

# Force Measurement-Based Discontinuity Detection during Friction Stir Welding

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## Abstract

The objective of this work is to develop a method for detecting the creation of discontinuities (i.e., voids, volume defects) during friction stir welding. Friction stir welding is inherently cost effective,; however, the need for significant weld inspection can make the process cost prohibitive. A new approach to weld inspection is required in which an in situ characterization of weld quality can be obtained, reducing the need for postprocess inspection. To this end, friction stir welds with subsurface voids and without voids were created. The subsurface voids were generated by reducing the friction stir tool rotation frequency and increasing the tool traverse speed in order to create “colder” welds. Process forces were measured during welding, and the void sizes were measured postprocess by computerized tomography (i.e., 3D X-ray imaging). Two parameters, based on frequency domain content and time-domain average of the force signals, were found to be correlated with void size. Criteria for subsurface void detection and size prediction were developed and shown to be in good agreement with experimental observations. With the proper choice of data acquisition system and frequency analyzer the occurrence of subsurface voids can be detected in real time.

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*Keywords:* Friction Stir Welding, Discontinuity detection, Force measurement, Aluminum

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# Nomenclature

## Symbols

dp	Probe diameter [mm]
f	Feed rate [mm/min]
Fy	Force in weld direction [N]
Fy <sub>av</sub>	Average force in weld direction [N]
Fy <sub>1<sup>3</sup></sub>	3rd harmonic of y-force normalized by 1 <sup>st</sup> harmonic of y-force [-]
Fy <sub>Av</sub> <sup>3</sup>	3rd harmonic of y-force normalized by average y-force [-]
hp	Probe height [mm]
n	Number of flats on the friction stir tool [-]
V <sub>Sz</sub> <sup>D</sup>	Discontinuity volume per revolution normalized by probe stir zone volume [-]

## Greek Symbols

$\omega$	Rotation frequency [rad/sec]
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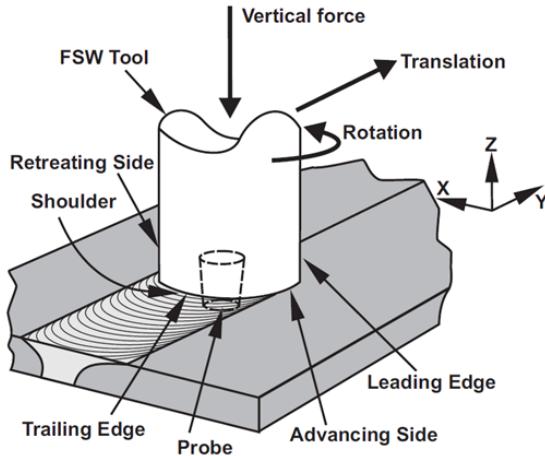
## Acronyms

APR	Advance per revolution (mm/rev)
CT	Computerized tomography
DAQ	Data acquisition
FFT	Fast Fourier transform
FS	Friction stir
FSW	Friction stir welding
ROI	Region of interest
TWI	The welding institute

## 1 Introduction

Friction stir welding (FSW) was invented at The Welding Institute in the United Kingdom (Thomas et al. 1991, 1995). This relatively new joining process differs from most other welding processes by typically not melting the workpiece. As a result, the joining process is energy efficient, environment friendly, and versatile and generates high-quality joints.

FSW is a metal joining process in which two or more components are plastically deformed and mechanically intermixed under mechanical pressure at elevated temperatures (Mishra and Ma, 2005; Threadgill et al., 2009). However, these joints are created at or below the solidus temperature of the workpiece, making FSW a solid-state welding process. Figure 1 shows a schematic of the FSW process for a butt weld. The process involves a nonconsumable rotating friction stir (FS) tool, with a specifically designed probe (pin) and shoulder, which is plunged with a downward force into the workpiece. Once the probe is completely inserted in the workpiece and the shoulder makes contact with the surface, the FS tool is traversed along the weld seam (butt welding) or defined path (lap welding, bead-on-plate, friction stir processing). At the end of the weld the FS tool is retracted. Initially, the FS tool generates heat due to friction, which facilitates plastic deformation of the parent material (i.e., stirring). Once the material is being plastically deformed in the stir zone, heat is generated due to friction and heat dissipation due to plastic deformation. The plasticized material is mixed and extruded past the FS tool, after which it is forged together in the wake of the FS tool. Friction stir welding results in intense plastic deformation at elevated temperature in the weld zone, which leads to significant microstructural evolution, for example, grain refinement (Mishra and Ma, 2005; Threadgill et al., 2009).



**Figure 1:** Schematic of friction stir [butt] welding showing global coordinate system of forces acting on the FS tool

The advantages of FSW are significant and include energy savings, superior mechanical joint properties, and lower process environmental impact as compared with fusion welding processes. While the creation of a friction stir weld can be cost effective, the need for significant weld inspection, particularly in the case of high-reliability applications, can increase the cost by a factor of 3 or more, making it cost prohibitive. Therefore, a new approach to weld inspection is required where an in situ characterization of weld quality can be obtained, significantly reducing the need for post-process inspection.

Boldsaikhan et al. (2011) presented a real-time approach for detecting continuous-void discontinuities in FSW in a nondestructive manner. A discrete Fourier transform and a multilayer neural network were used for evaluating the feedback forces observed during FSW. Fleming et al. (2008) investigated methods for implementing in-process fault avoidance in robotic FSW. They showed that statistical methods can be used as a prestep to derive representations of force data that provide good insight into the state of the on-going weld. Burford et al. (2012) used an e-NDE technique based on monitoring the force feedback signals that were previously correlated with the discontinuity formation. Their work showed promising results for increasing the accuracy and precision of probability of detection analyses when compared with conventional inspection techniques. Singh and Hamilton (2009) assessed FSW quality through dynamic characterization. Modal parameters were measured and correlated with the physical parameters of the welded components such as axial and flexural rigidities. The authors showed that the assessment of weld quality of FSW beams using dynamic interrogation techniques is viable.

Chen et al. (2006) investigated the formation of the discontinuities in 5456 aluminum alloy friction stir welds. Based on the microscopic examination of the nugget zone and the fracture location of the weld, the authors suggested that the tilt angle can change the plastic material flow pattern in the stir zone. They also suggested that the  $\text{Al}_2\text{O}_3$  particles from initial butt surface are the major cause of the failure of the joints. Khan et al. (2015) investigated the effect of FS tool probe offset and plunge depth on the formation of tunneling discontinuities and kissing bonds in friction stir welds with dissimilar alloys (AA5083-H116 and AA6063-T6). The authors reported that tunneling and kissing bond defects were formed in welds with the FS tool probe offset toward the stronger alloy. The size of the tunneling discontinuity decreased significantly by increasing the plunge depth. Kumar et al. (2015) discussed discontinuity detection during FSW using discrete wavelet transform of force and torque signals. Their work showed that the discontinuities present in friction stir welds produce sudden changes in the

features of the force signals. The statistical tool known as square of errors, when implemented on the discrete wavelet transform coefficients, localized the abrupt changes more evidently. Ramulu et al. (2013) analyzed the effect of welding speed, rotation speed, plunge depth, and shoulder diameter on the formation of internal discontinuities during FSW. Friction stir welds created with 2.1 mm thick Al 6061-T6 alloy were investigated in that work. As a criterion for identifying the onset of a discontinuity-free weld region, the authors proposed observing the change in axial force and torque with respect to welding parameters.

Rosado et al. (2010) used an eddy current probe based non-destructive testing system focusing on micro size superficial discontinuities in metallic friction stir welds. The testing results showed that the system was able to detect superficial discontinuities less than 60  $\mu\text{m}$  deep. This method predicts only superficial voids, however, and does not predict the subsurface discontinuities deeper than 60  $\mu\text{m}$ . Santos et al., (2014) presented a concept of FSW assisted by an electric oule effect. This was aimed at minimizing the root discontinuities (lack of penetration) in friction stir welds. Experimental results showed that passing an electrical current through the weld root can significantly reduce the lack of penetration discontinuity. Weld macrographs were made for visualizing the discontinuities. This method allows mitigation of a common discontinuity in FSW: root defect. However, it does not facilitate the detection or estimation of the discontinuity sizes. Zhang et al., (2012) examined the characteristics of discontinuities in underwater friction stir welds and investigated the formation mechanism of the discontinuities. After welding, joints were cross-sectioned perpendicular to the weld direction, and the weld cross-sections were imaged via light microscopy. The authors observed that at relatively high rotation speeds and low welding speed (feed), the material beneath the shoulder tends to be extruded into the probe stirred zone after flowing back to the advancing side. An unstable flow condition results, creating discontinuities in the probe stirred zone. Shrivastava et al. (2015) presented an FSW dynamic force model and discontinuity model for predicting forces and discontinuities during friction stir welding. The weld joints were cross-sectioned and imaged for confirming and measuring the discontinuities. Experimental results showed that the welds with discontinuities are accompanied by higher force amplitudes at higher harmonics corresponding to the number of flats on the FSW tool in addition to the tool rotation frequency.

Yasui et al. (2014) performed dissimilar friction stir welds of aluminum alloy (Al 6061) and steel (S45C). The distribution and size of the steel chips in the weld were studied with an X-ray computerized tomography (CT) method. The macrostructures and CT results were presented for welds without defects. Their work provided direct evidence of the material movement due to the dissimilar nature of the welds and three-dimensional information captured from CT data. However, information regarding any discontinuity formed during FSW was missing. Morisada et al. (2015) used a real-time X-ray imaging system to obtain three-dimensional flow patterns during FSW of Aluminum 1050 plates. The tungsten tracer was used to track the material movement. In that study, X-rays could transmit through workpiece material, backing plate material, and tool material. X-rays were blocked only by the tungsten tracer. A concentric material flow zone was reported around the probe under the optimal FSW conditions. However, any discontinuity formed during FSW was not visible in X-ray images because the X-rays would transmit through all but the tungsten tracer. Edwards and Ramulu (2015) carried out a friction stir weld of 6mm thick Ti-6Al-4V butt joints with a tracer material embedded in the joint. The material flow pattern in these welds was established by examining post-weld X-ray radiographs. That work also made no comments about the discontinuity formation during FSW. To date, all the works that have included CT X-ray for analysis in FSW have focused on studying material flow.

Researchers have explored different types of discontinuities formed during FSW and associated formation mechanisms. Efforts also have been made to detect these discontinuities by measuring various parameters such as force, torque, and temperature during FSW. However, the relationship between measured quantities and discontinuity sizes is missing. Among most of the explored methods for discontinuity detection, discontinuities can be detected without any prediction of the discontinuity

size. Our work focuses on detecting discontinuities by measuring forces during FSW. Our main objective is to develop a relationship between the force transients and the discontinuity sizes. This will enable the detection of discontinuity and prediction of the discontinuity size at the same time.

## 2 Experimental Methods

The friction stir welds were performed on a commercial 3-axis CNC mill (HAAS TM-1). The spindle motor's maximum rating is 5.6 kW, the maximum spindle torque is 45 Nm, and the maximum spindle speed is 4,000 rpm. The FS tool travel angle was held constant at 3 degrees for all the welds. FS tools made of H13 tool steel with a concave shoulder and a threaded, conical probe with flats were used. The FS tool shoulder diameter was 15 mm, and the probe diameter tapered from 7 to 5.4 mm. The FS tool probe was 4 mm long. Workpieces were 203 mm long, 102 mm wide, and 4.76 mm thick Aluminum 6061-T6 alloy. Weld parameters that were held constant throughout the experiments are listed in Table 1.

Advance per revolution (APR) is the ratio of feed/weld rate (mm/min) and spindle speed (RPM) of FS tool during a friction stir weld and has units of mm/rev. Welds were performed at five different APRs: 0.78, 0.83, 0.89, 0.94, and 1.00 mm/rev. For each APR, spindle speed was varied from 600 rev/min to 1000 rev/min in steps of 100 rev/min. These weld parameters are known to produce friction stir welds with discontinuities (i.e., volume defects). Table 2 shows the feed rate corresponding to each APR and rotation speed (RPM) combination for the welds with discontinuities. Beside these 25 welds, 7 welds were performed at conditions known to produce friction stir welds without discontinuities. Table 3 shows the rotation speed and feed rate for the welds without discontinuities. Additional friction stir welds were created in order to validate the discontinuity detection method developed in this work. These welds are discussed in Section 4. Welding forces were measured by using a 3-axis force dynamometer (Kistler model 9265). The FS tool was zeroed in the z-direction (Figure 1) with respect to the FS tool shoulder.

**Table 1:** Weld parameters that were held constant throughout the experiments

Type of Weld	Butt Weld
Workpiece material	6061-T6 aluminum
Workpiece dimensions	203 x 102 x 4.76 mm
Backing plate material	Mild steel
Travel angle	3°
Work angle	0°
Gap	None
Plunge depth	0.2 mm
Weld length	175 mm
FS Tool material	H13 tool steel
FS Tool shoulder: concave angle	3°
FS Tool shoulder: dia.	15 mm
FS Tool probe: conical angle (2θ)	22.6°
FS Tool probe: major dia.	7 mm
FS Tool probe: minor dia.	5.4 mm
FS Tool probe: length	4 mm
FS Tool probe: thread pitch	1.588 mm

Since the FS tool shoulder cannot contact the workpiece top surface (because of the FS tool probe: 4 mm height) directly, a 7.62 mm precision gage-block was placed between the trailing edge of the FS tool and the top surface of the workpiece. Then the FS tool was lowered with minimum increment (0.001 mm) setting in the z-axis, to achieve a defined preload of 20 N in z-direction. This ensured complete contact between the workpiece-precision gage and precision gage-FS tool shoulder interfaces. This method eliminates the inconsistencies in zeroing the z-axis, which results in inconsistent plunge depth between friction stir welds.

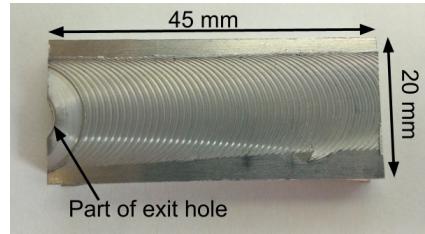
**Table 2:** Feed rate corresponding to each APR and RPM combination for welds with discontinuities

RPM (rev/min)	APR (mm/rev)				
	0.78	0.83	0.89	0.94	1.00
	Feed (mm/min)				
600	467	500	533	567	600
700	544	583	622	661	700
800	622	667	711	756	800
900	700	750	800	850	900
1000	778	833	889	944	1000

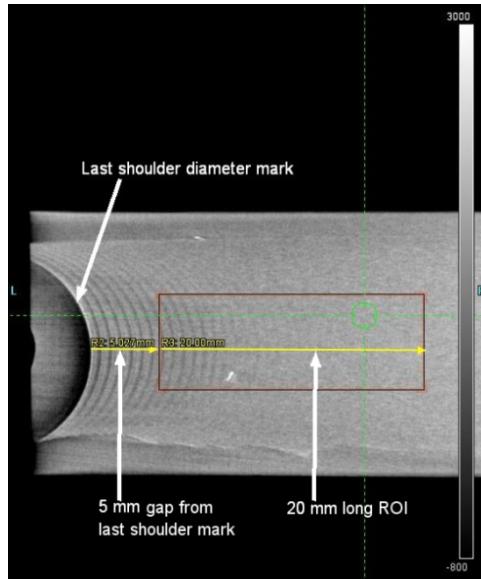
**Table 3:** Rotation speed and feed rate for the welds without discontinuities

Serial No.	RPM (rev/min)	Feed (mm/min)
1	1100	400
2	1100	500
3	1300	300
4	1300	400
5	1300	500
6	1500	400
7	1500	500

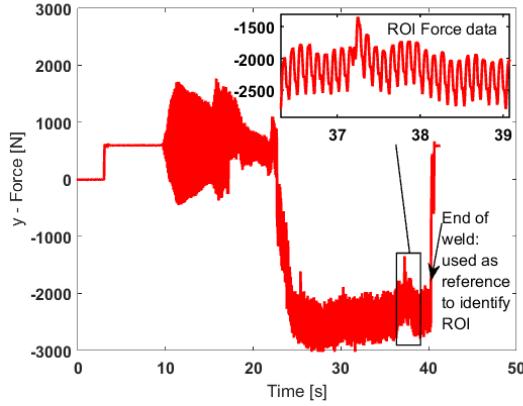
One 20 mm wide and 45 mm long specimen was cut from each weld. Each specimen was cut such that it included a small part of the exit hole. Figure 2 shows an image of a representative specimen. CT scans of these specimens were performed on a Siemens microCATII scanner. The 3D dataset from CT scans was analyzed by using “Inveon Research Workplace” software. The voxel size of the CT scan was  $34 \mu\text{m}^3$ . For consistency, a 20 mm long region of interest (ROI) at a distance of 5 mm from the last shoulder mark was defined for each specimen. Figure 3 shows a representative section. The CT scan datasets from all the welds were analyzed with same threshold values (-800 to 1225 Hounsfield units). The analysis of the CT scan dataset from each weld specimen provided the total discontinuity volume ( $\text{mm}^3$ ) present in the ROI. The force data (along the weld direction: y-direction, Fig. 1) corresponding to the 20 mm long ROI was identified. Figure 4 shows the complete force data and section of force data corresponding to the ROI for a representative friction stir weld. Average force and force amplitudes for the first five harmonics (of the tool rotation frequency) were evaluated for each friction stir weld.



**Figure 2:** Image of a representative specimen for CT scan



**Figure 3:** ROI section defined for a representative CT scan data set



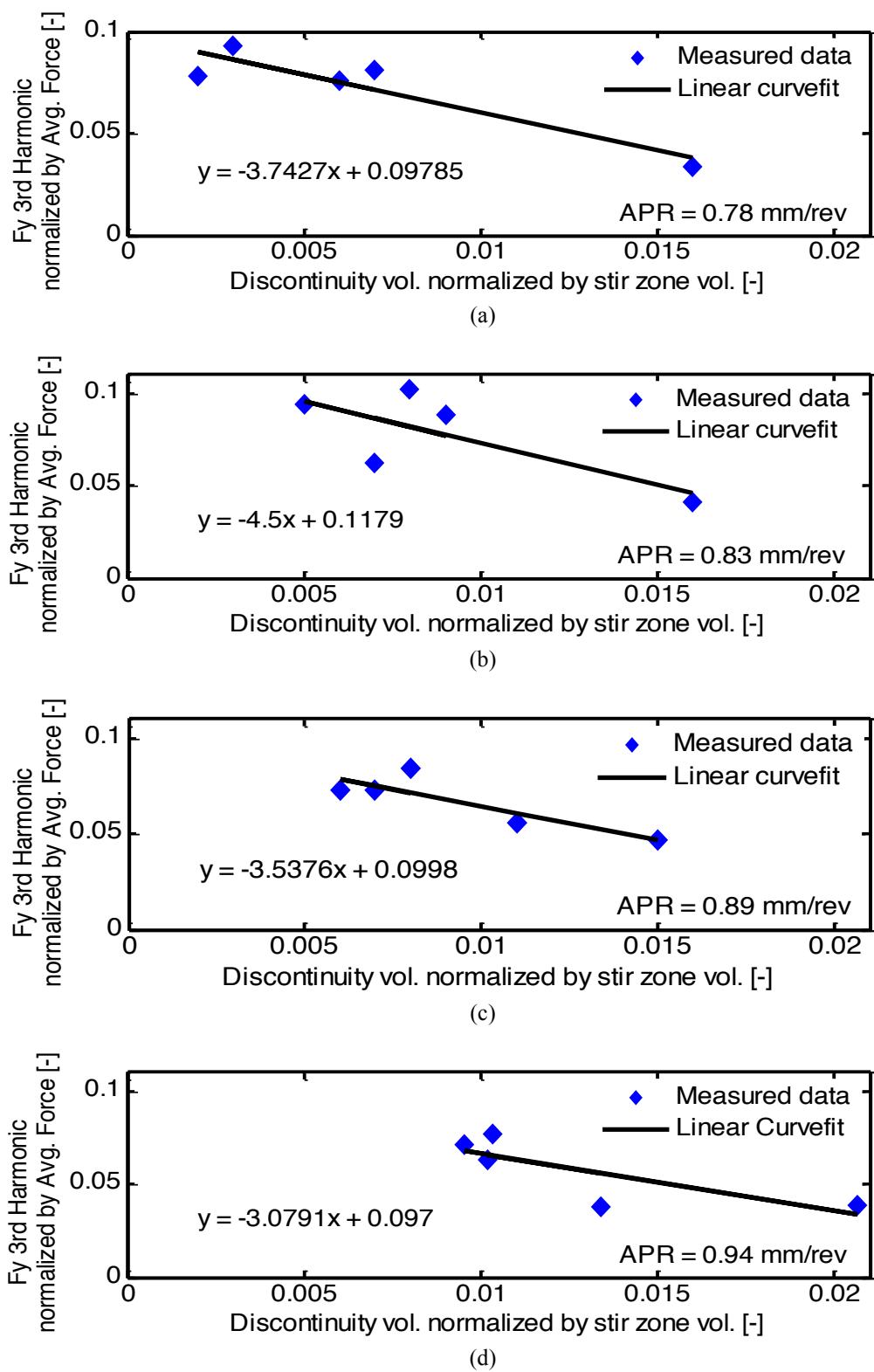
**Figure 4:** Complete force data (along y-direction) and section of force data corresponding to the ROI for a representative friction stir weld

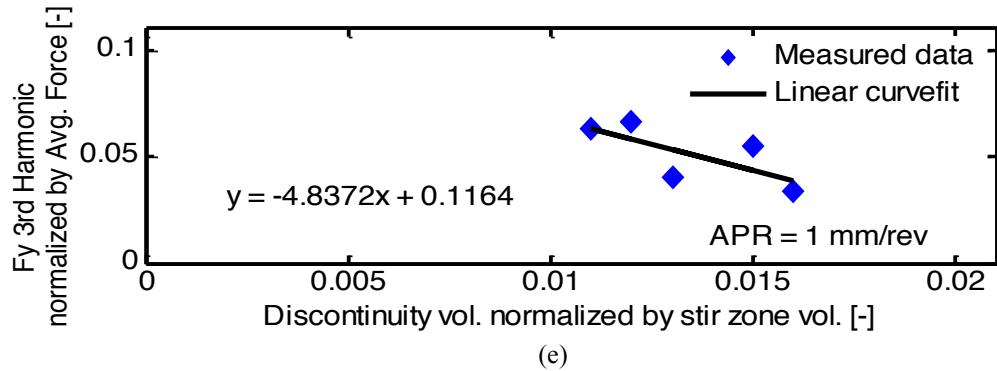
### 3 Results

Analyses of CT datasets provided the total volume of discontinuities present in the ROI of each specimen. The average discontinuity volume formed per revolution was estimated for each weld (total discontinuity volume  $\times$  APR / ROI length). The relationship between the average discontinuity volume formed per revolution and different parameters from the force data (average force, force amplitude at tool rotation frequency and higher harmonics) was investigated. At first no relationship was observed. Next, the relationship between the ratio of different force parameters and the ratio of discontinuity volume per revolution and probe stir zone volume ( $\pi \times$  average probe radius  $\times$  probe height  $\times$  APR) was investigated. The third harmonic of the y-force normalized by the average y-force ( $Fy_{Av}^3$ ) showed a consistent linear relationship with the discontinuity volume per revolution normalized by the probe stir zone volume ( $V_{Sz}^D$ ) for the welds with discontinuities (Figure 5). This result suggests that a linear relationship between  $Fy_{Av}^3$  and  $V_{Sz}^D$  can be used for estimating the discontinuity size.

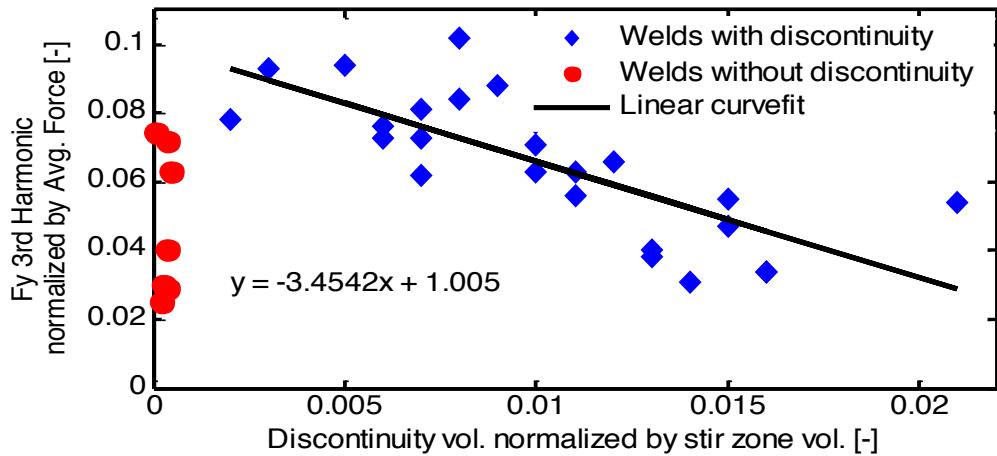
In this work, a normalized parameter's symbol is accompanied with a subscript and a superscript. The subscript represents the “normalized by” parameter or the denominator, and superscript represents the “normalized” parameter or the numerator. For example,  $Fy_{Av}^3$  is the third harmonic of the forces in the y-direction normalized by the average force in the y-direction. Similarly,  $V_{Sz}^D$  is the discontinuity volume formed per revolution normalized by the probe-stir zone volume. Figure 6 shows the plot of  $Fy_{Av}^3$  vs  $V_{Sz}^D$  for all the welds (with and without discontinuities: Tables 2 and 3). One can see from the figure that the range of the magnitude of  $Fy_{Av}^3$  for welds without discontinuities is also appreciable and comparable to the range of the magnitude of  $Fy_{Av}^3$  for welds with discontinuities. This result suggests that  $Fy_{Av}^3$  cannot be used for differentiating between welds with and without discontinuities.

Figure 7 shows the plot of  $Fy_1^3$  vs  $V_{Sz}^D$  for all the welds (with and without discontinuities: Tables 2 and 3). One can see that  $Fy_1^3$  for welds with discontinuities does not indicate any trend with respect to  $V_{Sz}^D$ . This result suggests that a relationship between  $Fy_1^3$  and  $V_{Sz}^D$  cannot be effectively used for estimating discontinuity sizes for the welds with discontinuities. However,  $Fy_1^3$  for welds without discontinuities is distinctly smaller than  $Fy_1^3$  for the welds with discontinuities. This distinction in  $Fy_1^3$  can be used for distinguishing between welds with and without discontinuity.

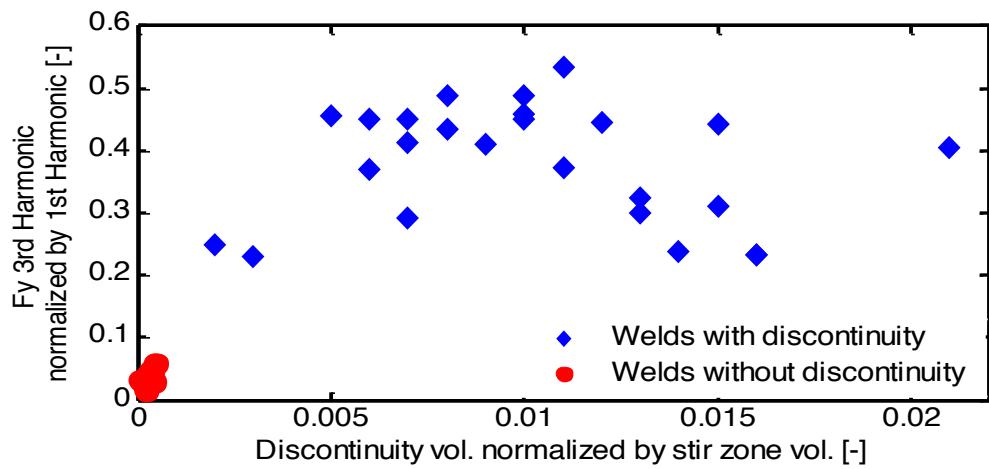




**Figure 5:**  $Fy_{Av}^3$  as a function of  $V_{Sz}^D$  for the welds with discontinuities performed at (a) 0.78 mm/rev APR (b) 0.83 mm/rev APR (c) 0.89 mm/rev APR (d) 0.91 mm/rev APR (e) 1 mm/rev APR



**Figure 6:**  $Fy_{Av}^3$  as a function of  $V_{Sz}^D$  for the welds with and without discontinuities



**Figure 7:**  $Fy_1^3$  as a function of  $V_{Sz}^D$  for the welds with and without discontinuities

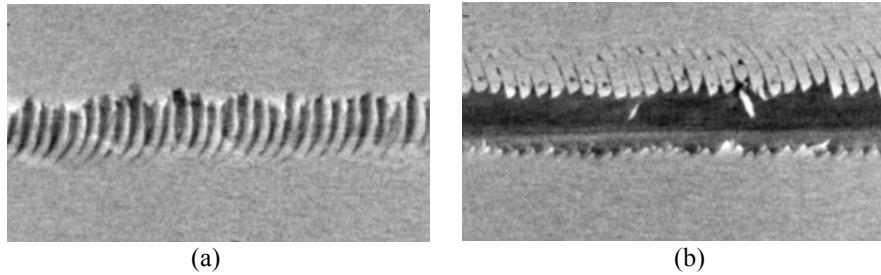
## 4 Discussion

In this paper, welds with discontinuity were created by increasing the feed rate and reducing the spindle rotation speed. This process results in a relatively lower weld temperature than the temperature required for a weld without discontinuity. The reduced temperature makes it difficult to plastically deform the material and move the material around the tool, thus increasing the resistance offered by the material to the FSW tool movement in the weld direction. As a result the average force experienced by the FSW tool in the weld direction increases. More aggressive conditions (higher feed rate and reduced spindle speed) resulted in the formation of larger discontinuities in the stir zone volume. These conditions also resulted in a higher average force in the weld direction, as evident from the negative slope of the linear trend line (for welds with discontinuities) in Figure 6. In that figure, as the ratio of the discontinuity volume to the stir zone volume ( $V_{Sz}^D$ , along the x-axis) increases, the average force in the weld direction increases. The result is an overall reduction in the ratio of the Fy third harmonic amplitude to the average force in the weld direction ( $Fy_{Av}^3$ ). The mean value of the “average force in the weld direction” for all the welds without discontinuities is 235 N, whereas for all the welds with discontinuities it is 1776 N. In Figure 6, however, the magnitude of  $Fy_{Av}^3$  for welds without discontinuities compares well with the  $Fy_{Av}^3$  for the welds with discontinuities. The reason is the difference in the magnitude of the Fy third harmonic amplitude between the welds with and without discontinuities. The mean value of the Fy third harmonic amplitude for all the welds without discontinuities is 11 N, whereas for all the welds with discontinuities it is 109 N. For welds with discontinuities, the relatively higher magnitude of Fy third harmonic amplitude is attributed to the discontinuities formed in the stir zone (discussed later in this section).  $Fy_{Av}^3$  captures the effect of this difference in weld conditions as well as the discontinuity formation during welding. Accounting for the difference in the weld conditions is important because the welds with and without discontinuities were performed with different weld parameters (Tables 2 and 3), and a change in a given metric can be due either to different weld conditions or to discontinuity formation. This result gives trust in the relationship between  $Fy_{Av}^3$  and  $V_{Sz}^D$  for the welds with discontinuities. However, the range of the magnitude of  $Fy_{Av}^3$  for welds without discontinuities is also appreciable and comparable to the range of the magnitude of  $Fy_{Av}^3$  for welds with discontinuities (Figure 6). Therefore,  $Fy_{Av}^3$  cannot be used for differentiating between welds with and without discontinuities.

In a previous work (Shrivastava et al., 2015), experimental results suggested that the welds with discontinuities are accompanied by higher force amplitudes at higher harmonics corresponding to the number of flats on the FSW tool in addition to the tool rotation frequency. The process force oscillations at higher harmonics originate from the interaction of the discontinuities with flats on the FSW tool probe. That is, the FSW tool experiences additional force components every time an FSW tool probe flat passes through the region where the discontinuity is being formed. The force magnitude at the higher harmonics (corresponding to the number of flats) will depend on the size of the discontinuity, morphology of the discontinuity, and weld parameters. All these parameters varied across the experiments reported here, resulting in the scatter in the  $Fy_3^3$  data shown in Figure 7.

To explain the scatter in Figure 7, consider Figure 8 which shows two extremely different discontinuity morphologies observed among the welds with discontinuity. These discontinuities are at the depth of 2.4 mm (half of the workpiece height) from the top surface of the workpiece. In Figures 8(a) and 8(b) discontinuities are present in the advancing side. In Figure 8(a), the discontinuities have the form of a stack of arcs aligned in the weld direction. In Figure 8(b), the discontinuity looks like a continuous trench. However, a closer look at the discontinuities reveals not-so-pronounced arc-shaped features preceding the trench. Further investigation confirmed the formation and filling of a cavity by the material once per revolution at the rear of the tool, resulting in the oscillation of the forces in the y-direction at the tool rotation frequency (first harmonic). The magnitude of the Fy oscillations at the tool rotation frequency will be decided by the amount of the material rotated around the FSW tool per revolution. The maximum size of the discontinuity formed per revolution in this work was about 2%

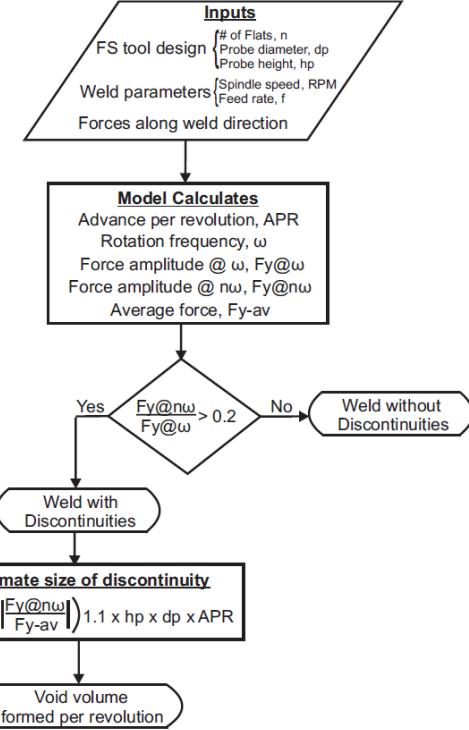
of the probe stir zone volume. This should minimally affect the force amplitudes at the tool rotation frequency. A comparison shows that the mean value of the  $F_y$  first harmonic amplitude for welds with discontinuities is 295 N (with standard deviation of 53 N) and without discontinuity is 298 N (with standard deviation of 36 N). Therefore,  $F_y^3$  essentially represents the variation in the  $F_y$  third harmonic amplitude (Figure 7). Despite the scatter in  $F_y^3$  for the welds with discontinuity in Figure 7,  $F_y^3$  for welds without discontinuities is distinctly smaller than  $F_y^3$  for welds with discontinuities. This distinction in  $F_y^3$  can be used for distinguishing between welds with and without discontinuity. It is believed that a normalized  $F_y$  third harmonic metric ( $F_y^3$ ) would be better applicable across different FS tool designs and weld conditions.



**Figure 8:** Images from CT scans of two representative friction stir weld regions of interest: (a) discontinuities in the form of sub-surface stack of arcs, and (b) discontinuities in form of a subsurface continuous trench (field of view = 16 mm×8.8 mm; image plane is 2.4 mm below the surface)

#### 4.1 Discontinuity detection method

Based on the findings of this work, we propose a discontinuity detection method; see Figure 9 for the flowchart of the proposed method. This method takes into consideration the FS tool design (number of flats, probe diameter, and probe height) and weld parameters (spindle rotation speed and feed rate). Forces along the weld direction ( $F_y$ ) are used as the input to the method. Advances per revolution, tool rotation frequency,  $F_y$  amplitude corresponding to tool rotation frequency,  $F_y$  amplitude at the harmonic corresponding to the number of flats on the FS tool, and average  $F_y$  are discerned from the available information. Next, the ratio of the  $F_y$  third harmonic amplitude to the  $F_y$  first harmonic amplitude are compared with a threshold value of 0.2 (from Figure 7). If the ratio is smaller than the threshold value, the weld is evaluated as a “weld without discontinuity.” Otherwise, the weld is evaluated as a “weld with discontinuity,” and the size of the discontinuity formed per revolution is calculated in accordance with the linear trend identified from Figure 6.



**Figure 9:** Flowchart of the proposed discontinuity detection and discontinuity size prediction method

## 4.2 Method validation

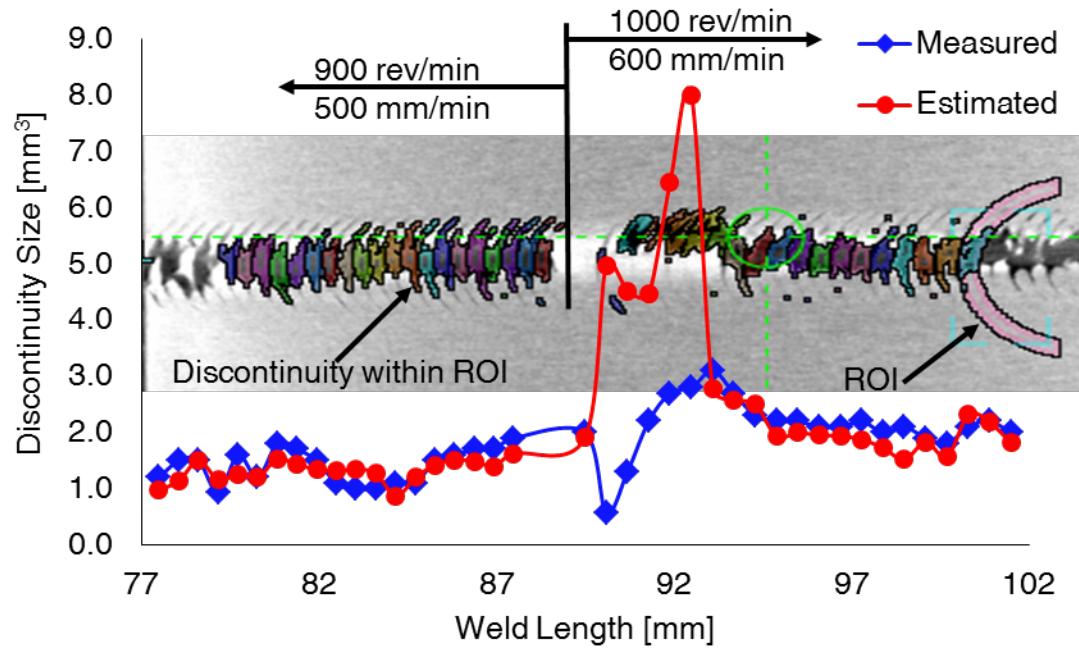
Experiments with additional friction stir welds were performed in order to validate the proposed discontinuity method. The RPM, feed rate, workpiece thickness, and tool design (number of flats) were varied in these experiments. The friction stir welds were CT scanned in order to measure the discontinuity sizes. Table 4 shows the weld conditions, measured discontinuity volume per rev, estimated discontinuity volume per revolution, and error for the validation welds.

**Table 4:** Weld conditions, measured discontinuity volume per rev, estimated discontinuity volume per revolution, and error for the validation welds

RPM (rev/min)	Feedrate (mm/min)	No. of FS Tool Flats	Fy@nw Fy@ω	Discontinuity		Discontinuity		
				Observed in Weld?	Estimated (mm <sup>3</sup> /rev)	Measured (mm <sup>3</sup> /rev)	Error (%)	
900	300	3	0.03	No	-	-	-	
900	350	3	0.09	No	-	-	-	
900	400	3	0.21	Yes	0.92	0.96	4.2	
900	450	3	0.23	Yes	1.24	1.18	4.6	
900	500	3	0.75	Yes	1.19	1.30	8.9	
1000	600	3	0.86	Yes	1.90	2.20	13.5	
900	500	2	0.82	Yes	2.38	2.85	19.9	

A friction stir weld experiment was performed such that the weld parameters were switched from 900 rev/min (spindle speed) and 500 mm/min (feed) to 1000 rev/min (spindle speed) and 600 mm/min

(feed) midway (90 mm from beginning of weld) along the weld length (180 mm). Both sets of parameters are known to create welds with discontinuities. A 45-mm-long CT scan specimen was prepared and was centered at the middle of the weld length. Multiple semicircular ROIs were created such that each ROI covered the material moved in each APR. This configuration was achieved by aligning the ROIs with the features created by the discontinuities in the weld. The discontinuity sizes were measured for each ROI. Figure 10 shows the discontinuity size for each ROI along the length of the CT scan specimen. One can see that the estimated discontinuity size (red line) tracks the measured discontinuity size (blue line) well during the steady state. However, the estimated discontinuity size does not follow the measured discontinuity size during the transition from one set of weld conditions to a second set of weld conditions. Figure 10 shows that approximately 5–7 revolutions were needed for the transition from one set of weld conditions to another. This discrepancy between the measured and estimated discontinuity sizes is tied to the formulation of the discontinuity detection method. The method looks for any deviation from the steady-state behavior and assumes that the deviation is due to the discontinuity formation. However, when weld parameters transition from one set of conditions to another, there will be additional dynamics in the force signal due to the acceleration or deceleration of the tool (in both spindle speed and feed) and CNC response.



**Figure 10:** Discontinuity sizes along the weld length as weld parameters change

#### 4.3 Uncertainty involved with measurements

The force dynamometer, charge amplifier, and data acquisition were identified as the uncertainty sources for the force measurement. An uncertainty of  $\pm 9.4$  N was involved with the measurement of forces in the y-direction. This uncertainty in force measurement was used to estimate the uncertainty in the normalized forces presented in Figures 5, 6, and 7. The order of uncertainty involved with the normalized forces in Figures 5 and 6 is -3; the order of normalized forces in Figures 5 and 6 is -2; the order of uncertainty involved with the normalized forces in Figure 7 is -2; and the order of normalized

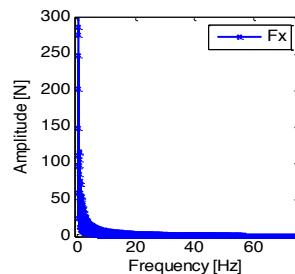
forces in Figure 7 is -1. Therefore, uncertainty involved with the normalized forces is smaller than the magnitudes presented in this work by order of -1.

A representative CT specimen (with discontinuity) was scanned five times, and dark-light calibration was performed for each scan. The discontinuity size measurement had a standard deviation of  $0.3 \text{ mm}^3$ . For the given FS tool dimensions and this standard deviation, the order of the uncertainty involved with the normalized discontinuity volume (Figures 5, 6, and 7) is estimated to be -4. Some of the normalized discontinuity volume magnitudes have an order of -3, while the rest have an order of -2. In either case the uncertainty involved with the normalized discontinuity volume is smaller than the magnitudes presented in this work by an order of -1. For welds without discontinuity, some measurements had the same order as the order of the estimated uncertainty (-4). Thus it could be assumed that the void size given by CT software is essentially measurement uncertainty, and void size could be shown in results as zero  $\text{mm}^3$ . However, no such assumption was made and the void sizes for the welds without discontinuities are presented as such (as given by the CT software).

#### 4.4 Method limitations

Two particular limitations of the discontinuity detection method have been identified thus far.

1. The proposed method can be used only for FS tools with two or more flats. Figure 11 shows the frequency content of the force data measured during the FSW of a weld performed with an FS tool with only one flat. This weld was performed at conditions known to create a weld with discontinuities (i.e., subsurface voids). A macrograph was made to confirm the presence of discontinuities in the weld. The discontinuity detection method presented in this paper is based on the assumption that the generation of discontinuities is accompanied by force dynamics at a frequency corresponding to the number of flats on the FS tool (number of flat times the tool rotation frequency). These force dynamics occur in addition to the force dynamics associated with cavity formation and filling that occur during every tool rotation, whether a discontinuity remains in the weld or not. The discontinuity detection method relates the additional force dynamics (for welds with discontinuity) with the discontinuity size. However, for a friction stir weld with discontinuities created with the 1-flat FS tool, the additional force dynamics and the regular force dynamics occur at the same (tool rotation) frequency and appear to nullify each other (Figure 11). Hence, the proposed method is inapplicable in the case of FSW with the 1-flat FS tool.



**Figure 11:** Frequency domain content of x-force signal measured during FSW performed with the 1-flat FS tool

2. The proposed discontinuity detection method inaccurately captures the size of the discontinuities during the transition of weld parameters. Figure 10 shows that the estimated discontinuity size does not follow the measured discontinuity sizes during the transition from one set of weld parameters (spindle speed and feed) to another set of conditions. The discontinuity detection method does not account for the additional force dynamics observed during the transition. For such applications a model (in addition to the proposed discontinuity model) needs to be developed

that can capture the force dynamics originating from the transition of the weld parameters (acceleration or deceleration of the spindle speed or feed of FS tool).

## 5 Conclusions

The frequency and time-domain content of process force signals can be correlated to the occurrence and size of discontinuities (i.e., subsurface voids, volume defects) during friction stir welding of 6061-T6 aluminum. One force-signal parameter is needed to predict the onset of a subsurface void, and another is needed to predict the size of the volume defect(s) being generated.

In order to predict the occurrence of a subsurface void, a force parameter is defined based on a ratio of force magnitudes taken from the frequency spectrum of the force signal: amplitude of the third harmonic of the weld-direction force ( $F_y$ ) divided by the amplitude of the first harmonic of  $F_y$ . The third harmonic is used because it corresponds to the number of FS tool flats. This is referred to as a normalized force transient. The force amplitude at the higher harmonic corresponds to the number of flats on the friction stir (FS) tool's probe. The normalized force transient data and normalized discontinuity size were correlated to develop criteria for discontinuity detection and discontinuity estimation. A threshold value of 0.2 for the ratio of the  $F_y$  third harmonic (corresponding to number of FS tool flats) amplitude to the  $F_y$  first harmonic amplitude was determined for discontinuity detection. If the ratio is smaller than the threshold value, the weld is evaluated as a "weld without discontinuity." Otherwise, the weld is evaluated as a "weld with discontinuity."

In order to predict the total volume of voids formed during FSW, a different parameter was used: the amplitude of the third harmonic of  $F_y$  divided by the average  $F_y$  force. A linear relationship between this normalized force parameter and discontinuity size normalized by the stir zone volume was determined. This relationship allows the estimation of discontinuity size.

The force-signal parameters were discerned from the force measurements taken during each rotation of the FS tool. The frequency content of the force signal can be calculated with a fast Fourier Transform. The amplitudes of the first and third harmonics (for the FS tool with three flats on its probe) can be pulled from the frequency spectrum. With the proper choice of data acquisition system and frequency analyzer, the occurrence and size of sub-surface voids can be detected in real time, so that corrective actions can be taken.

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