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X-Y SPACIAL DISTRIBUTION EXPERIMENTS WITH PARMELA
or, What I Did on my Summer Vacation*

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Abstract: Experiments using the Parmela simulation program predict that the potentially uneven spacial distributions in the electron beam generated by laser emission from the photo cathode gun has no appreciable effect on the beam outcome when compared to the more uniform thermionic gun.

The first step in making comparisons is to establish a proper reference. This required learning the Parmela system and becoming adept at running it using a variety of standard inputs. While I was learning the system, the actual magnetic fields of the optics following the photo cathode gun were measured. This gave me the opportunity to tune the parmela input to more closely approximate the working magnetic fields (see figure 1). Using Roger Miller's procedure, I created theoretical bucking coils to cancel stray fields which are in reality eliminated by steel mirrors. These bucking fields are located on either side of the Helmholtz coils in the position of the two lenses (see figure 2). These bucking fields are directly proportional to the Helmholtz coils and can be adjusted in proportion to the amount the coils are altered. A third, smaller bucking field is established across the second and third lenses to cancel stray fields from the sub-harmonic buncher. This coil collection is independent of the Helmholtz fields and so does not need to be altered unless the bunching fields are themselves changed.

Once I established appropriate lens currents to successfully run existing standard inputs, I created a reference run. All other runs would use the same parameters except for their spacial distributions. The reference run was a Parmela-generated gaussian random in X and Y but non-random in Z. It was later suggested that X and Y should be non-random as well, since a collection of 10expl particles is a very uniform gaussian while 999 particles makes for an irregular curve. After finishing the primary work, I found a way to generate distributions that are non-random in X, Y and Z. I have included such a run, called Second Standard, along with the reference for making comparisons to the other runs. As predicted, the random X and Y run was in no way discernably different from the equivalent non-random X and Y run in particle density or emmitance.

By contrast, the Parmela program seems to be highly sensitive to randomness in the longitudinal, Z distribution. A randomly formed gaussian in Z begins with high and low density areas which quickly become exaggerated by the effects of space-charge until the program crashes (see figure 3). Thus, all Z distributions are non-random gaussians. The Z distribution I used in the first reference is much taller and narrower than that created by Parmela (see figure 4) as they were generated differently. This difference expresses itself as a stronger space-charge spreading and probably accounts for some of the slight loss of particles and most of the change of emittance

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by the end of the run. By comparing the emittance of the reference run and the second standard run (see table 2) which vary primarily by the shape of the Z gaussian (that is sigma Z), it is easy to see just how sensitive Parmela is to Z distributions. Because the run called Second Standard uses the same Z distribution as the other runs ($\sigma_Z = 15.6$ cm with a curve width of two sigmas), I have decided to use it as my primary comparison.

Another quality to be considered when comparing runs to a standard is the timing. Often when the spacial distribution or the energy was changed, the relative timing would change, sometimes by considerable amounts. Timing has to be monitored whenever changing the input and usually adjusted to bring it close to the reference timing. This is done by making a run, determining the phase difference and estimating by trial and error (the effect is not generally linear) how much to change it by. The change is made on the "start" card of the parmela input in the first value (the clock starting phase).

Once longitudinal distribution and phase are properly accounted for, the user can vary the X-Y makeup. I did this in three ways. The first distribution I used was a random double gaussian across the X axis. This can be represented by a histogram lego plot in figure 5. I also created a double gaussian across the Y axis (that is, rotated by 90 degrees) for comparison. There was no essential difference between these except for the minor assymetry beyond the bend magnet. The next variation I tried was a symmetric volcano shape with a peak in the center (see figure 6). The last run used a similiar volcano shape but with a rim that varied sinusoidally (see figure 7). This last distribution best represents the intensity distribution measured for the laser destined to be the photo cathode source (see figure 8). These three distributions, along with the reference can be compared in figure 9. A lego plot of the Second Standard is seen in figure 17.

The spacial distributions of the three variations at the end of their runs compare very favorably with that of the reference beam. The end of the run corresponds here to element #37, 420 cm from the cathode, past the first and second sub-harmonic and s-band bunchers. These results are illustrated in figures 10, 11 and 18. Apparently, the X and Y distribution and the Z bunching for each of the runs is virtually the same and the total number of particles that completed a given run varied by less than 2% for either standard (see table 1).

TABLE 1

RUN NAME	# OF GOOD PARTICLES	MAX # IN 20 BAND
REFERENCE	981	737
2ND STANDARD	977	758
DOUBLE X	973	740
VOLCANO	970	726
VOLCANO2	963	731

The greatest differences between these runs were the emittances. Tables of the X and Y emittances for the runs are found in figures 12 and 13, the Z emittances are found in figures 14 and 15 and the X, Y and Z emittances for the second standard are found in figure 16. Table 2 lists the emittances for each run after the last (37th) element and the percent difference from the second standard value:

TABLE 2

RUN NAME	RMS X	E MAX X, 90%	E MAX X, 100%	RMS Y	E MAX Y, 90%	E MAX Y, 100%	RMSZ X10	Z, 90% X10	Z, 100% X10
REFERENCE	6.79	36.2	180	7.61	39.2	205	114	560	7770
2ND STAND	8.05	40.3	184	8.54	43.9	234	114	562	7440
DOUBLE X % DIF	7.25 -11%	38.8 -3.1%	192 4.2%	7.96 -7.3%	41.1 -6.8%	180 -30%	98.5 -16%	483 -16%	8810 18%
VOLCANO % DIF	8.02 -0.3%	39.0 -3.3%	221 23%	8.30 -2.9%	39.1 -12%	254 7.9%	121 5.8%	568 -1.1%	8310 10%
VOLCANO2 % DIF	8.79 8.4%	44.2 8.8%	251 36%	8.25 -3.5%	41.7 -5.3%	320 27%	109 -4.5%	505 -11%	8760 17%

After running the preceding set of experiments, I repeated the runs with data sets that are all non-random in X and Y and use a more realistic non-random Z gaussian. This Z distribution used a sigma of 19.5 cm, formed across 1.60 sigmas. They have similiar shapes (see figure 19) as the previous runs and the names differ by an added "G" at the end. Table 3 represents the number of particles that completed the 410 cm run and the concentration in the largest 20 degree band (see figures 20-23):

TABLE 3

RUN NAME	# OF GOOD PARTICLES	MAX # IN 20 BAND
2ND STANDARD G	981	806
DOUBLE X G	977	801
VOLCANO G	976	709
VOLCANO2 G	982	800

Table 4 lists the emittances for each run after the last (37th) element and the percent difference from the Second Standard G value:

TABLE 4

RUN NAME	RMS X	E MAX X, 90%	E MAX X, 100%	RMS Y	E MAX Y, 90%	E MAX Y, 100%	RMSZ X10	Z, 90% X10	Z, 100% X10
2ND STND G	7.84	40.8	187	7.48	37.9	143	90.0	510	7320
DOUBLE X G	7.66	38.8	136	7.23	36.4	236	94.1	508	7440
% DIF	-2.3%	-5.2%	-38%	-3.5%	-4.1%	65%	4.4%	-0.4%	1.6%
VOLCANO G	8.16	39.3	167	8.97	43.0	227	89.4	495	7720
% DIF	3.9%	-3.8%	-12%	17%	12%	37%	-0.7%	-3.0%	5.2%
VOLCANO2 G	8.00	39.6	313	8.07	39.5	366	114	586	7970
% DIF	2.0%	-3.0%	67%	7.4%	4.1%	156%	21%	13%	7.2%

I conclude from this data, to the degree that Parmela is faithful to reality, irregular X-Y spacial distributions of particles will not run noticeably differently from true gaussian distributions. However, It should be noted that Parmela calculates the space-charge effects for each particle as though they were axially-symmetric rings. This means the program automatically ignores X-Y spacial irregularities in the space-charge calculations. It is very possible that the high degree of precision in these results is due in large part to this programming simplification (where it was assumed that only regular spacial gaussians could be formed). The only ways to be certain are to run the same sets of inputs on a similar program that treats the particles as point charges or to wait for the photo cathode gun to come on line and compare the distribution patterns to the outcomes. All the same, I found this project very worthwhile and challenging.

Special Thanks to: Roger Miller, Ted Lavine, Barbara Woo, Tom Knight, Tor Raubenheimer, Bill Gabella, Mina Petradza and Margie Bangali.

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APPENDIX 1

The smallest spacial constrictions used in the Parmela simulation have radius of 1.40 cm and are found in elements 3, 4, 6 and 7. These elements correspond to, respectively: the start of the Helmholtz coil (40.7cm), the end of the Helmholtz (66.7cm), the second lens (93.7cm) and the end of the bend magnet (102.7cm). The following table shows the X or Y spacial limits of the beam in these four elements. It does not account for the radial limits off the X and Y axes, but it gives a good sense of the general beam size (all measurements in centimeters).

RUN NAME	ELEMENT 3	ELEMENT 4	ELEMENT 6	ELEMENT 7
REFERENCE	0.65	0.60	0.80	0.70
2ND STANDARD	0.70	0.70	0.80	0.85
DOUBLE-X	0.75	0.50	0.80	0.85
VOLCANO	0.75	0.55	0.80	1.00
VOLCANO2	0.80	0.55	0.85	1.00
<hr/>				
2ND STAND G	0.70	0.70	0.75	0.80
DOUBLE-X G	0.70	0.55	0.80	0.75
VOLCANO G	0.75	0.50	0.75	0.75
VOLCANO2 G	0.70	0.50	0.75	0.80

Calc vs Meas For L390, S390, S396, S400

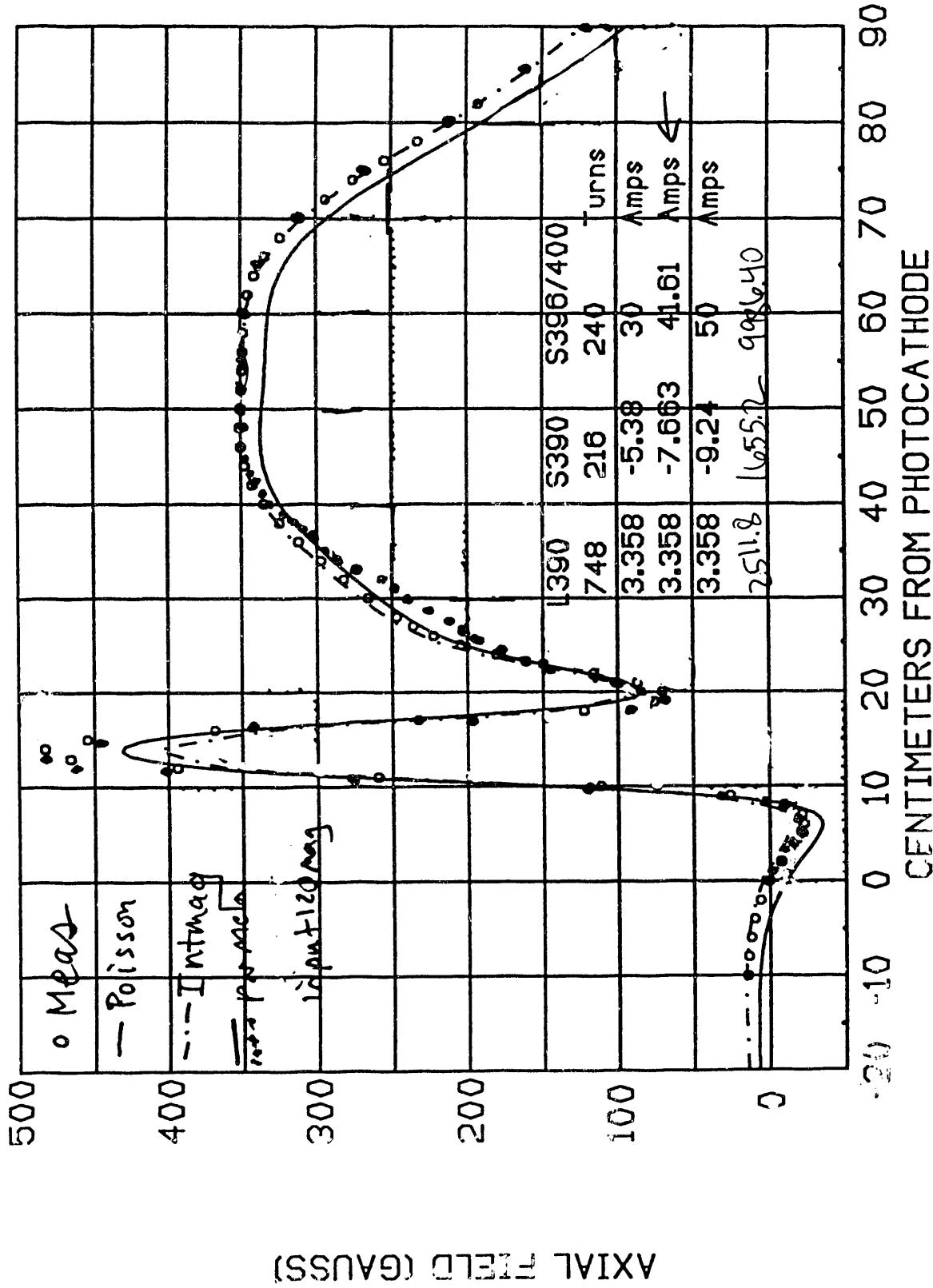


Figure 1

Parmela Input without lenses or bending magnets

coil	-7	4	-20	0	500
coil	-3	4	-75		
coil	1	4	-110		
coil	5	4	-280		
coil	9	4	-245		
coil	13	4	-230		
coil	17	4	-320		
coil	19	4	-190		
coil	9.9	2.54	0		

bucking
coil

PARMELA INPUT Al Dated 07/15/91 12:20:17 From disk JRH192 Page 2

coil	11.1	2.54	0
coil	12.4	2.54	0
coil	13.7	2.54	0 ← 1st lens
coil	15.0	2.54	0
coil	16.3	2.54	0
coil	17.5	2.54	0
coil	40.7	25.0	8000
coil	66.7	25.0	8000
coil	89.9	2.54	0
coil	91.1	2.54	0
coil	92.4	2.54	0
coil	93.7	2.54	0 ← 2nd lens
coil	95.0	2.54	0
coil	96.3	2.54	0
coil	97.5	2.54	0
coil	90	4	-320
coil	94	4	-290
coil	98	4	-195
coil	102	4	-155
coil	106	4	-127
coil	110	4	-100
coil	114	4	-90
coil	118	4	-67
coil	122	4	-70
coil	126	4	-50
coil	119.9	2.54	0
coil	121.1	2.54	0
coil	122.4	2.54	0
coil	123.7	2.54	0 ← 3rd lens
coil	125.0	2.54	0
coil	126.3	2.54	0
coil	127.5	2.54	0
coil	88	4.4	-5
coil	92	4.4	-10
coil	96	4.4	-10
coil	100	4.4	-10
coil	104	4.4	-10
coil	108	4.4	-12
coil	112	4.4	-15
coil	116	4.4	-20
coil	120	4.4	-30
coil	124	4.4	-50
coil	128	4.4	-75

3 Helmholtz coils

Helmholtz
bucking

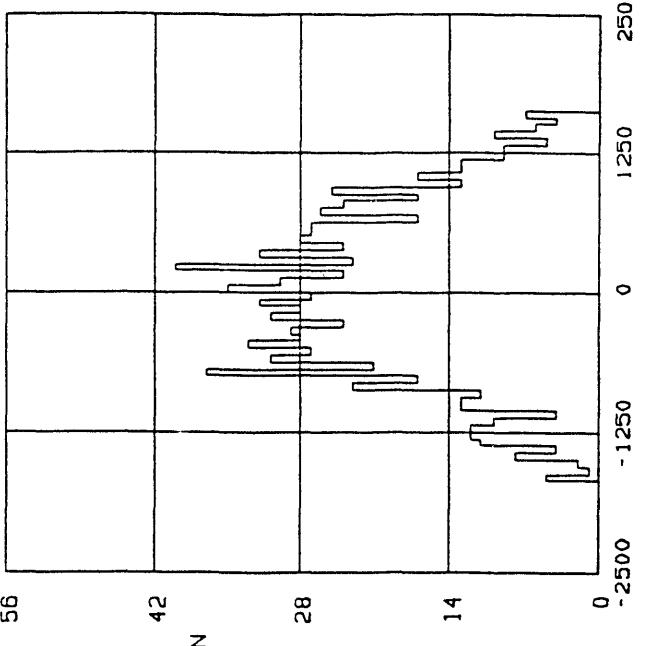
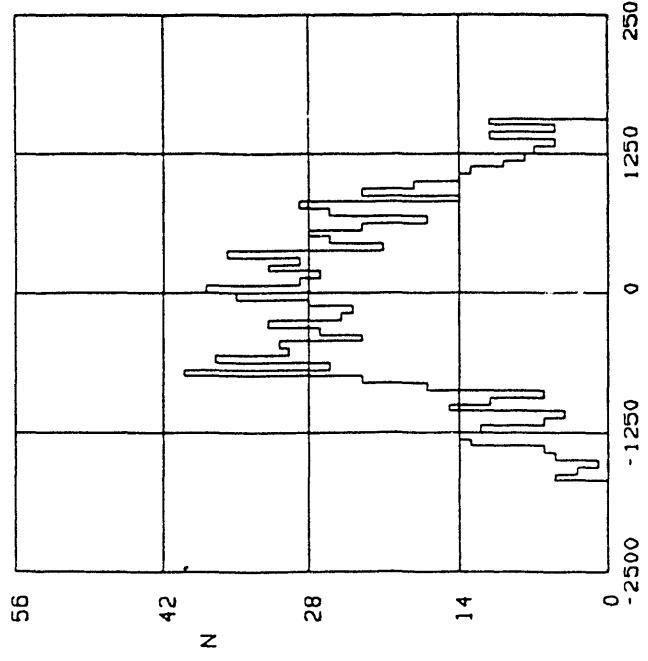
← 3rd lens

bunching coil
bucking

Figure 2

C10POL, RUN#37, I=60, 21NC, 3NS, V0=160KV, 12/14/90, |

C10POL, RUN#37, I=60, 21NC, 3NS, V0=160KV, 12/14/90, E=14MV/M,



Random
Gaussian
Distribution
in Z

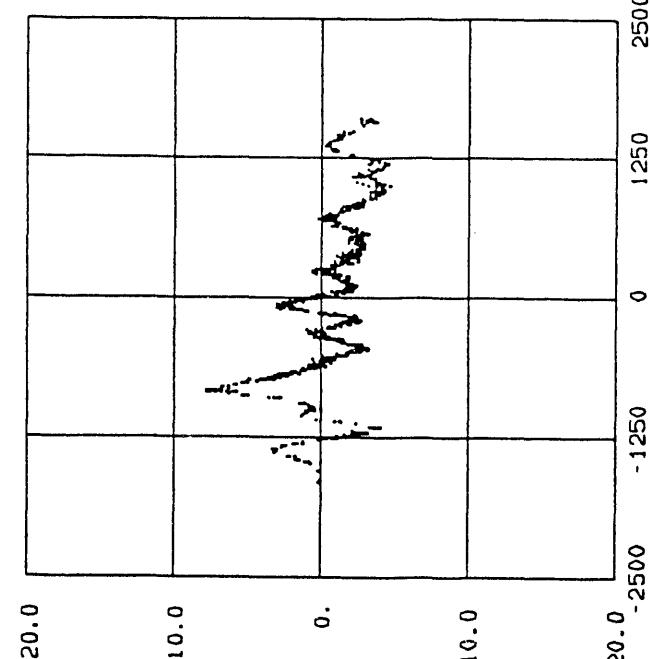
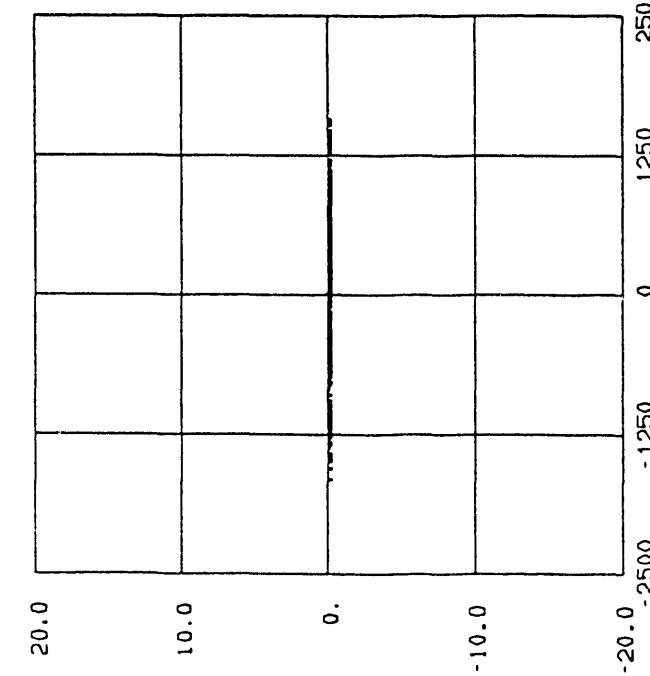
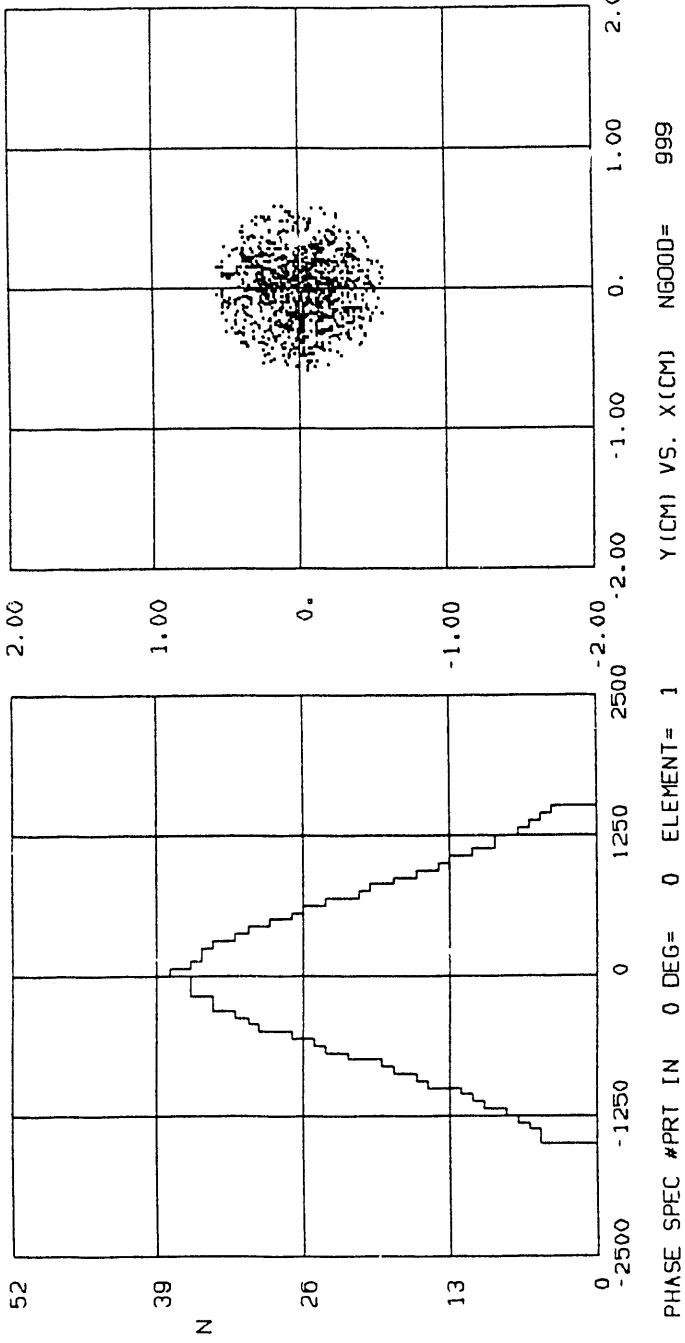


Figure 3

C10POL, RUN# 37, I=60, 21NC, 3NS, V0=160KV, 12/14/ ϵ = 14MV/M,

RUN# 37



9

C10POL, RUN# 1, I=60, 21NC, 3NS, V0=160KV, 7/25/91. E=14MV/M,

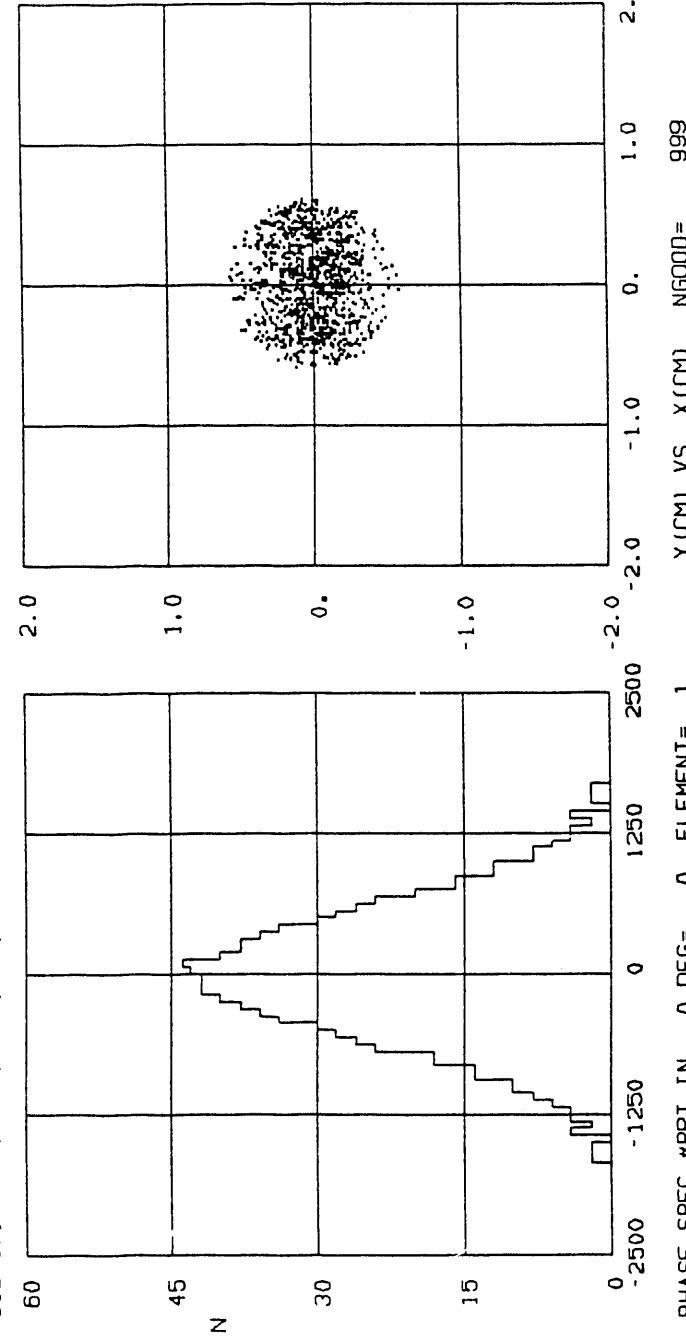


Figure 4

Start

X - Y DISTRIBUTION

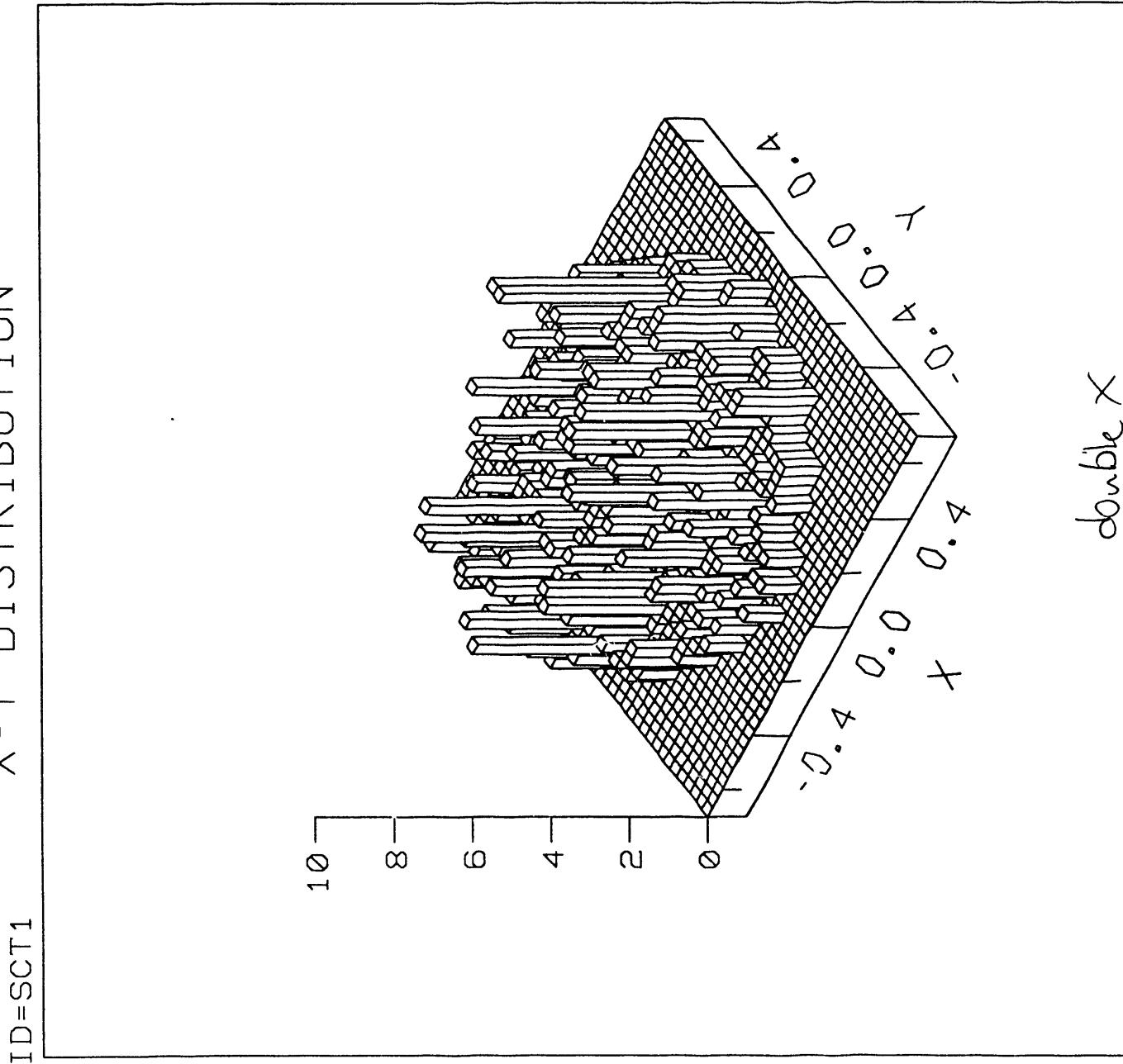
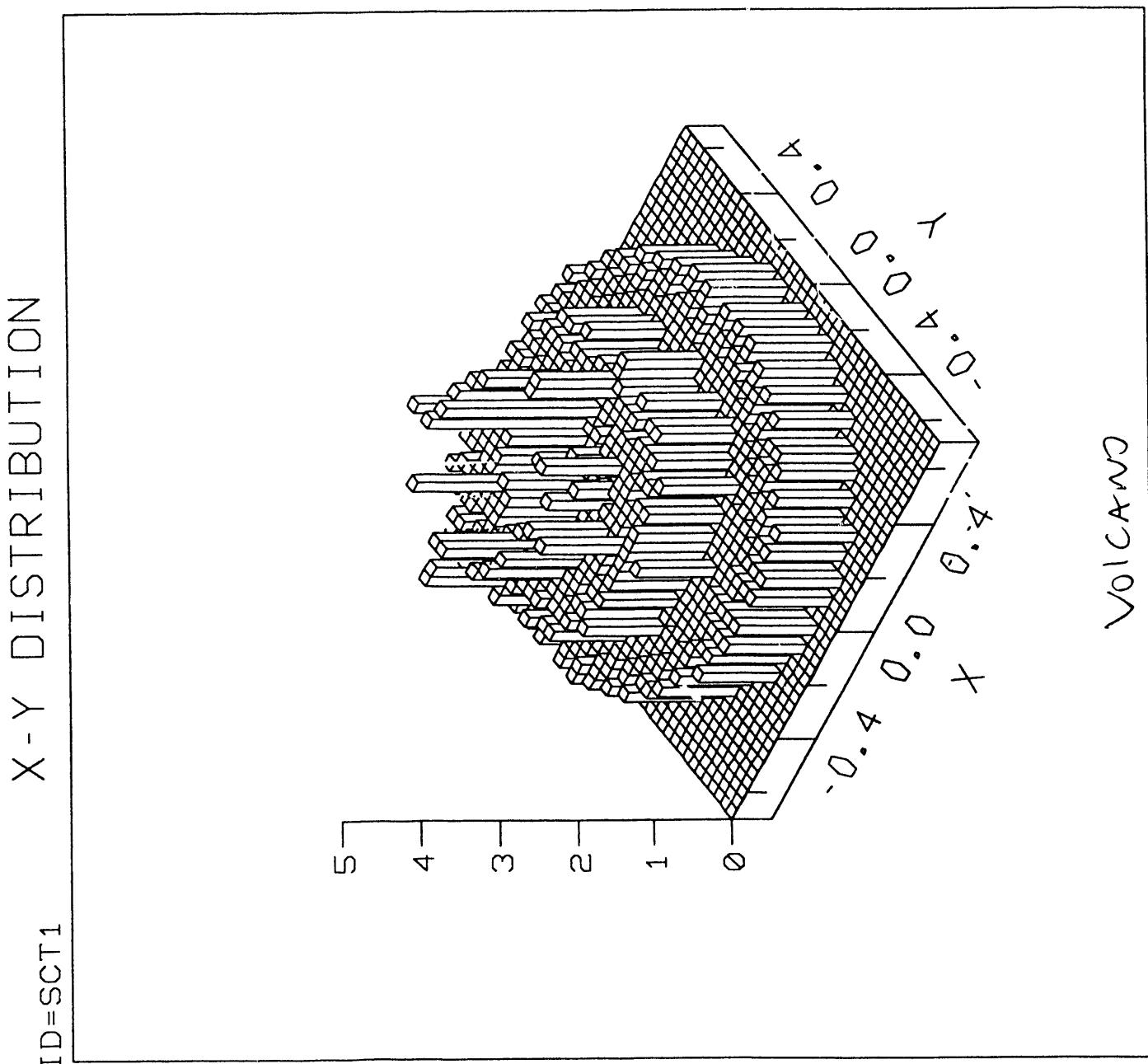


Figure 5

Figure 6



X - Y DISTRIBUTION
ID=SCT1

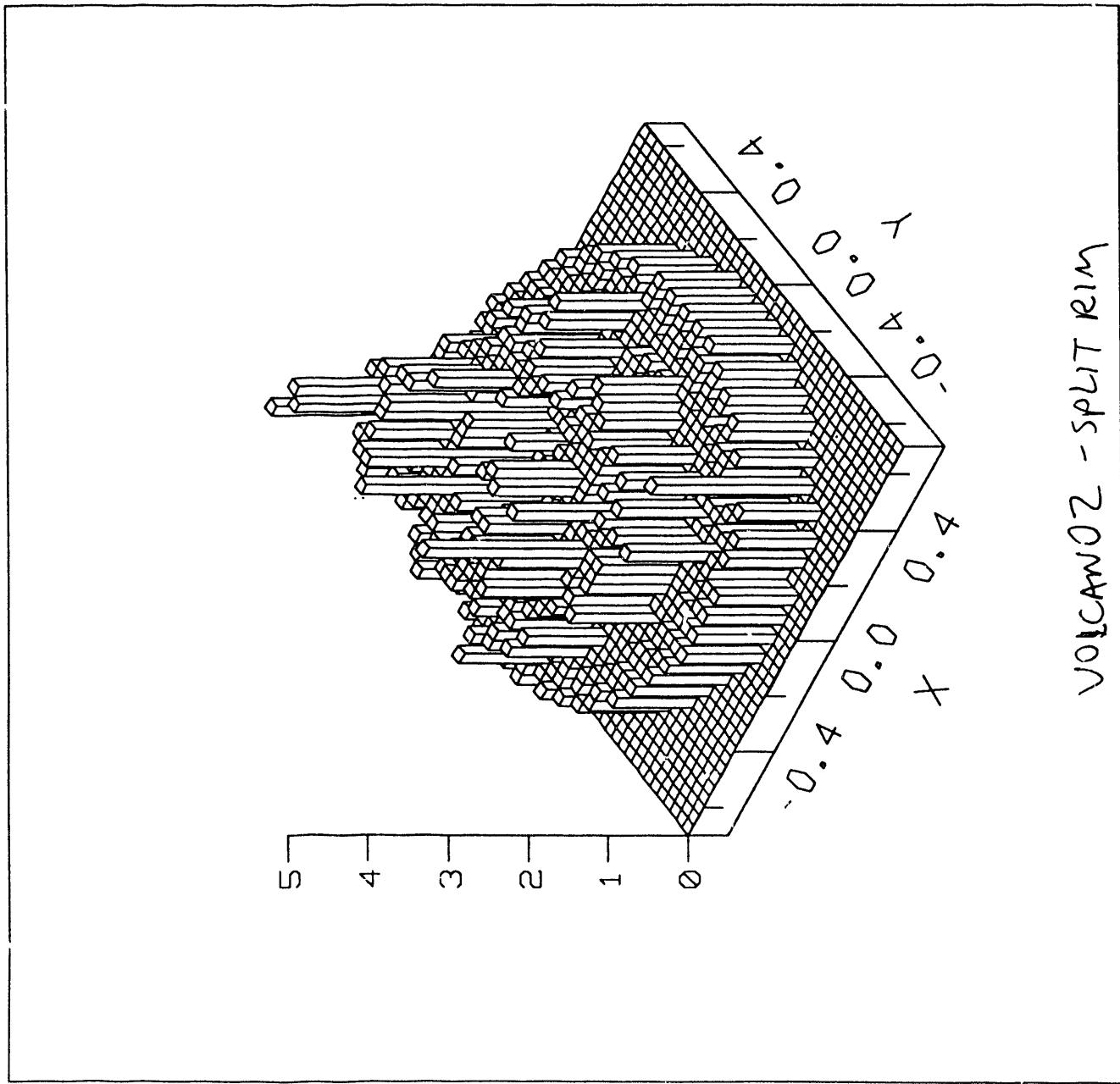


Figure 7

Laser Intensity Plot

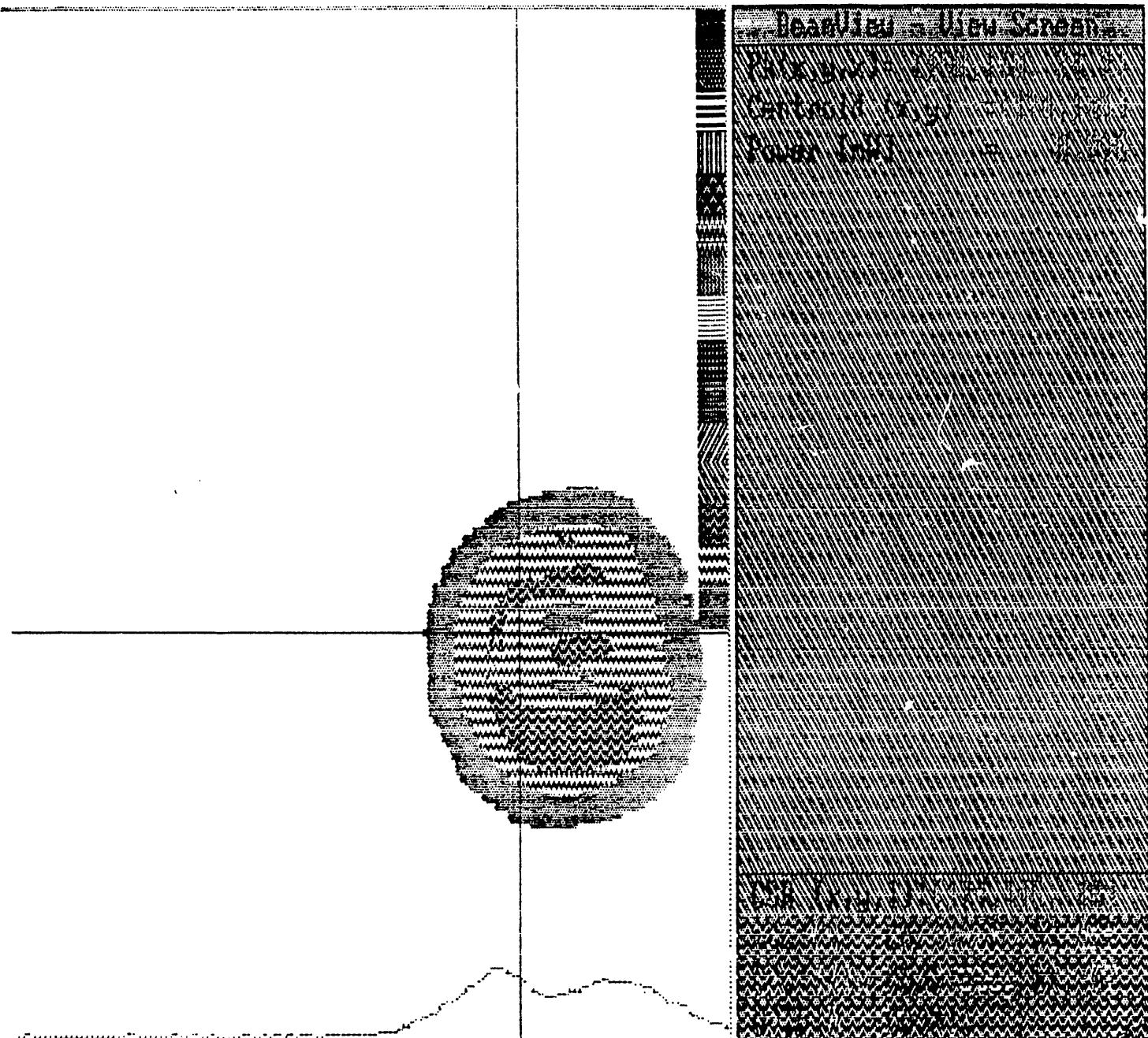


Figure 8

Initial X-Y distributions for the beam at 0.2cm

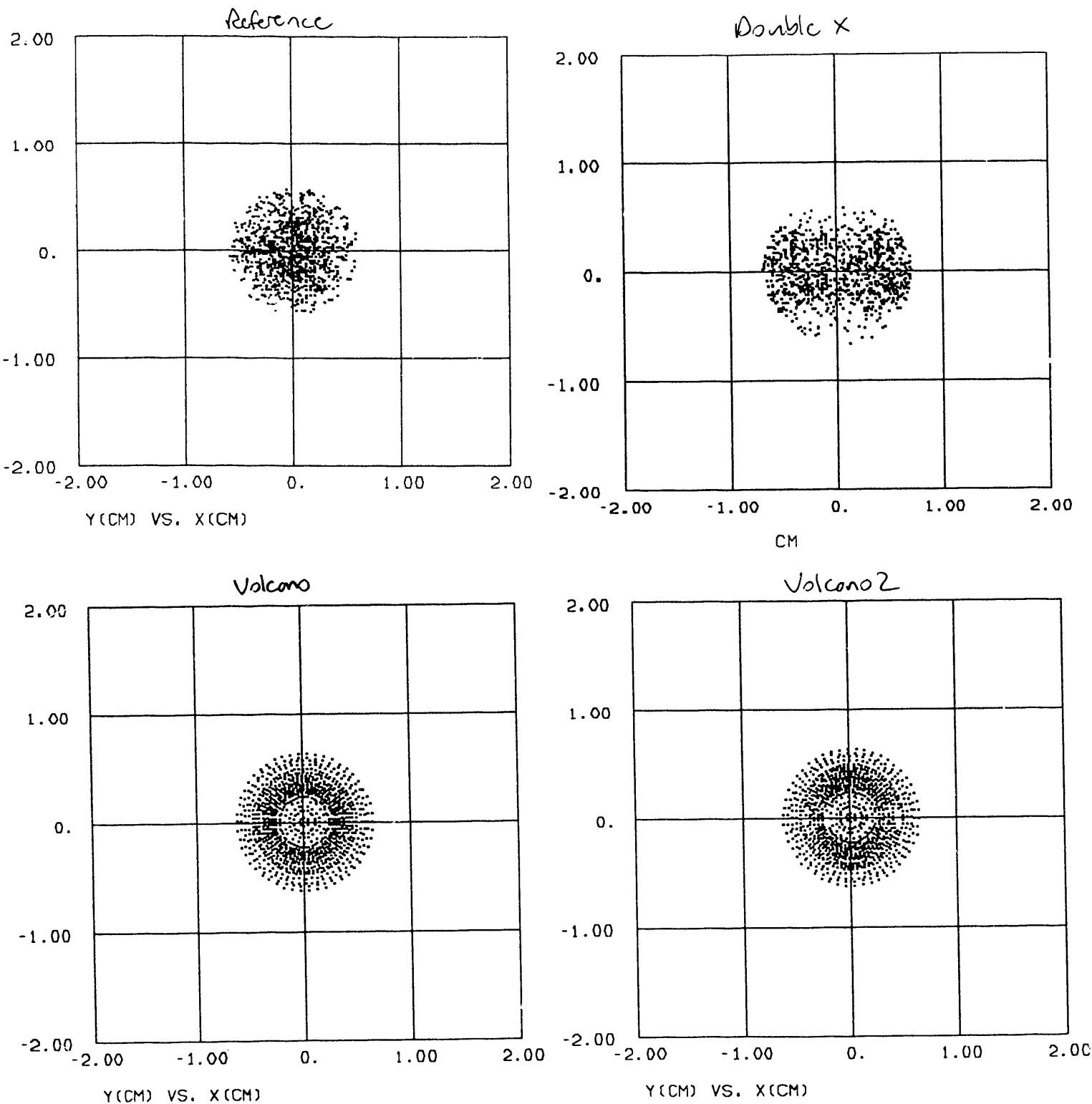
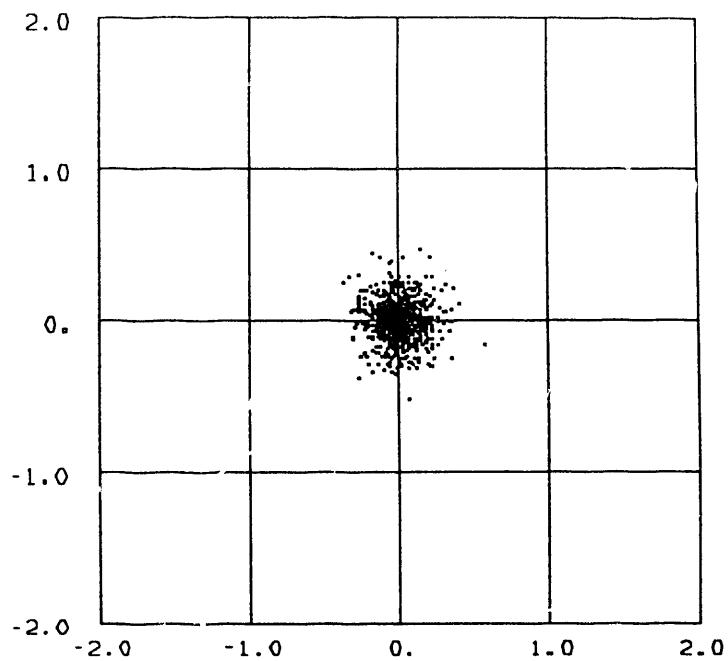
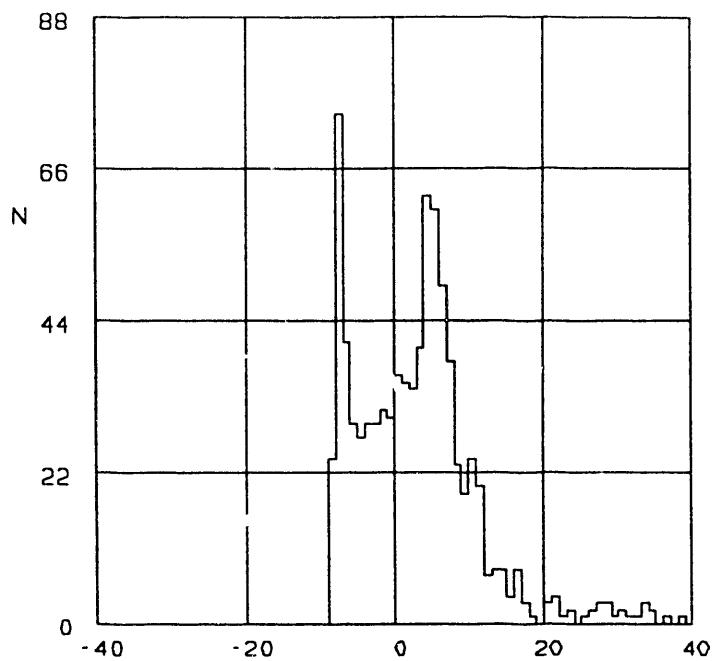


Figure 9

CIDPOL, RUN#37, I=60, 21NC, 3NS, V0=160KV, 12/14

, E=14MV/M, Reference

RUN# 37



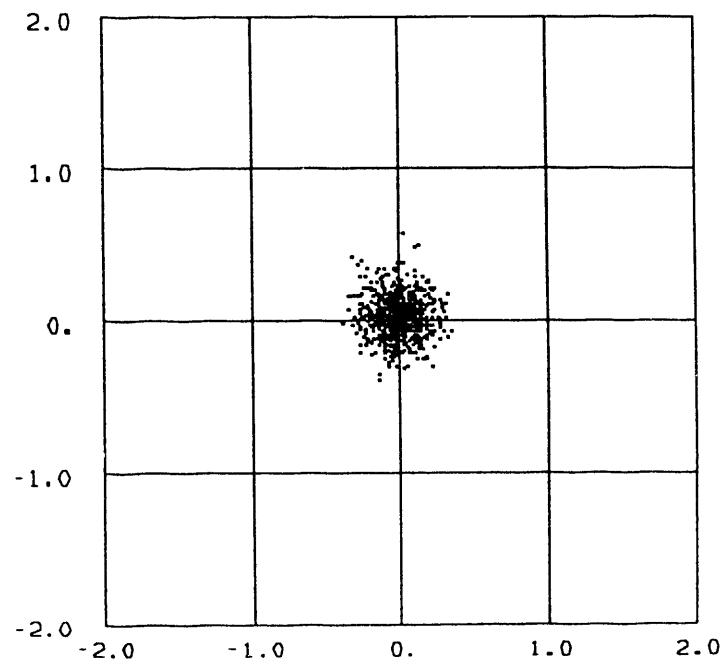
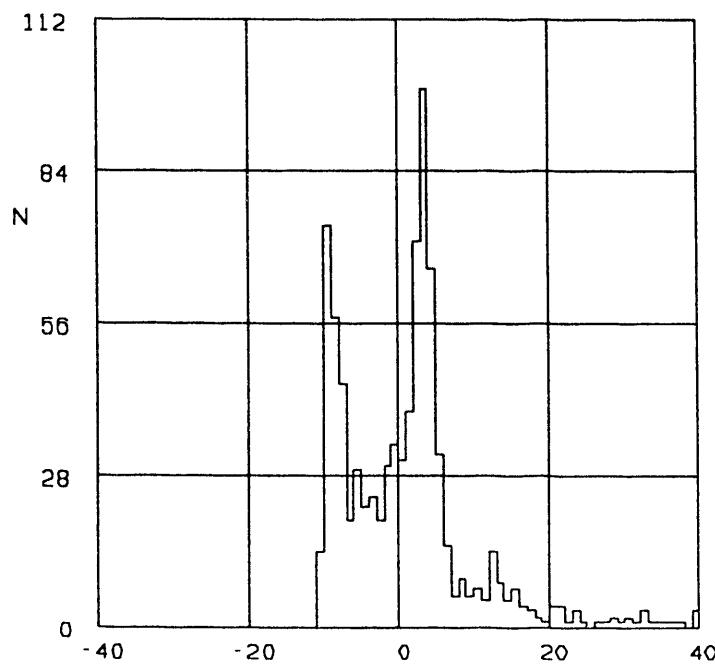
PHASE SPEC #PRT IN [20 DEG= 736] ELEMENT= 37
PS = 134.4 Deg

Y(CM) VS. X(CM) N6000= 981

Reference

CIDPOL, RUN#1, I=60, 21NC, 3NS, V0=160KV, 7/25/91

=14MV/M, double-X RUN# 37



PHASE SPEC #PRT IN [20 DEG= 740] ELEMENT= 37
PS = 137.3°

Y(CM) VS. X(CM) N6000= 973

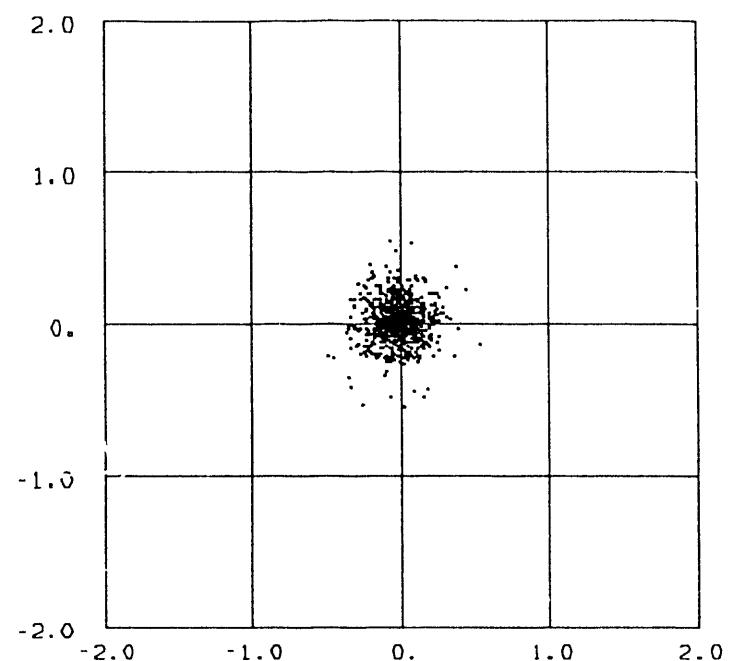
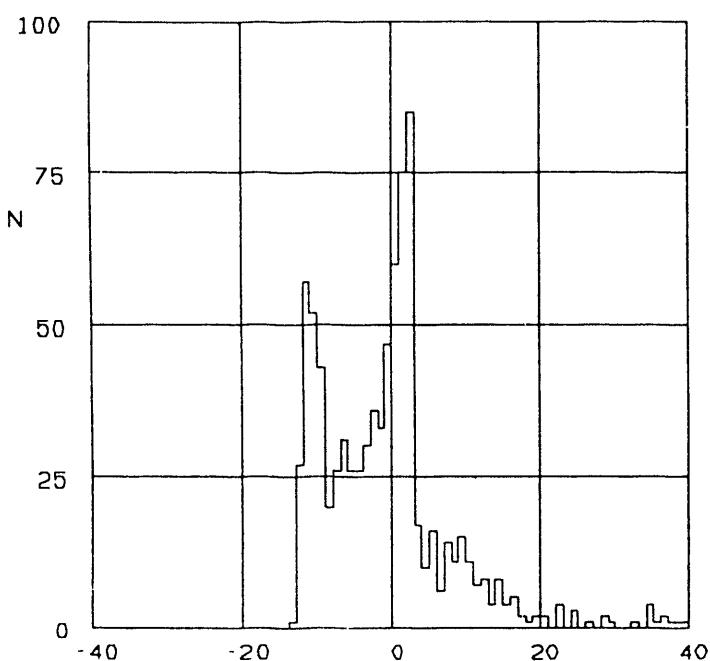
Double-X

Figure 10

CIDPOL, RUN#1, I=60, 21NC, 3NS, V0=160KV, 7/30/81

=14MV/M, Volcano

RUN# 37



PHASE SPEC #PRT IN [20 DEG= 726] ELEMENT= 37
PS = 139.2°

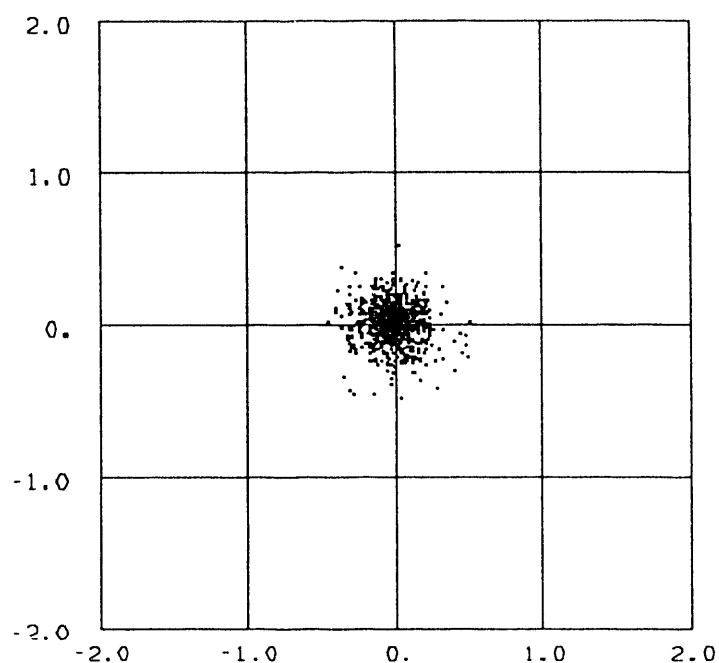
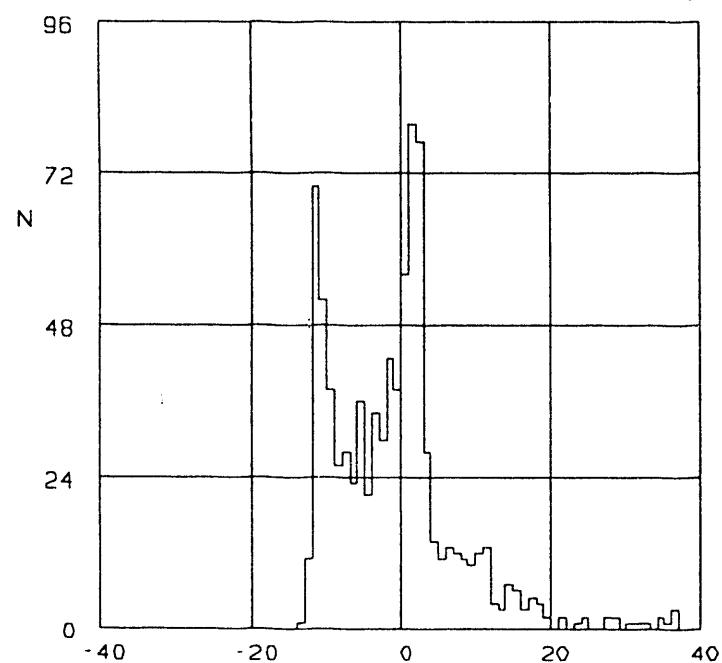
Y(CM) VS. X(CM) N6000= 970

Volcano

CIDPOL, RUN#1, I=60, 21NC, 3NS, V0=160KV, 8/01/81

=14MV/M, Volcano 2

RUN# 37



PHASE SPEC #PRT IN [20 DEG= 731] ELEMENT= 37
PS = 138.9°

Y(LM) VS. X(CM) N6000= 963

Volcano 2

Figure 11

subnum 7
 output 2 1 1 38
 optcon 3 2.0 2 80 1 600 0 800 1
 begin

CIDPOL,

NEL	PART	PART	RMS,N	EMAX,N	EMAX,N	RMS,N	EMAX,N	EMAX,N	ALPHA	BETA	ALPHA	BETA
NO.	IN	OUT	X	X,90%	X,100%	Y	Y,90%	Y,100%	X	X	Y	Y
			CM_mr	CM_mr	CM_mr	CM_mr	CM_mr	CM_mr	CM	CM	CM	CM
1	999	999	0.145	0.711	2.158	0.147	0.761	2.412	-0.9178	0.4063	-0.9152	0.4072
2	999	999	1.629	7.568	40.963	1.532	6.968	38.040	-0.3153	0.0826	-0.2796	0.0833
3	999	999	1.423	6.548	49.378	1.578	7.018	37.667	-0.2797	0.0407	-0.2886	0.0412
4	999	999	1.394	5.857	63.370	1.471	6.069	42.584	-0.0156	0.0240	0.0265	0.0230
5	999	999	2.277	8.964	118.989	2.057	8.515	96.397	0.3116	0.0930	0.2211	0.0972
6	999	999	2.804	11.303	144.102	2.302	9.515	93.688	1.3051	0.0373	1.4189	0.0399
7	999	999	2.520	8.892	125.193	2.043	8.041	83.769	-0.0729	0.0230	-1.0247	0.0372
8	999	999	2.453	9.649	93.136	2.363	9.561	87.366	-0.1566	0.0442	-0.5083	0.0595
9	999	999	2.681	10.269	145.960	2.402	9.139	120.684	-1.5321	0.0601	-1.1303	0.0378
10	999	996	2.991	12.337	96.756	3.343	11.839	115.301	1.1364	0.0321	1.5793	0.0393
11	999	996	3.907	15.159	219.538	3.370	14.024	172.568	0.4553	0.0374	0.2349	0.0289
12	999	996	4.115	17.341	159.997	4.311	19.836	183.999	0.4813	0.0290	0.2101	0.0236
13	999	996	3.273	12.778	165.391	2.983	13.145	119.581	-0.3973	0.0206	-0.4114	0.0197
14	999	996	4.255	15.737	219.623	4.821	18.379	234.448	0.3710	0.0274	0.3569	0.0251
15	999	999	3.513	12.421	215.286	3.833	13.320	216.714	-0.3466	0.0212	-0.3248	0.0109
15	999	12										
16	999	999	4.278	16.729	184.751	3.874	14.005	166.808	0.2416	0.0172	0.4184	0.0181
16	999	5										
17	999	996	3.478	12.648	132.319	4.015	14.412	143.632	0.1427	0.0176	0.0692	0.0149
18	999	996	3.860	14.317	228.860	4.435	17.250	251.091	-0.3274	0.0160	-0.3542	0.0173
19	999	996	4.599	19.002	201.546	5.189	20.536	195.594	0.4215	0.0163	0.3611	0.0142
21	999	999	5.351	23.594	190.961	5.518	22.535	261.298	-0.0122	0.0041	0.1175	0.0037
20	999	996	4.770	18.432	179.163	4.782	19.667	144.275	0.0877	0.0044	0.1827	0.0039
21	999	15										
22	999	996	6.095	28.565	206.849	6.121	30.777	242.071	-0.1413	0.0034	-0.1017	0.0033
26	999	999	5.949	26.865	175.532	5.911	29.846	211.797	0.1646	0.0024	0.1431	0.0025
26	999	4										
27	999	999	6.260	31.248	193.000	6.171	28.873	312.846	-0.1230	0.0028	-0.1993	0.0029
26	999	1										
28	999	998	6.610	30.762	194.896	6.298	28.597	229.578	-0.1806	0.0029	-0.1460	0.0029
33	999	985	7.984	40.034	407.560	7.740	35.841	993.640	0.2007	0.0025	0.1841	0.0026
37	999	981	6.794	36.181	179.755	7.614	39.279	205.045	0.0305	0.0019	-0.0429	0.0019

subnum 7
 output 2 1 1 38
 optcon 3 2.0 2 80 1 600 0 800 1
 begin

CIDPOL,

NEL	PART	PART	RMS,N	EMAX,N	EMAX,N	RMS,N	EMAX,N	EMAX,N	ALPHA	BETA	ALPHA	BETA
NO.	IN	OUT	X	X,90%	X,100%	Y	Y,90%	Y,100%	X	X	Y	Y
			CM_mr	CM_mr	CM_mr	CM_mr	CM_mr	CM_mr	CM	CM	CM	CM
1	999	999	0.187	0.852	3.157	0.142	0.680	2.182	-0.9611	0.4967	-0.8659	0.3367
2	999	999	1.993	8.401	51.587	1.846	8.401	45.555	-0.1015	0.0910	-0.3337	0.0666
3	999	999	1.671	7.439	37.162	1.541	7.275	44.885	-0.5531	0.0492	-0.2455	0.0402
4	999	999	1.658	5.991	75.340	1.877	7.995	45.870	0.0545	0.0270	-0.0855	0.0170
5	999	999	2.893	12.558	122.424	2.818	9.775	136.162	0.1919	0.0743	0.3391	0.0912
6	999	999	2.924	12.102	135.171	3.719	13.656	132.258	1.0367	0.0324	1.2915	0.0347
7	999	999	2.639	10.653	101.633	3.018	10.536	103.362	-0.3040	0.0244	-0.9250	0.0349
8	999	999	2.098	8.271	113.053	3.024	13.126	114.679	-0.0803	0.0578	-0.3417	0.0655
9	999	999	3.469	12.483	212.783	3.166	13.437	135.848	-1.0378	0.0416	-0.9108	0.0324
10	999	990	2.692	11.746	98.130	3.625	13.841	170.963	1.7428	0.0482	1.5564	0.0419
11	999	990	3.348	12.967	236.193	4.021	16.138	263.999	0.1411	0.0398	0.1509	0.0310
12	999	990	3.889	15.072	271.249	4.689	19.898	243.777	0.2064	0.0319	0.1782	0.0266
13	999	990	2.946	12.434	104.947	2.684	10.470	83.628	-0.2568	0.0190	-0.1869	0.0212
14	999	990	5.106	18.848	320.696	3.869	13.314	351.854	0.2622	0.0281	0.2725	0.0351
15	999	990	3.385	12.501	253.190	3.591	12.359	223.956	-0.3646	0.0189	-0.3023	0.0192
16	999	990	4.003	16.404	155.636	4.205	14.453	168.841	0.4675	0.0185	0.4322	0.0193
17	999	990	3.620	12.500	158.129	3.282	11.938	180.383	0.2433	0.0164	0.2487	0.0170
18	999	998	4.180	13.806	277.161	3.920	13.145	262.678	-0.2519	0.0151	-0.2589	0.0152
19	999	990	4.828	18.109	326.014	4.778	19.023	320.215	0.4122	0.0156	0.3861	0.0154
20	999	990	5.128	20.850	201.616	4.684	21.333	154.415	0.2601	0.0034	0.2884	0.0037
21	999	999	5.741	25.146	423.260	6.038	25.639	285.490	-0.2961	0.0042	-0.1536	0.0040
22	999	990	7.241	31.875	329.990	6.945	30.464	354.863	-0.2787	0.0041	-0.2743	0.0040
26	999	994	6.607	32.606	204.990	6.497	30.475	188.089	-0.0418	0.0025	0.0407	0.0023
27	999	991	7.491	36.790	333.559	18.274	55.220	15407.645	-0.0572	0.0029	-0.1100	0.0013
28	999	993	7.275	36.196	317.743	7.389	41.585	281.114	-0.0708	0.0029	0.1075	0.0030
33	999	979	8.412	42.366	288.585	7.823	39.379	221.146	0.2074	0.0028	0.2774	0.0032
37	999	973	7.252	38.818	191.839	7.959	41.111	179.529	0.1084	0.0017	0.0499	0.0017

Figure 12

subnum 7
output 2 1 1 38
optcon 3 2.0 2 80 1 600 0 800 1
begin

Volcano Emittance

CIDPOL,

NEL	PART	PART	RMS,N	EMAX,N	EMAX,N	RMS,N	EMAX,N	EMAX,N	ALPHA	BETA	ALPHA	BETA
NO.	IN	OUT	X	X,90%	X,100%	Y	Y,90%	Y,100%	X	X	Y	Y
1	999	999	CM_mr	0.177	0.797	CM_mr	2.953	0.173	0.779	2.671	-0.8552	0.4685
2	999	999	CM_mr	1.976	9.149	CM_mr	53.231	1.884	8.837	52.366	0.1653	0.0809
3	999	999	CM_mr	1.484	7.115	CM_mr	46.128	1.578	7.369	39.684	-0.7471	0.0444
4	999	999	CM_mr	2.039	7.729	CM_mr	60.915	2.106	7.988	63.669	0.2444	0.0217
5	999	999	CM_mr	3.330	13.603	CM_mr	147.166	2.968	12.256	169.991	0.0892	0.0646
6	999	999	CM_mr	4.035	16.130	CM_mr	154.674	3.618	14.770	147.748	0.7807	0.0292
7	999	999	CM_mr	3.873	14.616	CM_mr	139.308	2.977	11.285	140.567	-0.2793	0.0232
8	999	998	CM_mr	2.987	12.004	CM_mr	84.251	2.757	10.835	83.460	0.1173	0.0533
9	999	998	CM_mr	3.705	14.961	CM_mr	117.005	3.369	13.983	124.290	-0.8778	0.0377
10	999	995	CM_mr	3.473	14.666	CM_mr	90.038	4.190	17.860	98.291	1.2610	0.0397
11	999	995	CM_mr	3.988	16.039	CM_mr	206.575	3.939	17.481	216.715	0.1364	0.0382
12	999	995	CM_mr	4.485	19.948	CM_mr	179.439	4.979	23.528	270.641	0.2409	0.0321
13	999	995	CM_mr	3.505	15.535	CM_mr	129.339	3.248	13.729	79.272	-0.3250	0.0158
14	999	995	CM_mr	5.027	19.747	CM_mr	208.247	4.671	20.198	334.990	0.4285	0.0309
15	999	995	CM_mr	3.873	15.440	CM_mr	250.488	3.901	14.924	208.046	-0.3807	0.0205
16	999	995	CM_mr	4.959	21.907	CM_mr	135.355	4.611	19.194	191.357	0.2084	0.0163
17	999	995	CM_mr	3.904	15.763	CM_mr	140.843	4.590	18.682	122.669	0.1065	0.0168
18	999	995	CM_mr	4.086	16.540	CM_mr	316.114	4.890	19.917	258.316	-0.4571	0.0184
18	999	5	CM_mr	5.699	21.741	CM_mr	260.059	5.291	21.129	206.850	0.2273	0.0136
19	999	4	CM_mr	5.082	21.061	CM_mr	176.252	5.668	24.613	216.971	0.0905	0.0034
20	999	999	CM_mr	6.457	30.304	CM_mr	230.112	6.479	32.040	294.435	-0.2180	0.0041
22	999	999	CM_mr	7.274	35.255	CM_mr	330.776	7.534	32.897	250.566	-0.0982	0.0039
20	999	7	CM_mr	999	999	CM_mr	999	999	999	999	999	999
21	999	12	CM_mr	999	999	CM_mr	999	999	999	999	999	999
22	999	5	CM_mr	999	999	CM_mr	999	999	999	999	999	999
27	999	999	CM_mr	7.414	34.356	CM_mr	228.130	7.307	33.540	291.891	-0.0331	0.0029
26	999	996	CM_mr	6.487	30.513	CM_mr	190.501	7.328	32.411	189.052	0.0509	0.0027
27	999	6	CM_mr	999	995	CM_mr	7.904	39.305	273.685	6.886	32.923	224.053
33	999	973	CM_mr	8.323	39.583	CM_mr	285.594	8.631	38.258	221.609	0.2164	0.0025
37	999	970	CM_mr	8.015	39.025	CM_mr	220.631	8.304	39.143	254.314	-0.0591	0.0017

subnum 7
output 2 1 1 38
optcon 3 2.0 2 80 1 600 0 800 1
begin

Volcano2 Emittance

CIDPOL,

NEL	PART	PART	RMS,N	EMAX,N	EMAX,N	RMS,N	EMAX,N	EMAX,N	ALPHA	BETA	ALPHA	BETA
NO.	IN	OUT	X	X,90%	X,100%	Y	Y,90%	Y,100%	X	X	Y	Y
1	999	999	CM_mr	0.171	0.804	CM_mr	2.990	0.184	0.792	2.569	-0.8335	0.4471
2	999	999	CM_mr	1.938	9.299	CM_mr	50.672	1.933	8.818	50.194	0.1390	0.0789
3	999	999	CM_mr	1.481	7.033	CM_mr	45.912	1.599	7.430	41.391	-0.7166	0.0427
4	999	999	CM_mr	2.106	7.971	CM_mr	60.818	2.013	7.561	67.296	0.2132	0.0205
5	999	999	CM_mr	3.220	13.239	CM_mr	139.927	3.141	12.835	170.504	0.1169	0.0650
6	999	999	CM_mr	4.100	15.843	CM_mr	152.559	3.518	14.349	164.914	0.8371	0.0296
7	999	999	CM_mr	3.875	14.485	CM_mr	136.493	2.918	10.931	138.267	-0.2278	0.0227
8	999	998	CM_mr	3.213	12.769	CM_mr	82.602	2.568	9.807	85.681	0.1436	0.0502
9	999	998	CM_mr	3.833	14.532	CM_mr	97.304	3.257	13.786	119.873	-0.9094	0.0386
10	999	996	CM_mr	3.740	15.656	CM_mr	97.481	3.985	16.713	103.888	1.1665	0.0369
11	999	996	CM_mr	4.469	19.233	CM_mr	205.351	3.755	17.098	187.413	0.2410	0.0350
12	999	996	CM_mr	4.998	24.209	CM_mr	199.961	4.994	23.871	197.828	0.2937	0.0293
13	999	996	CM_mr	3.815	17.911	CM_mr	98.027	3.548	17.346	74.072	-0.4188	0.0179
14	999	996	CM_mr	4.752	19.075	CM_mr	182.470	5.361	22.982	289.697	0.4457	0.0294
15	999	996	CM_mr	4.014	15.852	CM_mr	280.688	4.397	19.220	188.600	-0.4397	0.0215
16	999	996	CM_mr	5.081	22.025	CM_mr	134.562	4.838	20.650	119.094	0.1226	0.0155
17	999	996	CM_mr	3.817	15.365	CM_mr	158.068	5.172	24.319	137.897	0.0345	0.0170
18	999	996	CM_mr	4.585	18.457	CM_mr	340.281	5.634	27.394	252.251	-0.4252	0.0180
19	999	996	CM_mr	5.458	20.623	CM_mr	227.948	5.868	22.797	199.262	0.1034	0.0138
21	999	999	CM_mr	6.514	26.430	CM_mr	237.255	7.321	37.768	215.631	-0.1360	0.0039
22	999	999	CM_mr	7.911	35.403	CM_mr	291.778	7.746	35.158	246.072	-0.1269	0.0037
20	999	996	CM_mr	5.823	25.003	CM_mr	164.473	5.372	21.704	204.024	0.0235	0.0032
21	999	22	CM_mr	999	999	CM_mr	999	999	999	999	999	999
22	999	5	CM_mr	999	999	CM_mr	999	999	999	999	999	999
28	999	999	CM_mr	7.824	40.399	CM_mr	212.861	8.406	39.175	735.842	-0.0070	0.0027
26	999	996	CM_mr	7.503	33.203	CM_mr	207.905	7.183	31.725	171.776	-0.0364	0.0023
28	999	3	CM_mr	999	988	CM_mr	8.099	8.340	43.673	303.349	-0.0578	0.0030
33	999	980	CM_mr	9.073	43.763	CM_mr	340.146	8.690	41.536	273.338	0.2003	0.0027
37	999	963	CM_mr	8.792	44.219	CM_mr	250.645	8.251	41.730	320.493	0.0311	0.0018

Figure 13

PARGRAF OUTGRAF AL Dated 08/07/91 10:44:19 From disk SPC200 Page 1

Reference Z Emissance

PARMELA 10:41:59: 0 AM THURSDAY AUGUST 7, 1991 RUN NO. 0

```

subnum 7
output 2 1 1 11
option 1 2 0 1 80 1 2500 0 20 1
begin
      NEL PART PART Z-EMITTANCE (DEG-KEY) 100%
      IN   OUT    RMS   90%   100%
      1   999  999   4.6   23.7   52.6   -0.8   0.0   1.0   88357.1
      2   999  999  114.9  430.5  1344.5  -0.4   0.1   1.3   3555.8
      3   999  999  224.9  923.5  2404.4  -0.5   0.0   2.0   1824.1
      4   999  999  326.6  1241.9  3856.4  -10.0  -0.1   2.3   1260.5
      4   999  999   4     482.7  1873.1  6429.8   2.0   0.2   2.2   868.2
      5   999  999   5     467.3  1717.7  6475.1   2.5   0.1   2.4   901.5
      6   999  999   6     505.1  1840.6  7235.9   1.4   0.1   2.5   842.2
      7   999  999   7     566.4  2148.5  7631.7   1.7   -0.1   2.4   755.7
      8   999  999   8     636.0  2471.7  9065.8   2.4   -0.3   2.5   682.9
      10  999  996   10    662.3  11582.0  11598.6   0.1   -0.9   2.9   682.4
      11  999  996   11    805.7  3154.0  14485.7   5.7   0.0   3.0   585.0
      subnum 7
      output 2 1 12 18
      option 1 2 0 1 80 1 2500 0 120 1
      begin
      NEL PART PART Z-EMITTANCE (DEG-KEY) 100%
      IN   OUT    RMS   90%   100%
      12  999  996  2810.7  9396.2  120556.1  5.7   2.8   -6.5   165.9
      13  999  996  2684.6  9007.5  121142.7  10.0  2.3   -5.9   138.5
      14  999  996  2478.9  8266.2  117442.1  13.7  2.3   -5.5   114.3
      15  999  999  2199.5  7327.4  115369.0  5.0   2.5   -4.9   89.9
      16  999  12    16    999  1965.8  6864.4  108051.9  12.0  3.2   -4.4   72.6
      17  999  996  17    999  1955.7  6822.9  104979.7  16.7  3.8   -4.3   69.4
      18  999  996  18    999  2821.0  10854.8  181000.5  17.7  6.7   -5.4   43.6
      subnum 7
      output 2 1 19 38
      option 1 2 0 1 80 1 800 0 200 1
      begin
      NEL PART PART Z-EMITTANCE (DEG-KEY) 100%
      IN   OUT    RMS   90%   100%
      19  999  996  1566.3  5605.9  140946.1  35.1   7.2   -5.7   29.4
      21  999  999  3618.9  9818.5  97734.6  24.0   9.1   -1.2   2.5
      20  999  996  1869.9  8822.8  38244.7  34.4   9.9   -2.0   8.3
      21  999  15    21    999  6327.1  22966.0  212831.7  44.0  -0.4   1.4
      22  999  996  26    999  13213.6  90392.2  450544.2  78.7  -80.7   0.9
      26  999  4     26    999  14063.7  93071.9  513455.5  90.7  17.0   0.2
      27  999  999  28    999  998  28652.4  147966.4  1414198.0  92.8  137.8   0.1
      33  999  985  33    999  81502.5  393710.9  5626899.0  67.3  396.4   0.2
      37  999  981  37    999  114267.6  560467.0  7774995.0  65.0  359.5   0.3
      subnum 7
      output 2 1 1 11
      option 1 2 0 1 80 1 2500 0 20 1
      begin
      NEL PART PART Z-EMITTANCE (DEG-KEY) 100%
      IN   IN    RMS   90%   100%
      1   999  999   1     999  999   7.3   30.5   2598.0  -0.7   -0.2   0.7   45944.2
      2   999  999   2     999  999   147.4  515.6   3335.7  -0.1   -0.1   1.1   2287.9
      3   999  999   3     999  999   324.9  1110.2   7688.1  -1.6   -0.3   1.5   1044.0
      4   999  999   4     999  999   533.4  1575.6  13650.3  -3.3   -0.4   1.6   642.8
      5   999  999   5     999  999   769.7  2325.3  19676.9  -5.3   -0.2   1.6   468.8
      6   999  999   6     999  999   836.2  2419.6  20448.4  -6.2   -0.3   1.6   456.2
      7   999  999   7     999  999   802.8  2639.3  20545.8  -6.5   -0.2   1.7   424.0
      9   999  999   9     999  999   1043.9  3060.7  27653.0  -7.9   -0.5   1.7   349.0
      10  999  999  10    999  990   1155.5  3531.4  34033.4  -12.9  -0.7   1.9   333.6
      11  999  996  11    999  990   1378.1  4171.3  41402.0  -17.0  -1.4   2.0   295.3
      subnum 7
      output 2 1 12 18
      option 1 2 0 1 80 1 2500 0 120 1
      begin
      NEL PART PART Z-EMITTANCE (DEG-KEY) 100%
      IN   IN    RMS   90%   100%
      12  999  990   12    999  990   1923.7  7047.0  156490.2  -17.1  1.7   -8.0   209.5
      13  999  990   13    999  990   1819.5  6784.2  151831.1  -20.0  2.4   -7.4   177.6
      14  999  990   14    999  990   1547.6  5581.4  145341.3  -22.3  2.9   -7.4   160.3
      15  999  990   15    999  990   1398.3  5475.5  134006.9  -23.3  3.1   -6.8   132.3
      16  999  990   16    999  990   1172.1  4866.1  120320.2  -22.7  3.3   -6.6   114.0
      17  999  990   17    999  990   1156.2  4919.9  113751.1  -22.2  3.3   -6.3   106.4
      18  999  998   18    999  998   2318.5  8778.5  175532.8  -14.7  5.5   -6.1   51.3
      subnum 7
      output 2 1 19 38
      option 1 2 0 1 80 1 800 0 200 1
      begin
      NEL PART PART Z-EMITTANCE (DEG-KEY) 100%
      IN   IN    RMS   90%   100%
      19  999  990   19    999  990   3597.1  144473.2  -34.0  6.4   -9.0   49.1
      20  999  990   20    999  990   1286.8  5331.8  65300.2  -33.8  9.6   -3.1   11.9
      21  999  999   21    999  999   4633.1  14134.1  232903.6  -31.5  18.2  -1.1   2.4
      22  999  999   22    999  999   6373.1  20845.8  272970.9  -45.8  -11.5  -0.2   1.3
      24  999  999   24    999  999   12966.9  66678.7  469781.7  -84.5  -66.2  -1.0   1.6
      25  999  999   25    999  999   13712.0  80789.4  478194.0  -88.5  -30.5  0.1   1.7
      26  999  999   26    999  999   25189.1  140008.8  1436733.0  -87.9  158.0  0.0   1.1
      28  999  999   28    999  999   68159.9  382448.2  4453922.0  -57.8  376.8  0.0   0.4
      33  999  999   33    999  999   973  38521.1  482712.7  -8813949.0  -59.1  312.8  0.2   0.3
      
```

Figure 14

PARGRAF OUTGRAF AI Dated 08/07/91 10:18:29 From disk SPC200 Page 1

Volcano 2 Emissanc

PARMELA 10: 9:46: 0 AM THURSDAY AUGUST 7, 1991 RUN NO. 0

PARMELA 10:47:57: 0 AM THURSDAY AUGUST 7, 1991 RUN NO. 0

```

subnum 7
output 2 1 1 11
option 1 2 0 1 80 1 2500 0 20 1
begin
    NEL PART PART Z-EMITTANCE (DEG-KEV) 100%
    IN OUT RMS 90% 100%
    1 999 999 7.3 30.2 2659.9 -0.7 -0.2 0.7 46127.2
    2 999 999 137.8 484.1 3112.4 0.0 -0.1 1.1 2448.9
    3 999 999 324.6 1164.2 7837.1 1.7 -0.3 1.5 1045.5
    4 999 999 536.3 1745.8 13563.5 3.5 -0.4 1.5 639.6
    5 999 999 764.2 2495.4 18759.8 5.7 -0.2 1.5 456.6
    6 999 999 789.1 2387.7 19644.2 6.6 -0.2 1.6 445.1
    7 999 999 855.2 2638.1 21687.8 8.7 -0.2 1.6 415.7
    8 999 998 914.3 2851.7 23793.1 7.9 -0.1 1.6 390.1
    9 999 998 1046.0 3018.9 26886.1 9.1 -0.2 1.7 347.5
    10 999 995 1136.8 33413.2 34413.2 11.6 0.1 1.9 331.9
    11 999 995 1357.7 3989.3 41883.3 14.0 -0.1 2.0 293.6
    subnum 7
    output 2 1 12 18
    option 1 2 0 1 80 1 2500 0 120 1
begin
    NEL PART PART Z-EMITTANCE (DEG-KEV) 100%
    IN OUT RMS 90% 100%
    12 999 995 1872.0 7037.8 151734.1 14.1 2.7 -8.1 210.9
    13 999 995 1753.8 6654.1 147298.6 16.9 2.5 -7.6 180.2
    14 999 995 1495.7 5663.9 138759.6 19.4 2.8 -7.6 161.9
    15 999 995 1343.9 5165.7 125442.6 20.8 3.0 -7.0 134.1
    16 999 995 1174.9 4811.7 108017.7 21.0 3.1 -6.4 110.5
    17 999 995 1151.9 4653.1 100795.6 20.9 3.1 -6.1 103.6
    18 999 995 1793.4 7283.2 194301.5 17.5 5.3 -7.0 57.7
    subnum 7
    output 2 1 19 38
    option 1 2 0 1 80 1 800 0 200 1
begin
    NEL PART PART Z-EMITTANCE (DEG-KEV) 100%
    IN OUT RMS 90% 100%
    19 999 999 916.9 3842.6 111499.6 32.4 5.5 -8.1 43.7
    20 999 999 1475.9 5685.7 18885.2 149873.4 45.2 -6.3 -0.3 1.1
    21 999 999 3795.2 11579.4 90707.1 30.3 21.2 -1.1 2.2
    22 999 999 13522.9 78754.1 333509.0 89.2 52.0 0.2 1.6
    23 999 995 14434.7 86479.1 1868099.0 87.8 -57.9 1.1 1.6
    24 999 973 80771.1 393876.4 5581255.0 59.8 342.0 0.2 1.1
    33 999 970 120965.7 5681411.1 8310048.0 61.4 280.2 0.5 0.3
    subnum 7
    output 2 1 1 11
    option 1 2 0 1 80 1 2500 0 20 1
begin
    NEL PART PART Z-EMITTANCE (DEG-KEV) 100%
    IN OUT RMS 90% 100%
    1 999 999 7.3 30.2 2641.3 -0.7 -0.2 0.7 45911.3
    2 999 999 138.3 486.0 3122.9 0.0 -0.1 1.1 2440.7
    3 999 999 324.9 1145.1 7825.0 1.7 -0.3 1.5 1044.6
    4 999 999 534.7 1735.5 13628.4 3.6 -0.4 1.5 641.6
    5 999 999 761.0 2466.8 18721.5 5.7 -0.2 1.5 458.5
    6 999 999 787.1 2395.8 19595.3 6.7 -0.3 1.6 446.3
    7 999 999 855.0 2606.6 21610.5 8.4 -0.2 1.6 416.1
    8 999 999 914.3 2756.8 23730.2 7.7 -0.2 1.6 390.3
    9 999 998 1039.8 3016.2 26809.2 8.9 -0.2 1.6 349.9
    10 999 996 1133.9 3252.8 34221.6 10.8 -0.2 1.6 332.7
    11 999 996 1354.5 3852.1 41515.1 12.9 -0.3 2.0 294.3
    subnum 7
    output 2 1 12 18
    option 1 2 0 1 80 1 2500 0 120 1
begin
    NEL PART PART Z-EMITTANCE (DEG-KEV) 100%
    IN OUT RMS 90% 100%
    12 999 996 1886.6 7244.4 151259.8 12.9 2.5 -8.0 209.3
    13 999 996 1760.0 6870.1 147314.8 15.3 2.1 -7.6 179.6
    14 999 996 1508.1 5809.7 138576.0 17.5 2.3 -7.5 160.6
    15 999 996 1354.2 5553.4 125360.6 18.4 2.9 -6.9 133.1
    16 999 996 1185.6 4895.4 10794.7 18.1 2.9 -6.3 109.3
    17 999 996 1155.9 4911.6 100764.6 17.7 2.5 -6.1 103.3
    18 999 996 1843.3 7663.6 197295.0 18.3 5.0 -7.2 59.0
    subnum 7
    output 2 1 19 38
    option 1 2 0 1 80 1 800 0 200 1
begin
    NEL PART PART Z-EMITTANCE (DEG-KEV) 100%
    IN OUT RMS 90% 100%
    19 999 996 967.9 3901.2 107814.8 31.5 6.6 -8.1 43.9
    21 999 999 3549.0 10518.9 98128.2 24.1 13.1 -1.2 2.1
    22 999 999 5634.8 18331.2 15000.4 44.2 -0.3 1.1
    20 999 996 1392.5 633545.6 633545.6 33.5 8.0 -2.7 10.4
    21 999 22
    22 999 5
    28 999 999 27424.2 148150.6 690543.0 92.7 155.2 0.2 1.1
    26 999 996 13537.2 92138.4 620226.9 85.1 -61.2 1.1 1.5
    28 999 3
    27 999 999 988 14001.7 78224.5 805072.6 89.4 49.0 0.3 1.8
    33 999 999 76744.7 344704.7 6061405.0 55.4 346.4 0.1 0.4
    37 999 963 108553.9 505137.9 8761921.0 55.8 305.4 0.3 0.3

```

Figure 15

Figure 16

PARGRAF OUTGRAF A1 Dated 08/09/91 16:15:19 From disk SPC200 Page 1 RUN NO.

Second Standard Emissances

PAMELA 4:10:19: 0 PM SATURDAY AUGUST 9, 1991
 Output 2 1 1 11 Optcon 1 2.0 1 80 1 2500 0 20 1
 begin

subnum 7
 Output 2 1 1 11 Optcon 1 2.0 1 80 1 2500 0 20 1
 begin
 NEL PART PART Z-EMITTANCE (DEG-KEV) 100%
 IN OUT RMS 90%
 1 999 999 7.7 31.6 2544.5 -0.7 -0.2 0.7 43916.1
 2 999 999 160.8 585.6 -0.1 0.1 1.0 2098.8
 3 999 999 320.7 1078.3 8029.3 1.4 -0.1 1.5 1058.3
 4 999 999 528.5 1562.0 13108.1 2.7 -0.3 1.6 649.2
 5 999 999 733.3 2276.0 19605.1 4.2 -0.1 1.6 0.0155
 6 999 999 742.3 2195.0 20375.1 5.5 -0.1 1.7 473.3
 7 999 999 817.3 2386.0 21521.8 5.9 -0.2 1.7 434.1
 8 999 999 900.7 2691.9 23842.7 6.5 -0.2 1.7 397.1
 9 999 999 1019.5 3007.5 27753.7 7.6 -0.4 1.7 357.6
 10 999 994 1103.1 3170.0 32959.7 12.2 -0.3 1.9 347.8
 11 999 994 1322.9 3697.7 40742.4 16.1 -1.2 2.0 306.0
 subnum 7
 Output 2 1 12 18 Optcon 1 2.0 1 80 1 2500 0 120 1
 begin

NEL PART PART Z-EMITTANCE (DEG-KEV) 100%
 IN OUT RMS 90%
 12 999 994 2048.9 7406.7 157803.0 16.2 2.1 -7.5 195.7
 13 999 994 1930.6 6943.6 152536.9 18.7 2.4 -7.0 166.5
 14 999 999 1680.4 6244.1 145617.7 15.9 2.4 -6.7 144.3
 15 999 994 1523.7 5953.7 134217.4 22.3 2.8 -6.2 120.8
 16 999 999 1289.7 5259.7 119468.1 20.0 3.0 -5.8 99.8
 17 999 994 1299.1 5431.4 113346.8 22.3 3.0 -5.5 94.2
 18 999 994 2087.0 8728.6 222340.3 23.0 5.7 -6.4 53.4
 subnum 7
 Output 2 1 19 38 Optcon 1 2.0 1 80 1 800 0 200 1
 begin

NEL PART PART Z-EMITTANCE (DEG-KEV) 100%
 IN OUT RMS 90%
 19 999 994 998.7 3747.4 167789.4 36.2 6.0 -8.0 43.6
 20 999 999 3931.0 11748.2 100154.6 34.4 21.4 -1.1 2.1
 21 999 999 5170.3 14830.0 118277.0 43.5 -10.0 -0.2 1.1
 22 999 999 1128.3 4886.0 37137.4 38.9 -7.8 -3.3 12.4
 23 999 999 11514.4 73582.0 443572.9 74.5 -38.7 1.0 1.4
 24 999 999 13676.9 91915.8 307479.2 84.4 57.2 0.2 1.6
 25 999 999 26319.2 149613.4 729422.1 87.6 156.7 0.2 1.1
 26 999 999 87833.6 401401.6 58456.8 601.8 337.7 0.3 0.5
 27 999 999 113621.5 562200.5 7442646.0 56.6 254.1 0.4 0.3

begin
 NEL PART PART Z-EMITTANCE (DEG-KEV) 100%
 IN OUT RMS 90%
 28 999 999 47.139 225.477 2200.131 -0.1139 0.0028 -0.10271 0.0024
 29 999 999 198.503 42.877 225.477 -0.1040 0.0028 -0.1013 0.0030
 30 999 999 7.639 37.643 200.271 0.0046 0.0027 0.0018 -0.0472 0.0027
 31 999 999 40.015 283.898 183.720 0.2322 0.234.247 0.0027 0.0018
 32 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 33 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 34 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 35 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 36 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 37 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 38 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 39 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 40 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 41 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 42 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 43 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 44 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
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 46 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 47 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 48 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 49 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
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 51 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
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 94 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
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 116 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
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 118 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 119 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 120 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
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 127 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
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 129 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 130 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
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 137 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 138 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 139 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 140 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
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 146 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 147 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 148 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234.247 0.0027
 149 999 999 8.730 40.049 40.015 283.898 183.720 0.2322 0.234

2nd Standard

ID=XY@Q

2nd Standard

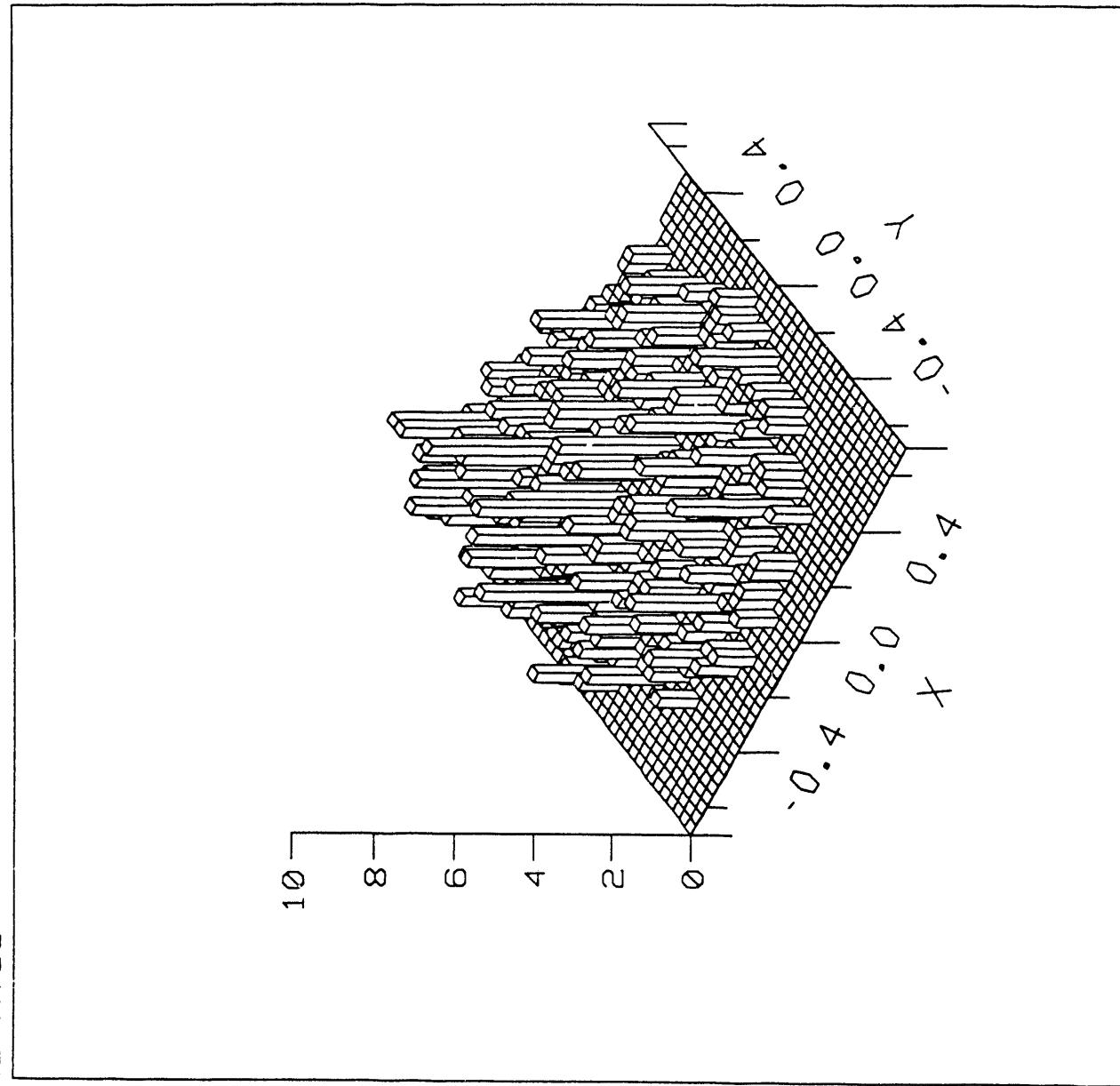
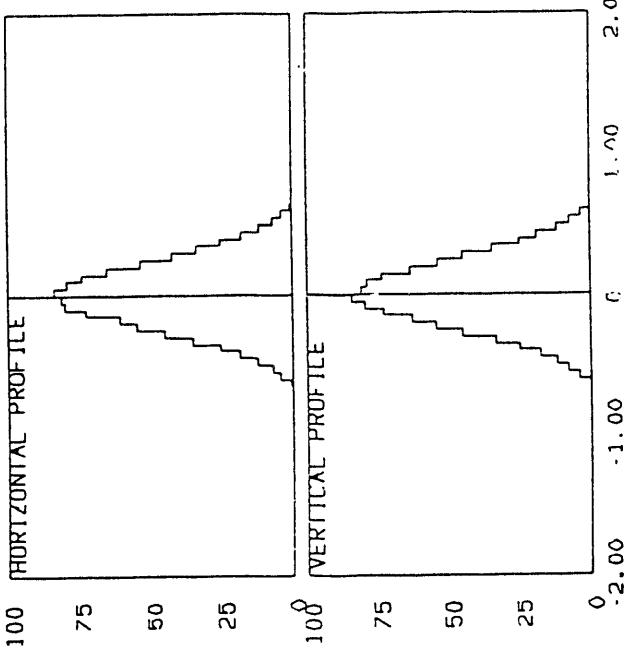
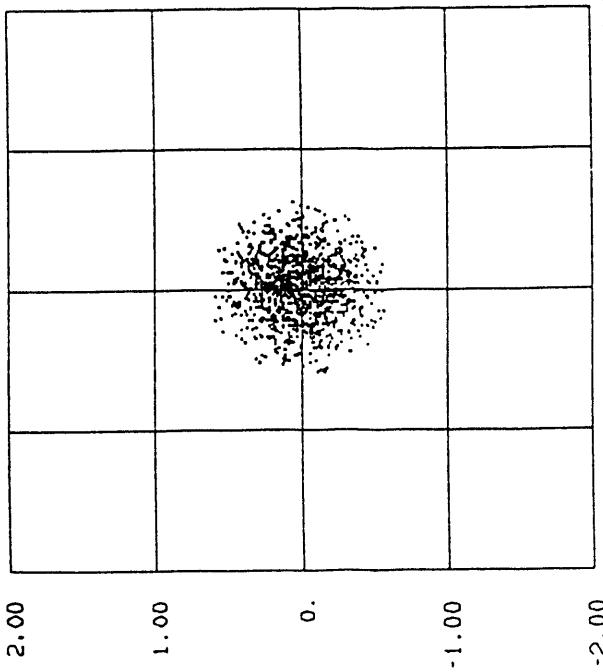


Figure 17

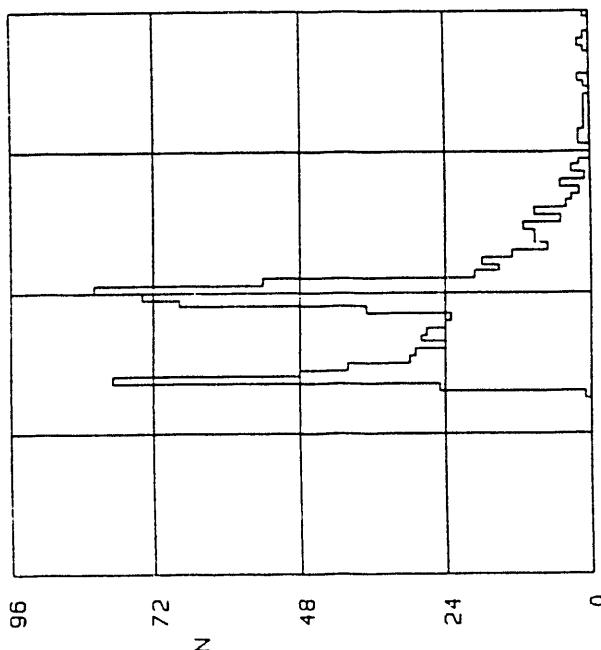


2nd Standard

C10POL, RUN# 1, I=60, 21NC, 3NS, V0=160KV, 8/09/91, F = 4MV/M,

RUN# 37

23



PHASE SPEC #PRT IN [20 DEG= 758] ELEMENT= 37
 $\rho_X = 140.3$ deg
 $\text{NGOOD} = 977$

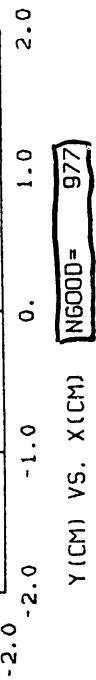
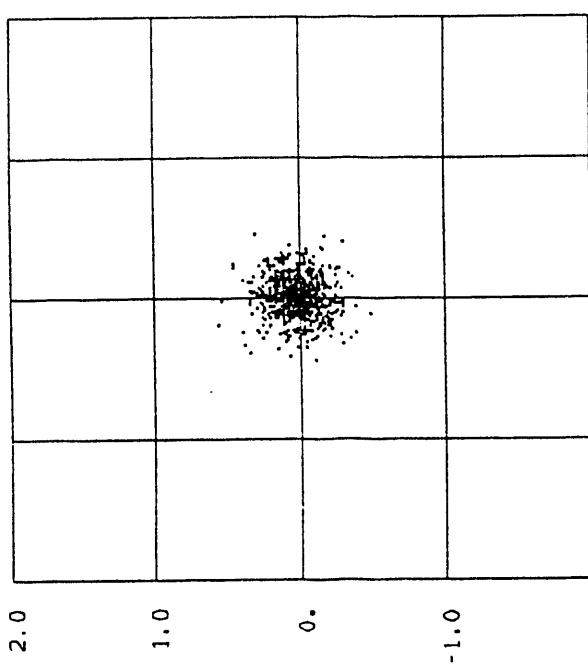
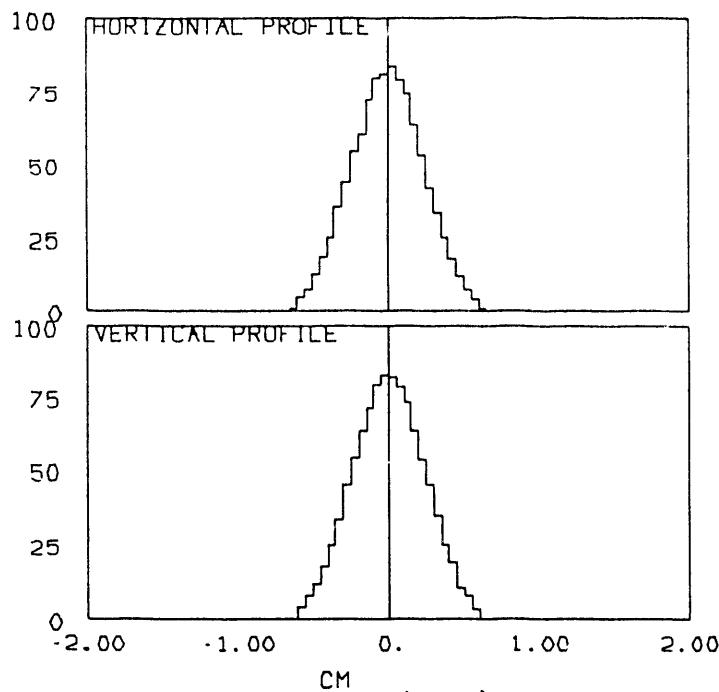
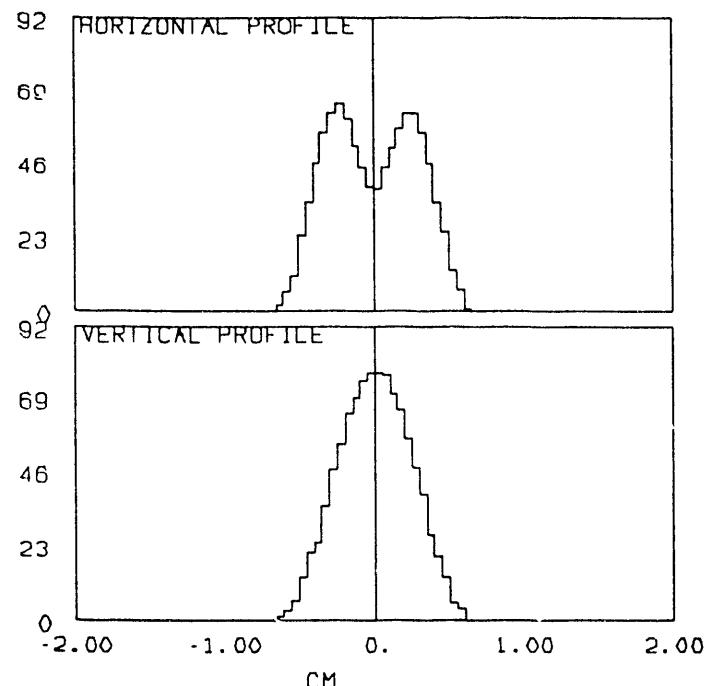


Figure 18

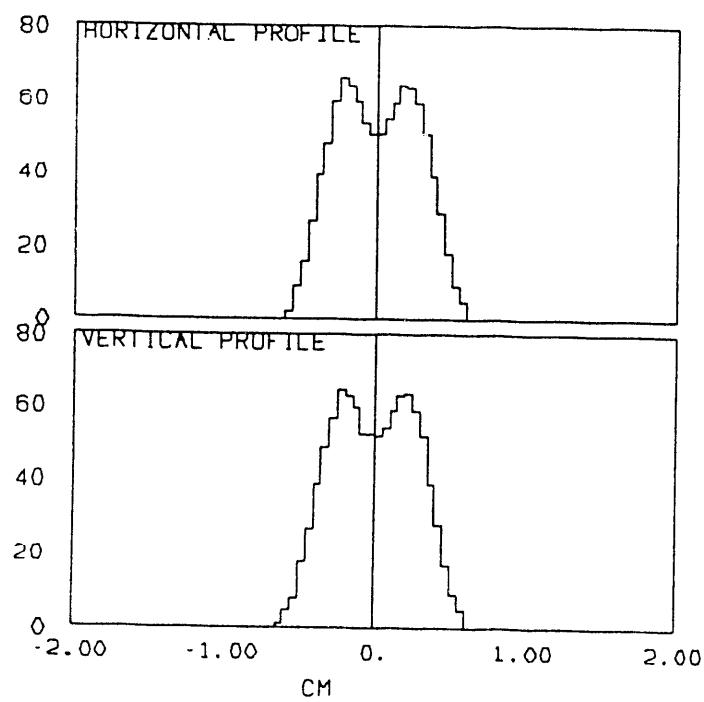
X, Y Spacial Distributions at Start



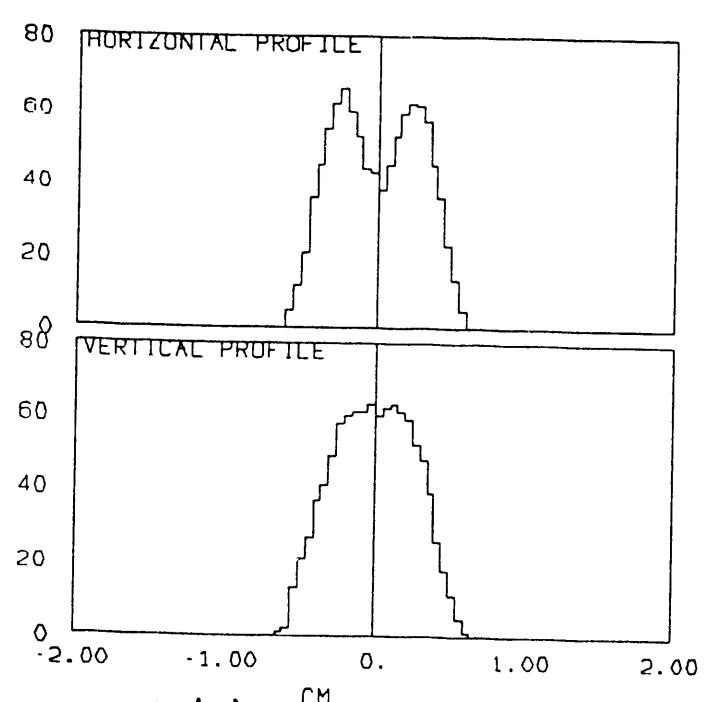
2nd Standard Gauss



Double X Gauss



Volcano Gauss

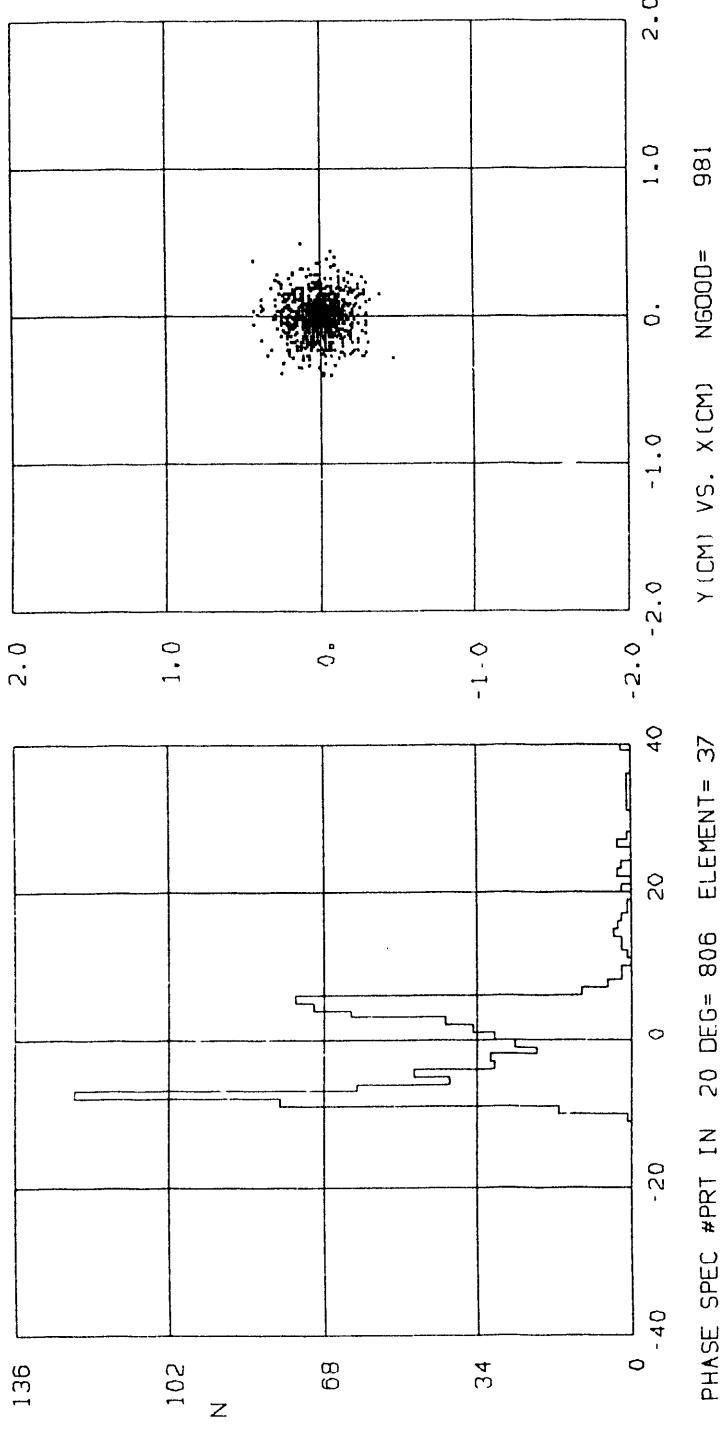


Volcano 2 Gauss

Figure 19

CIDPOL, RUN#1, I=60, 21NC, 3NS, V0=160KV, 8/09/91, 4MV/M,

RUN# 37



2nd
Standard
Gauss

25

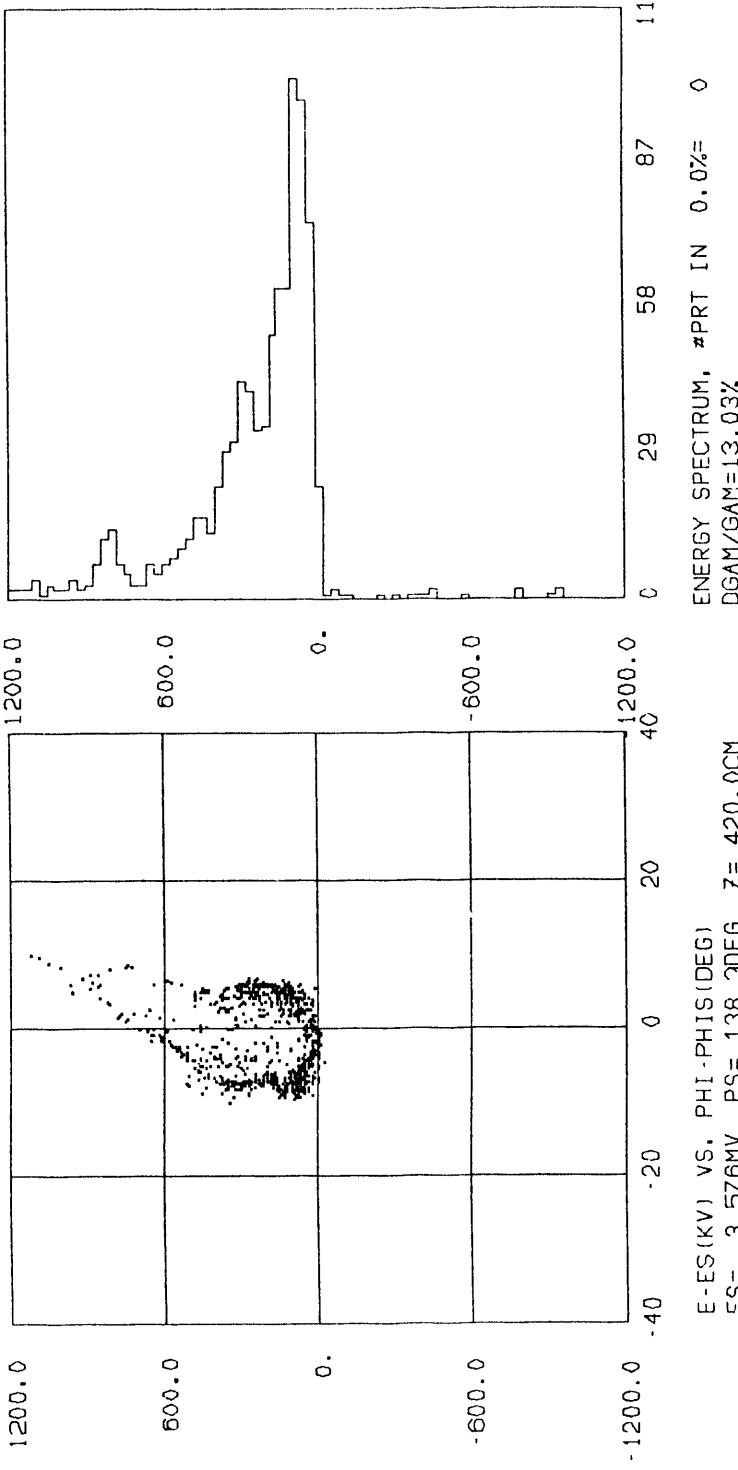
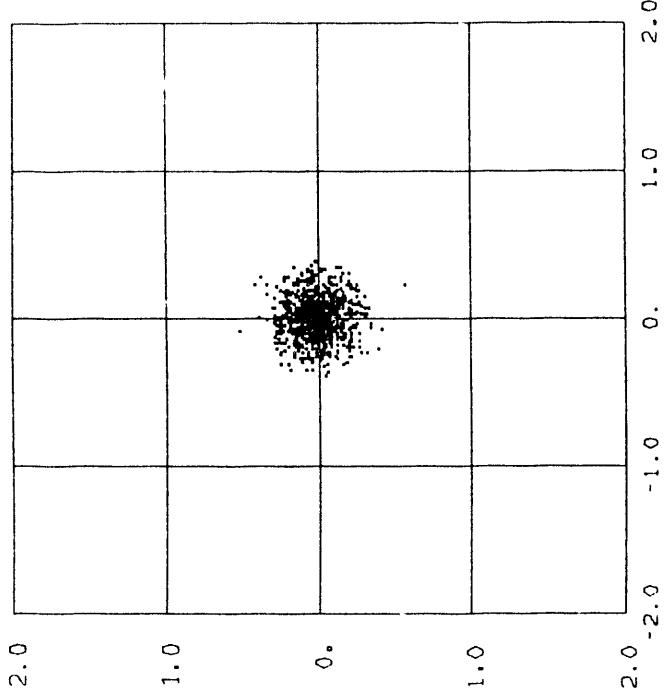
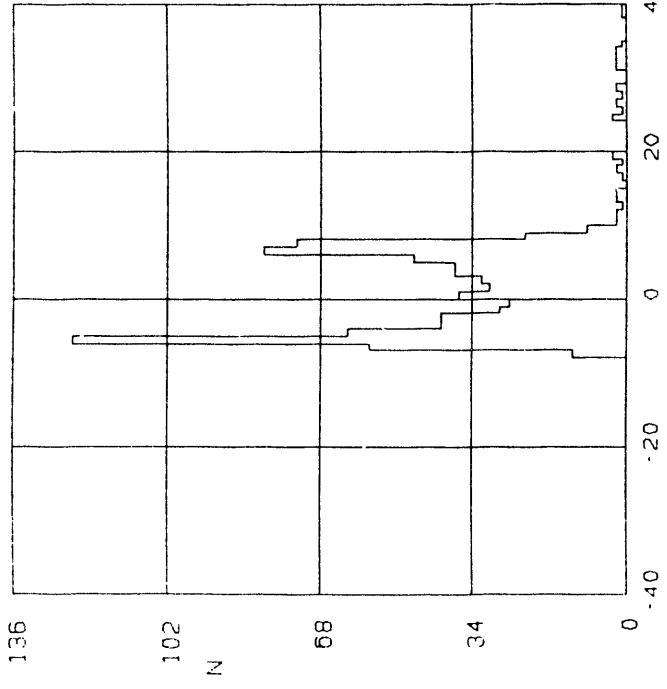


Figure
20

C10POL, RUN# 1, I=60, 21INC, 3NS, V0=160KV, 8/09/91

RUN# 37



PHASE SPEC #PRT IN 20 DEG= 801 ELEMENT= 37

26

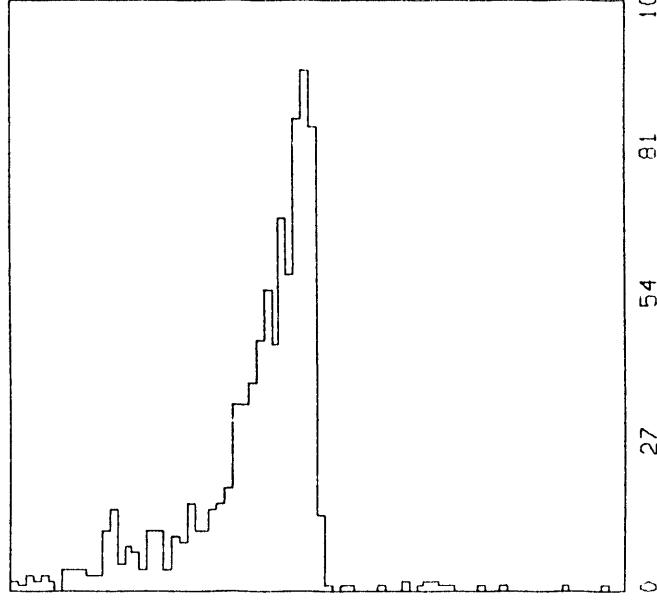
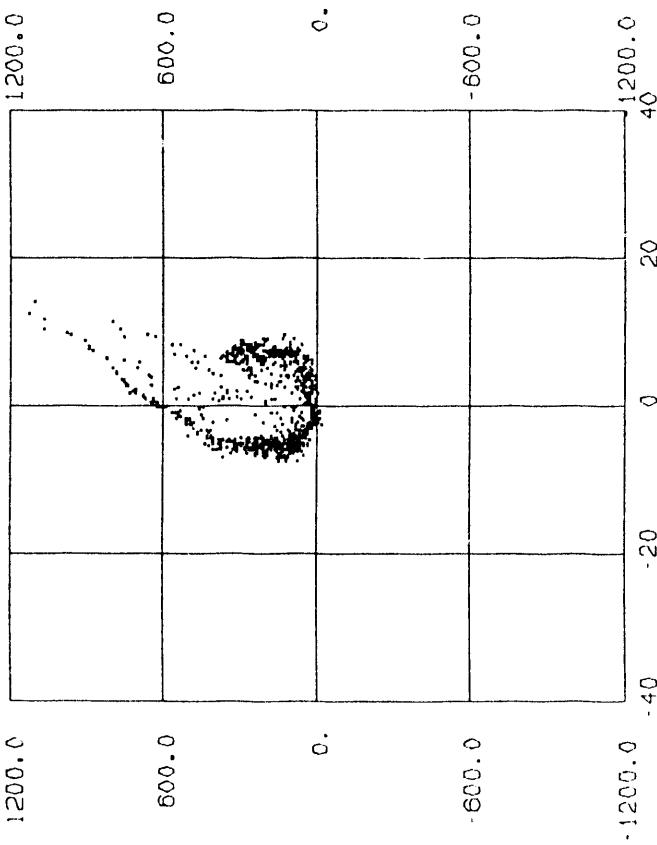


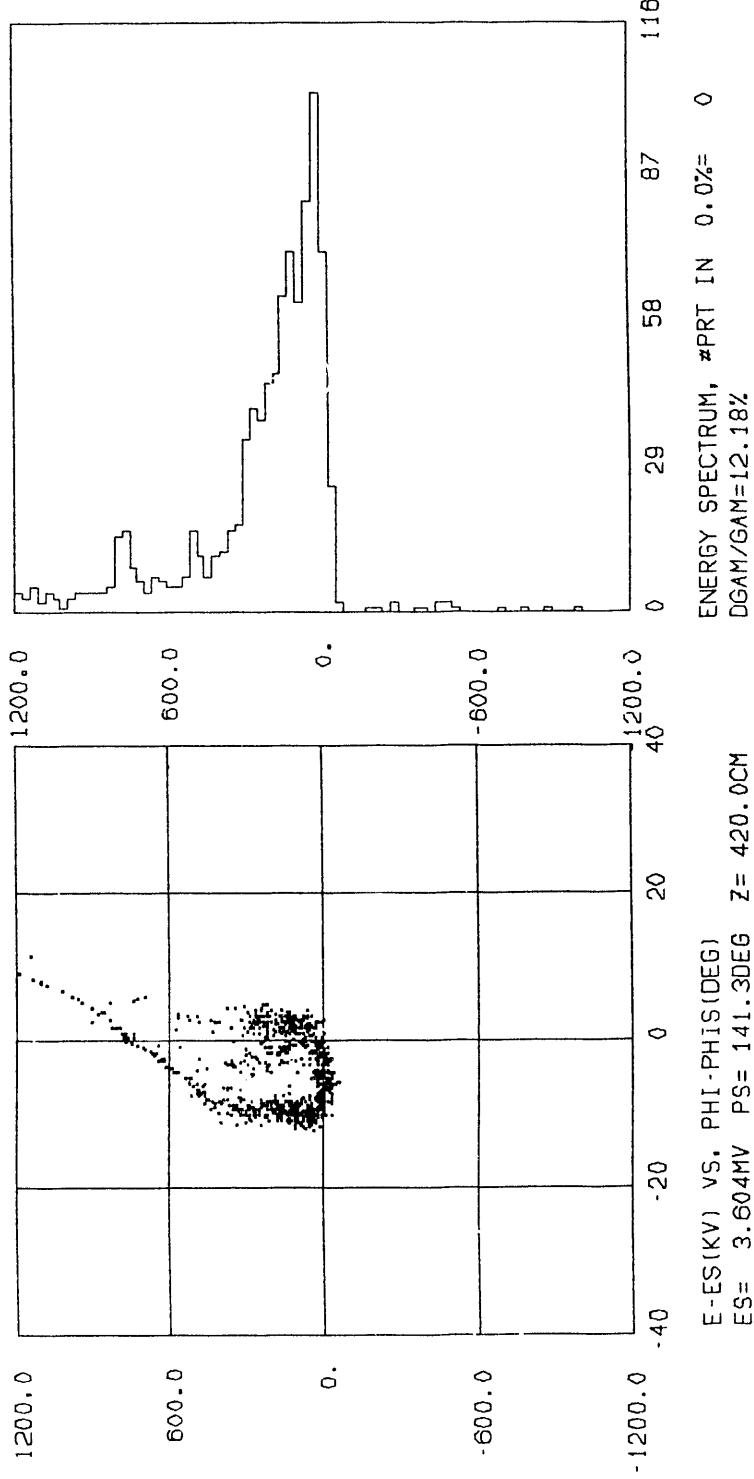
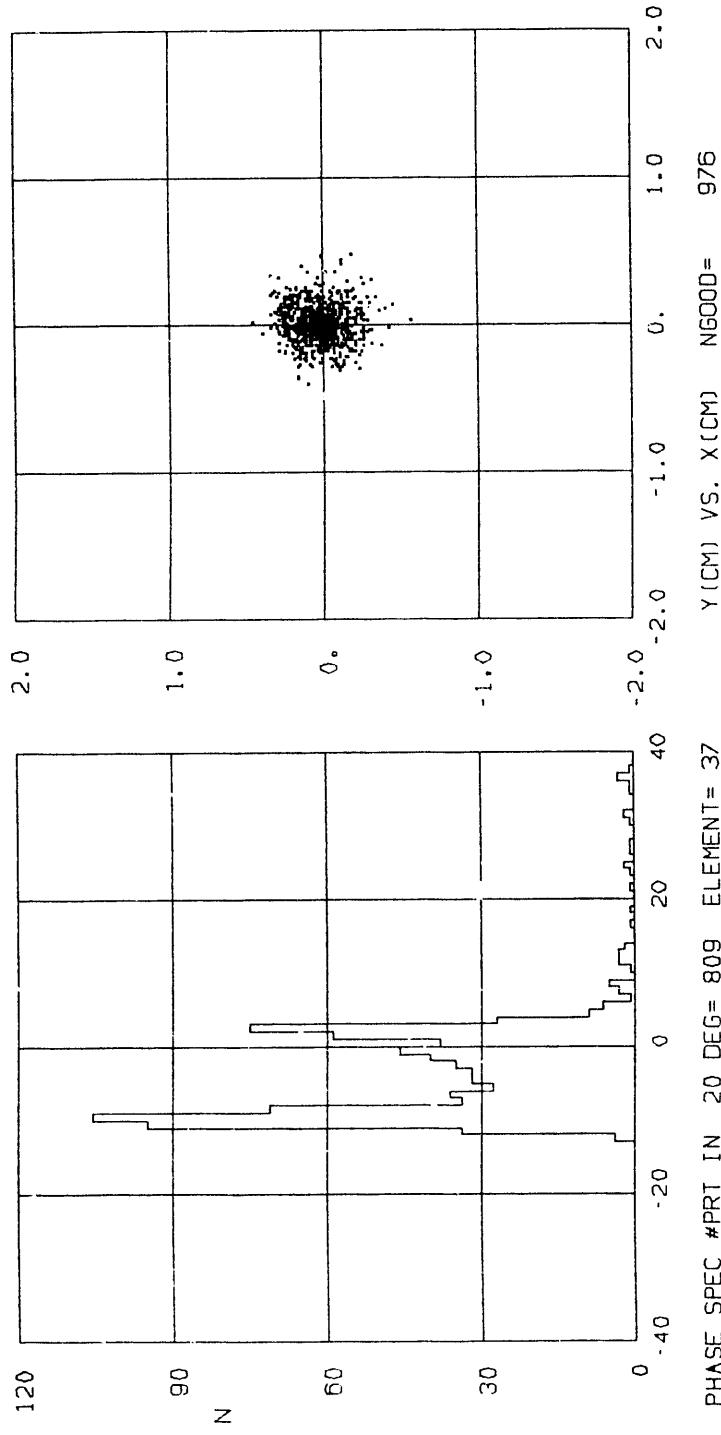
Figure
21

E-ES (KV) VS. PHI-PHI\$ (DEG)
FS= 3.573MV PS= 136.50FG θ = 420.0CM

ENERGY SPECTRUM, #PRT IN 0.0%
DGAM/GAM=12.53%

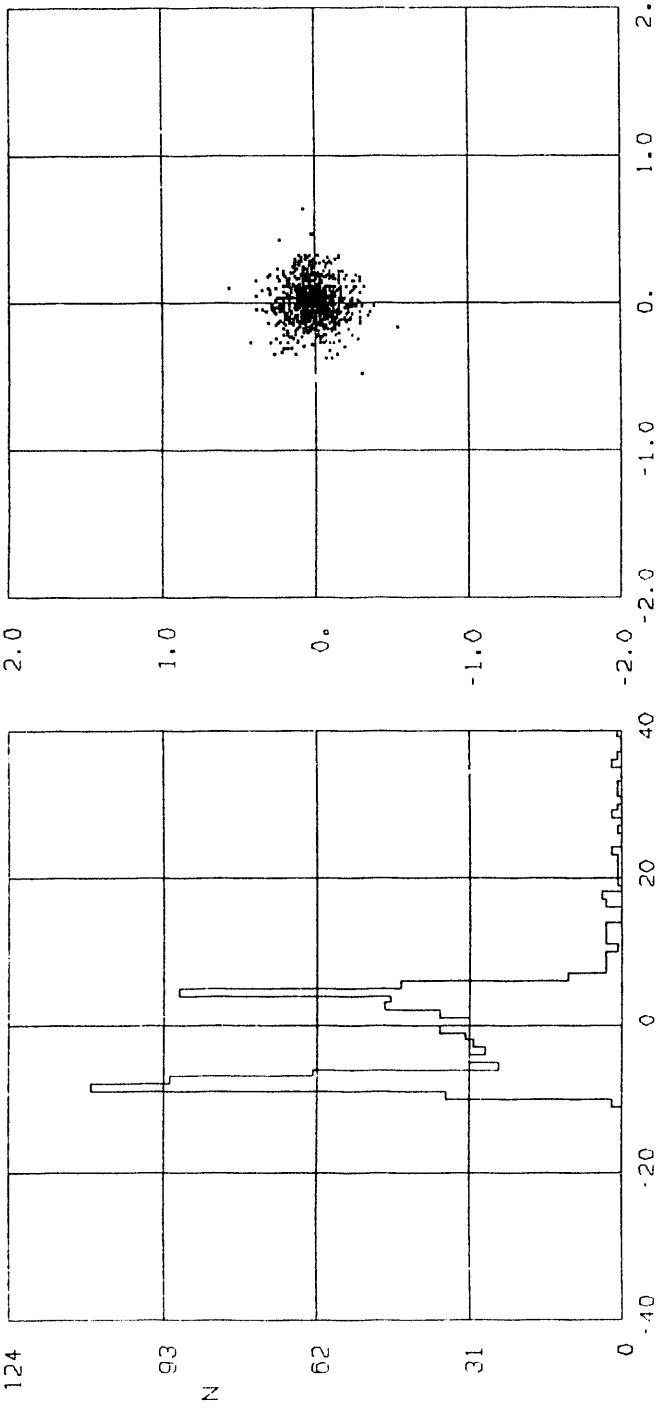
Volcano
Crater

Figure
22

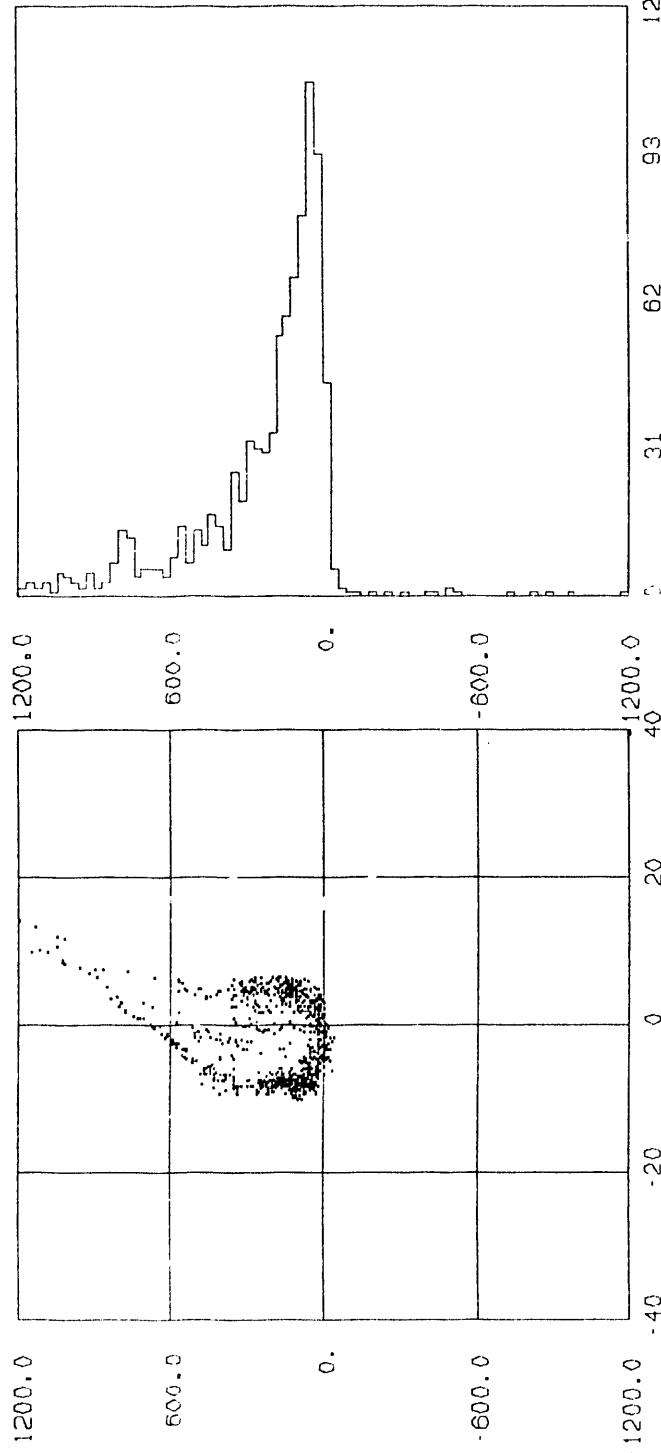


C1OPOL, RUN#1, I=60, 21INC, 3NS, V0=160KV, E,'09/91.

RUN# 37
4MV/M_i



PHASE SPEC #PRT FN 20 DEG= 800 ELEMENT= 37



E - EES (KV) VS. PHI - PHIS (DEG)

ENERGY SPECTRUM. #PPT IN 0.0% = 0

Figure 23

Gauss

23

END

**DATE
FILMED**

1/12/91

