



MIT Plasma Science & Fusion Center

Pacific Northwest  
National Laboratory

Operated by Battelle for the  
U.S. Department of Energy



# Millimeter-Wave High Temperature Process Monitoring

Paul P. Woskov

*Massachusetts Institute of Technology*

*In collaboration with:*

S. K. Sundaram<sup>2</sup>, Gene Daniel<sup>3</sup>, K. Hadidi<sup>1</sup>, P. Thomas<sup>1</sup>,  
and L. Bromberg

<sup>1</sup>*Massachusetts Institute of Technology*

<sup>2</sup>*Pacific Northwest National Laboratory*

<sup>3</sup>*Savannah River Technology Center*

*IRMMW 2002 Sept. 26, 2002, San Diego, CA*



**EMSP**

Environmental Management Science Program



# High Temperature Process Monitoring Needs

- Many process environments inaccessible to conventional sensors

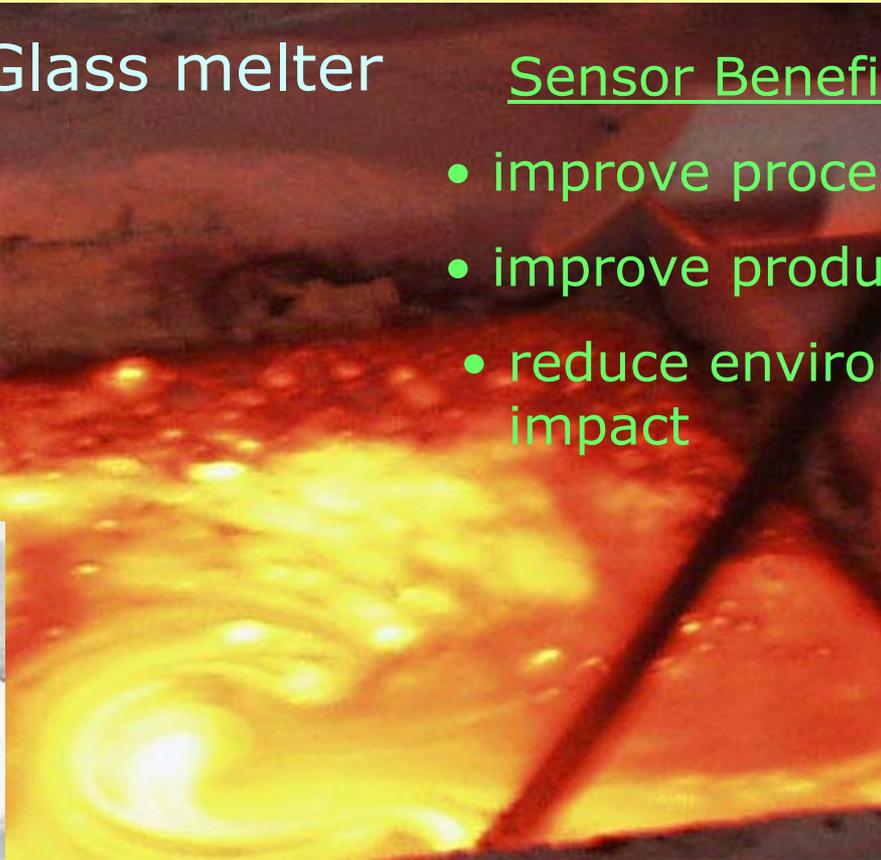
- too hot
- corrosive
- dirty
- radioactive

Glass melter

## Sensor Benefits

- improve process efficiency
- improve product quality
- reduce environmental impact

Glass pour



- Many processes could benefit
  - metals refining, glass manufacturing, and waste remediation

# Defense Waste Processing Facility

- **Predictive Model Feed Forward Control**

- ✓ Processing limited by prediction uncertainties

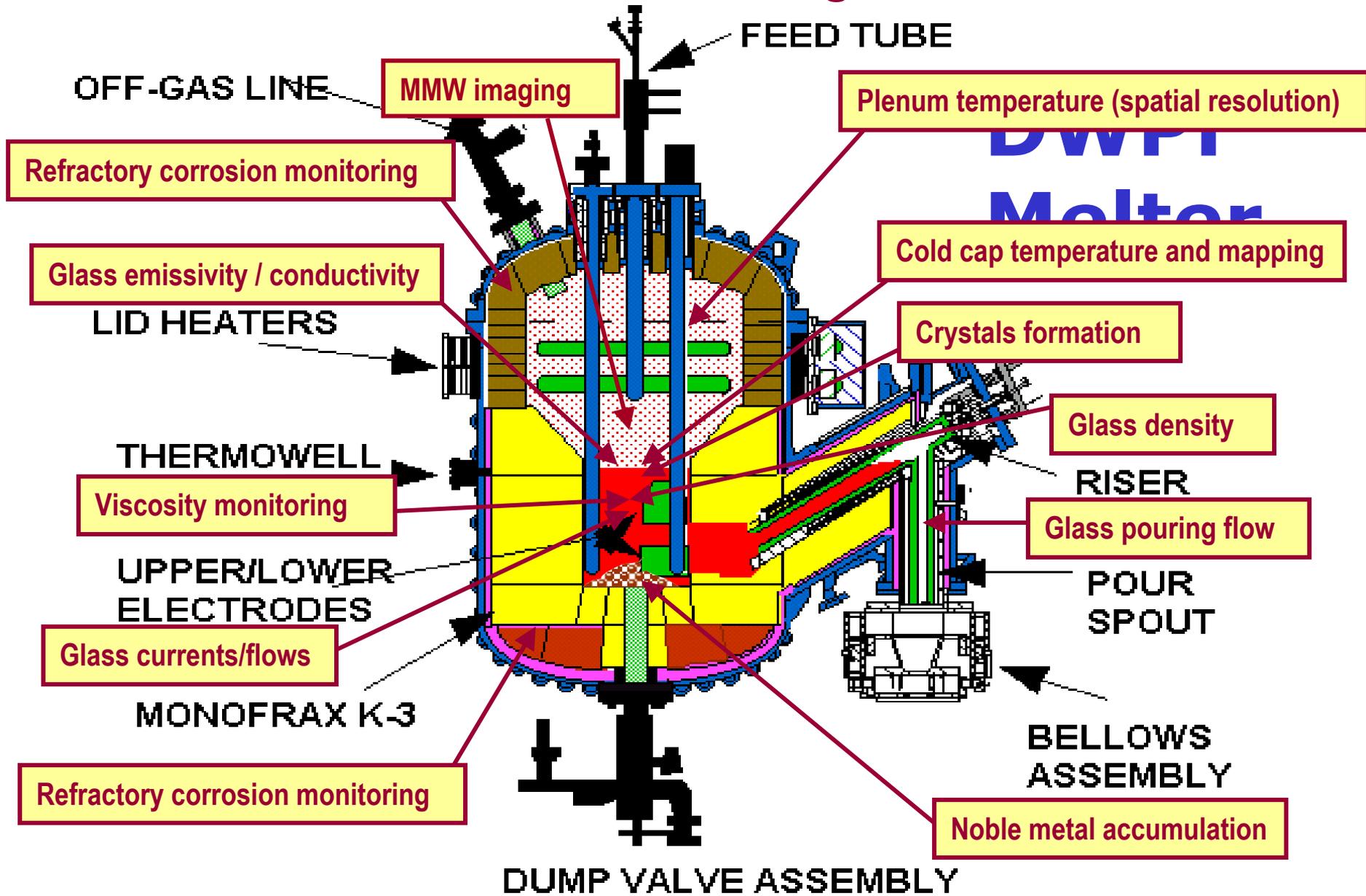
- **Operation Susceptible to Anomalies and Unknowns**

- ✓ Foaming
- ✓ Combustion gas build up
- ✓ Nobel metals accumulation
- ✓ Pour spout problems

- **With Advanced On-Line Monitoring**

- ✓ Reduce uncertainties
- ✓ Improve processing efficiencies (faster processing and smaller waste volumes)
- ✓ Reduce risks

# A Vision of Millimeter Wave Diagnostics for DWPF

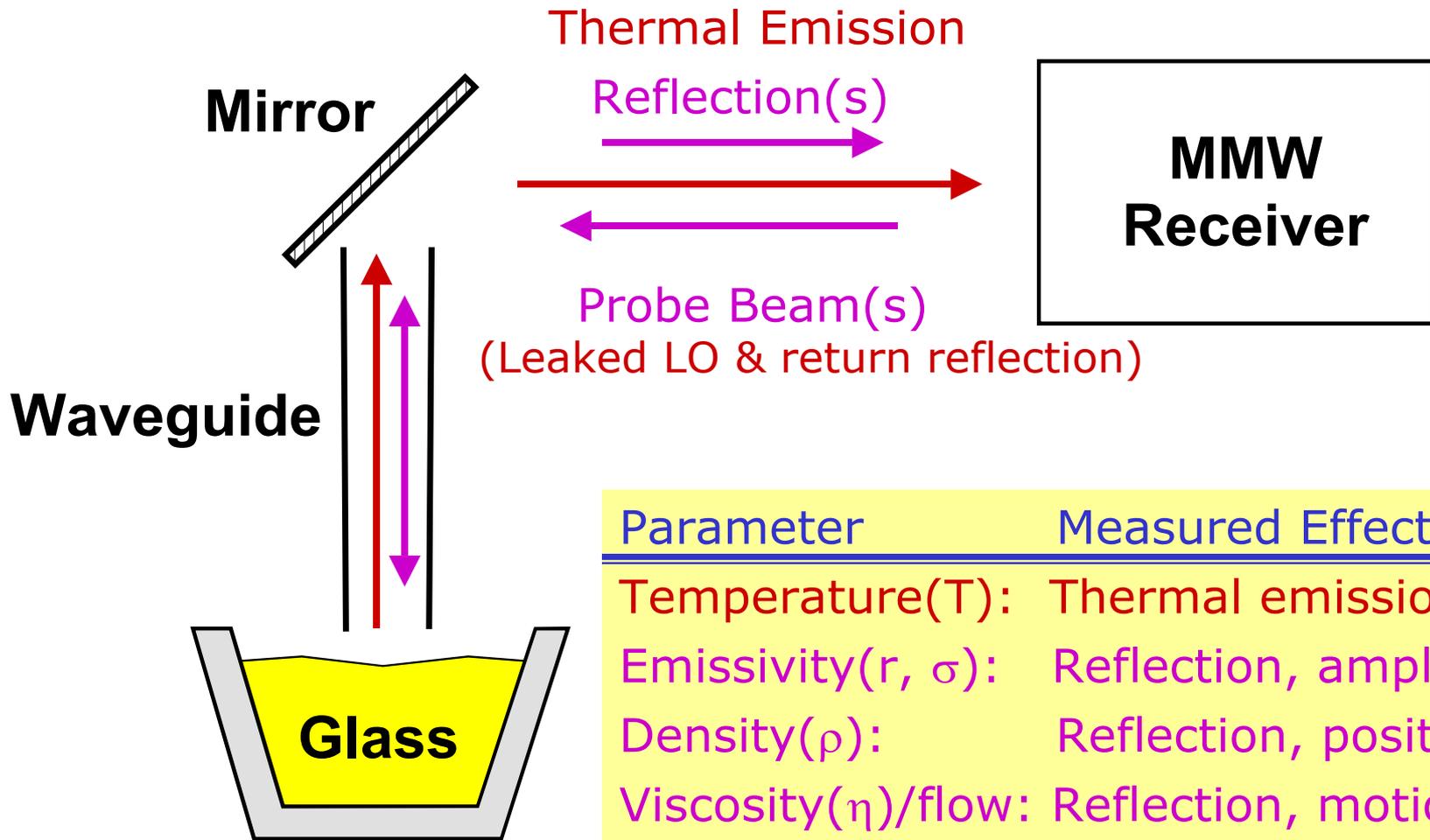


# Millimeter-Wave Advantages

10-0.3 mm (30-1000 GHz)

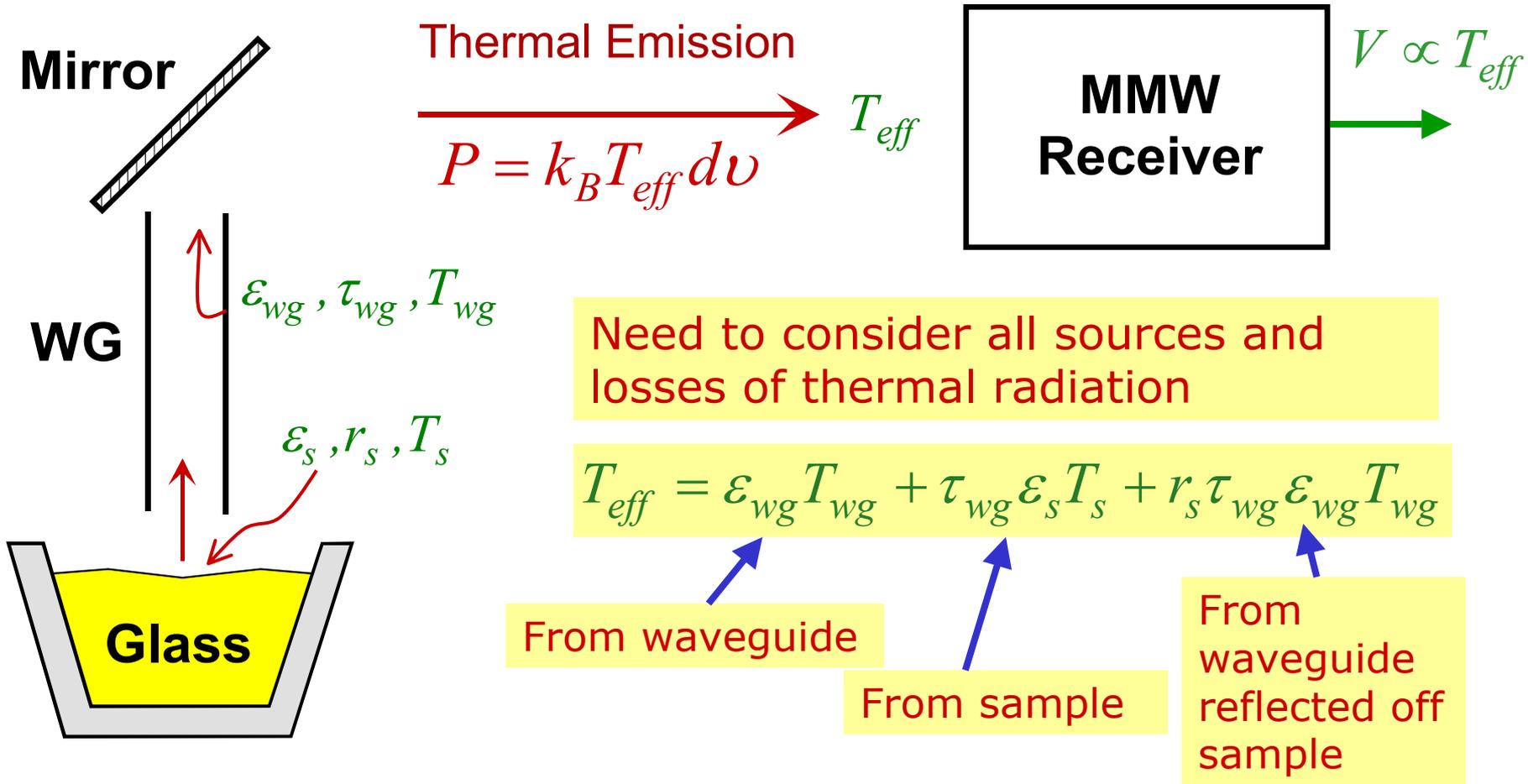
- Wavelengths are **long enough** to penetrate optical/infrared obscure viewing paths through dust, smoke, and debris
- Wavelengths are **short enough** for spatially resolved point measurements and profiles
- Robust **refractory material** melter interface and remote electronics

# MMW Sensor Approach



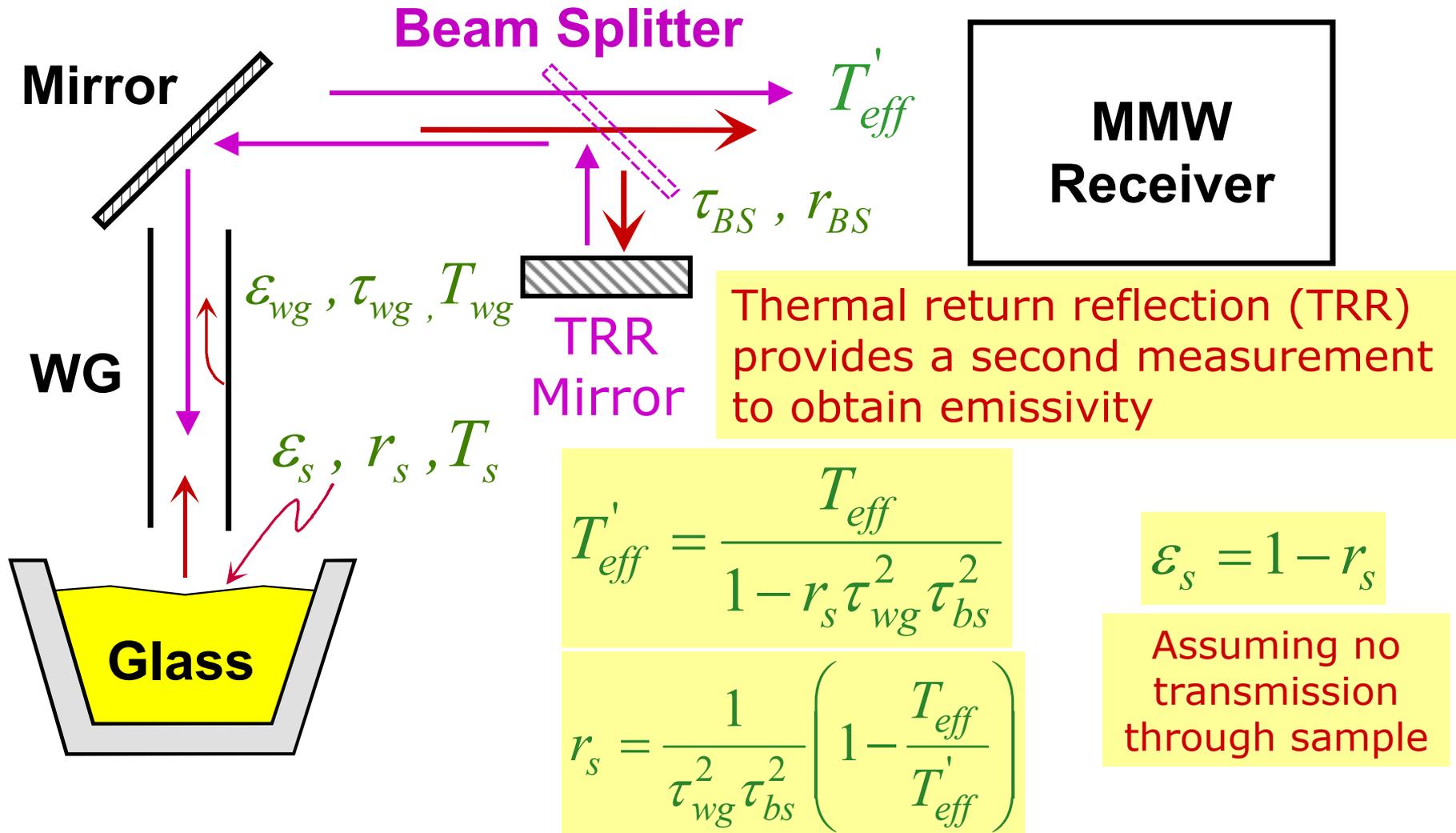
Parameter	Measured Effect
Temperature( $T$ ):	Thermal emission
Emissivity( $r, \sigma$ ):	Reflection, amplitude
Density( $\rho$ ):	Reflection, position
Viscosity( $\eta$ )/flow:	Reflection, motion
Fluctuations:	Reflection, fluctuations

# Analytic Basis for Temperature Measurement

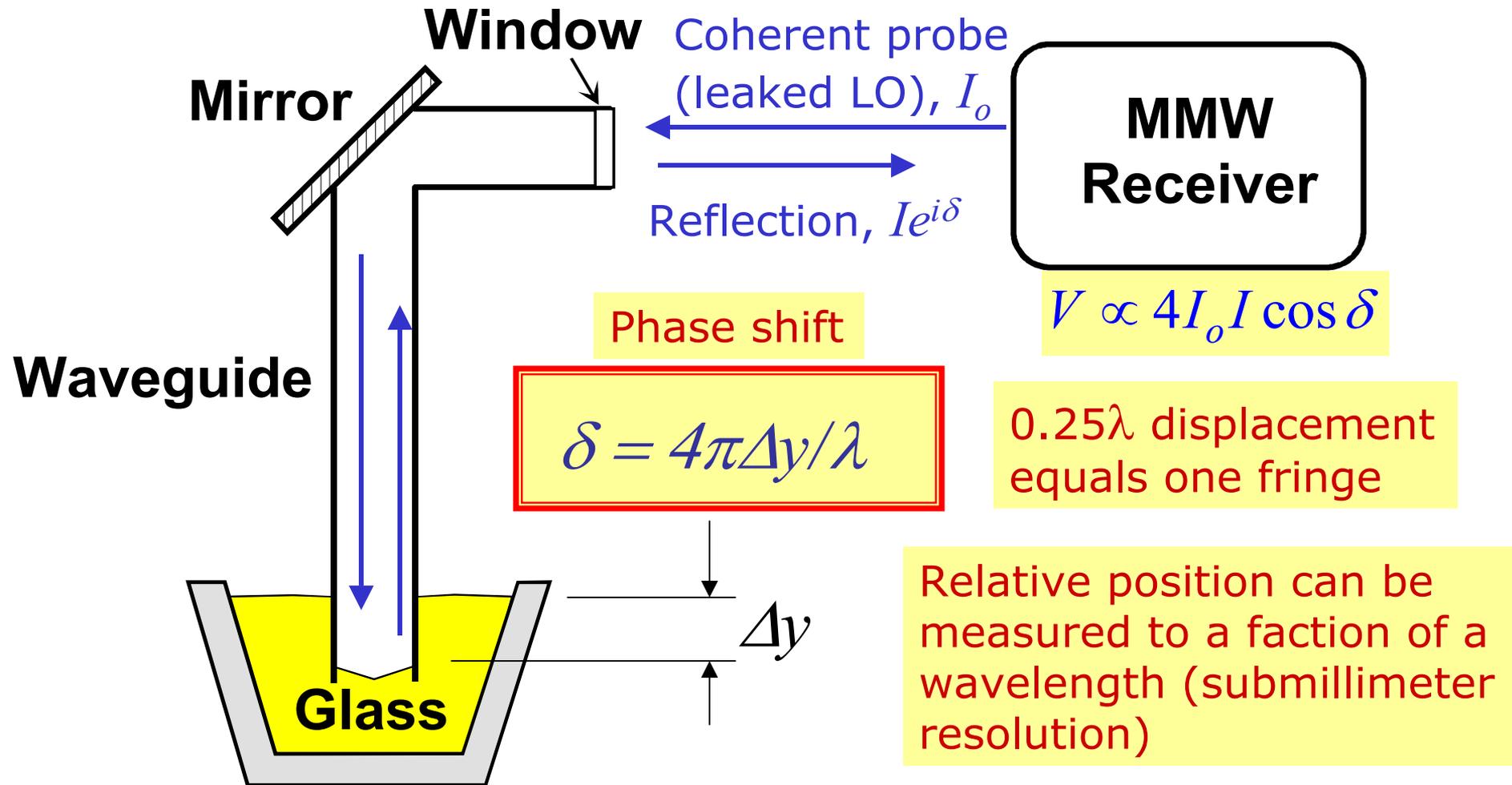


$T_{eff} = T_s ; \text{ when } \epsilon_s = \tau_{wg} = 1 (\epsilon_{wg} = 0)$

# Analytic Basis for Emissivity Measurement

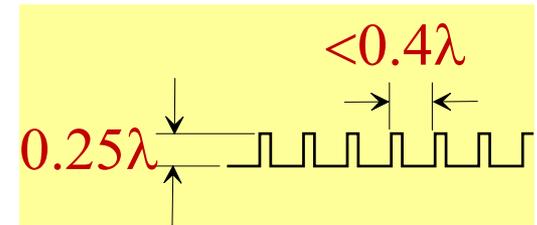


# Analytic Basis for Position and Flow Measurements



# High-Temperature MMW Process Interface

- Refractory materials must be used for MMW interfacing components (*waveguides, mirrors*)
- Efficient waveguides can be fabricated from large diameter pipes (*propagating the  $HE_{11}$  mode*)
- Conducting materials (*Inconel, Graphite*) require corrugated walls



$$\alpha = 0.00767 \frac{R_s}{k^2 a^3}$$

0.026% loss/meter  
Inconel at 140 GHz, 28 mm dia.

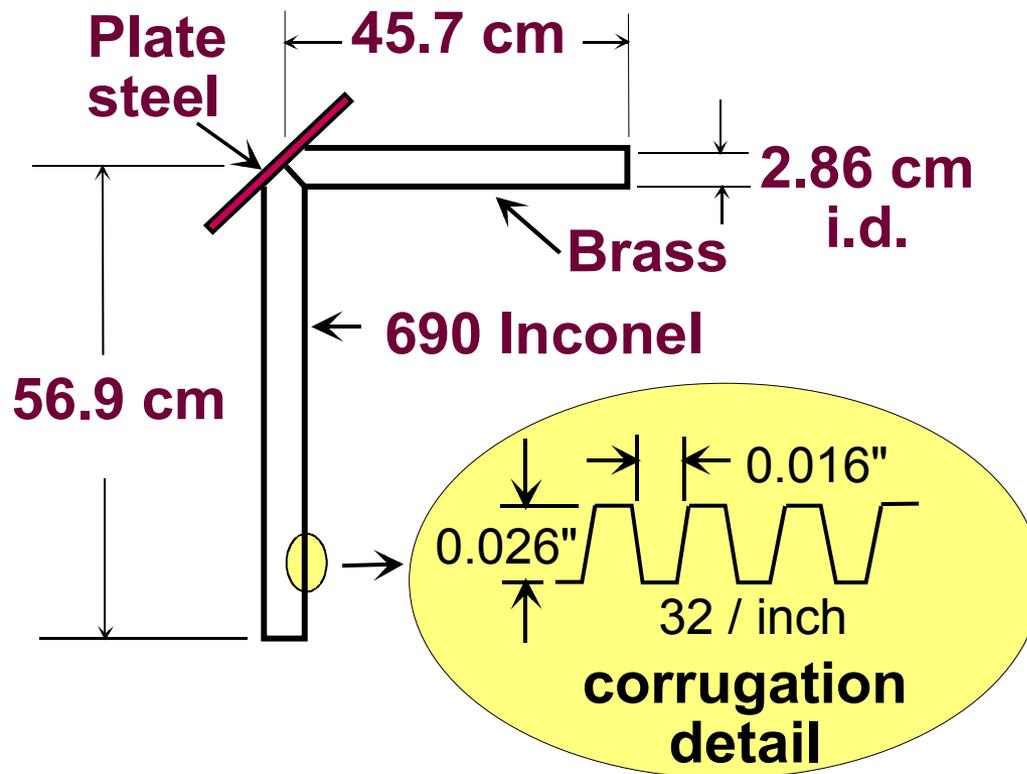
- Dielectric materials (*i.e. ceramics*) require smooth inner wall, dielectrics

$$\alpha = \frac{2.892 (n^2 + 1)}{k^2 a^3 \sqrt{n^2 - 1}}$$

32% loss/meter  
( $n=2.55$ ) 140 GHz, 28 mm dia.  
12% loss/m at 41 mm dia.

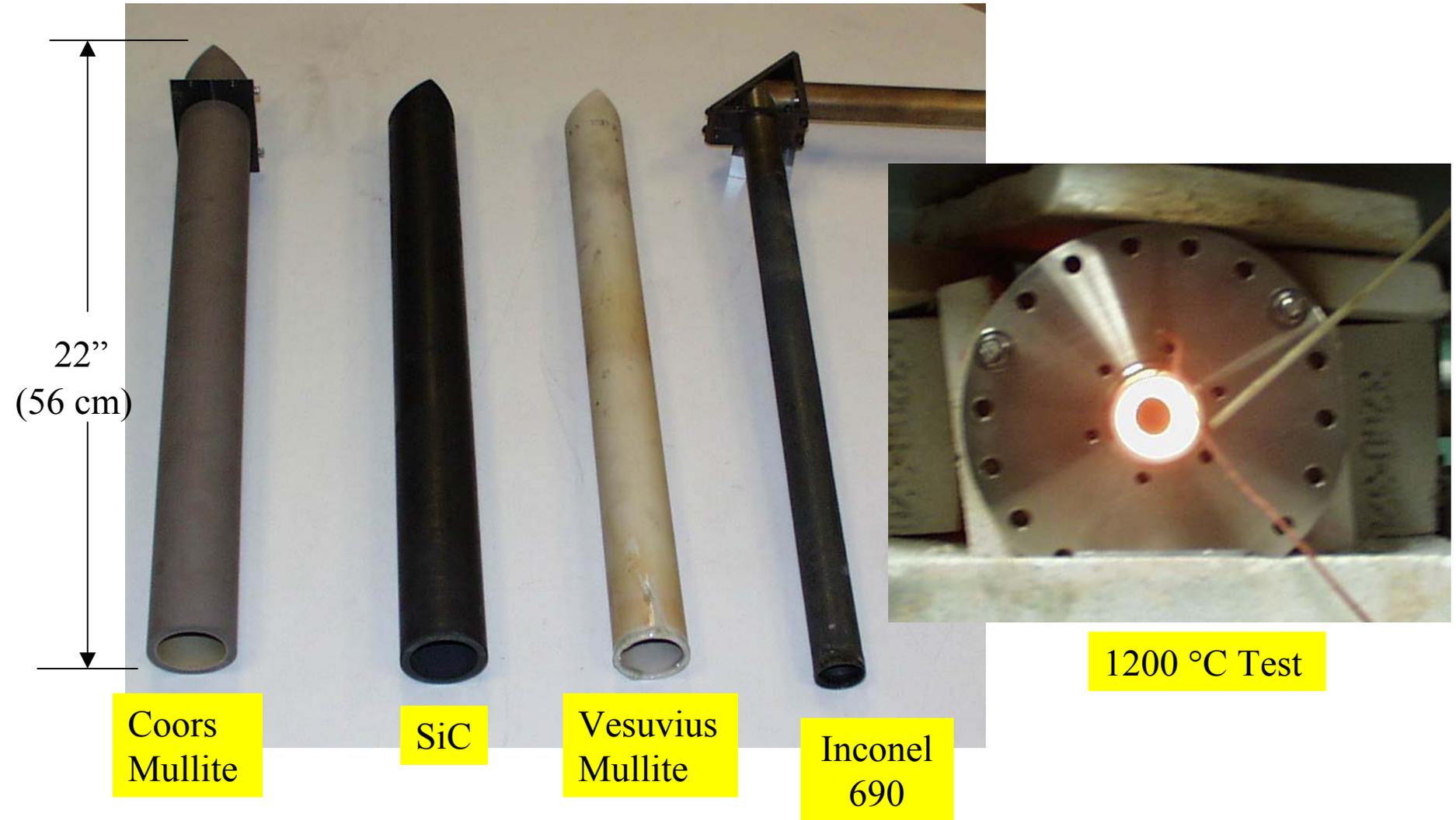
# Composite Waveguides

- Transmission efficiency maximized by using refractory guide only in hot region and mating to conventional guide or optics



- For large diameter
  - ✓ propagation constants approach free space value
  - ✓ little mismatch between different waveguide types including ceramics and metals

# Refractory Waveguides



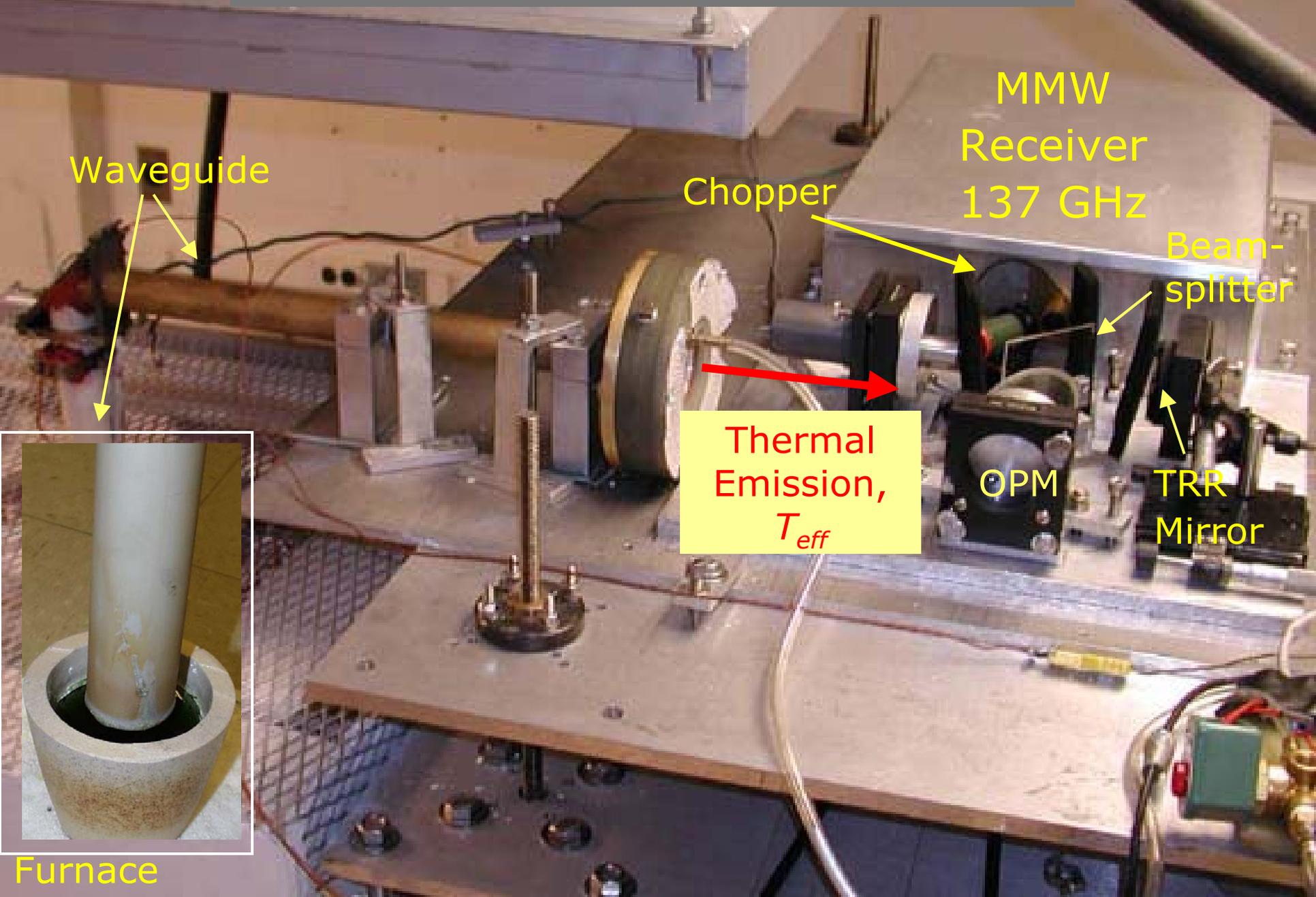
# Room Temperature Performance at 137 GHz

<b>Guide Material</b>	<b>Inside Surface</b>	<b>Inside Diameter</b>	<b>Wall Thickness</b>	<b>Measured Transmission</b>
690 Inconel	Corrugated	28.6 mm	N/A	94.6%
690 Inconel <i>(after use to 1180 °C in Air)</i>	“	“	“	83.0%
Vesuvius Mullite	Smooth	41.3 mm	3.2 mm	97.6%
Coors Mullite	Smooth	41.3 mm	6.4 mm	87.5%
Silicon Carbide	Smooth	41.3 mm	12.7 mm	79.5%

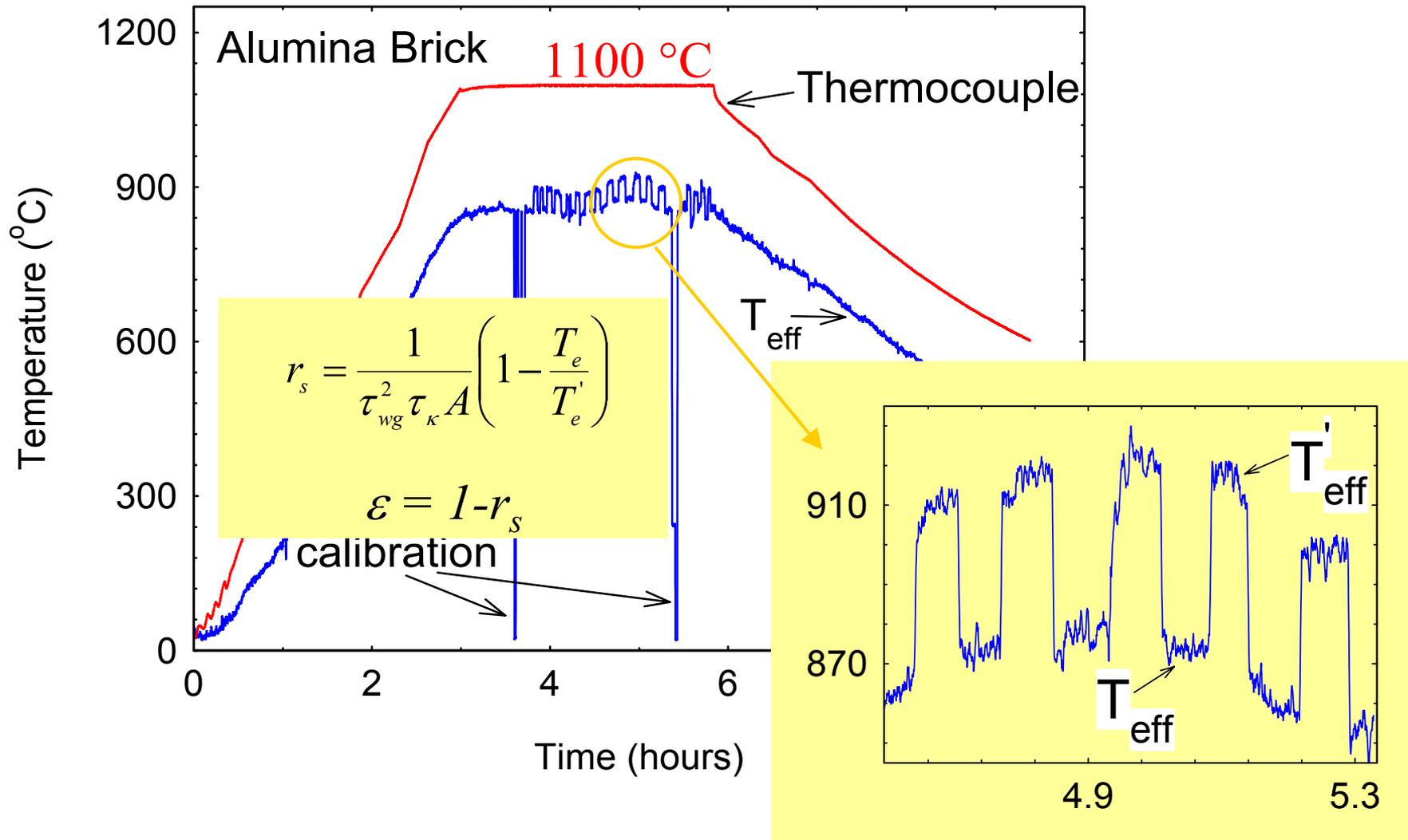
Transmission efficiency scales as  $1/(\text{dia.})^3$  for a given material

- Refractory waveguides could be made large enough to transmit power into a melter for profile control

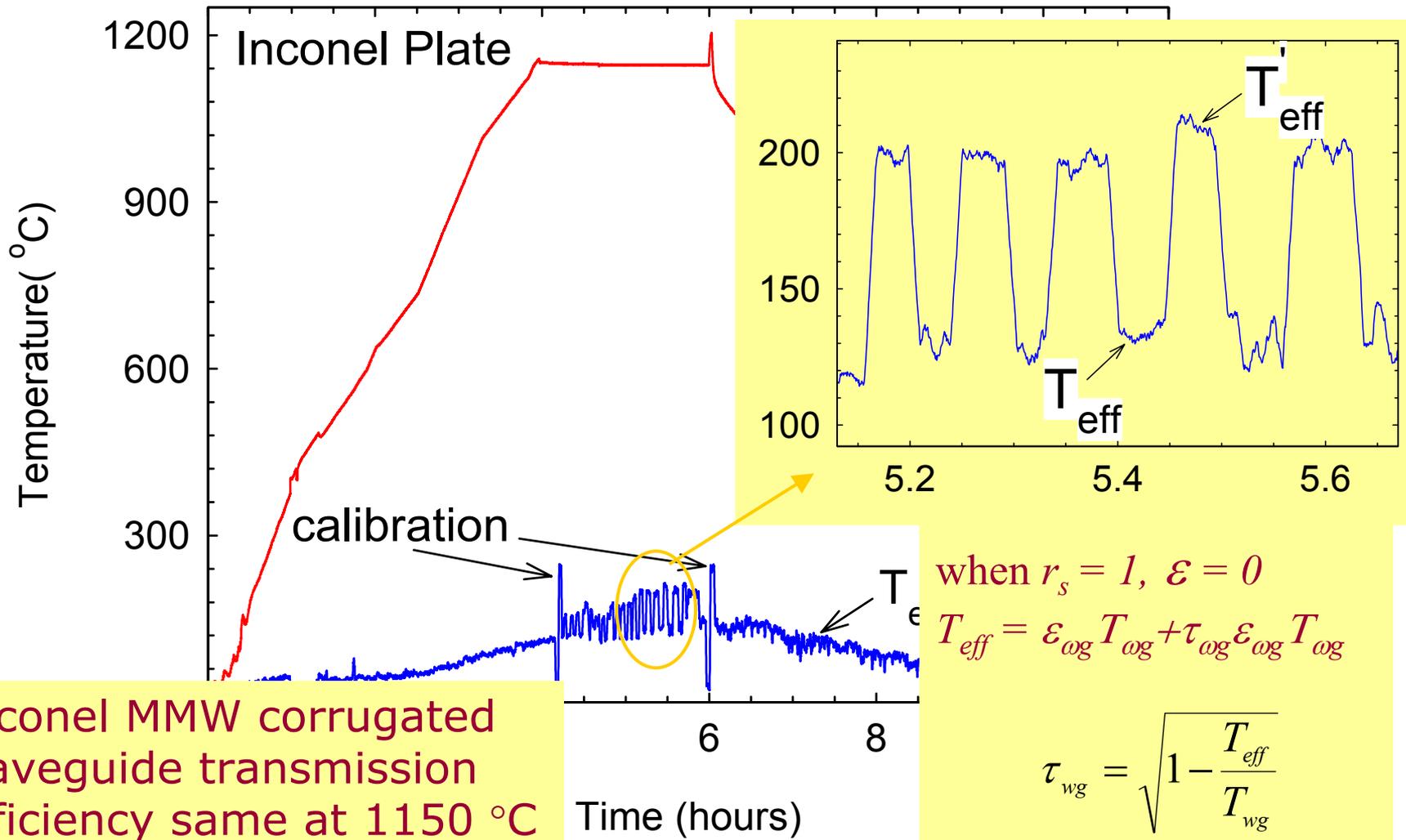
# Laboratory Research Setup



# Measurements with Inconel Waveguide of Alumina Brick

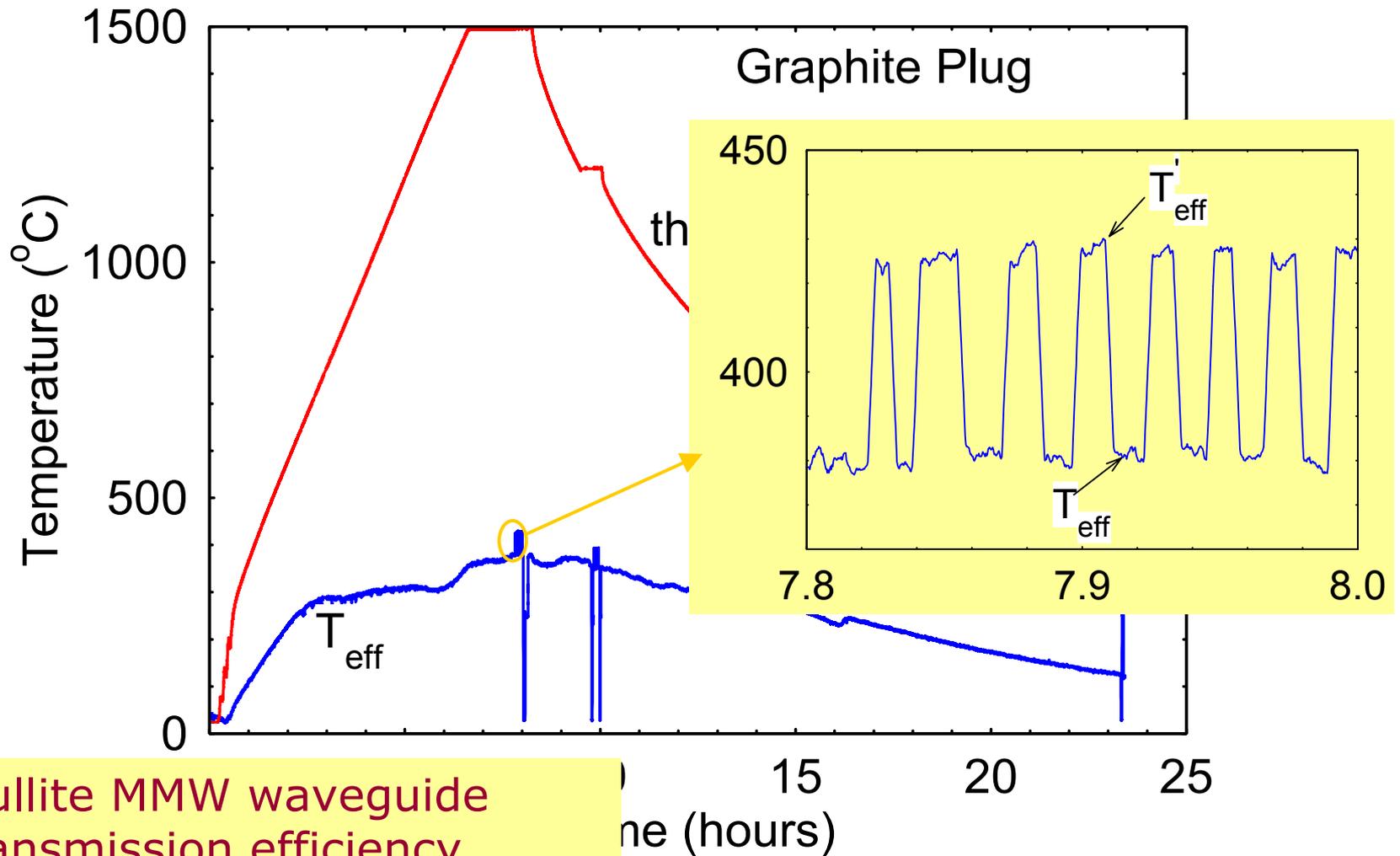


# Inconel Waveguide Measurements at 1150 °C



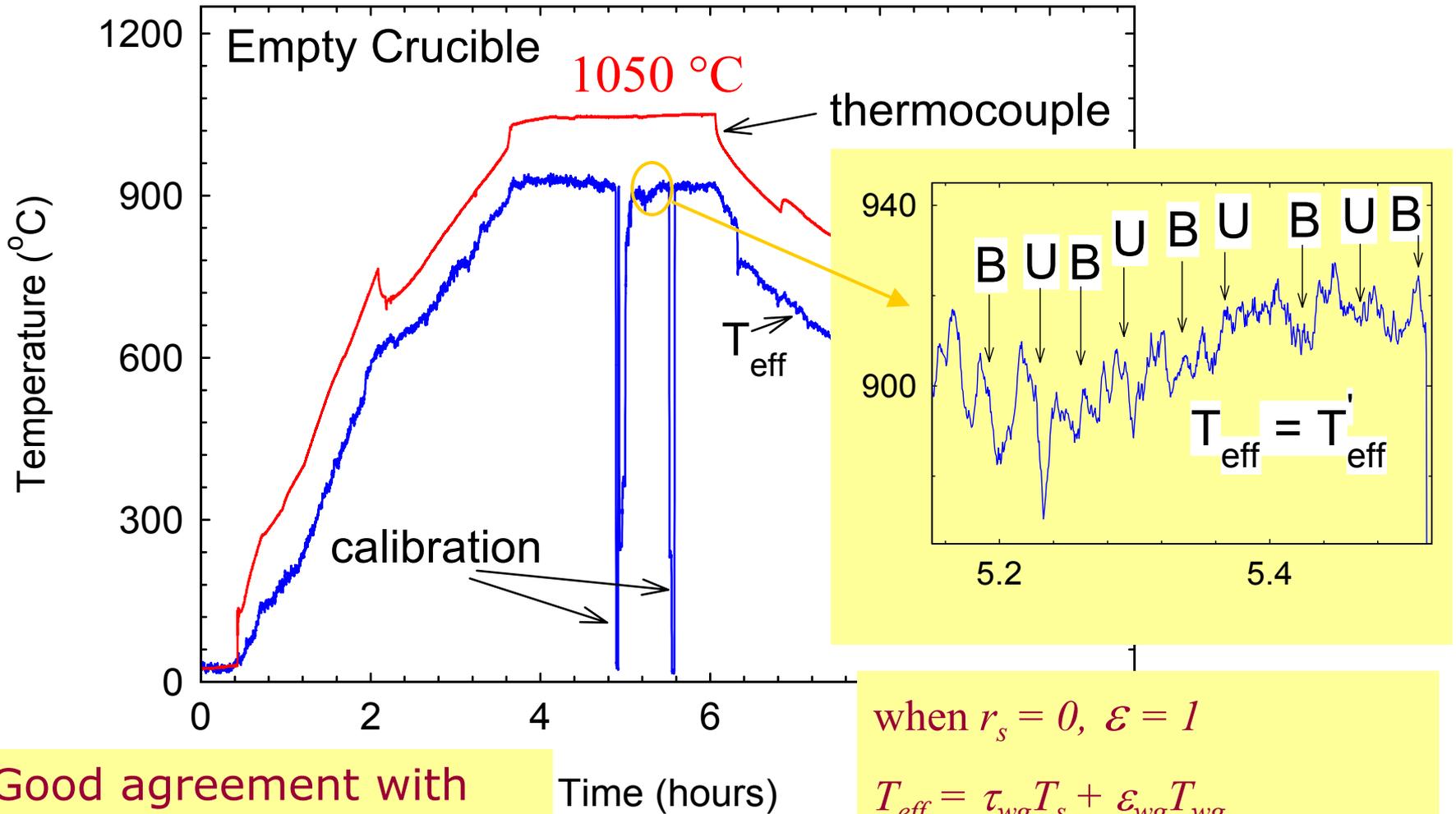
Inconel MMW corrugated waveguide transmission efficiency same at 1150 °C and room temperature ~95%

# Mullite Waveguide Measurements to 1500 °C



Mullite MMW waveguide transmission efficiency appears constant to 1500 °C ~90% for 1 5/8" diameter

# Measurements of an Ideal Blackbody



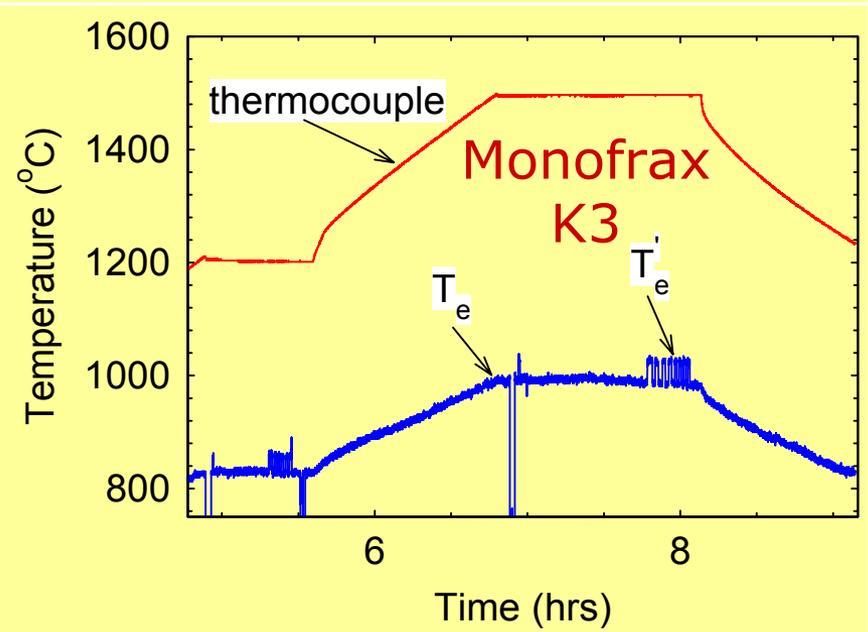
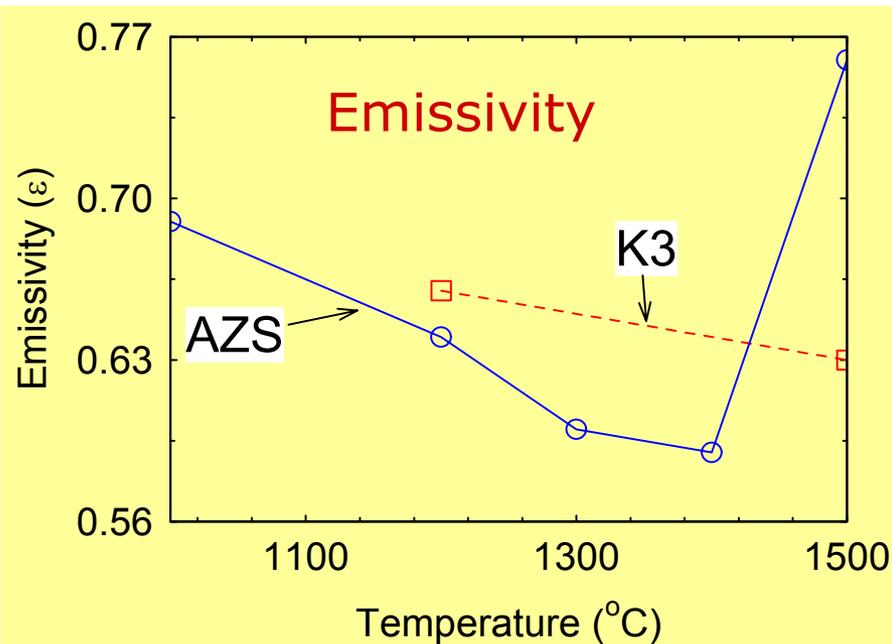
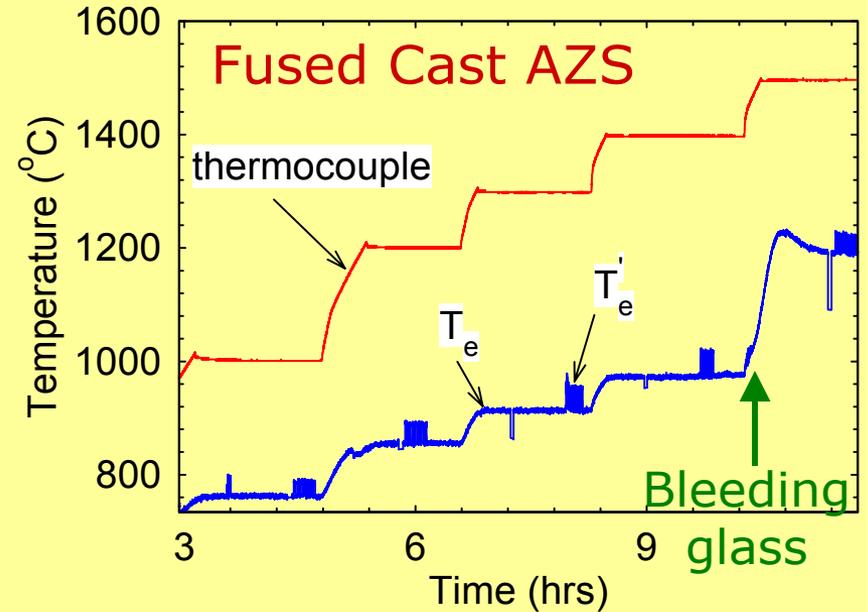
- Good agreement with thermocouple
- Typical case for cold cap melter measurements

when  $r_s = 0$ ,  $\epsilon = 1$

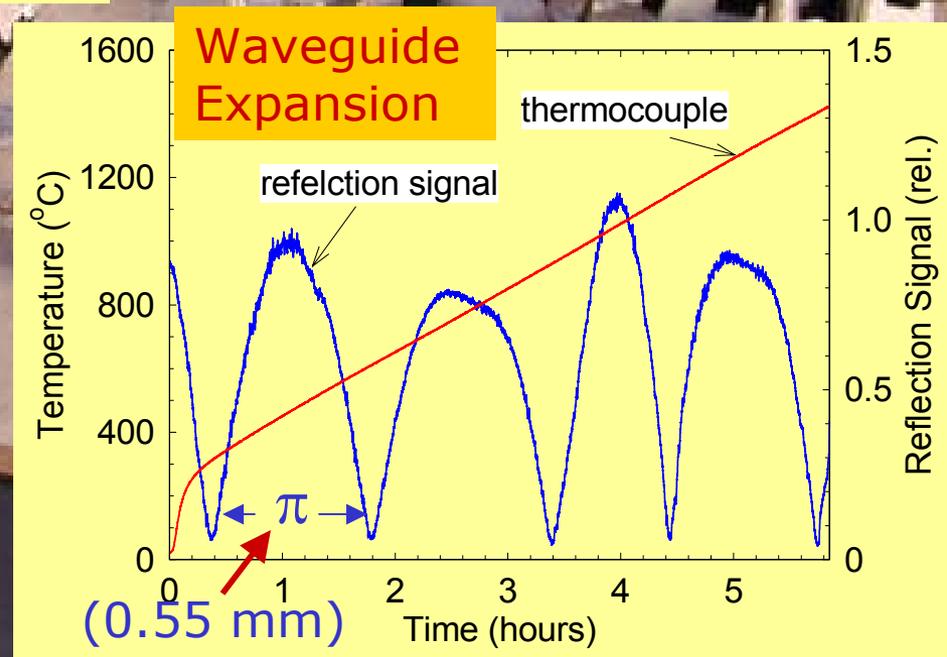
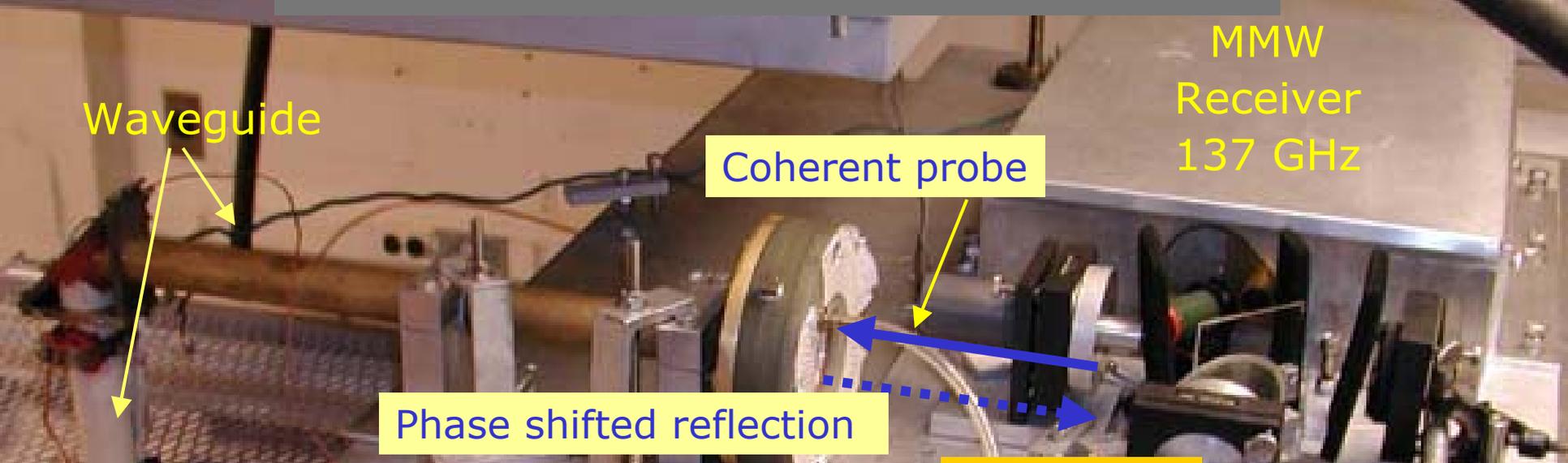
$$T_{eff} = \tau_{wg} T_s + \epsilon_{wg} T_{wg}$$

# Thermal Analysis of Materials

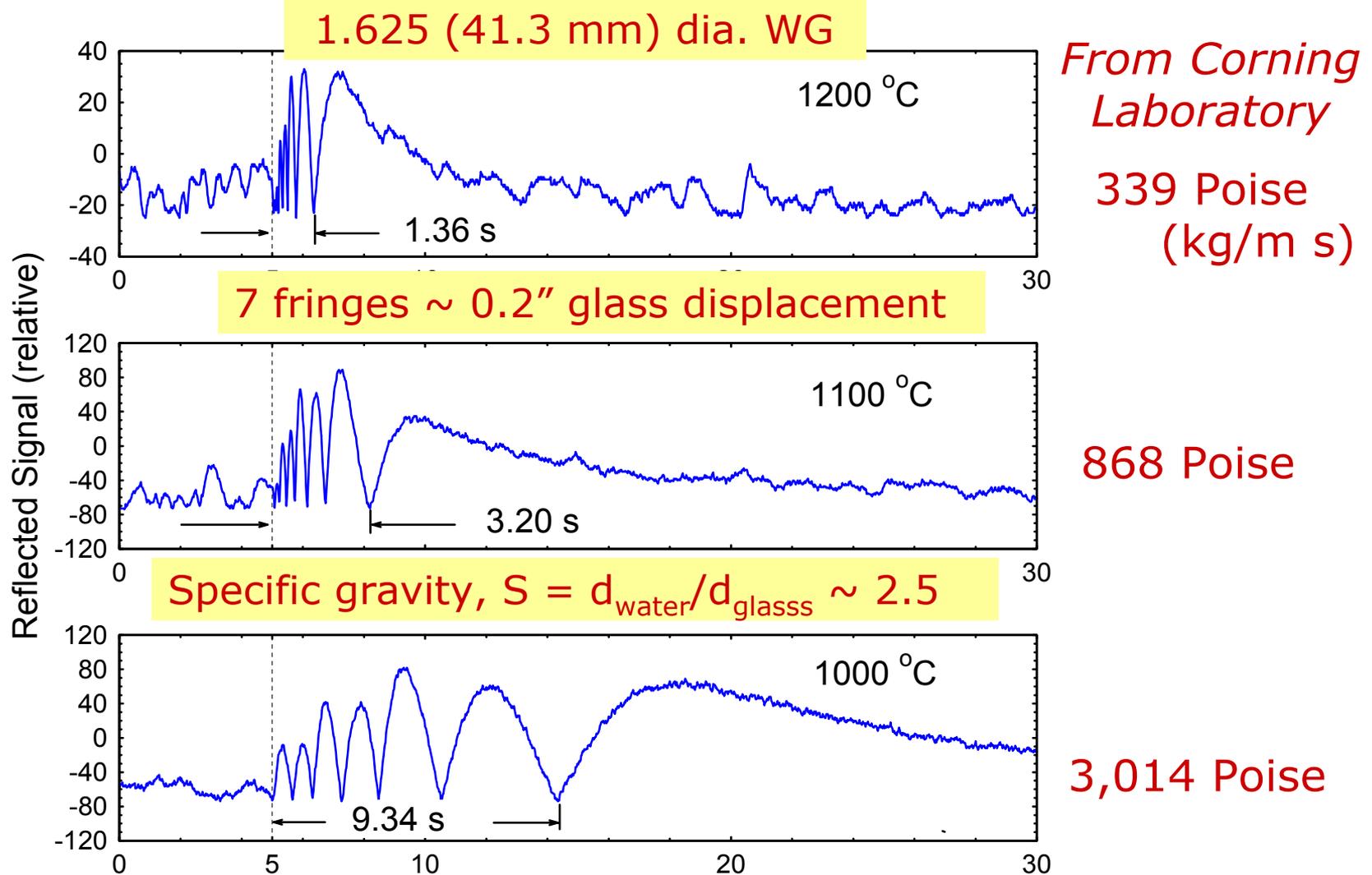
- Molten glass corrosion resistant materials studied
- Alumina-Zirconia-Silica (AZS) has unstable MMW properties
- Monofrax K3 more stable at MMW wavelengths



# Laboratory Research Setup Flow Measurements



# Hanford #7 Glass Flow in Waveguide for ~ 0.5" Water Pressure Displacement

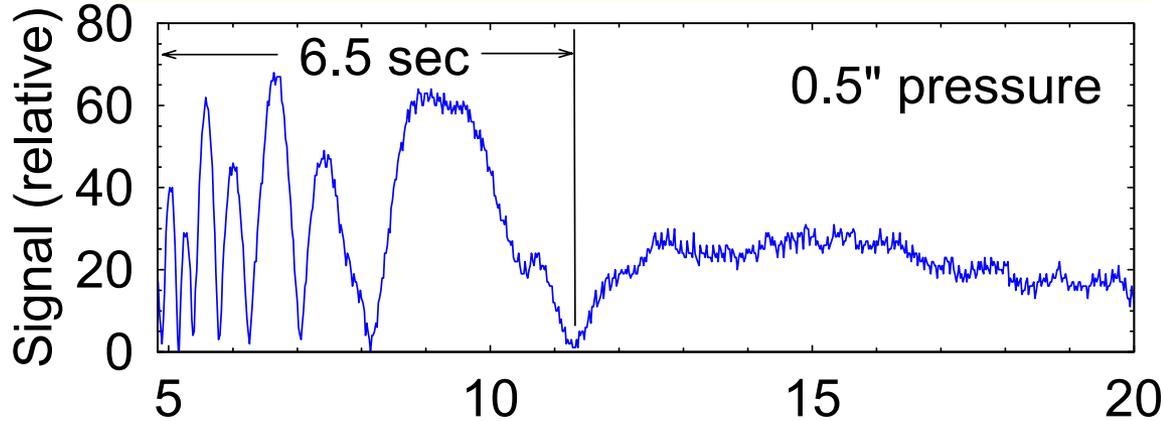


Glass density and flow velocity both determined simultaneously

100 Poise goal for pouring

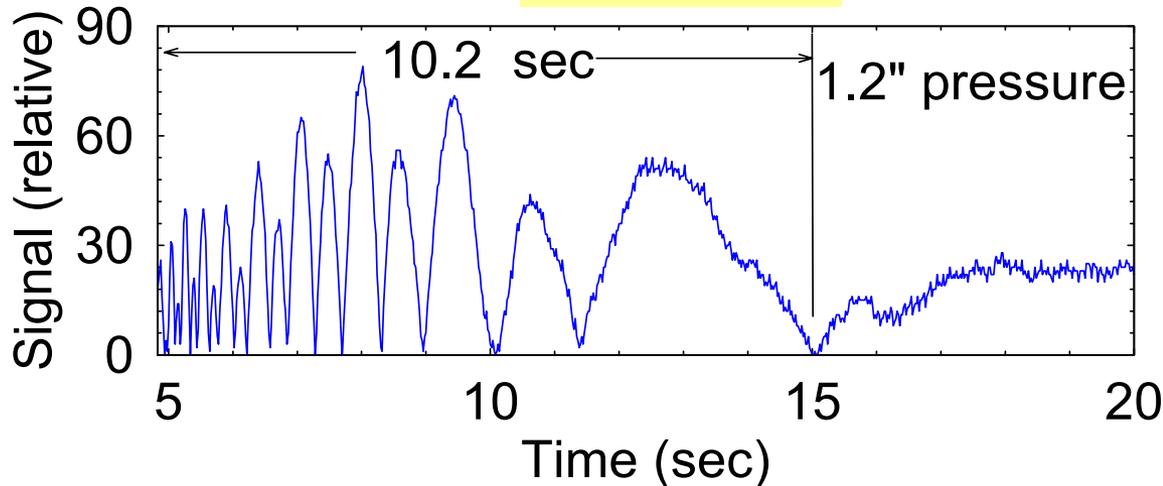
# Hanford #8 Glass at 1000 °C and Two Pressures

Waveguide i.d. = 1.125" (28.6 mm)



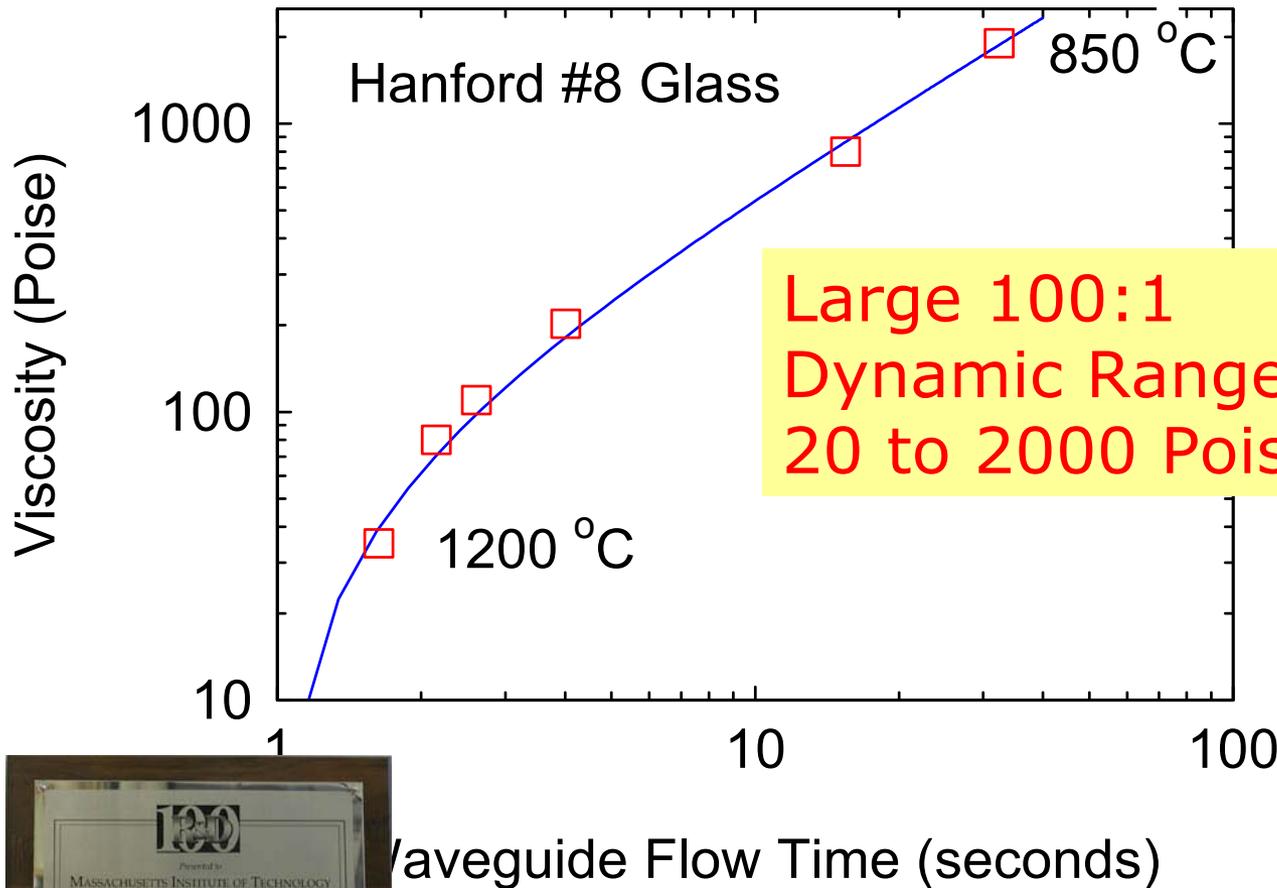
- smaller diameter waveguide reduces flow velocity as  $1/a^2$

210 Poise



- Difference of two pressure displacements taken to eliminate surface tension effects

# Good Correlation Between Viscosity and MMW Waveguide Flow Time Delay



For 0.7" (17.8 mm) flow at 1 atmosphere

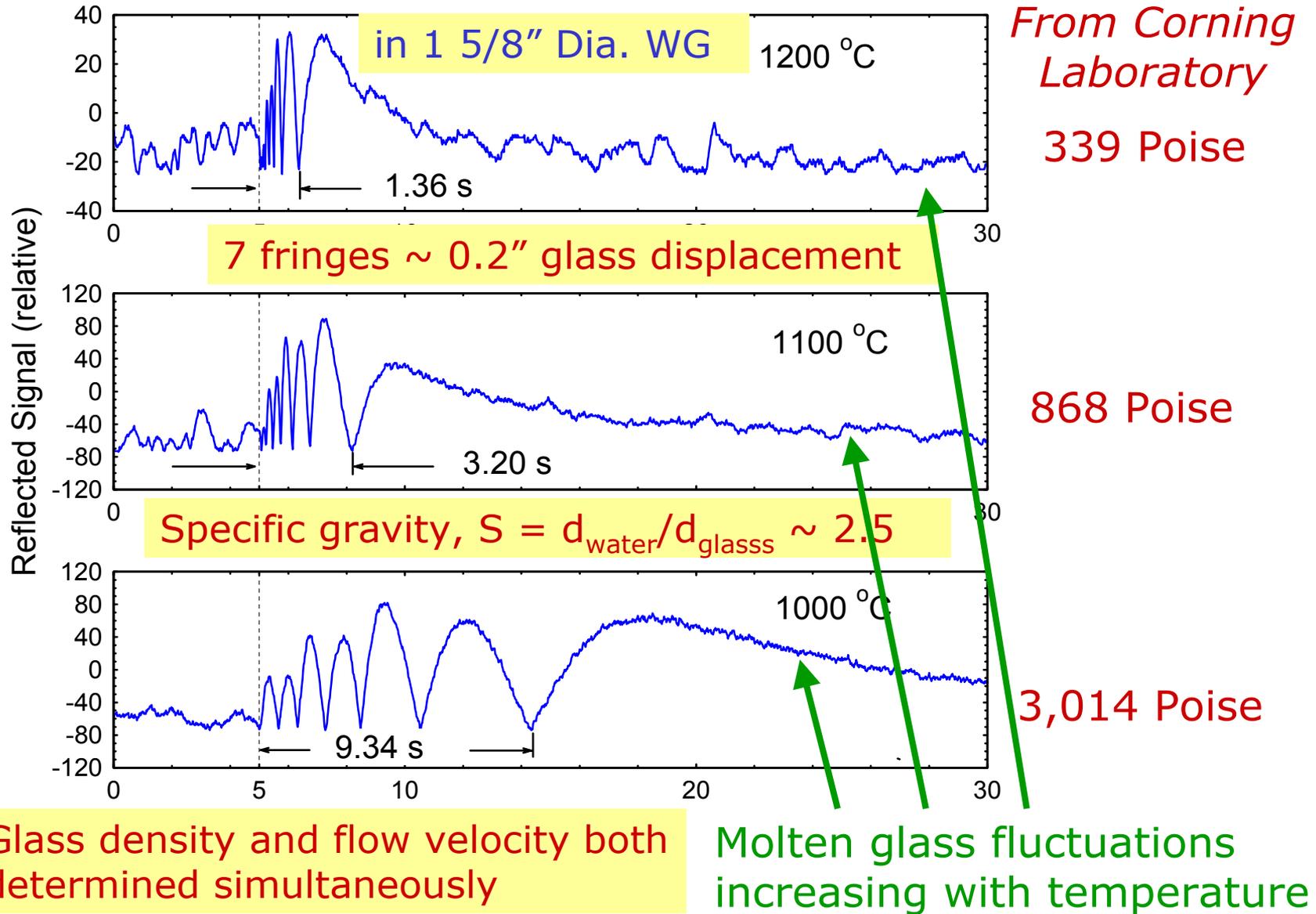
Large 100:1 Dynamic Range  
20 to 2000 Poise

Waveguide i.d. = 1.125" (28.6 mm)

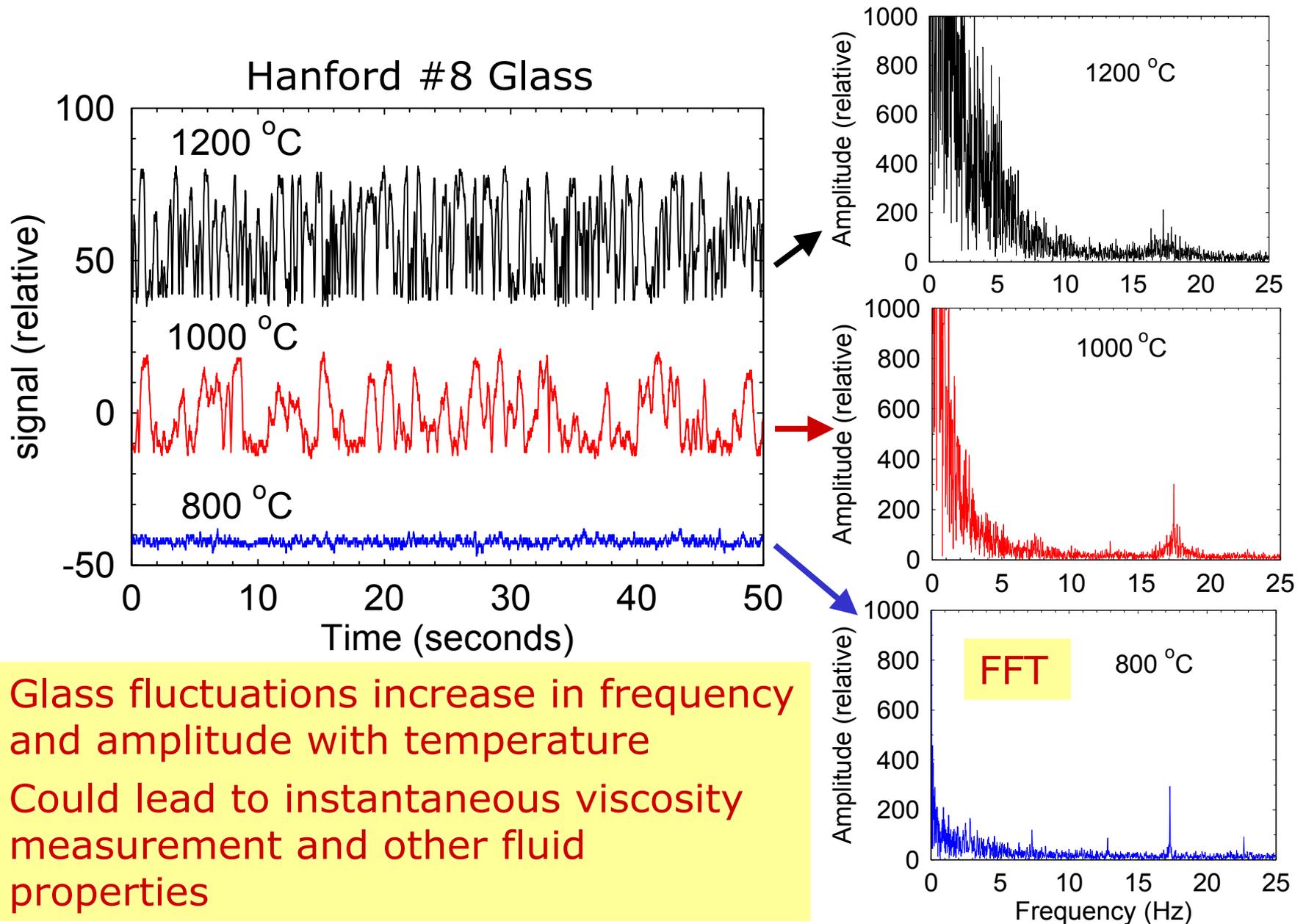


Waveguide Flow Time (seconds)

# Hanford #7 Glass Flow in Waveguide for ~ 0.5" Water Pressure Displacement



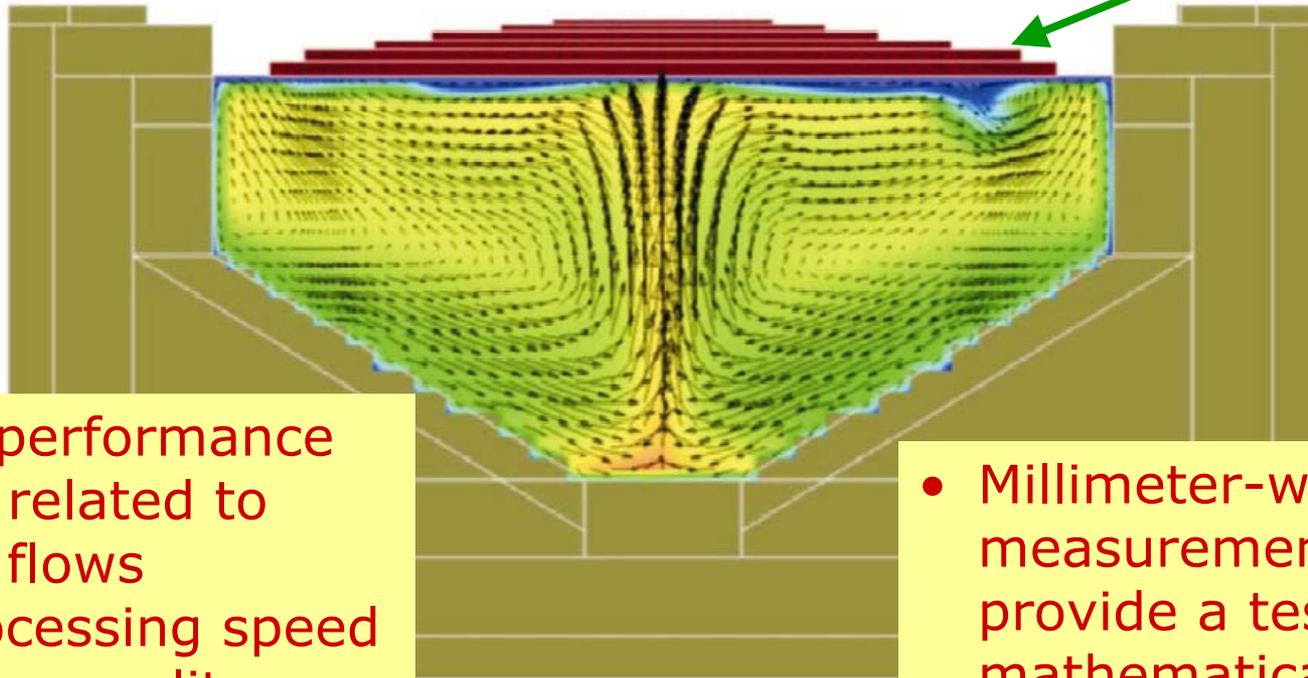
# Molten Glass Turbulence



# Glass Flow Modeling

Temperature and velocity fields in a high level waste melter cross-section

Cold cap

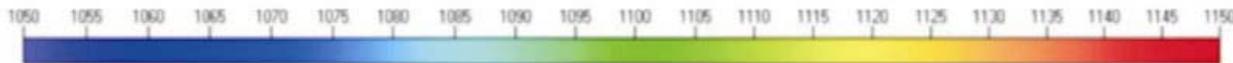


- Melter performance closely related to mixing flows
  - ✓ processing speed
  - ✓ glass quality

- Millimeter-wave measurements could provide a test of mathematical models



temperature [°C]



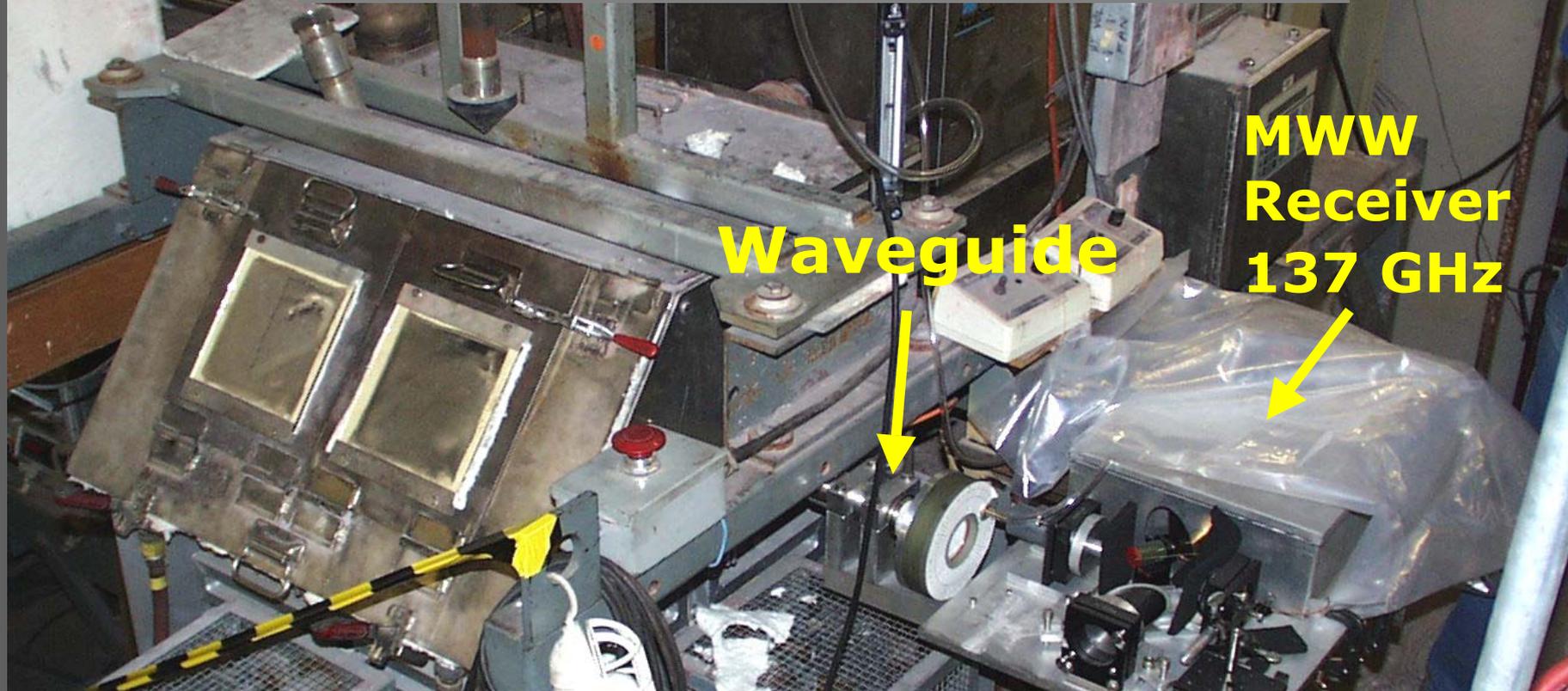
# Cold-Cap Monitoring

- Currently there is no proven technology to measure cold-cap temperature and profile it directly in a melter. Often plenum temperature is a good indicator.
- Cold-cap temperature and temperature distribution determine the cold-cap movement and dynamics in a melter, which in turn determine the productivity.
- A reliable on-line measuring and monitoring technology will help improve processability. Optical techniques do not work well (gases, steam, dust, particulates). Millimeter waves can penetrate smoke and dust.

# MMW Technology Field Tested Cold Cap Profile Monitoring

- Engineering scale EV-16 Melter at Clemson Environmental Technologies Laboratory (CETL)
- Millimeter-wave temperature surface **profile** measurement capability implemented
- Millimeter-Wave monitoring technology operated reliably
  - 24 hours a day over two week period

# EV-16 Melter at CETL



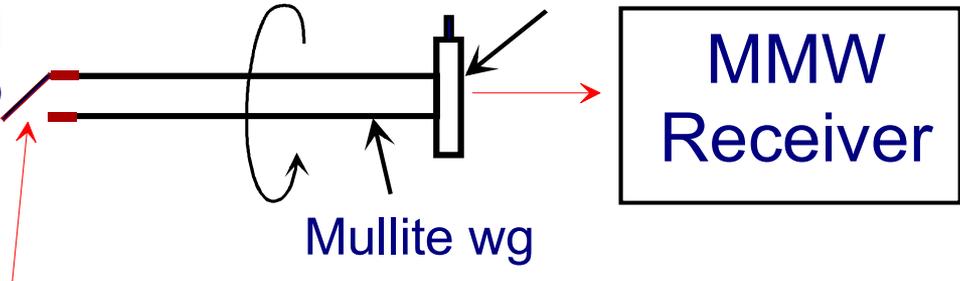
## Rotating Waveguide

Inconel  
Mirror cap

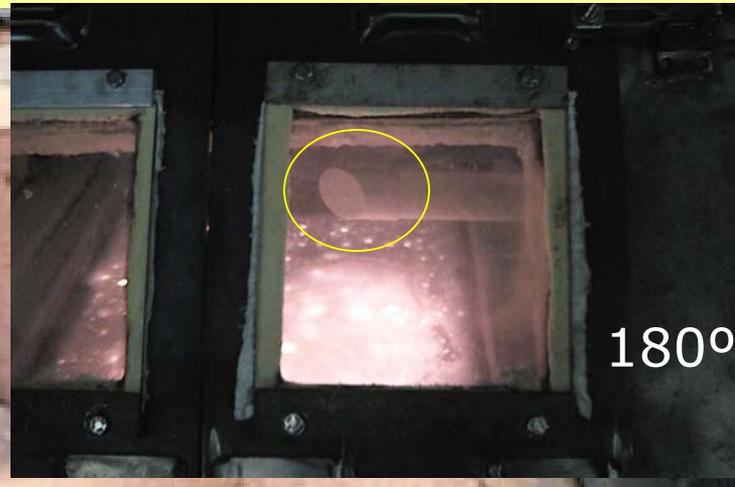
Window

Mullite wg

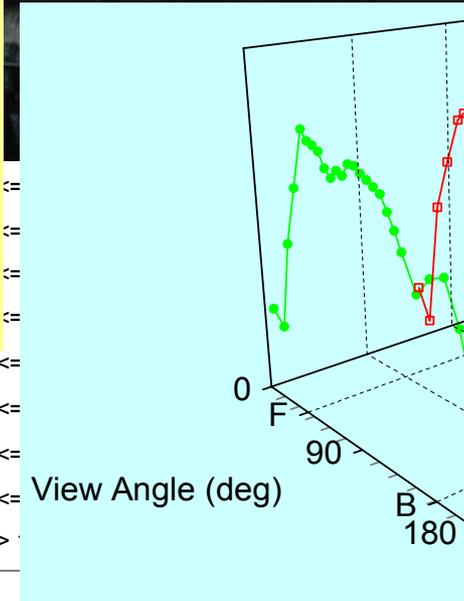
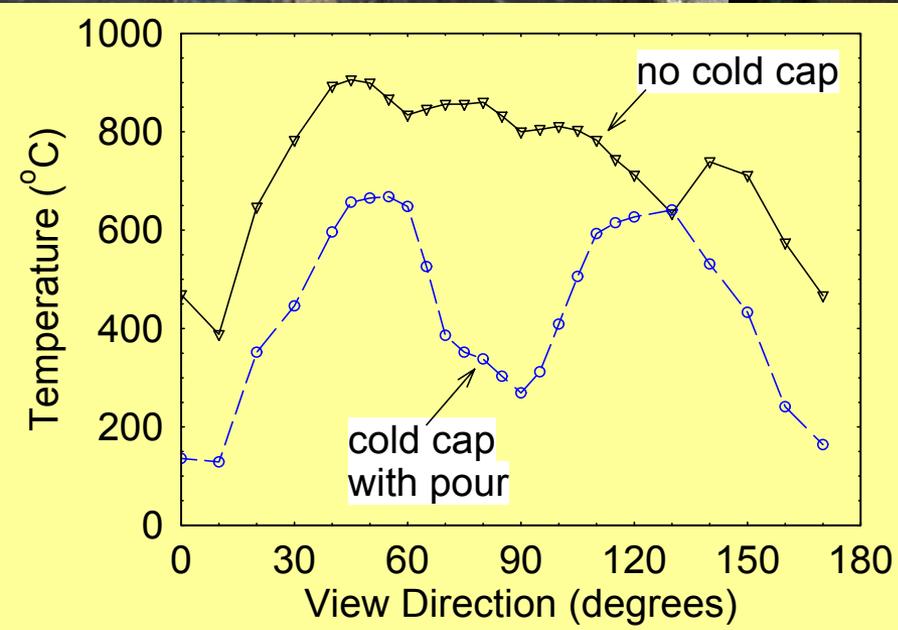
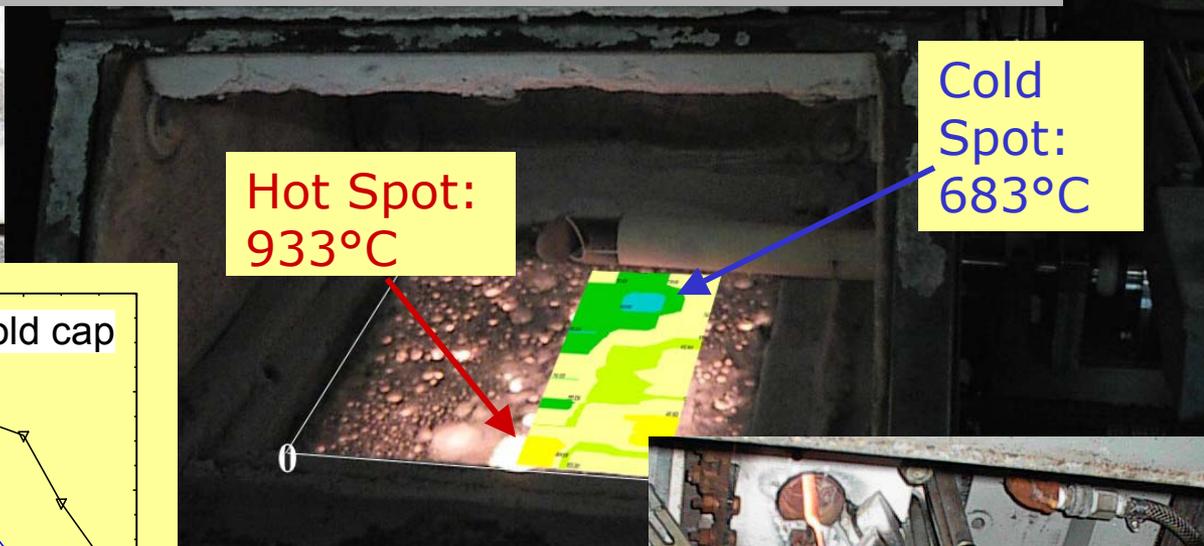
MMW  
Receiver



# Inside Melter

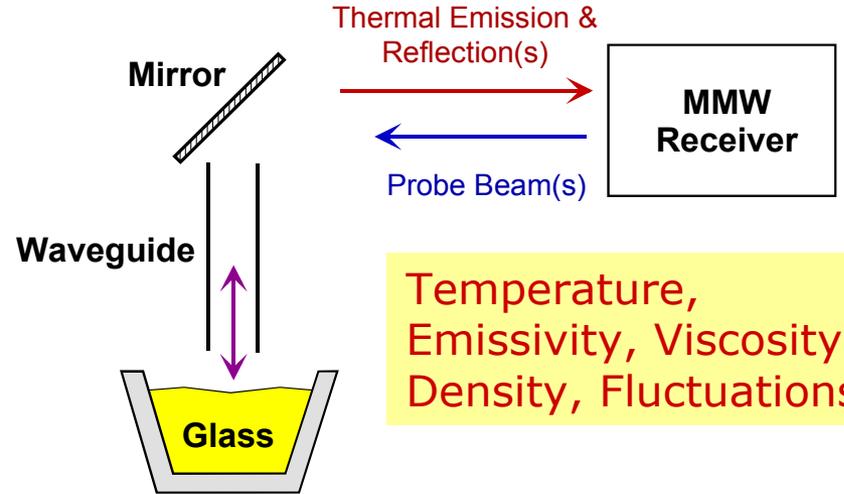


# Surface Temperature Profiles/Contours



- Cold-cap temperature profiles indicative of melter process conditions of value to process control
- Potential to control plenum off gasses

# Summary

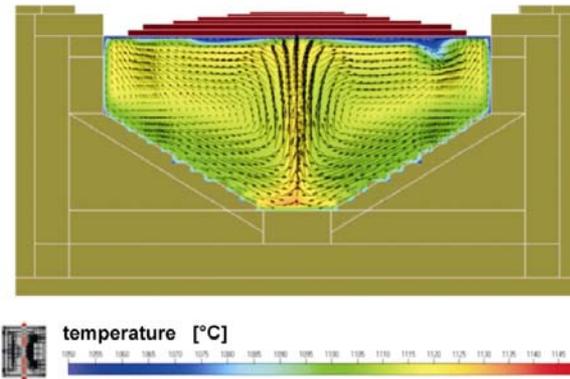


## • New High Temperature MMW Monitoring Capability Demonstrated

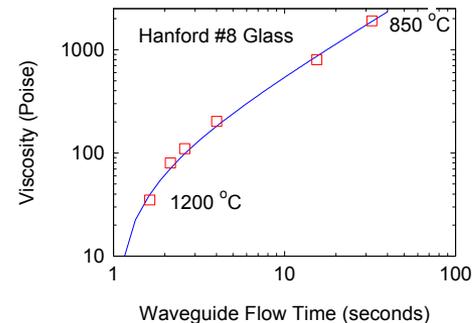
- ✓ Improve process efficiencies
- ✓ Improve product quality
- ✓ Reduce environmental impact



Efficient waveguides future potential for heating



Potential to test melter models



# Further Reading

“Millimeter-Wave Monitoring of Nuclear Waste Glass Melts – An Overview”,  
*P. P. Woskov, J. S. Machuzak, P. Thomas, S. K. Sundaram, and W. E. Daniels, Jr.*, in Environmental Issues and Waste Management Technologies VII (*Ceramic Transactions, Volume 132*) pp. 189-201.

“Thermal return reflection method for resolving emissivity and temperature in radiometric measurements”, *P. P. Woskov and S. K. Sundaram*, J. Appl. Physics, (to be published December 1, 2002).