}\text{Mn}_{1/3}\text{Co}_{1/3}\text{O}_2$) battery by
12 following the structural change in the lattice parameters of the electrodes and current collectors
13 during operation. The mapping of spatial inhomogeneity of component material strains is used to
14 identify the role of internal strain in the early demise of certain sections of the battery assembly
15 during current cycling.
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22 **2. Experimental details**

23 **2.1 Battery design**

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25 Among the commercially available batteries for automotive electric vehicles a 5 Ah
26 Graphite-Li-NMC ($\text{Li}_x\text{Ni}_{1/3}\text{Mn}_{1/3}\text{Co}_{1/3}\text{O}_2$) prismatic cell was chosen for this study. The schematic
27 of the battery assembly has been shown in Fig. 1a and 1c. Layers of anode, cathode, separator and
28 current-collectors were flattened by a mechanical press and submerged in a bath of liquid
29 electrolyte. The electrode layers were comprised of aluminum and copper foils coated on both
30 sides by cathode and anode, respectively. The metallic current collectors, copper and aluminum,
31 extend out and were crimped and connected to the battery terminals. The assembly was sealed in
32 a steel case.
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42 **2.2 Energy dispersive X-ray diffraction (EDXRD)**

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44 The 2θ angle was chosen to be 3° in order to allow for the x-ray spectrum to match with
45 the d-spacings of the diffraction peaks of interest. The experiments were carried out at the 6-BM-
46 A beamline of the Advanced Photon Source at Argonne National Laboratory. This beamline is
47 designed for phase transformation and mapping as well as strain mapping analysis in engineering
48 components [26]. A bending magnet source generates a broad spectrum of incident beam x-rays
49 with a useable spectral flux of up to 250 keV. The height and width of the incident X-ray beam
50 was kept constant (0.2 mm x 1.0 mm) for *in-plane* and *out-of-plane* measurements. As a battery
51 has a lamellar structure, the strain developed in the perpendicular direction would differ from strain
52 in the plane of layered sheets. The diffraction vector limits the diffraction only from the grains
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4 with a particular orientation. This comparison of *in-plane* and *out-of-plane* measurement would
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6 enable differentiation of the strain developed in two directions. A micro-positioning X-Y-Z stage
7 translated the battery cell so that the diffraction gauge volume probed different locations of the
8 battery. A Canberra germanium solid-state detector collected the diffracted spectra from the
9 battery. A Canberra germanium solid-state detector collected the diffracted spectra from the
10 sample using a transmission geometry with an acquisition time of 60 s per scan. This rate of
11 acquisition was required to obtain sufficient counts from relatively faint peaks, since the x-rays are
12 highly attenuated due to the 120 mm length of steel casing and battery materials. The detector
13 output spectra were converted into energy and d-spacing of different materials using reference
14 diffraction spectra standards. A program was developed in MATLAB[®] to automate the data
15 processing and peak fitting. The error is calculated for the peak fitting with 95% confidence
16 interval. The height of the error for strain in NMC (101) is too small (~ 0.005 %) to be visible in
17 the plot. Of course, the error in fitting depends on the peak counts so the stronger the peak the
18 smaller the error. Thus, the NMC (101) peaks are compared to understand the change in lattice
19 parameters during the battery's operation.
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31 32 **2.3 Battery data acquisition**

33 During the measurements, the battery was cycled through the charge-discharge routine at
34 two rates, 1 C at 5 A for 1 h and a fast discharge of 4 C at 20 A for 5 min, using an Arbin battery
35 cyclers. The electrical parameters, voltage and current, during a charge-discharge cycle are shown
36 in Fig. 2 (a) while a complete XRD plot for an entire cycle is shown in a contour plot in Fig. 2 (b)
37 where the y-axis corresponds to energy, the x-axis to time and the color to intensity. A slice of this
38 plot gives an XRD pattern at a particular time which can be converted into interplanar spacing as
39 shown in Fig. 2 (c). The peaks have been identified using powder diffraction pattern (PDF) cards
40 corresponding to Li-NMC (No. 00-062-0431), delithiated Li-NMC (Li_{0.63} (No. 01-075-3918),
41 Li_{0.58} (No. 01-075-3919) and Li_{0.48} (No. 01-075-3920),), aluminum (No. 04-012-7848), copper
42 (No. 04-009-2090), graphite (No. 00-056-0159) and lithiated graphite (LiC₆ (No. 01-083-4148),
43 LiC₁₂ (No. 01-083-4147) and LiC₂₄ [2]. Table 1 shows the Miller indices and interplanar spacing
44 of different materials. Unfortunately, the two measured peaks for aluminum overlap with two of
45 the peaks for NMC and could not be resolved.
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Table 1. The Miller Indices with corresponding d-spacing for anode, cathode and current collectors in the energy range under current study.

Material	Interplanar spacing (Å)	(h k l)
NMC	2.438	1 0 1
NMC	2.337	0 1 2
NMC	2.031	1 0 4
NMC	1.867	0 1 5
C	3.355	0 0 2
LiC ₁₂	3.518	0 0 2
Cu	2.080	1 1 1
Cu	1.802	2 0 0
Cu	1.274	2 2 0
Al	2.339	1 1 1
Al	2.025	2 0 0

Since the beam time at the synchrotron source is limited, the complete set of experiments were performed over three visits, each separated by 4 months. In the first visit, out of plane XRD measurements were performed at point M2 (refer to Fig. 1a). In the second run three points (gauge volumes) were selected across the thickness at three different locations (middle, anode and cathode). A total of 9 scans of the battery were collected for the *in-plane* configuration. In the third visit a macro was written to scan the thickness profile of the battery *in-plane* with each point separated by 2 mm. Once the thickness profile was completed, the stage moved back to its initial position and the next profile was initiated. This procedure continued until a total of 23 scans were taken for each of the 6 positions across the thickness of the battery during a complete charge-rest-discharge cycle of 130 minutes. This schedule was followed for the three locations, Middle (M), Cathode (C) and Anode (A), as shown if Fig. 1(a).

2.4 *In-plane and out-of-plane* measurements

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4 For *in-plane* measurements the incident and diffracted beams were in the same plane as the
5 battery electrodes. When the diffraction vector is perpendicular to the sheets of the battery
6 electrodes, they are referred to as *out-of-plane* measurements (Fig. 1c). These two orthogonal
7 directions of strain measurements within the battery were designed to examine the effect of texture
8 and electrode sheet orientation.
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15 3. Results

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17 The goal of these experiments is to measure the strain in different regions of the battery to
18 identify sections of the battery that were underperforming or failing. In Fig. 3, the change in
19 interplanar spacing is shown for the graphite anode corresponding to the stage-of-charge. Notably
20 a much stronger intensity of graphite is observed for *out-of-plane* compared to *in-plane*
21 measurements (Fig. 4). For the *out-of-plane* measurements, the peaks corresponding to LiC₁₂,
22 LiC₂₄, and graphite appear as step functions in the graph, whereas for *in-plane* there is a relatively
23 continuous transition from one phase to another.
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26 The literature [2, 17, 25, 28-31] suggests that graphite layers are highly orientated with the
27 ‘c’ axis perpendicular to the plane of the current collector such that lithium atoms intercalate
28 between the carbon layers that are oriented along the c-axis. The orientation becomes more
29 pronounced when the sheets are pressed during the compaction of battery electrode layers which
30 is the reason for the low intensity of $\langle 0\ 0\ n \rangle$ planes of graphite during *in-plane* measurements.
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32 For the case of the Li-NMC cathode, the lattice parameter ‘c’ expands while ‘a’ shrinks
33 during the charge and this trend reverses during discharge, shown in Fig. 5. This observation agrees
34 with previous reports [32-34] where the lattice expansion in ‘c’ follows linearly with the
35 intercalation of lithium up to 90% of charge before leveling off. It has been suggested by Dolotko
36 et al. [32] that initial lithium diffusion is accommodated by a change in the oxidation state of Ni⁴⁺
37 to Ni²⁺, but as the c/a ratio deviates from linearity (Fig. 5c), a phase transformation occurs which
38 changes the the bonding environment and oxidation state of Co [8]. Mn is believed to be
39 electronically inactive and a stabilizer of the crystal structure, which is a crucial factor for a safe
40 battery. Since the battery was in use before the current set of experiments, no irrecoverable loss
41 was observed during the cycle, as is seen in the first discharge of a new battery [8]. During
42 discharge, Li moves from anode to cathode which changes the stoichiometry of the Li-NMC
43 cathode. Based on the calculated lattice parameters, the cathode stoichiometry is found to change
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4 from $\text{Li}_{0.85}\text{Ni}_{1/3}\text{Mn}_{1/3}\text{Co}_{1/3}\text{O}_2$ and $\text{Li}_{0.35}\text{Ni}_{1/3}\text{Mn}_{1/3}\text{Co}_{1/3}\text{O}_2$ for fully discharged and charged states,
5 respectively [12, 36, 37]. Unlike the anode, the cathode (Li-NMC) does not show any preferred
6 orientation for *in-plane* and *out-of-plane* as supported by the literature [18] since grains of Li-
7 NMC were found to be equiaxed. This indicates isotropic macroscopic expansion and contraction
8 during battery cycling.
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13 Fig. 7 shows a detailed study of full-width at half-maximum (FWHM) and normalized
14 relative intensity for the cathode (101) for *in-plane* and *out-of-plane* configurations. There is a
15 slight difference in the d-spacing for the two cycles, which may have been the result of the battery
16 being stored idle for four months between two runs at the synchrotron. While the intensity of the
17 (101) peak for *in-plane* measurements stays relatively constant the out of plane normalized
18 intensity drops to 0.65 of its initial intensity. Similar patterns were noticed by Paxton et al. [24]
19 which was related to the physical movement of layers due to mechanical stress. As the layers of
20 the cathode moved out of the gauge volume, the intensity of the peaks decreased. No discernable
21 trend was seen in elastic strain as estimated from the full-width at half-maximum (FWHM) of the
22 peak.
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32 Referring to Fig. 1a, the cathode (positive), anode (negative) and middle sections of the
33 battery were investigated to compare the relative responses during charging and discharging. It
34 was found that while the majority of the battery functioned as expected the negative end of the
35 battery had a non-uniform response, as indicated in Fig. 8. Utilizing strain in the lattice related to
36 the state of charge, a lag during charging is observed. This section of the battery did not undergo
37 complete discharge as a good contact between anode and cathode is constrained by the dog bone
38 structure of the wrapped cell stack. This contact problem gets worse over the lifetime of the battery,
39 which has been indicated by the presence of an inactive cathode (Li-NMC) in Fig. 6 and Fig. 8.
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46 Profile measurements were conducted by scanning across the thickness of the battery to
47 compare the response of the middle region of the battery with the region near the negative terminal,
48 the anode side of the battery. Results from Fig. 9 confirm the earlier finding that while all of the
49 layers of the middle section (M) of the battery were lithiating and delithiating to the same extent,
50 the negative end, A, shows variability across the layers, from A1 to A6. While the outermost layer
51 (A1) neither lithiates nor delithiates completely and layers at A2, A5 and A6 do not return to their
52 initial state at the end of the cycle. The middle layers, A3 and A4, behaved as expected. Another
53 interesting observation is that although A1 is symmetrical to A6, the strain in the two sections are
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4 different. This may be the result of the assembly design. The prismatic battery assembly involves
5 jelly-rolling the layers into a spiral with two bends (a link showing the design is embedded in ref
6 [38]). The strain at one face of the battery will differ from the other end because the boundary
7 condition changes from near no strain under loop stress to no stress at the free end. The analytical
8 and numerical stress analysis is part of a future work. Interestingly, these lattice strains recovered
9 quickly after the battery was put in its rest state. This suggests that the outermost battery layers
10 have poor point of contact to sustain the steady exchange of Lithium ion at the interface during
11 operation. However, once the battery goes to ‘rest’ state, Lithium ions move along the sheets to
12 maintain equipotential in the cathode and anode. This local “delamination” does not cause
13 permanent loss in battery capacity, but could be one of the primary factors of battery degradation
14 over long run. This quick recovery highlights the importance of *in-situ* diffraction techniques to
15 study the strain measurements directly and non-destructively during operation.

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17 Batteries are customarily tested in continuous charge and discharge at a slower rate such
18 as 1 C to measure their performance at equilibrium. Pulse (or burst) discharge is normally
19 discouraged as it exceeds the sustainable rate of discharge and adversely affects the battery’s
20 longevity. Depending on the level and duration of the stress during high current discharge, the
21 battery’s capacity has been reported [39] to drop to 2% compared to constant current discharge.
22 The battery was tested at 4 C (20 A current) and the analysis followed the change in the (101)
23 interplanar spacing of the Li-NMC cathode. During high current rate experiments, the interplanar
24 spacing and hence the strain changes four times faster for a 4 C discharge rate compared to 1 C.
25 This will cause peak broadening for the same acquisition time of X-ray diffraction. Hence, the
26 accuracy in measurement is lowered for faster processes. After removing the load, the battery
27 electrical potential gradually recovered as can be seen in Fig. 10. When the strain resulting from
28 the pulse discharge in the battery is analyzed, it is observed that even though the battery is in its
29 rest state, the Li-NMC cathode continues to take in lithium at a higher rate compared to the
30 discharge rate of 1 C. In other words, the recovery rate of strain for pulse discharge is higher than
31 the normal discharge rate, which is expected as the battery was forced to operate at high power in
32 pulse mode, beyond its equilibrium condition.

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34 Heat generation during continuous use of the battery has been suggested to negatively
35 affect the battery life [40]. To understand this effect, the lattice parameters of the cathode were
36 compared before and after a continuous use of the battery for 24 hours at a rate of 1C for the same
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4 state of discharge of the battery (at complete discharge state). The values were found to be
5 comparable, suggesting that the thermal contribution for continuous use of the battery at 1 C is not
6 a significant degradation mechanism that can be measured by residual stress for the battery.
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10 11 **4. Discussion**

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14 Scaling up the capacity of Li-ion rechargeable batteries from low power consumer devices
15 to high power devices such as automobiles comes with many engineering challenges. To build a
16 higher capacity battery larger and greater numbers of layers in the battery stacks are needed. Layers
17 in prismatic batteries are tightly compressed to maintain stack pressure so that the battery layers
18 stay in contact during cycling. Cycling induces mechanical stresses in the battery layers and may
19 damage the electrodes and alter the structure of the battery components during each cycle. The
20 relative expansion of the layers of different battery components introduce stresses at the interfaces
21 whose effects can build up over time and lead to increasing damage to of the battery layer
22 structures. The jelly roll structure used in this battery cell design appears to create regions of poor
23 cyclability in the regions of high curvature. This situation may be worsened as more battery layers
24 are added, limiting the possibility of scaling. To understand this problem better, an analytical stress
25 analysis and node base simulation is needed, which is beyond the scope of this work.
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37 **5. Conclusion**

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39 The structural changes in the cathode and anode of the 5 Ah Li-NMC battery were
40 investigated using *in-situ* energy dispersive X-ray diffraction to track the movement of lithium
41 between the anode and cathode during the charge-discharge cycle, using *in-plane* and *out-of-plane*
42 measurements. We observe that the graphite is highly oriented with the ‘c’ axis perpendicular to
43 the plane of the electrode sheet, which expands to accommodate the lithium. The
44 $\text{Li}_x\text{Ni}_{0.33}\text{Mn}_{0.33}\text{Co}_{0.33}\text{O}_2$ cathode expands along its ‘c’ axis and contracts in its ‘a’ axis during the
45 charging cycle. However, random orientation of the grains of Li-NMC make this expansion
46 isotropic on the macroscopic level [18]. While most measured regions of the battery had
47 completely reversible cycles, we observed irregular cycling behavior at the bottom of the negative
48 terminal, believed to be caused by poor contact locally of the battery layers. The profile scan across
49 the thickness of the battery confirms that the outermost layers at the negative end of the battery
50 cycle non-uniformly. Pulse discharge of the battery at the rate of 4 C (20 A) shows a non-
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4 equilibrium strain in the cathode, which continues to recover for a considerably long time after the
5 current stops flowing, demonstrating the detrimental nature of burst mode discharge and, therefore,
6 why it is strongly discouraged. This work also highlights the versatility of EDXRD measurements
7 in strain analysis as well as for identification of phase changes of individual materials in
8 multicomponent systems for different charge rates.
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28 Compliance with ethical standards

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30 **Conflict of interest:** All authors declare that they have no conflict of interest.
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10 **List of Figures**

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13 **Figure 1.** (a) Schematic design of Li-NMC battery and (b) the experimental set-up at the
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Figure 2. (a) Typical full charge-discharge cycle for 5 Ah battery at 1 C. (b) Contour plot of a
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discharged stage, with fitting and remaining residuals.

Figure 3. (a) Measured lattice parameters for the anode (graphite and Li-graphite) peaks with
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A typical battery I-V characteristic plot.

Figure 4. Comparison of graphite and Li-C phases, out-of-plane and in-plane peak intensities
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Figure 5. Change of lattice parameters (a) 'a', (b) 'c' and (c) ratio of c/a taken at M2 of the battery,
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Figure 6. Comparison of cathode and anode at the negative end (inactive area) and middle section
(active area) of the battery. The inactive area of the battery shows no intercalation of Li in graphite
as well as delayed shift of the Li-NMC [1 0 1] peak.

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6 with space group R-3m [16]. Interplanar spacing (b), peak intensity (c) and full-width at half-
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8 maxima (d) of cathode peak (101). A corresponding state of charge for battery during the charge
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10 and discharge cycle is shown in (e). No significant elastic deformation is observed from FWHM
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37 **Figure 10.** (a) Pulse discharge of the battery at 20 A for 5 min and its effect on the battery
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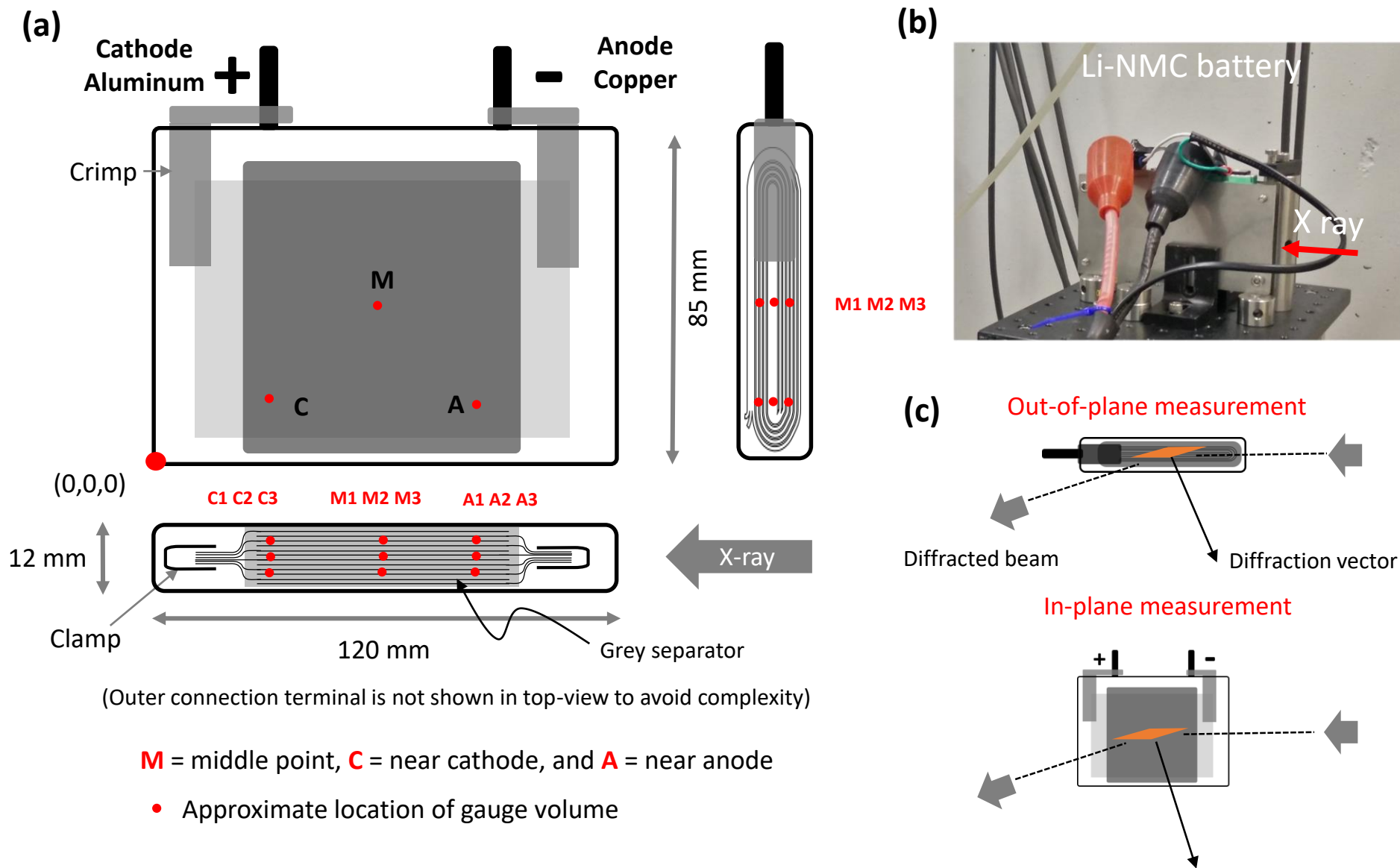


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Figure

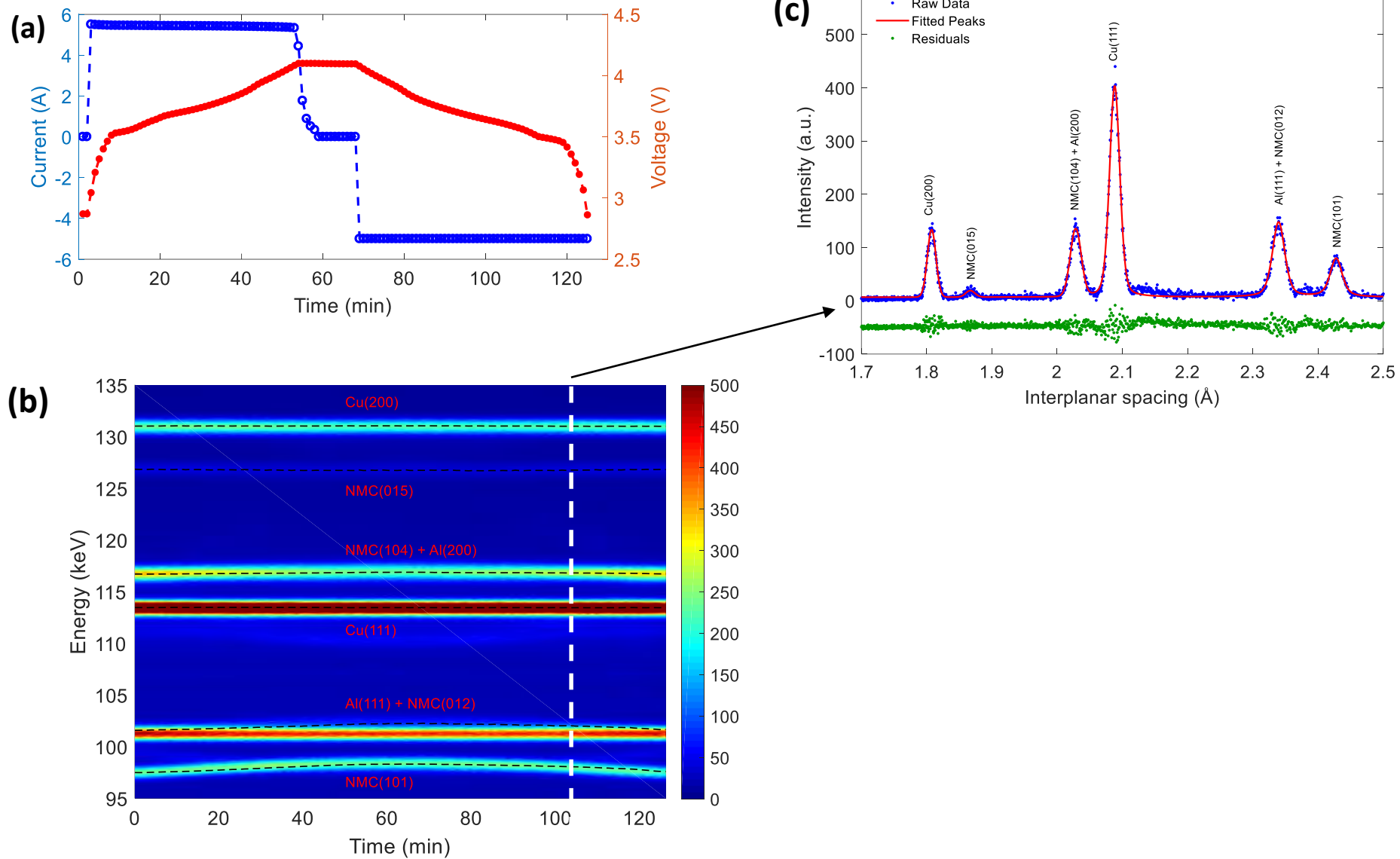


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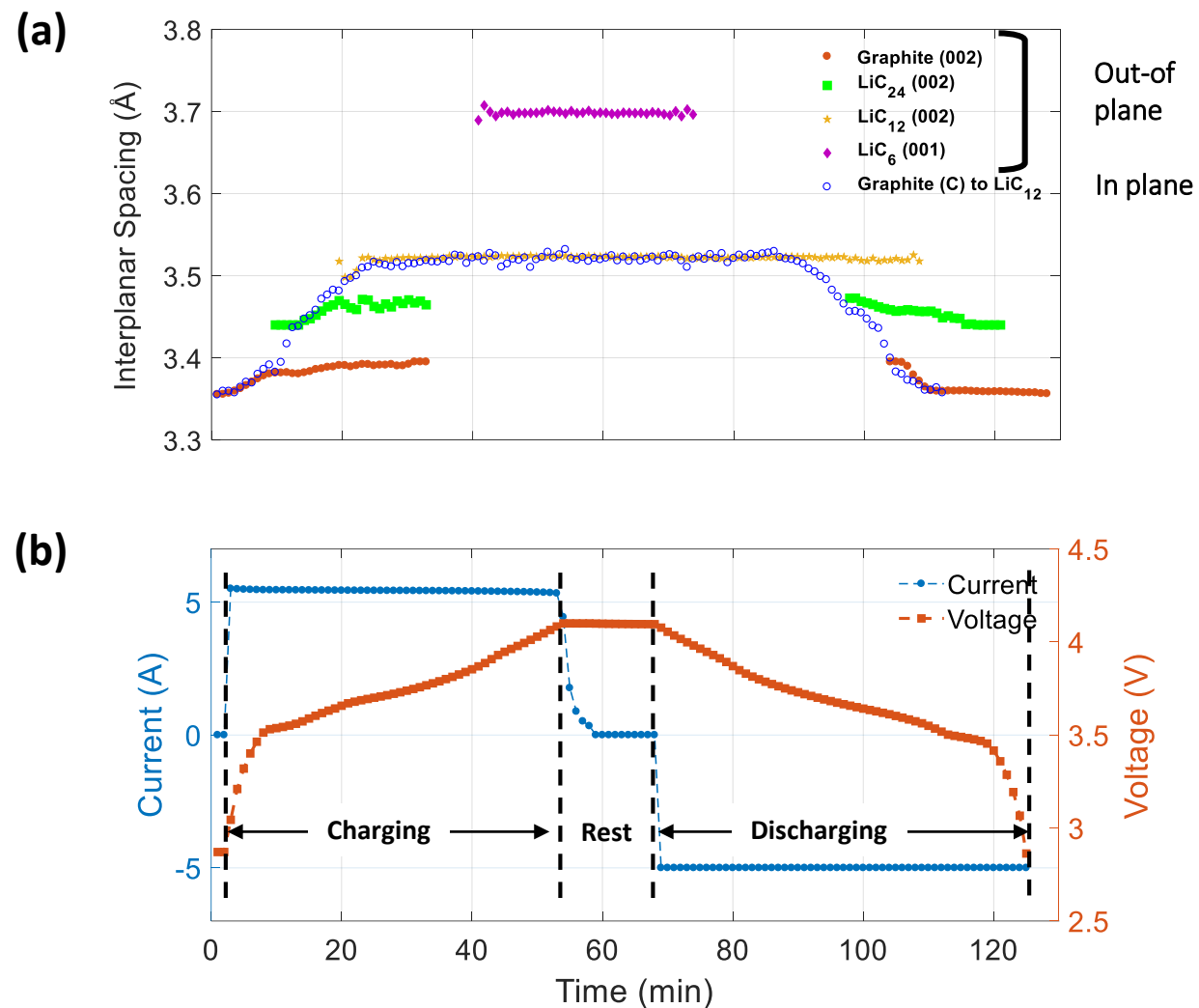
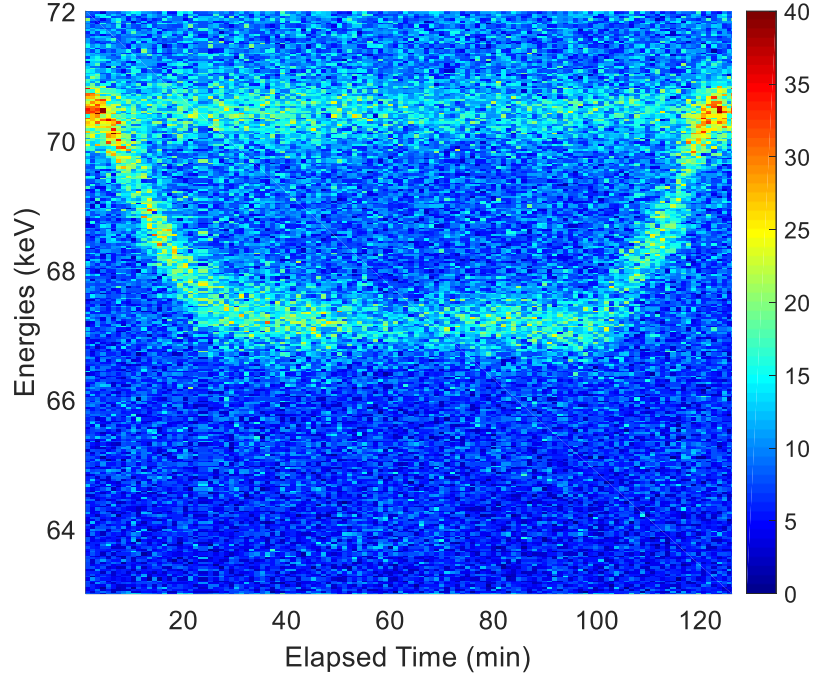
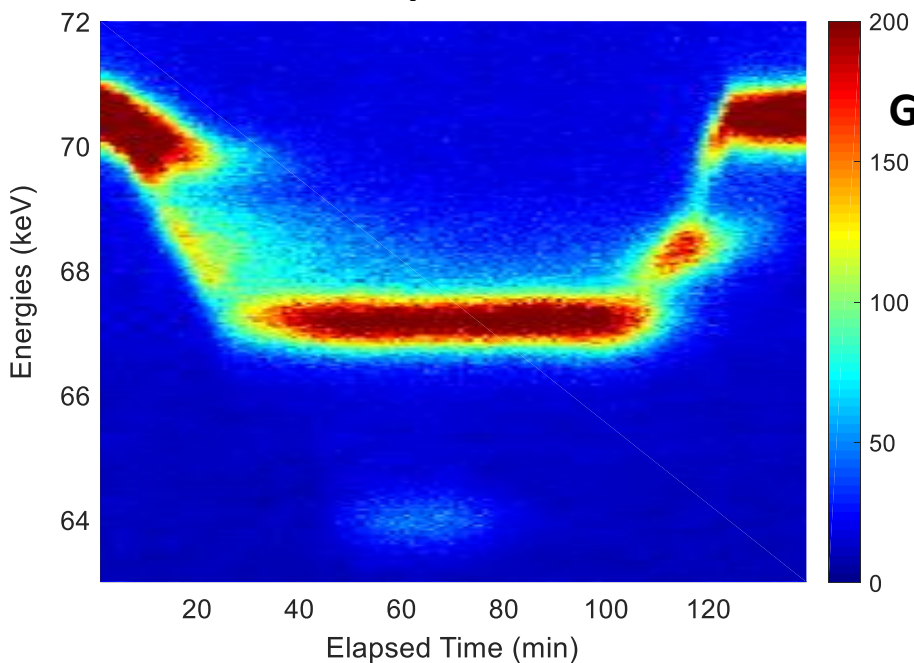


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Figure

Out-of-plane

In - plane

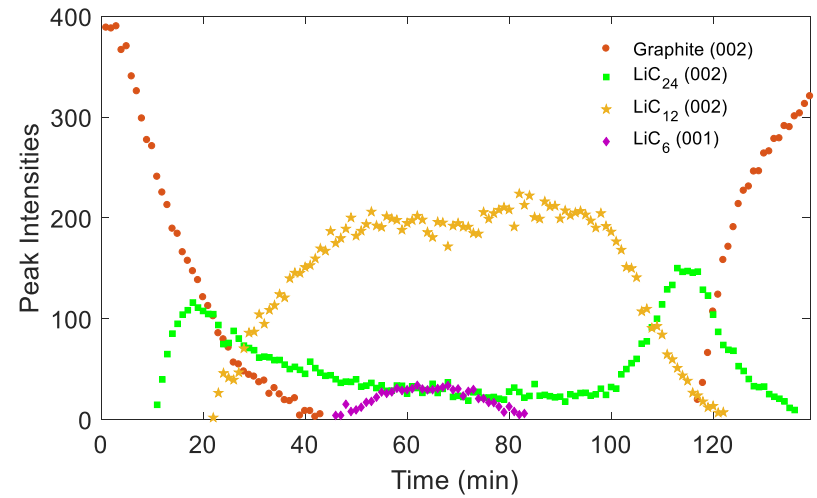


Graphite

LiC_{24}

LiC_{12}

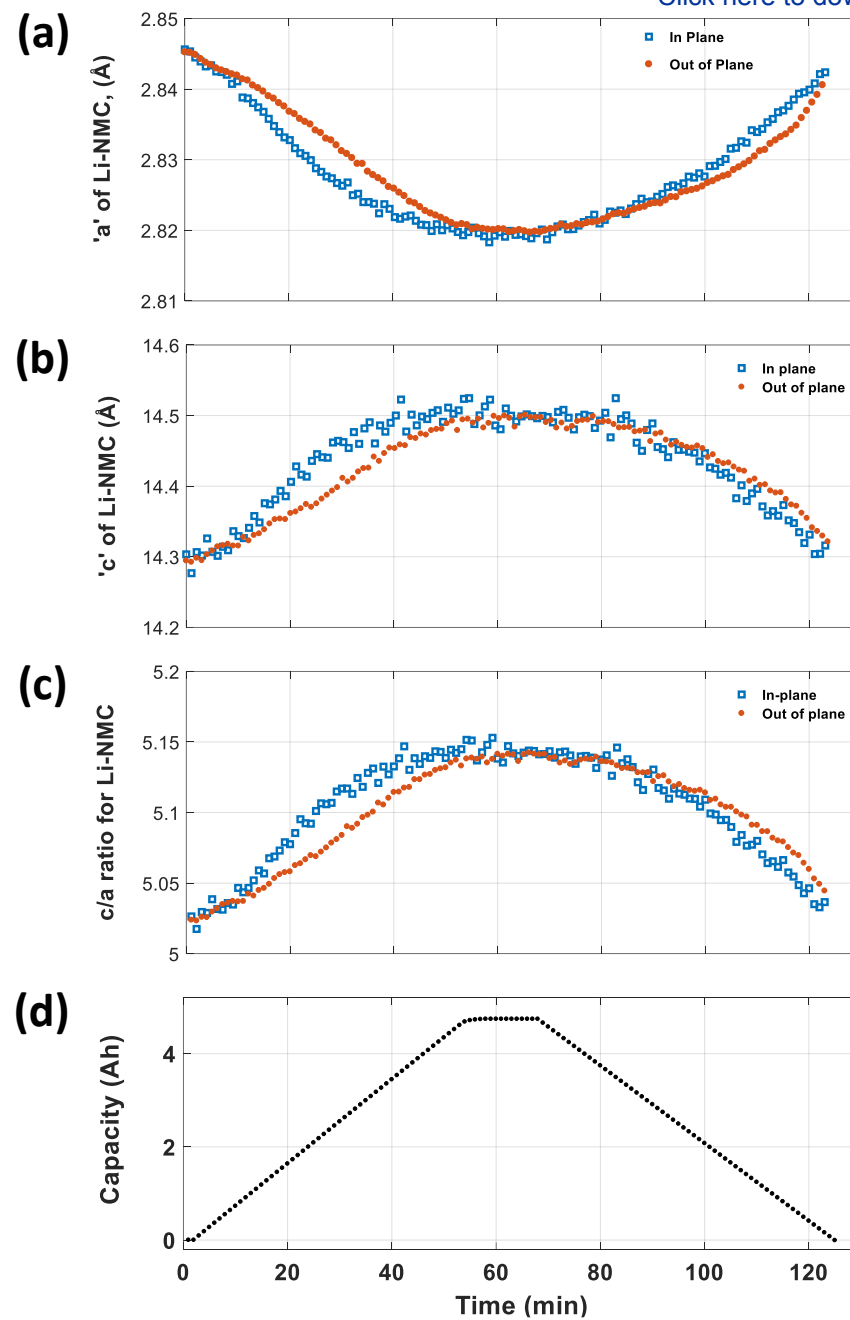
LiC_6



Intensity of in-plane graphite peak too weak to accurately fit for quantitative comparison with out-of-plane data.

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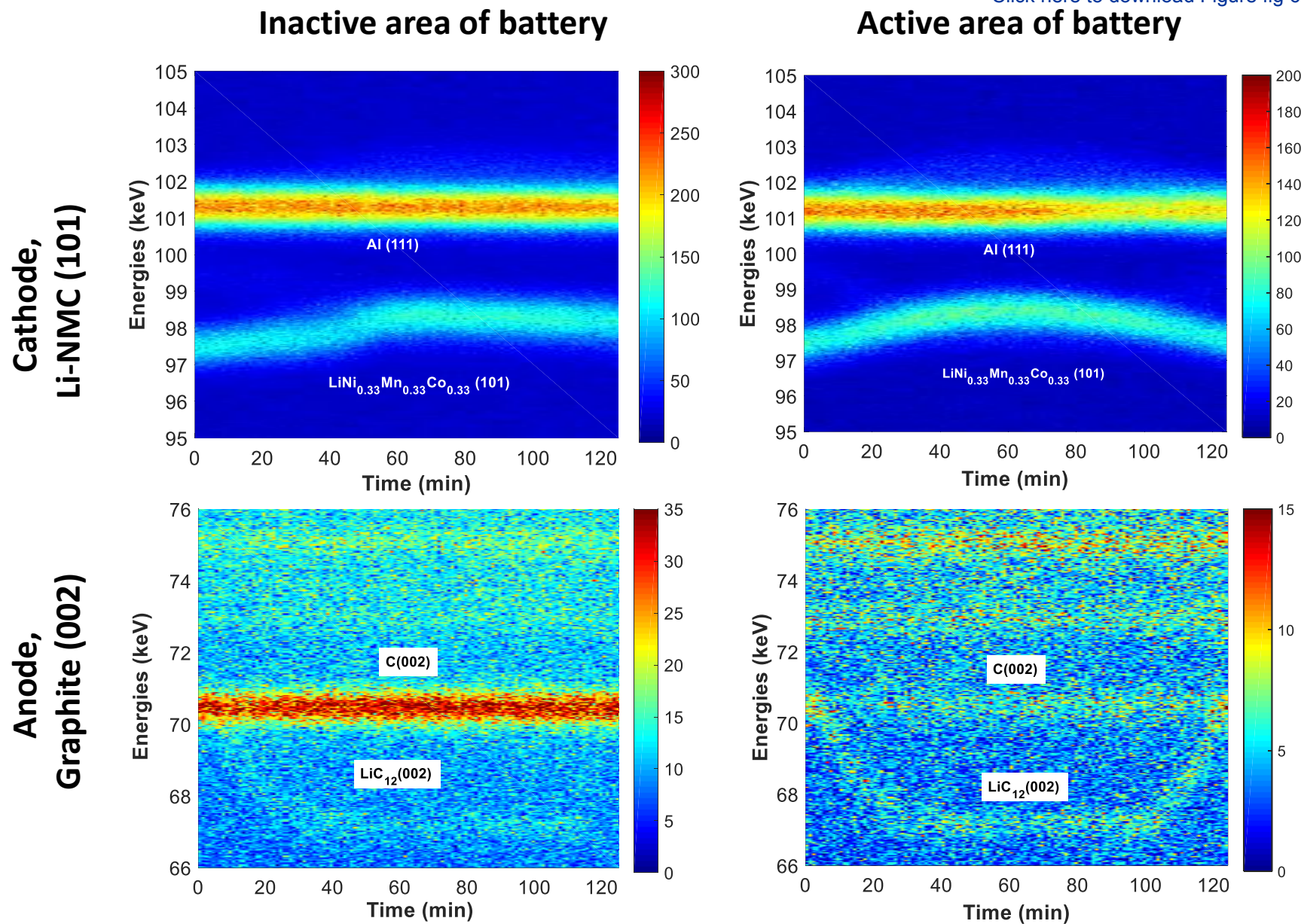


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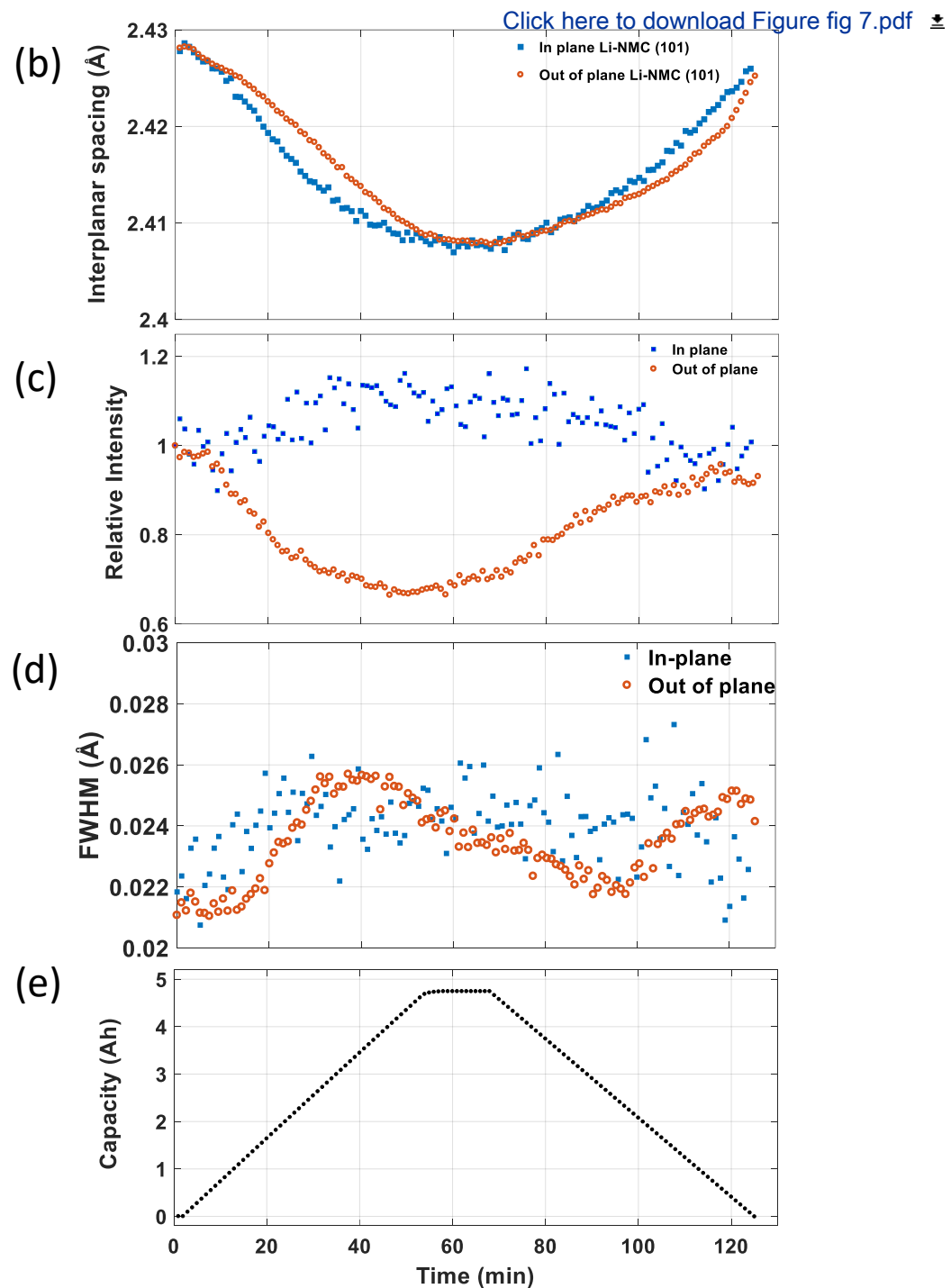
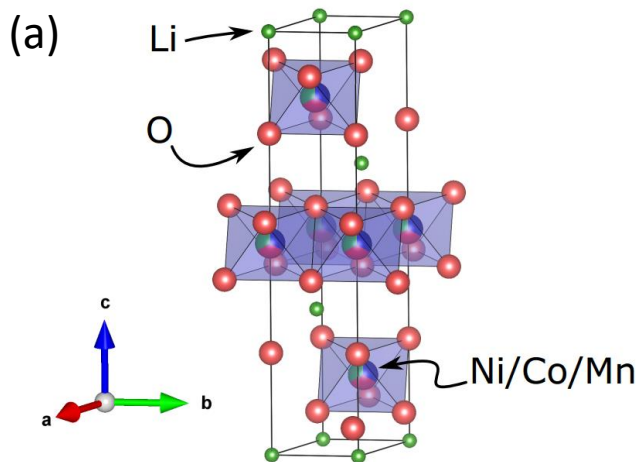
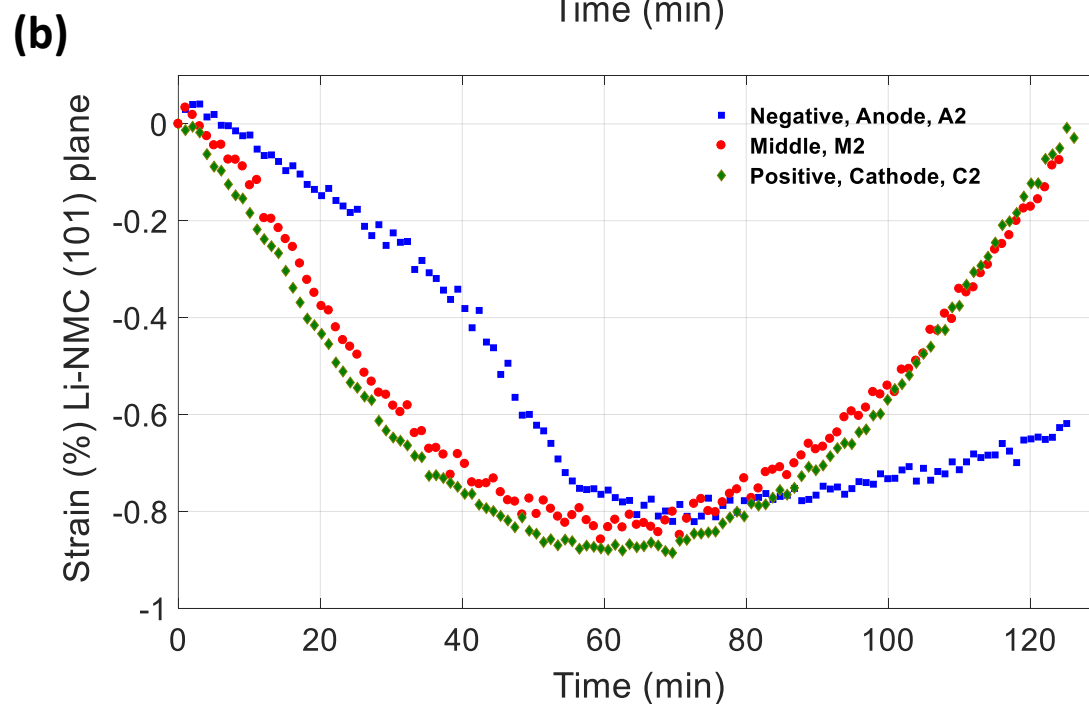
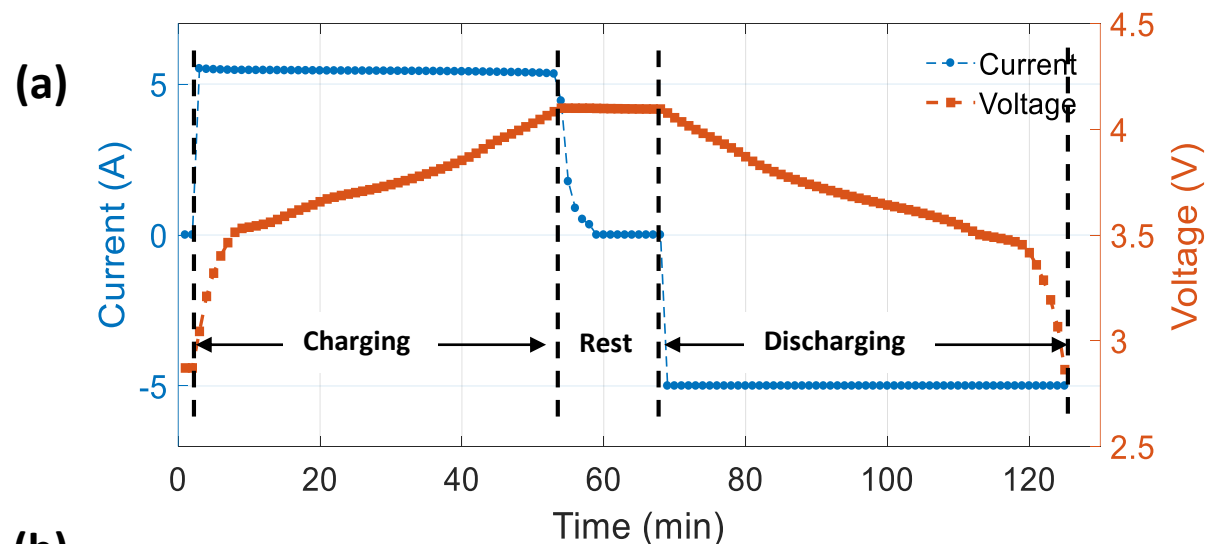
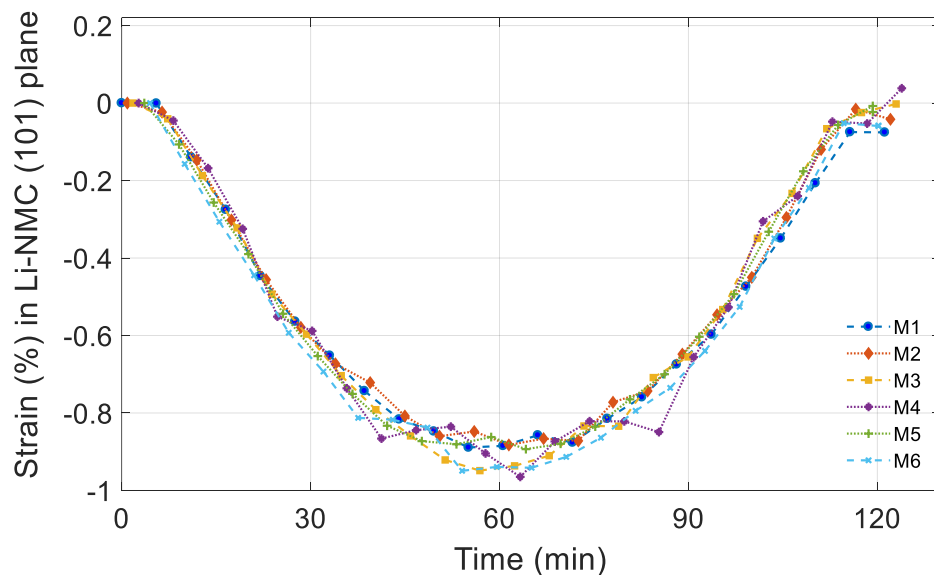


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(a)



(b)

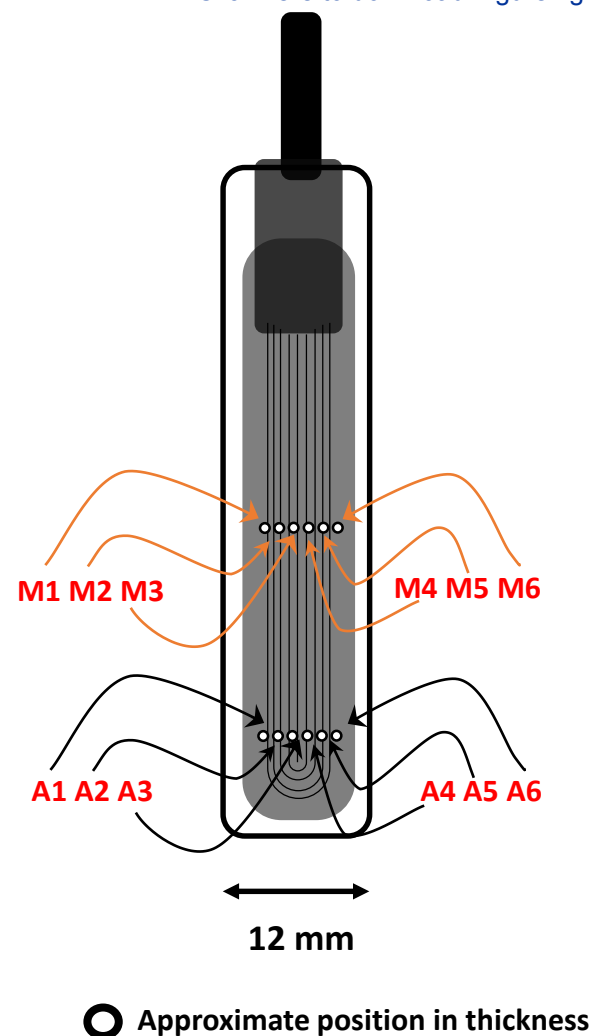
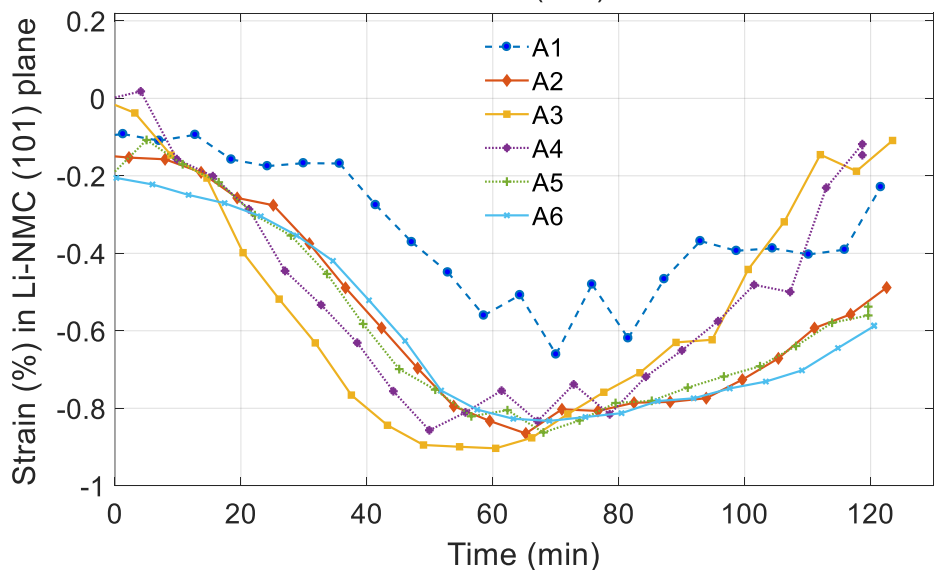


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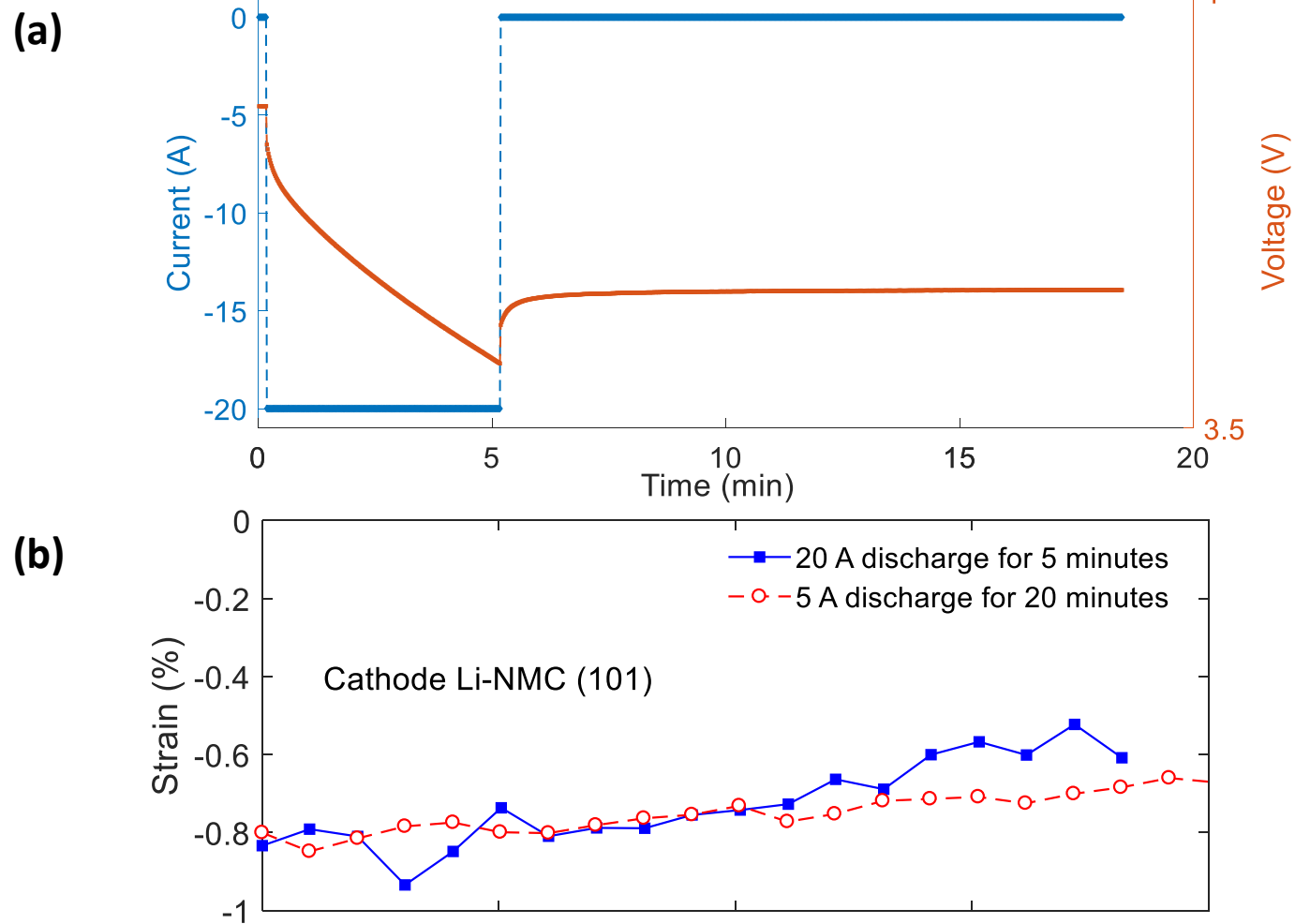


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