

AE-307

UDC 519.281:53.088

AE-307

Solution of Large Systems of Linear Equations
with Quadratic or Non-Quadratic Matrices
and Deconvolution of Spectra

K. Nygaard



AKTIEBOLAGET ATOMENERGI

STOCKHOLM, SWEDEN 1967

SOLUTION OF LARGE SYSTEMS OF LINEAR EQUATIONS WITH
QUADRATIC OR NON-QUADRATIC MATRICES AND
DECONVOLUTION OF SPECTRA

K Nygaard

AB Atomenergi, Studsvik, Nyköping, Sweden

ABSTRACT

The numerical deconvolution of spectra is equivalent to the solution of a (large) system of linear equations with a matrix which is not necessarily a square matrix. The demand that the square sum of the residual errors shall be minimum is not in general sufficient to ensure a unique or "sound" solution. Therefore other demands which may include the demand for minimum square errors are introduced which lead to "sound" and "non-oscillatory" solutions irrespective of the shape of the original matrix and of the determinant of the matrix of the normal equations.

Printed and distributed in December, 1967

LIST OF CONTENTS

	<u>Page</u>
Introduction	3
I. Description of the problem	4
II. Transforming a rectangular matrix into an equivalent triangular matrix	7
III. The computer solution	11
IV. Discussion of errors	13
Acknowledgement	15

INTRODUCTION

The classical measuring theories deal mainly with a statistical treatment of data obtained by measurements on identified objects. However, in modern physics one often collects a series of data and the task is then to identify some objects by means of a statistical treatment of the collected data. Hereby the conditions for using the classical theories on modern measurements are altered, a fact which is often overlooked and which might give rise to completely misleading results. For instance, there is a great difference in evaluating data from a spectrum consisting of known spectral lines and in evaluating which lines are present in a measured spectrum. Naturally one ought to use different statistical methods in the two cases, but the classical theories which are applicable to the former problem have such an authority that they are often applied without reservation to the latter despite the fact that one of the conditions (identified objects) is missing. It is the aim of this paper to present a new method for deconvolution of spectra. This is done numerically and is equivalent to the solving of a system of linear equations with square or non-square matrices.

I. DESCRIPTION OF THE PROBLEM

Let

$$y(t) = \int_{u_1}^{u_2} x(u)g(t, u)du \quad (1)$$

represent a known (measured) spectrum $t_1 \leq t \leq t_2$, $g(t, u)$ the generating function and $x(u)$, $u_1 \leq u \leq u_2$, the wanted spectrum. In order to treat the problem numerically it is common to write the numerical values of y and g in a, naturally finite number of points or

$$\begin{aligned} y(t_1) &= \Delta u [g(t_1, u_1)x(u_1) + g(t_1, u_1 + \Delta u)x(u_1 + \Delta u) + \dots] \\ y(t_1 + \Delta t) &= \Delta u [g(t_1 + \Delta t, u_1)x(u_1) + g(t_1 + \Delta t, u_1 + \Delta u)x(u_1 + \Delta u) + \dots] \end{aligned} \quad (2)$$

With the abbreviations

$$y_r = y(t_1 + (r-1)\Delta t) \quad (3)$$

$$\underline{y} = \begin{Bmatrix} y_1 \\ y_2 \\ \cdot \\ \cdot \\ y_N \end{Bmatrix} \quad (4)$$

$$x_s = [x(u_1 + (s-1)\Delta u)] \Delta u \quad (5)$$

$$\underline{x} = \begin{Bmatrix} x_1 \\ x_2 \\ \cdot \\ \cdot \\ x_M \end{Bmatrix} \quad (6)$$

$$a_{rs} = g(t_1 + (r-1)\Delta t, u_1 + (s-1)\Delta u) \quad (7)$$

$$\underline{a}_s = \begin{Bmatrix} a_{1s} \\ a_{2s} \\ \cdot \\ \cdot \\ a_{Ns} \end{Bmatrix} \quad (8)$$

$$\underline{A} = \left\{ \begin{array}{cccc} a_{11} & a_{12} & \dots & a_{1M} \\ a_{21} & & & \\ \vdots & & & \\ a_{N1} & & & a_{NM} \end{array} \right\} \quad (9)$$

the equations (2) are written

$$\underline{y} = \underline{A} \underline{x} \quad (10)$$

In (10) \underline{y} and \underline{A} are known quantities and \underline{x} is to be found. Seemingly (10) can be solved by assuming that $N = M$ and that $|\underline{A}_{NM}|$, the determinant of \underline{A} , is different from zero. In that specific case

$$\underline{x} = \underline{A}_{NN}^{-1} \underline{y} \quad (11)$$

If \underline{x} found from (11) is to be regarded as a sound solution to (1) it must be only marginally dependent on the chosen number $N = M$. In practice N , the dimension of \underline{y} , has an upper limit. If \underline{y} is a spectrum recorded by means of a multichannel analyzer, N_{\max} is equal to the number of channels and, if \underline{y} is logged from a continuously recorded spectrum, it is of no use to go beyond the point at which any value of $y(t)$ can be found - within the experimental error limits - by means of linear interpolation between two chosen neighbour points y_2 and y_{r+1} . Now suppose that $M = N_{\max}$ and $|\underline{A}_{NN}| \neq 0$. Then (11) represents a solution which can be found with a computer in the well known way. Let the solution be denoted \underline{x}_0 . The solution \underline{x}_0 inserted in (10) yields

$$\underline{y} = \underline{A}_{NN} \underline{x}_0 + \underline{\varepsilon}$$

where $\underline{\varepsilon}$ represents the unavoidable computational errors which ought to be well within the limit of the experimental errors. To judge the "quality" of \underline{x}_0 a new subdivision $\Delta_1 u = \frac{1}{2} \Delta u$ is made.

By defining

$$\underline{x}_d = \left\{ \begin{array}{c} x_1 \\ x_3 \\ x_5 \\ \cdot \\ \cdot \\ x_{2N-1} \end{array} \right\} \quad (13)$$

and

$$\underline{x}_f = \left\{ \begin{array}{c} x_2 \\ x_4 \\ \cdot \\ \cdot \\ x_{2N-2} \end{array} \right\} \quad (14)$$

we get

$$\underline{A}_{NN} \underline{x}_d + \underline{B} \underline{x}_f = \underline{y}_N \quad (15)$$

where B is an (N-1)·N dimensional matrix. As it is assumed that $|A_{NN}| \neq 0$, (15) can be solved for \underline{x}_d by assuming an arbitrarily chosen vector \underline{x}_f . This simply means means that we can choose half of the x coordinates arbitrarily and calculate the other half or, in other words, there are infinitely many functions $x(u)$ which satisfy (1) for given $y(t)$ and given $g(t, u)$ in a finite interval t_1 through t_2 and u_1 through u_2 . A unique solution does not exist unless further conditions are forced on $x(u)$. One might, for instance, demand that $x(u)$ shall be a, in some sense, smooth function of u, but first it is valuable to study (10) a little further. It is evident that the better this equation represents (1), the greater the probability of finding a representative solution. That means that a very small Δu is desirable. On the other hand it is desirable to have as few numbers as possible in \underline{A} to save computational work. A suitable compromise is to make the interval Δu so small that any three succeeding \underline{a}_s , \underline{a}_{s+1} and \underline{a}_{s+2} (see (8)) are mutually linearly dependent (within the error limits). In that case the equation (10)

contains all information available from (1) because any $g(t, u)$ value can be obtained by linear interpolation if necessary. We might say that any \underline{x} vector which satisfies (10) is a solution to the deconvolution of the $y(t)$ spectrum, but the fact that the physicist who poses the problem will not accept such an answer means that he has certain expectations on the solution which are not contained in (10). Such expectations are very hard to express in a way that is understandable to a computer, especially because they may be contradictory to the demand that (10) must also be satisfied. Thus the expectations must be expressed in such a way that they are satisfied as far as possible - i. e. without violating (10). A very fruitful way to express the expectations is to deliver an expected solution \underline{x}_e and to demand $(\underline{x}_e - \underline{x})^T (\underline{x}_e - \underline{x}) = \text{minimum}$ on condition that (10) is satisfied. Then the problem has a unique solution and a series of computations has shown that the solution does not depend much on \underline{x}_e , which therefore might be put equal to the zero vector. Even if the solution found in this way is not quite satisfactory, it is nevertheless much better than the assumed \underline{x}_e . It can therefore be used as basis for an estimation of a new \underline{x}_e provided that one can present a more explicit formulation of one's demands. At least one should be able to tell why the solution found was not satisfactory.

II. TRANSFORMING A RECTANGULAR MATRIX INTO AN EQUIVALENT TRIANGULAR MATRIX

The problem of deconvolution of spectra has now turned into the problem of solving the equation

$$\underline{y} = \underline{A} \underline{x} \tag{16}$$

for given \underline{y} and \underline{A} which is not necessarily a square matrix. If there is more than one solution, the one which gives

$$(\underline{x} - \underline{x}_e)^T (\underline{x} - \underline{x}_e) = \text{minimum} \tag{17}$$

is chosen. \underline{x}_e represents an "expected" solution which is considered to be given. The system of equations (16) might be overdetermined ($N > M$) and in that case we may write

$$\underline{y} = \underline{A} \underline{x} + \underline{\epsilon} \quad (18)$$

and determine the solution which yields $\underline{\epsilon}^T \underline{\epsilon} = \text{minimum}$. The vector $\underline{\epsilon}$ may be considered to consist of experimental errors and for a "sound" problem we shall have $\underline{y}^T \underline{y} \gg \underline{\epsilon}^T \underline{\epsilon}$. In practice, especially when larger systems are considered, $\underline{\epsilon}$ also depends on computational errors which cannot be disregarded, in fact the computation itself is often the main source of errors. It is therefore necessary to choose a suitable method for the computation. First (18) is considered for $N > M$ (the number of equations is larger than the number of unknowns) with the condition that $\underline{\epsilon}^T \underline{\epsilon} = \text{minimum}$. A traditional method of solving (18) is to multiply both sides by \underline{A}^T and solve

$$\underline{A}^T \underline{y} = \underline{A}^T \underline{A} \underline{x} \quad (19)$$

as it can be proved that $\underline{A}^T \underline{\epsilon} = 0$ for $\underline{\epsilon}^T \underline{\epsilon} = \text{minimum}$. This method has the drawbacks that it only works for $N \geq M$ and when the determinant of $|\underline{A}^T \underline{A}| \neq 0$, and that it is very sensitive to small errors. A much more direct method which demands less computational work and is less sensitive to errors is shown next.

Consider \underline{y} to be a linear combination of the \underline{a} vectors

$$\underline{y} = \underline{a}_1 x_1 + \underline{a}_2 x_2 + \dots + \underline{a}_M \quad (20)$$

Now each vector in (20) is split into a sum of two vectors, the one being proportional to \underline{a}_1 , the other orthogonal to \underline{a}_1 . Thus

$$\underline{a}_s = k_s \underline{a}_1 + \underline{b}_s$$

and

$$\underline{y} = k_y \underline{y} + \underline{b}_y \quad (21)$$

As \underline{b}_s is orthogonal to \underline{a}_1 , ($\underline{a}_1^T \underline{b}_s = 0$), k_s is found by multiplying the equations (21) by \underline{a}_1^T or

$$k_s = \frac{\underline{a}_1^T \underline{a}_s}{\underline{a}_1^T \underline{a}_1} \quad (22)$$

and

$$\underline{b}_s = \underline{a}_s - \frac{\underline{a}_1^T \underline{a}_s}{\underline{a}_1^T \underline{a}_1} \cdot \underline{a}_1 \quad (23)$$

Hence (20) can be written

$$k_y \underline{a}_1 + \underline{b}_y = \underline{a}_1 \{ x_1 + k_2 x_2 + \dots + k_M x_M \} + \underline{b}_2 x_2 + \underline{b}_3 x_3 + \dots + \underline{b}_M x_M \quad (24)$$

Equations (24) consist of two systems which are orthogonal to each other and can therefore be split into two independent systems, namely

$$k_y \underline{a}_1 = (x_1 + k_2 x_2 + \dots + k_M x_M) \underline{a}_1 \quad (25)$$

and

$$\underline{b}_y = \underline{b}_2 x_2 + \underline{b}_3 x_3 + \dots + \underline{b}_M x_M \quad (26)$$

Equations (25) are mutually proportional and are transformed into a single equation by multiplying by \underline{a}_1^T . Using the abbreviations

$$z_1 = k_y (\underline{a}_1^T \underline{a}_1) = \underline{a}_1^T y \quad (27)$$

$$c_{1s} = k_s (\underline{a}_1^T \underline{a}_1) = \underline{a}_1^T \underline{a}_s \quad (28)$$

Equations (25) become

$$z_1 = c_{11} x_1 + c_{12} x_2 + c_{13} x_3 + \dots + c_{1M} x_M \quad (29)$$

Equations (26) do not contain x_1 . They are now treated as the original system, namely each vector in (26) is split into two vectors, one proportional to \underline{b}_2 and one orthogonal to \underline{b}_2 , and so the result becomes a new equation

$$z_2 = c_{22}x_2 + c_{23}x_3 + \dots + c_{2M}x_M \quad (30)$$

and a new set of equations which do not contain x_2 and the process can proceed. The final result becomes

$$\begin{aligned} z_1 &= c_{11}x_1 + c_{12}x_2 + \dots + c_{1M}x_M \\ z_2 &= c_{22}x_2 + c_{23}x_3 + \dots + c_{2M}x_M \\ &\cdot \\ &\cdot \\ z_M &= c_{MM}x_M \end{aligned} \quad (31)$$

or in shorthand $\underline{z} = \underline{C} \underline{x}$ (31a)

Equations (31) form a very interesting system containing M equations with M unknowns. It can be computed for any N irrespective of the rank of \underline{A} , and any solution \underline{x} which satisfies the system also satisfies (18) with $\underline{\epsilon}^T \underline{\epsilon} = \text{minimum}$ (the easy proof will be omitted here). The system might be well fitted for determining \underline{x} by starting with the last equation; c_{MM} , however, is often small, so that x_M is poorly defined. Whenever there is a small value of c_{ss} in the main diagonal, the corresponding x_s will be poorly defined and a possible error will be transmitted to the x_p 's with $p < s$. (When the calculations are carried out with a computer, the probability that any c_{ss} will be exactly zero is almost null owing to residual errors). Even a poorly defined solution to (31), however, satisfies all conditions presented so far. It satisfies (18) with $\underline{\epsilon}^T \underline{\epsilon} = \text{minimum}$. If the solution is not satisfactory, it must be because further expectations are placed on the solution which are not expressed by means of the original system of equations. The only way to get out of the dilemma is to express the expectations in a logical way and find the \underline{x} vector which satisfies (18) within the error limits and which is as close to the expectations as possible. This can be done, for instance, by introducing an "expected" vector \underline{x}_e and demanding that $(\underline{x} - \underline{x}_e)^T (\underline{x} - \underline{x}_e) = \text{minimum}$ with the condition that (18) is satis-

fied within the error limits. In general the assumption that \underline{x}_e is equal to the zero vector suffices to deliver an acceptable "non-oscillatory" solution. So we are again at the starting point: solve (16) and (17). However, on the way we have got a method for transforming a matrix, square or non-square, into an equivalent triangular matrix which can be used to solve the complete problem as shown below.

III. THE COMPUTER SOLUTION

The problem: find \underline{x} such that

$$(\underline{x} - \underline{x}_e)^T (\underline{x} - \underline{x}_e) = \text{minimum} \quad (17) \quad (32)$$

on the condition that

$$\underline{y} = \underline{A} \underline{x} \quad (16) \quad (33)$$

within the experimental errors. \underline{x}_e , \underline{y} and \underline{A} are given. Further \underline{y} is subject to experimental errors, the mean square of which is approximately known. Naturally the elements of \underline{A} are also subject to errors. This might play a certain role when large systems are considered and will be discussed in the last chapter. We start by assuming that $\underline{\epsilon}^T \underline{\epsilon} \ll \underline{y}^T \underline{y}$ such that (33) is essentially correct. Differentiating (32) yields

$$(\underline{x} - \underline{x}_e)^T d\underline{x} = 0 \quad (34)$$

and from (33)

$$\underline{A} d\underline{x} = 0 \quad (35)$$

For any vector

$$\underline{q} = \begin{Bmatrix} q_1 \\ q_2 \\ \cdot \\ \cdot \\ q_N \end{Bmatrix} \quad (36)$$

we then have

$$(\underline{x} - \underline{x}_e)^T d\underline{x} = - \underline{q}^T \underline{A} d\underline{x} (= 0) \quad (37)$$

On the other hand, if we can find a vector \underline{q} (Lagrangeian factors) such that

$$(\underline{x} - \underline{x}_e)^T = - \underline{q}^T \underline{A} \quad (38)$$

then (34) is satisfied when (35) is satisfied. Thus (32) and (33) are equivalent to (33) and (38), which can be symbolized together in one system of equations

$$\begin{Bmatrix} \underline{O} & \underline{A} \\ \underline{A}^T & \underline{E} \end{Bmatrix} \begin{Bmatrix} \underline{q} \\ \underline{x} \end{Bmatrix} = \begin{Bmatrix} \underline{Y} \\ \underline{x}_e \end{Bmatrix} \quad (39)$$

where \underline{O} is the $N \cdot N$ dimensional zero matrix and \underline{E} the $M \cdot M$ dimensional unit matrix. The matrix of (39) is an $(N+M)(N+M)$ square matrix which can be transformed into a triangular matrix according to the procedure described in the previous chapter. We get

$$\begin{Bmatrix} c'_{11} & c'_{12} & c'_{13} & \dots & c'_{1, M+N} \\ 0 & c'_{22} & \dots & & \\ 0 & 0 & c'_{33} & \dots & \\ & & & c'_{NN} & \dots \\ 0 & & & 0 & c'_{N+1, N+1} \\ & & & & \dots \\ 0 & 0 & 0 & & c'_{M+N, M+N} \end{Bmatrix} \begin{Bmatrix} \underline{q} \\ \underline{x} \end{Bmatrix} = \underline{z}' \quad (40)$$

From (40) \underline{x} can be found immediately from the lower part of the matrix (the upper part and \underline{q} are without interest) and so the problem is solved apart from a discussion of errors.

IV. DISCUSSION OF ERRORS

First we consider the equations

$$\underline{y} = \underline{A}\underline{x} + \underline{\epsilon} \quad (41)$$

where $\underline{\epsilon}$ represents unknown errors in the \underline{y} elements. The complete solution of (41) implies that the errors have been found. As this is impossible, it is common to demand that $\underline{\epsilon}^T \underline{\epsilon} = \text{minimum}$. In general one knows the expected mean value of $\underline{\epsilon}^T \underline{\epsilon}$ and, if N (the dimension of \underline{y}) is large, $(\underline{\epsilon}^T \underline{\epsilon})_{\text{mean}}$ is known with a high degree of accuracy. From a logical point of view an \underline{x} vector which leads to a probable error vector $\underline{\epsilon}$ with $\underline{\epsilon}^T \underline{\epsilon} = (\underline{\epsilon}^T \underline{\epsilon})_{\text{mean}}$ should be a more probable solution than the \underline{x} vector which leads to $\underline{\epsilon}^T \underline{\epsilon} = (\underline{\epsilon}^T \underline{\epsilon})_{\text{minimum}}$ unless $(\underline{\epsilon}^T \underline{\epsilon})_{\text{mean}} \approx (\underline{\epsilon}^T \underline{\epsilon})_{\text{min}}$. The use of $(\underline{\epsilon}^T \underline{\epsilon})_{\text{min}}$, however, has the advantage that \underline{x} becomes uniquely defined if $N \geq M$ and the rank of \underline{A} is equal to M (the dimension of \underline{x}). On the other hand it has the drawback that one tries to compensate the errors (which are known to exist) in the \underline{y} vector by means of errors in the \underline{x} vector. If the \underline{a} vectors are not almost mutually orthogonal, there is a large risk that small errors in \underline{y} are exchanged for large errors in \underline{x} and we get the so-called "oscillatory" solutions. But only if one has some expectations as regards the proper solution is one able to judge whether a solution is "oscillatory" or "sound". We cannot disregard the fact that a system like (41) is uncertain to some degree and, pushing the matter to extremes, one may say that if one has no expectations on the solution whatsoever one has no reason to solve the system. As shown in the previous chapter the expectations can be used to remove uncertainties if they are logically expressed and fit into the system. The expectation that $\underline{\epsilon}^T \underline{\epsilon}$ shall be minimum is, under certain conditions, sufficient to ensure a proper solution, but not in general.

Equations (39) contain the original system $\underline{y} = \underline{A}\underline{x}$ and, theoretically that means - without paying attention to computational errors - that the solution of (39) by means of the method shown will be a "minimum square" solution. However, in the calculations the number of digits is limited and computational errors are unavoidable. Such errors depend both on the method of computation and on the relative size of the elements in the matrix. If, for instance, all elements of \underline{A} are very small compared to

1, the elements in the main diagonal of \underline{E} , then the system (39) in practice becomes nearly $\underline{x} = \underline{x}_e$, or, if all elements in \underline{A} are very large compared to 1, the lower part of the system loses in importance and $\underline{y} = \underline{A} \underline{x}$ becomes the essential part. That means that the solution obtained in practice might depend to some extent on the weight of the original system, which therefore must be given some thought. In practice the following method is recommended. Multiply each equation in $\underline{y} = \underline{A} \underline{x}$ by a constant divided by the expected mean error (not mean square error). Thereby we get a new system $\underline{y}' = \underline{A}' \underline{x}$ with equal mean error for each equation. Choose the constant such that the expected mean error per equation becomes $1 \cdot 10^{-v}$, where v is the number of digits used per element in the computation. Make the substitution

$$\underline{W} \underline{x}' = \underline{x} \tag{42}$$

with

$$\underline{W} = \begin{pmatrix} w_1 & & & \\ & w_2 & & 0 \\ & & \ddots & \\ & 0 & & w_M \end{pmatrix} \tag{43}$$

and choose the w 's such that the largest mean error in one element of $\underline{a}_s \cdot w_s$ is equal to $1 \cdot 10^{-v}$. Insert the new system

$$\underline{y}' = \underline{A}' \underline{W} \underline{x}' = \underline{A}'' \underline{x}' \tag{44}$$

in (39) (instead of $\underline{y} = \underline{A} \underline{x}$). Solve it according to (40) and the solution will be the very solution which satisfies $\underline{y} = \underline{A} \underline{x}$ within the error limits and is "closest" to the expected solution.

The use of the "expected" \underline{x}_e in (39) has an influence on the solution only if the rank of \underline{A} is small (compared to M , the number of unknowns). If not, the solution might still depend too much on experimental errors (in \underline{y}) to be acceptable, because the errors in \underline{y} are in general not due

to errors in \underline{x} . In such case the best way is to look for a more probable square error sum (which is in general known) and relax the demand that $\underline{\epsilon}^T \underline{\epsilon} = \text{minimum}$, for instance by demanding that $\underline{\epsilon}^T \underline{\epsilon} = \text{minimum}$ on condition that $x(u) = P(u)$, where $P(u)$ is a polynomial of maximum p th order. This leads to an expression similar to (39). Rather than the matrix inversion, the main problem is often to express one's demands in a rational way.

ACKNOWLEDGEMENT

Thanks are due to C. Lissing for making all the computer programs which have been necessary to test the theories.

LIST OF PUBLISHED AE-REPORTS

1-230. (See the back cover earlier reports.)

231. Calibration of the failed-fuel-element detection systems in the Ågesta reactor. By O. Strindehag. 1966. 52 p. Sw. cr. 8:--.
232. Progress report 1965. Nuclear chemistry. Ed. by G. Carleson. 1966. 26 p. Sw. cr. 8:--.
233. A summary report on assembly 3 of FR0. By T. L. Andersson, B. Brunfelter, P. F. Cecchi, E. Hellstrand, J. Kockum, S-O. Londen and L. I. Tirén. 1966. 34 p. Sw. cr. 8:--.
234. Recipient capacity of Tvären, a Baltic Bay. By P.-O. Agnedal and S. O. W. Bergström. 1966. 21 p. Sw. cr. 8:--.
235. Optimal linear filters for pulse height measurements in the presence of noise. By K. Nygaard. 1966. 16 p. Sw. cr. 8:--.
236. DETEC, a subprogram for simulation of the fast-neutron detection process in a hydro-carbonous plastic scintillator. By B. Gustafsson and O. Aspelund. 1966. 26 p. Sw. cr. 8:--.
237. Microanalysis of fluorine contamination and its depth distribution in zircaloy by the use of a charged particle nuclear reaction. By E. Möller and N. Starfelt. 1966. 15 p. Sw. cr. 8:--.
238. Void measurements in the regions of sub-cooled and low-quality boiling. P. 1. By S. Z. Rouhani. 1966. 47 p. Sw. cr. 8:--.
239. Void measurements in the regions of sub-cooled and low-quality boiling. P. 2. By S. Z. Rouhani. 1966. 60 p. Sw. cr. 8:--.
240. Possible odd parity in ^{136}Xe . By L. Broman and S. G. Malmkog. 1966. 10 p. Sw. cr. 8:--.
241. Burn-up determination by high resolution gamma spectrometry: spectra from slightly-irradiated uranium and plutonium between 400-830 keV. By R. S. Forsyth and N. Ronqvist. 1966. 22 p. Sw. cr. 8:--.
242. Half life measurements in ^{155}Gd . By S. G. Malmkog. 1966. 10 p. Sw. cr. 8:--.
243. On shear stress distributions for flow in smooth or partially rough annuli. By B. Kjellström and S. Hedberg. 1966. 66 p. Sw. cr. 8:--.
244. Physics experiments at the Ågesta power station. By G. Apelqvist, P.-Å. Bliselius, P. E. Blomberg, E. Jonsson and F. Åkerhielm. 1966. 30 p. Sw. cr. 8:--.
245. Intercrystalline stress corrosion cracking of inconel 600 inspection tubes in the Ågesta reactor. By B. Grönwall, L. Ljungberg, W. Hübner and W. Stuart. 1966. 26 p. Sw. cr. 8:--.
246. Operating experience at the Ågesta nuclear power station. By S. Sandström. 1966. 113 p. Sw. cr. 8:--.
247. Neutron-activation analysis of biological material with high radiation levels. By K. Samsahl. 1966. 15 p. Sw. cr. 8:--.
248. One-group perturbation theory applied to measurements with void. By R. Persson. 1966. 19 p. Sw. cr. 8:--.
249. Optimal linear filters. 2. Pulse time measurements in the presence of noise. By K. Nygaard. 1966. 9 p. Sw. cr. 8:--.
250. The interaction between control rods as estimated by second-order one-group perturbation theory. By R. Persson. 1966. 42 p. Sw. cr. 8:--.
251. Absolute transition probabilities from the 453.1 keV level in ^{183}W . By S. G. Malmkog. 1966. 12 p. Sw. cr. 8:--.
252. Nomogram for determining shield thickness for point and line sources of gamma rays. By C. Jönemalm and K. Malén. 1966. 33 p. Sw. cr. 8:--.
253. Report on the personnel dosimetry at AB Atomenergi during 1965. By K. A. Edwardsson. 1966. 13 p. Sw. cr. 8:--.
254. Buckling measurements up to 250°C on lattices of Ågesta clusters and on D_2O alone in the pressurized exponential assembly TZ. By R. Persson, A. J. W. Andersson and C-E. Wikdahl. 1966. 56 p. Sw. cr. 8:--.
255. Decontamination experiments on intact pig skin contaminated with beta-gamma-emitting nuclides. By K. A. Edwardsson, S. Hagsgård and Å. Swenson. 1966. 35 p. Sw. cr. 8:--.
256. Perturbation method of analysis applied to substitution measurements of buckling. By R. Persson. 1966. 57 p. Sw. cr. 8:--.
257. The Dancoff correction in square and hexagonal lattices. By I. Carlvik. 1965. 35 p. Sw. cr. 8:--.
258. Hall effect influence on a highly conducting fluid. By E. A. Witalis. 1965. 13 p. Sw. cr. 8:--.
259. Analysis of the quasi-elastic scattering of neutrons in hydrogenous liquids. By S. N. Purohit. 1966. 26 p. Sw. cr. 8:--.
260. High temperature tensile properties of unirradiated and neutron irradiated $20\text{Cr}-35\text{Ni}$ austenitic steel. By R. B. Roy and B. Solly. 1966. 25 p. Sw. cr. 8:--.
261. On the attenuation of neutrons and photos in a duct filled with a helical plug. By E. Aalto and Å. Krell. 1966. 24 p. Sw. cr. 8:--.
262. Design and analysis of the power control system of the fast zero energy reactor FR-0. By N. J. H. Schuch. 1966. 70 p. Sw. cr. 8:--.
263. Possible deformed states in ^{115}In and ^{117}In . By A. Bäcklin, B. Fogelberg and S. G. Malmkog. 1967. 39 p. Sw. cr. 10:--.
264. Decay of the 16.3 min. ^{182}Ta isomer. By M. Höjberg and S. G. Malmkog. 1967. 13 p. Sw. cr. 10:--.
265. Decay properties of ^{147}Nd . By A. Bäcklin and S. G. Malmkog. 1967. 15 p. Sw. cr. 10:--.
266. The half life of the 53 keV level in ^{197}Pt . By S. G. Malmkog. 1967. 10 p. Sw. cr. 10:--.
267. Burn-up determination by high resolution gamma spectrometry: Axial and diametral scanning experiments. By R. S. Forsyth, W. H. Blackadder and N. Ronqvist. 1967. 18 p. Sw. cr. 10:--.
268. On the properties of the $s_{1/2} \rightarrow d_{3/2}$ transition in ^{199}Au . By A. Bäcklin and S. G. Malmkog. 1967. 23 p. Sw. cr. 10:--.
269. Experimental equipment for physics studies in the Ågesta reactor. By G. Bernander, P. E. Blomberg and P.-O. Dubois. 1967. 35 p. Sw. cr. 10:--.
270. An optical model study of neutrons elastically scattered by iron, nickel, cobalt, copper, and indium in the energy region 1.5 to 7.0 MeV. By B. Holmqvist and T. Wiedling. 1967. 20 p. Sw. cr. 10:--.
271. Improvement of reactor fuel element heat transfer by surface roughness. By B. Kjellström and A. E. Larsson. 1967. 94 p. Sw. cr. 10:--.
272. Burn-up determination by high resolution gamma spectrometry: Fission product migration studies. By R. S. Forsyth, W. H. Blackadder and N. Ronqvist. 1967. 19 p. Sw. cr. 10:--.
273. Monoenergetic critical parameters and decay constants for small spheres and thin slabs. By I. Carlvik. 1967. 24 p. Sw. cr. 10:--.
274. Scattering of neutrons by an anharmonic crystal. By T. Höjberg, L. Bohlin and I. Ebbsjö. 1967. 38 p. Sw. cr. 10:--.
275. The $\Delta K=1$, E1 transitions in odd-A isotopes of Tb and Eu. By S. G. Malmkog, A. Marelus and S. Wahlborn. 1967. 24 p. Sw. cr. 10:--.
276. A burnout correlation for flow of boiling water in vertical rod bundles. By Kurt M. Becker. 1967. 102 p. Sw. cr. 10:--.
277. Epithermal and thermal spectrum indices in heavy water lattices. By E. K. Sokolowski and A. Jonsson. 1967. 44 p. Sw. cr. 10:--.
278. On the $d_{5/2} \rightarrow g_{7/2}$ transitions in odd mass Pm nuclei. By A. Bäcklin and S. G. Malmkog. 1967. 14 p. Sw. cr. 10:--.
279. Calculations of neutron flux distributions by means of integral transport methods. By I. Carlvik. 1967. 94 p. Sw. cr. 10:--.
280. On the magnetic properties of the $K=1$ rotational band in ^{188}Re . By S. G. Malmkog and M. Höjberg. 1967. 18 p. Sw. cr. 10:--.
281. Collision probabilities for finite cylinders and cuboids. By I. Carlvik. 1967. 28 p. Sw. cr. 10:--.
282. Polarized elastic fast-neutron scattering of ^{12}C in the lower MeV-range. I. Experimental part. By O. Aspelund. 1967. 50 p. Sw. cr. 10:--.
283. Progress report 1966. Nuclear chemistry. 1967. 26 p. Sw. cr. 10:--.
284. Finite-geometry and polarized multiple-scattering corrections of experimental fast-neutron polarization data by means of Monte Carlo methods. By O. Aspelund and B. Gustafsson. 1967. 60 p. Sw. cr. 10:--.
285. Power disturbances close to hydrodynamic instability in natural circulation two-phase flow. By R. P. Mathisen and O. Eklind. 1967. 34 p. Sw. cr. 10:--.
286. Calculation of steam volume fraction in subcooled boiling. By S. Z. Rouhani. 1967. 26 p. Sw. cr. 10:--.
287. Absolute E1, $\Delta K=0$ transition rates in odd-mass Pm and Eu-isotopes. By S. G. Malmkog. 1967. 33 p. Sw. cr. 10:--.
288. Irradiation effects in Fortiweld steel containing different boron isotopes. By M. Grounes. 1967. 21 p. Sw. cr. 10:--.
289. Measurements of the reactivity properties of the Ågesta nuclear power reactor at zero power. By G. Bernander. 1967. 43 p. Sw. cr. 10:--.
290. Determination of mercury in aqueous samples by means of neutron activation analysis with an account of flux disturbances. By D. Brune and K. Jirflow. 1967. 15 p. Sw. cr. 10:--.
291. Separation of ^{51}Cr by means of the Szilard-Chalmers effect from potassium chromate irradiated at low temperature. By D. Brune. 1967. 15 p. Sw. cr. 10:--.
292. Total and differential efficiencies for a circular detector viewing a circular radiator of finite thickness. By A. Lauber and B. Tollander. 1967. 45 p. Sw. cr. 10:--.
293. Absolute M1 and E2 transition probabilities in ^{233}U . By S. G. Malmkog and M. Höjberg. 1967. 37 p. Sw. cr. 10:--.
294. Čerenkov detectors for fission product monitoring in reactor coolant water. By O. Strindehag. 1967. 56 p. Sw. cr. 10:--.
295. RPC calculations for K-forbidden transitions in ^{183}W . Evidence for large inertial parameter connected with high-lying rotational bands. By S. G. Malmkog and S. Wahlborn. 1967. 25 p. Sw. cr. 10:--.
296. An investigation of trace elements in marine and lacustrine deposits by means of a neutron activation method. By O. Landström, K. Samsahl and C-G. Wenner. 1967. 40 p. Sw. cr. 10:--.
297. Natural circulation with boiling. By R. P. Mathisen. 1967. 58 p. Sw. cr. 10:--.
298. Irradiation effects at 160-240°C in some Swedish pressure vessel steels. By M. Grounes, H. P. Myers and N-E. Hannerz. 1967. 36 p. Sw. cr. 10:--.
299. The measurement of epithermal-to-thermal U-238 neutron capture rate (ρ_{28}) in Ågesta power reactor fuel. By G. Bernander. 1967. 42 p. Sw. cr. 10:--.
300. Levels and transition rates in ^{199}Au . By S. G. Malmkog, A. Bäcklin and B. Fogelberg. 1967. 48 p. Sw. cr. 10:--.
301. The present status of the half-life measuring equipment and technique at Studsvik. By S. G. Malmkog. 1967. 26 p. Sw. cr. 10:--.
302. Determination of oxygen in aluminum by means of 14 MeV neutrons with an account of flux attenuation in the sample. By D. Brune and K. Jirflow. 1967. 16 p. Sw. cr. 10:--.
303. Neutron elastic scattering cross sections of the elements Ni, Co, and Cu between 1.5 and 8.0 mev. By B. Holmqvist and T. Wiedling. 1967. 17 p. Sw. cr. 10:--.
304. A study of the energy dependence of the $\text{Th}232$ capture cross section in the energy region 0.1 to 3.4 eV. By G. Lundgren. 1967. 25 p. Sw. cr. 10:--.
305. Studies of the reactivity effect of polythene in the fast reactor FR0. By L. I. Tirén and R. Håkansson. 1967. 25 p. Sw. cr. 10:--.
306. Final report on IFA-10, the first Swedish instrumented fuel assembly irradiated in HBWR, Norway. By J-A. Gyllander. 1967. 35 p. Sw. cr. 10:--.
307. Solution of large systems of linear equations with quadratic or non-quadratic matrices and deconvolution of spectra. By K. Nygaard. 1967. 15 p. Sw. cr. 10:--.

Förteckning över publicerade AES-rapporter

1. Analys medelst gamma-spektrometri. Av D. Brune. 1961. 10 s. Kr 6:--.
2. Bestrålningsförändringar och neutronatmosfär i reaktortrycktankar - några synpunkter. Av M. Grounes. 1962. 33 s. Kr 6:--.
3. Studium av sträckgränsen i mjukt stål. Av G. Östberg och R. Attermo 1963. 17 s. Kr 6:--.
4. Teknisk upphandling inom reaktorområdet. Av Erik Jonson. 1963. 64 s. Kr 8:--.
5. Ågesta Kraftvärmeverk. Sammanställning av tekniska data, beskrivningar m. m. för reaktordelen. Av B. Lilliehöök. 1964. 336 s. Kr 15:--.
6. Atomdagen 1965. Sammanställning av föredrag och diskussioner. Av S. Sandström. 1966. 321 s. Kr 15:--.
7. Radiumhaltiga byggnadsmaterial ur strålskyddssynpunkt. Av Stig O. W. Bergström och Thor Wahlberg. 1967. 26 s. Kr 10:--.

Additional copies available at the library of AB Atomenergi, Studsvik, Nyköping, Sweden. Micronegatives of the reports are obtainable through Filmprodukter, Gamla landsvägen 4, Ektorp, Sweden.