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HIGH-INTENSITY DRYING PROCESS - IMPULSE DRYING

PROGRESS REPORT ON FURNISH EVALUATIONS
FOR IMPULSE DRYING
COMMERCIALIZATION DEMONSTRATION

Topical Report

By
D. Orloff
P. Phelan
I. Rudman

February 1995

Work Performed Under Contract DE-FG02-85CE40738

For
U.S. Department of Energy
Office of Industrial Technologies
Washington, D.C.

By
The Institute of Paper Science and Technology
Atlanta, GA

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SUMMARY

Laboratory- and pilot-scale experiments were performed in cooperation with Beloit Corporation and Union Camp Corporation to identify potential furnishes and operating parameters for upcoming high-speed pilot-scale trials and commercial demonstration of impulse drying. These initial experiments focused on determining the relationship between water permeability, refining, and prepressing for specific pulps. Also, mill refined pulp and machine paper were compared to laboratory samples in regards to water permeability and impulse drying performance.

Results indicate that hydrodynamic specific surface is highly dependent on sheet formation and prehandling. Without extreme care in sheet preparation, the permeability test results are highly variable. However, the trends indicate that minimum refining and prepressing as much as possible are necessary to lower the specific surface to the range ($1-2 \text{ m}^2/\text{g}$) necessary for maximum impulse drying efficiency.

Mill refined pulp and machine paper were comparable to laboratory prepared samples in regards to permeability and impulse drying. Impulse drying results in an outgoing solids improvement of up to eight percentage points compared to double-felted pressing. STFI index values showed an increase of up to 3.5% over double-felted pressing. These results were achieved with ingoing solids of 40-42%. At ingoing solids of 35%, impulse drying showed less improvement compared to double-felted pressing, indicating that an impulse dryer should be in the third or fourth press position for maximum efficiency. Ring crush improved 15% over double-felted pressing for the more open furnish, but double-felted pressing produced higher ring crush results for the closed furnish. For all cases impulse drying significantly decreased (up to 56%) Bendtsen roughness compared to double-felted pressing. Comparisons between Beloit and IPST results indicate consistent trends with IPST results being the most conservative.

Other process variables such as platen surface coating, felt type, felt moisture, and presteaming temperature profiles were investigated. In the laboratory simulations, high felt moisture (>32%) with the R felt resulted in excessive rewet and significant reduction in water removal. The laboratory equipment was not able to obtain presteaming temperature profiles comparable to machine conditions. Observations indicate that platen surface and felt type have an effect on water removal, sheet physical properties, rewet, and sheet sticking. Because of tradeoffs between these properties and others, the data obtained in these experiments were not sufficient to specify optimum process parameters.

These experiments used furnishes that simulated present commercial furnishes and a conservative nip load. Therefore, the water removal and strength improvements are less than what can potentially be achieved, yet substantial improvement in sheet smoothness was achieved. Maximum commercial nip loads are limited by present engineering constraints, but the top ply hydrodynamic specific surface could be substantially lowered to further improve impulse drying performance.

INTRODUCTION

Ongoing laboratory- and pilot-scale research at the Institute of Paper Science and Technology (IPST) has demonstrated that heavy weight grades of paper, such as linerboard, can be successfully impulse dried [1-21]. That research has shown that deleterious sheet delamination can be avoided by a combination of processing strategies. These strategies include steps to make the prepressed sheets highly permeable to water flow and steps to reduce excess heat transfer to the sheet that results in excessive internal flash evaporation at the exit of the impulse dryer.

Research at IPST suggests that high sheet Darcian permeability (low hydrodynamic specific surface) can be obtained by limiting refining to the minimum required for product aesthetics and by prepressing the sheet to as high a solids as possible. In addition, IPST research suggests that excessive pressure-dependent heat transfer can be eliminated by using press roll surfaces composed of materials having low thermal conductivity, low heat capacity, and low density.

Laboratory-scale experiments have been conducted with virgin Southern Pine, Douglas Fir, and OCC [1,2,4,6]. Two-ply sheets made from combinations of the above furnishes, at different levels of specific surface, have also been used. Both virgin furnishes have been successfully impulse dried in the laboratory. OCC performed best in regards to moisture removal and strength development when blended with a virgin kraft at concentrations of 50% or less by weight.

Pilot-scale experiments using a sheet-fed shoe press confirmed the laboratory-scale results [3,7]. The impulse drying critical temperature depends on the thermal properties of the roll coating and the specific surface of the heated ply of the sheet. Impulse drying was shown to be superior to single- and double-felted pressing in water removal and important physical properties. Both single-ply and two-ply sheets were successfully impulse dried.

RESEARCH OBJECTIVES

The overall objective of the work reported was to identify potential furnish types and operating windows to be used during the upcoming pilot-scale trials and commercial demonstration of impulse drying. To meet this objective, initial work was performed to meet the following specific objectives.

- Compare mill-refined pulp and machine paper to laboratory-refined pulp and handsheets in regards to water permeability and impulse drying performance.
- Determine the relationship between permeability, prepressing, and refining for specific pulps.
- Refine laboratory-scale operating parameters to better simulate commercial machine conditions.

EXPERIMENTAL PLANS AND PROCEDURES

This experimental program was a cooperative effort between Union Camp Corporation, Beloit Corporation, and IPST. Union Camp provided the pulp and prepared the handsheets for testing. Beloit prepressed the handsheets and performed some of the physical testing. IPST performed the permeability tests, impulse dried selected furnishes on the MTS laboratory press, and performed the ultrasonic testing. Beloit also performed MTS and pilot-scale impulse drying tests.

For machine linerboard samples, couch trim was grabbed from commercial Union Camp linerboard machines and sealed in plastic bags for transport. The couch trim samples were prepressed to 35% solids prior to testing.

The first set of furnishes evaluated was chosen to simulate present mill furnishes and is described in Table 1. All of these furnishes were made into handsheets for testing. Furnishes W1 and W5 were impulse dried. The remaining furnishes were used for permeability testing.

Table 1. Handsheet furnishes received for impulse drying evaluation.

| IPST ID No. | U. C. ID No. | Top Sheet | Bottom Sheet | Nominal Basis Weight ^a (g/m ²) | Nominal Sheet Solids (%) | No. of Sheets Rec'd |
|-------------|--------------|---|---|---|--------------------------|---------------------|
| W1 | 2P1 | 15% mill refined 4705-35-D, 260 ml CSF | 85% mill refined 4705-35-E, 660 ml CSF | 190 | 35 42 | 25 28 |
| W2 | 1P1 | none | 100% mill refined 4705-35-E, 660 ml CSF | 190 | 35 42 | 4 4 |
| W3 | 1P2 | 100% mill refined 4705-35-D, 260 ml CSF | none | 190 | 35 40 | 4 4 |
| W4 | 2P2 | 15% valley beaten 4705-35-B, 650 ml CSF | 85% mill refined 4705-35-E, 660 ml CSF | 190 | | none |
| W5 | 2P3 | 15% valley beaten 4705-35-B, 650 ml CSF | 85% valley beaten 4705-35-C, 640 ml CSF | 190 | 35 42 | 25 25 |
| W6 | 1P3 | none | 100% valley beaten 4705-35-C, 640 ml CSF | 190 | 35 42 | 4 4 |
| W7 | 1P4 | 100% valley beaten 4705-35-B, 650 ml CSF | none | 190 | 35 42 | 4 4 |
| W8 | 1P5 | 100% valley beaten Hard Wood, 650 ml CSF | none | 190 | 35 42 | 8 8 |

a) Basis Weight is nominal oven-dried value based on 42# sheets at 7.5% moisture.

b) Cases W1 through W7 are a mixture of hardwood and pine.

For each furnish to be impulse dried, the following matrix of conditions was used.

Table 2. Impulse drying experimental matrix.

| Case | D1 | D2 | D3 | D4 | A1 | A2 | C1 | C2 | A3 | A4 | C3 | C4 |
|-----------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Config. | DF | DF | DF | DF | ID |
| Felt Type | B | B | R | R | B | B | B | B | R | R | R | R |
| Pivot Position | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Platen Surface | n/a | n/a | n/a | n/a | A | A | C | C | A | A | C | C |
| Press Impulse (MPa·s) | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 | 0.14 |
| no. of temps | n/a | n/a | n/a | n/a | a.n. |
| Sin, % | 35 | 42 | 35 | 42 | 35 | 42 | 35 | 42 | 35 | 42 | 35 | 42 |
| repeats | 10 | 10 | 10 | 10 | a.n. |

a) Ingoing Sheet Temperature Impulse Drying = ~65°C (150°F)

Double-felted Pressing = Ambient

b) Ingoing Felt Moisture = 16% (0.2 mr)

c) a.n. = as needed.

A second set of experiments was performed to characterize the relationship of hydrodynamic specific surface to refining level and prepressing. The furnishes used are listed in Table 3.

Table 3. Furnishes used for permeability study.

| IPST ID No. | U. C. ID No. | Pulp Type | Freeness (ml) |
|-------------|--------------|--------------------------|---------------|
| W9 | 1P10 | 100% Hardwood | 691 |
| W10 | 1P11 | 100% Pine, 93.0 Kappa | 754 |
| W11 | 1P12 | 50% Hardwood 50% Pine | 707 761 |
| W12 | 1P13 | 100% Pine | 665 |
| W15 | 1P14 | 100% Hardwood | 670 |
| W16 | 1P15 | 100% Hardwood | 650 |
| W17 | 1P16 | 100% Hardwood | 630 |
| W18 | 1P17 | 100% Pine | 700 |
| W19 | 1P18 | 100% Pine | 620 |
| W20 | 1P19 | 50% Hardwood 50% Pine | 670 700 |
| W21 | 1P20 | 50% Hardwood 50% Pine | 650 660 |
| W22 | 1P21 | 50% Hardwood 50% Pine | 630 620 |

Each furnish was prepressed by Beloit as shown in Table 4, except as noted below. For case P1, furnishes W15-W17 and W22 were crushed resulting in questionable or lost samples. For case P2, furnishes W16, W17, and W22 were again crushed; furnish W15 was pressed at 300 and 800 pli. For cases P3-P5 and furnishes W15-W17 and W22, the first pressing was reduced to 300 pli. A few sheets were still crushed, and the data obtained from them were scrutinized.

Table 4. Pressing conditions.

| Pressing Case | Roll Nip Pressures (pli) | DF ENP Pressures (pli) | Total Impulse (psi-s) |
|---------------|--------------------------|------------------------|-----------------------|
| P1 | 800 | n/a | 2.42 |
| P2 | 500+800 | n/a | 3.94 |
| P3 | 500+800+1200 | n/a | 7.58 |
| P4 | 500+800 | 6000 | 22.12 |
| P5 | 800 | 6000+6000 | 38.78 |

a) Machine speed = 1650 fpm.

The water permeability tests were performed using procedures previously documented [24]. Compressive loads used were in the range of 200 to 650 lb.-force. Water pressure in the range of 2 to 15 psi was used to ensure flow rates in the range of 0.5 to 30 g/min.

The question was raised about whether the sheet temperature profile was constant in the z-direction during steaming. We embedded thermocouples in a sheet by pressing multiple thin layers (65 g/m^2) together with thermocouples between the layers. Top and bottom thermocouples were added to give a total of four measurements through the sheet. Table 5 lists the furnishes prepared with thermocouples.

Table 5. Multilayer sheets with thermocouples between the layers.

| IPST ID No. | Ply | U. C. ID No. | Pulp Type | Freeness (ml) |
|-------------|-----------------|--------------|--------------------------|---------------|
| W13 | Top | 1P6 | 100% Hardwood | 691 |
| | Middle & Bottom | 1P7 & 1P9 | 100% Pine, 93.0 Kappa | 659 |
| W14 | Top | 1P8 | 100% Hardwood | 297 |
| | Middle & Bottom | 1P7 & 1P9 | 100% Pine | 659 |

RESULTS

FIBER ANALYSIS

For each furnish used for the refining study, samples from the prepared sheets were sent to John D. Hankey & Associates for fiber analysis. The results of the fiber identification are shown in Table 6. Table 7 summarizes the average fiber dimensions.

Table 6. Fiber identification for various pulp samples.

| Furnish ID IPST U. C. | | USWK (%) | UHWK (%) | Softwood Species | | | Hardwood Species | |
|--------------------------|------|-------------|-------------|---|--|--|--|--|
| W9 | 1P10 | 2 | 98 | Mixed species of southern yellow pine (Hard Cook) | | | Oak, Gum, Yellow Poplar, Maple, and trace amounts of other mixed species | |
| W10 | 1P11 | 97 | 3 | Mixed species of southern yellow pine (Hard Cook) | | | Mixed, incl. Oak, Gum, Yellow Poplar, and Maple | |

Table 7. Fiber dimensions.

| Case | Pulp | Kappa No. | Freeness (ml CSF) | Length (mm) | | | Width (μm) | Perimeter (μm) | Cell Wall Thickness (μm) | Coarseness (mg/100 m) |
|------|------|-----------|-------------------|-------------|------|------|------------|----------------|--------------------------|-----------------------|
| | | | | Arith | LW | WW | | | | |
| W10 | Pine | 93.0 | 754 | 2.36 | 3.28 | 3.86 | 34.3 | 82.6 | 3.5 | 41.0 |
| W18 | Pine | 93.0 | 700 | 2.44 | 3.21 | 3.78 | 34.6 | 85.2 | 4.0 | 35.8 |
| W12 | Pine | 93.0 | 665 | 2.55 | 3.29 | 3.87 | 35.9 | 85.0 | 3.3 | 35.4 |
| W19 | Pine | 93.0 | 620 | 2.19 | 2.92 | 3.46 | 36.2 | 85.2 | 3.2 | 35.2 |
| W9 | Hard | - | 691 | 1.20 | 1.41 | 1.57 | 16.8 | 45.6 | 3.0 | 17.4 |
| W15 | Hard | - | 670 | 1.47 | 1.33 | 1.47 | 16.9 | 46.2 | 3.1 | 15.8 |
| W16 | Hard | - | 650 | 1.22 | 1.41 | 1.58 | 16.4 | 45.2 | 3.1 | 16.4 |
| W17 | Hard | - | 630 | 1.17 | 1.32 | 1.43 | 16.0 | 44.4 | 3.1 | 16.2 |
| W11 | Mix | - | 734 | 1.52 | 2.13 | 2.97 | 21.1 | 58.6 | 3.6 | 25.2 |
| W20 | Mix | - | 685 | 1.55 | 2.19 | 3.01 | 23.8 | 60.0 | 3.1 | 21.6 |
| W21 | Mix | - | 655 | 1.36 | 1.81 | 2.37 | 21.9 | 57.0 | 3.3 | 21.0 |
| W22 | Mix | - | 625 | 1.44 | 2.15 | 3.11 | 22.8 | 58.0 | 3.1 | 21.2 |

PERMEABILITY

All of the raw permeability data are summarized in Appendix D as permeability versus porosity plots.

Couch Trim Sample Set

The permeability data collected for the couch trim samples are summarized in Table 8. Some of the sheets were manually separated at the ply bond and each ply tested.

Table 8. Permeability results for the couch trim samples.

| Furnish | Sheet Solids (%) | 95% Conf. Interval | OD Basis Weight (g/m ²) | 95% Conf. Interval | Specific Surface (m ² /g) | 95% Conf. Interval | Specific Volume (cm ³ /g) | 95% Conf. Interval |
|-----------------------|------------------|--------------------|-------------------------------------|--------------------|--------------------------------------|--------------------|--------------------------------------|--------------------|
| Mill #1 | 36.7 | 1.6 | 180 | 3 | 5.0 | 1.2 | 1.7 | 0.3 |
| Mill #1 Top Ply | - | - | - | - | 15.8 | 6.0 | 3.1 | 0.4 |
| Mill #1 Bottom Ply | - | - | - | - | 16.3 | 8.2 | 2.95 | 0.2 |
| Mill #2 | 25.0 | 0.3 | 141 | 4 | 5.3 | 1.6 | 2.0 | 0.5 |
| Mill #2 Top Ply | - | - | - | - | 4.8 | 4.2 | 7.2 | 3.2 |
| Mill #2 Bottom Ply | - | - | - | - | 2.5 | 1.6 | 4.3 | 0.4 |

It was determined that the permeability test equipment was not working properly (note the large values for specific volume). Therefore, all of the above results are probably in error to some extent. Before continuing with additional tests, the equipment was repaired and checked. All of the data reported in subsequent sections of this report were collected after the repairs.

Impulse Drying Sample Set

Handsheets made from mill-refined and laboratory-refined pulps were evaluated for impulse drying. In addition to the two-ply sheets, one-ply sheets of each component pulp were tested for permeability. The results are shown in Table 9.

Table 9. Permeability results for the impulse drying samples.

| IPST ID No. | U. C. ID No. | Sheet Solids (%) | 95% Conf. Interval | OD Basis Weight (g/m ²) | 95% Conf. Interval | Specific Surface (m ² /g) | 95% Conf. Interval | Specific Volume (cm ³ /g) | 95% Conf. Interval |
|-------------|--------------|------------------|--------------------|-------------------------------------|--------------------|--------------------------------------|--------------------|--------------------------------------|--------------------|
| W1 | 2P1 | 36.8 | 1.1 | 174 | 5 | 7.3 | 1.0 | 2.0 | 0.1 |
| W1 | 2P1 | 47.0 | 2.3 | 184 | 8 | 5.2 | 0.6 | 1.8 | 0.1 |
| W2 | 1P1 | 35.7 | 1.2 | 171 | 9 | 4.9 | 1.6 | 2.0 | 0.1 |
| W2 | 1P1 | 43.5 | 1.6 | 169 | 6 | 4.9 | 2.0 | 1.8 | 0.1 |
| W3 | 1P2 | 32.3 | 1.8 | 178 | 7 | 60.9 | 4.9 | 1.2 | 0.1 |
| W3 | 1P2 | 39.6 | 1.8 | 175 | 6 | 45.7 | 6.9 | 1.6 | 0.2 |
| W5 | 2P3 | 37.1 | 1.3 | 183 | 6 | 6.0 | 1.9 | 1.9 | 0.1 |
| W5 | 2P3 | 42.4 | 1.3 | 176 | 7 | 5.2 | 0.8 | 1.8 | 0.1 |
| W6 | 1P3 | 30.7 | 2.4 | 182 | 4 | 6.4 | 2.2 | 2.0 | 0.04 |
| W6 | 1P3 | 36.6 | 0.9 | 181 | 3 | 4.0 | 0.8 | 2.0 | 0.02 |
| W7 | 1P4 | 31.1 | 0.2 | 174 | 2 | 11.8 | 1.2 | 1.8 | 0.04 |
| W7 | 1P4 | 43.5 | 1.7 | 176 | 5 | 4.7 | 0.5 | 1.7 | 0.05 |
| W8 | 1P5 | 35 ^a | - | 170 | 4 | 6.9 | 0.3 | 2.5 | 0.1 |
| W8 | 1P5 | 42 ^a | - | 174 | 3 | 6.7 | 2.1 | 2.5 | 0.1 |

a) Nominal sheet solids.

Refining Study Set

All the sheets fabricated from furnishes W9 to W12 and W15 to W22 were prepressed to five pressing conditions as described above. Figures 1 to 6 show sheet solids after each prepressing as a function of press condition and total impulse for pine, hardwood, and 50/50 blends. For the pine cases, solids ranged from 30 to 48%, while for the hardwood cases, solids ranged from 36 to 51%. For all cases, solids were directly proportional to total press impulse. The same press impulse results in higher solids for samples of higher freeness. The freeness values used for the mixed cases were averages of the component freenesses.

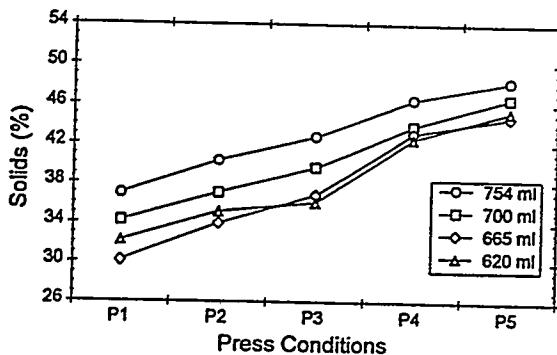


Figure 1. Average sheet solids for pine furnish.

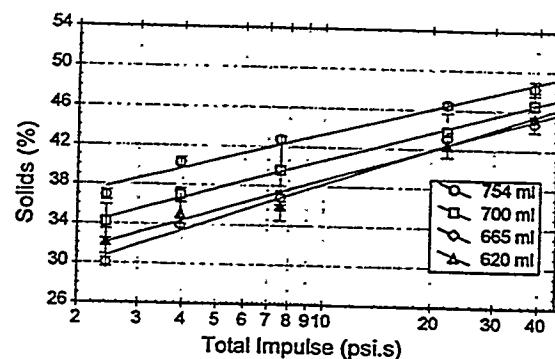


Figure 2. Average sheet solids for pine furnish.

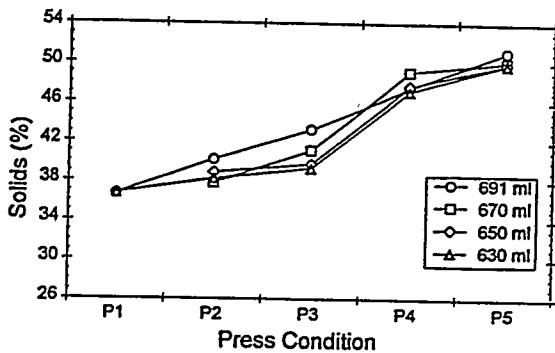


Figure 3. Average sheet solids for hardwood furnish.

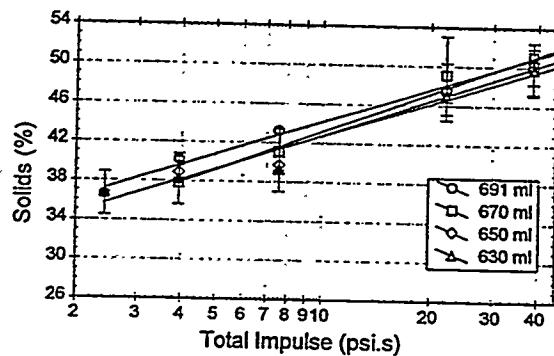


Figure 4. Average sheet solids for hardwood furnish.

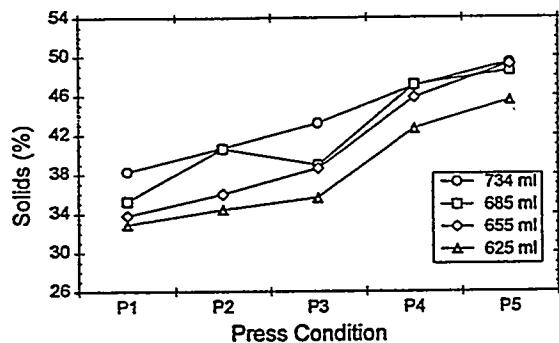


Figure 5. Average sheet solids for mixed furnish.

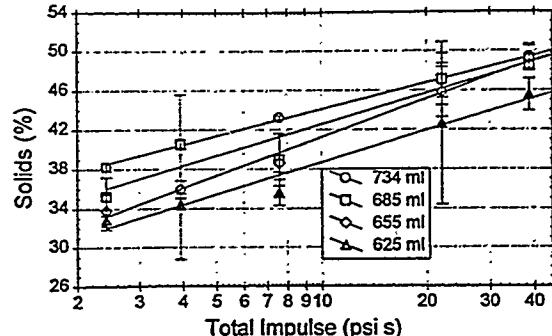


Figure 6. Average sheet solids for mixed furnish.

The sheets were formed and pressed in two batches. The first batch (W9-W12) was received and tested in early September. The second batch (W15-W22) was received about 1.5 months later. Between four and six samples were tested for each case (furnish and prepressing condition). All of the samples were stored in the refrigerator until tested. Since previous work [24] observed that fiber aging affects permeability results, the tests were performed in random order.

Figures 7 through 18 show the dependence of specific surface on storage time measured from pressing date. In general, for the least pressed cases (P1), specific surface increased with storage time. For the pine furnish, there is a general decrease in specific surface with time except for the highest freeness case (W10). For the case W10 (754 ml CSF), there was no aging effect observed.

For the hardwood sheets, the aging effect was more significant and resulted in increased specific surface with time except for the least refined case, W9 (691 ml CSF). For case W9, specific surface increases with time except for the least pressed sheets (P1). There was no observed time correlation for the mixed cases.

In general, the variability of the permeability test results was too great to accurately compensate for aging effects; therefore, for further analysis, all results were time averaged. For some of the cases plotted below, there were data points that were outside of the range plotted. These data points are shown in a box in the plot.

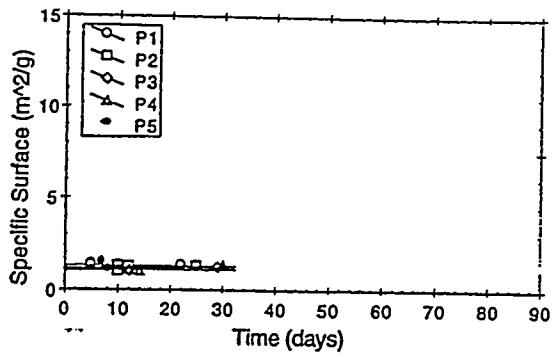


Figure 7. Case W10, pine, 754 ml CSF.

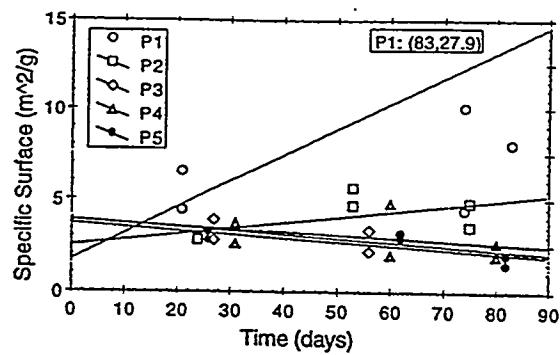


Figure 8. Case W18, pine, 700 ml CSF.

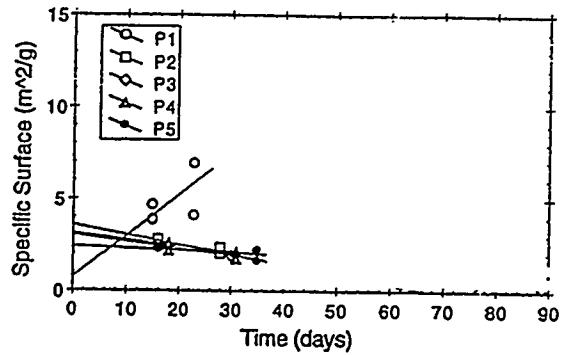


Figure 9. Case W12, pine, 665 ml CSF.

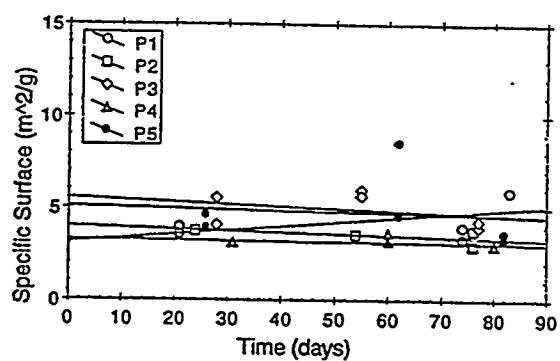


Figure 10. Case W19, pine, 620 ml CSF.

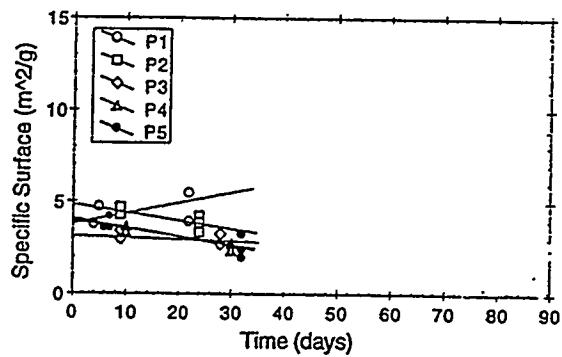


Figure 11. Case W9, hardwood, 691 ml CSF.

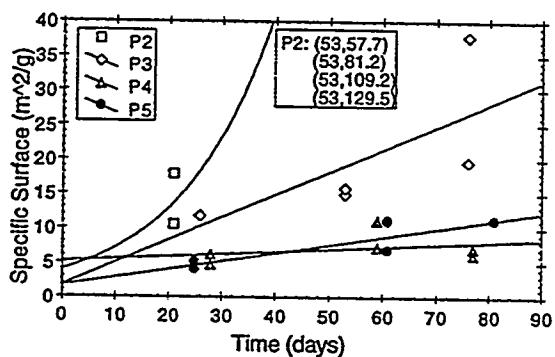


Figure 12. Case W15, hardwood, 670 ml CSF.

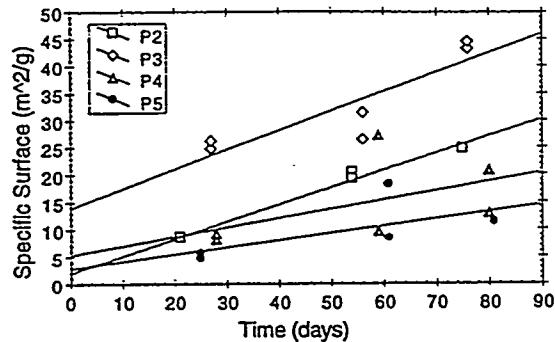


Figure 13. Case W16, hardwood, 650 ml CSF.

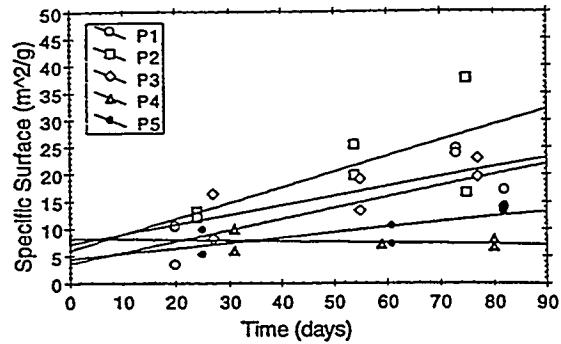


Figure 14. Case W17, hardwood, 630 ml CSF.

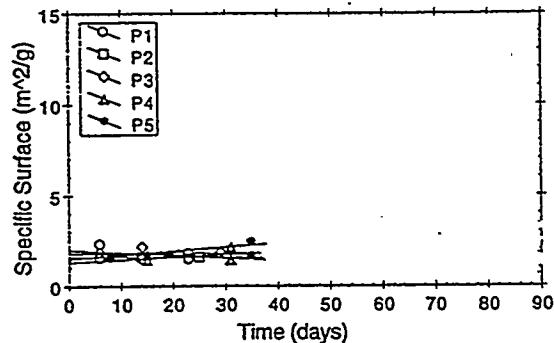


Figure 15. Case W11, mixture, 734 ml CSF.

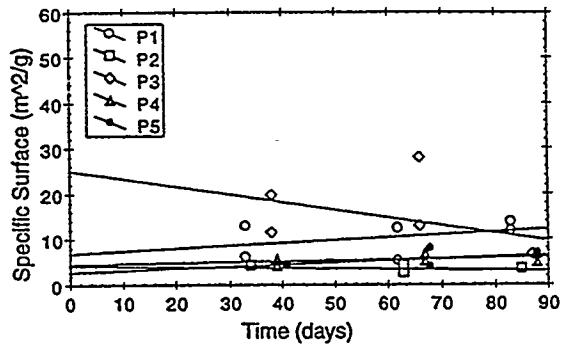


Figure 16. Case W20, mixture, 685 ml CSF.

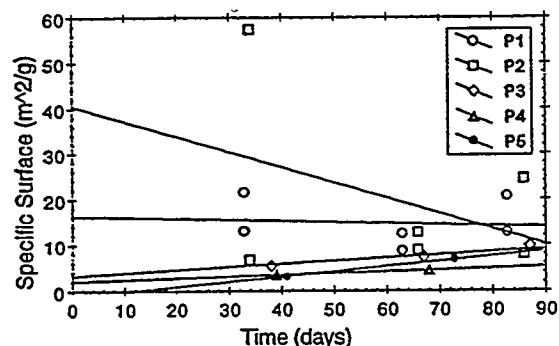


Figure 17. Case W21, mixture, 658 ml CSF.

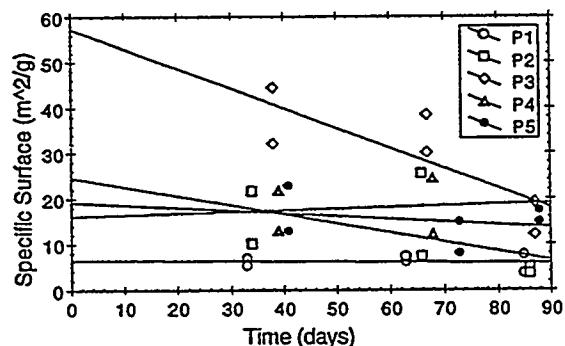


Figure 18. Case W22, mixture, 625 ml CSF.

It was observed that the variability of water permeability measurements for the first batch (furnishes W9-W12) was less than that for the second batch (W15-W22). During prepressing of the sheets from the second batch, sheet crushing was observed for some cases as noted in the procedures section. In general, for the crushed sheets, the specific surface was lower than what was expected.

The dependencies of specific surface and specific volume of swollen fibers on freeness are plotted in Figures 19 through 24. In general, specific surface (Figures 19, 21, and 23) tended to decrease with increased ingoing solids and freeness for both pine and hardwood furnishes. For a given freeness, the specific surface for pine was lower than that for hardwood. These results correspond with previously observed trends [3,6,7].

Figures 20, 22, and 24 show the dependence of specific volume on freeness for different prepressing conditions. Specific volume typically varies in the interval of 1.0 to 1.5 cc/g. Higher values were observed for pine compared to hardwood. Lower solids cases had higher values of specific volume. For pine, there was no observed correlation with freeness (Figure 20), while for hardwood, the specific volume tends to increase with increased freeness.

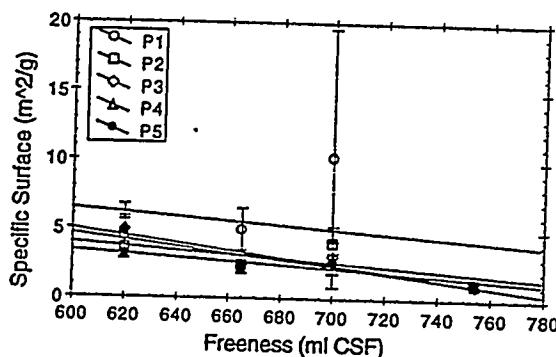


Figure 19. Average specific surface for pine furnish.

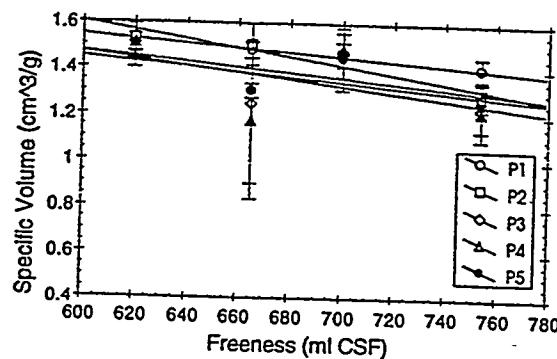


Figure 20. Average specific volume for pine furnish.

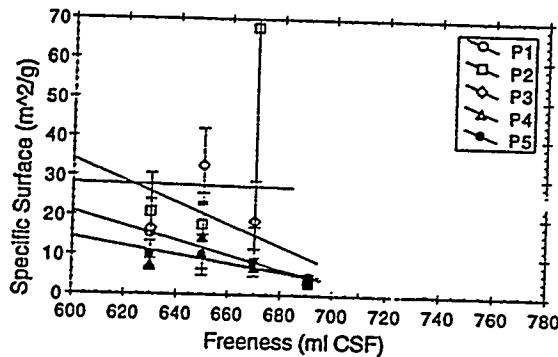


Figure 21. Average specific surface for hardwood furnish.

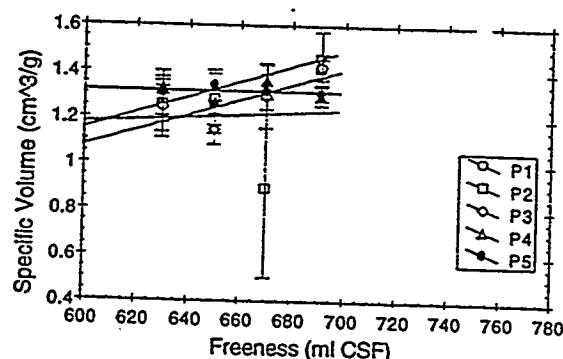


Figure 22. Average specific volume for hardwood furnish.

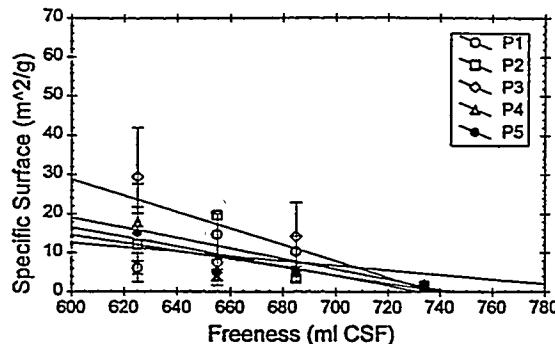


Figure 23. Average specific surface for mixed furnish.

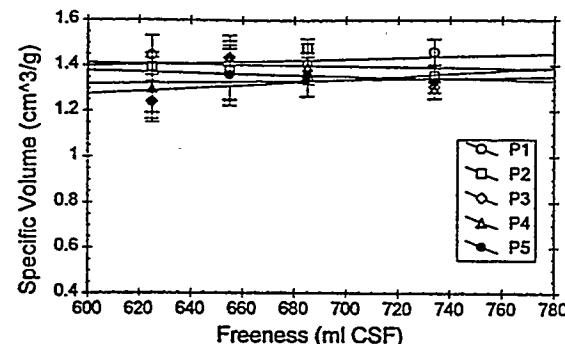


Figure 24. Average specific volume for mixed furnish.

The effect of pine fiber content, in a hardwood mixture, on specific surface for different pressing conditions is shown in Figures 25 through 29. In general, the addition of 50% pine fibers to the hardwood results in virtually the same specific surface as for 100% pine. Some deviations are primarily caused by high variability of specific surface for low freeness furnishes.

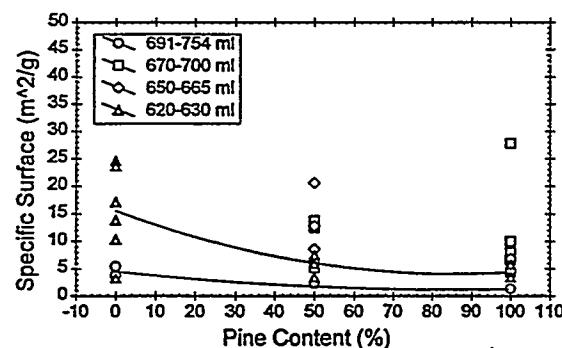


Figure 25. Pressing condition P1.

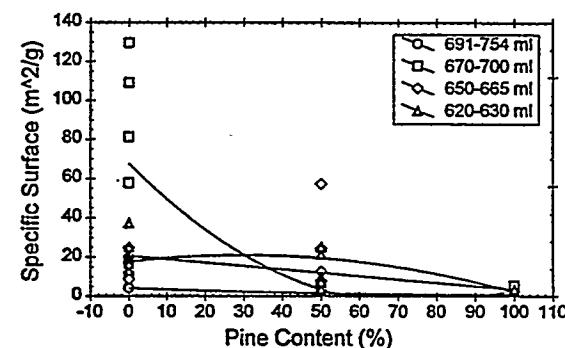


Figure 26. Pressing condition P2.

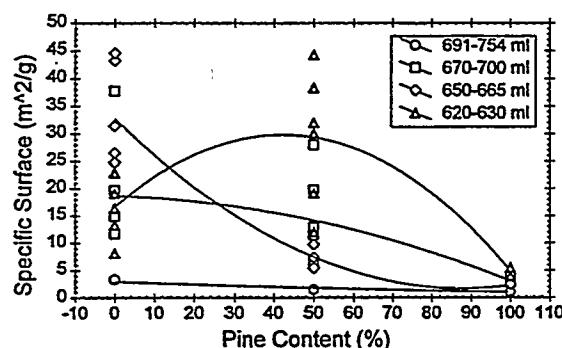


Figure 27. Pressing condition P3.

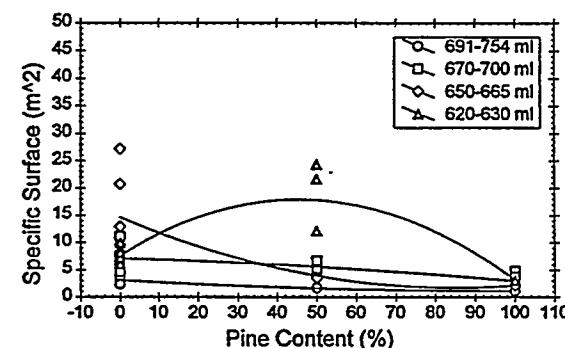


Figure 28. Pressing condition P4.

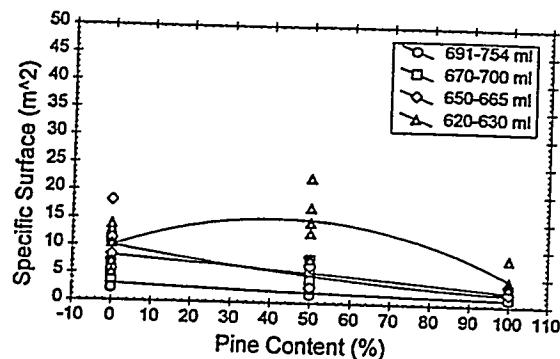


Figure 29. Pressing condition P5.

IMPULSE DRYING

All impulse drying was done with a presteaming temperature of 65°C. To determine the steaming time, two wire thermocouples were placed between the sheet and the felt, and the temperature was recorded while steaming with the platen surface temperature set at 200°C and the heat shield in place. The steaming time was set to the time at which the slowest temperature profile crosses 55°C. At this time, the sheet temperature should be between 55 and 75°C. The results of these calibrations are shown in Table 10, and the temperature profiles are in Appendix E.

Table 10. Presteam times and temperature ranges obtained.

| Furnish | Case | Time (s) | Temp Range (°C) |
|---------|------|----------|-----------------|
| W1 | A1 | 21 | 55-75 |
| | A2 | 18 | 55-70 |
| | A3 | 15 | 55-69 |
| | A4 | 15 | 55-66 |
| | C1 | 11 | 56-71 |
| | C2 | 14 | 55-74 |
| | D1 | 30 | 55-76 |
| | D2 | 34 | 55-83 |
| W5 | A1 | 19 | 55-72 |
| | A2 | 15 | 55-73 |
| | A3 | 14 | 55-64 |
| | A4 | 16 | 55-69 |
| | C1 | 14 | 55-68 |
| | C2 | 14 | 55-71 |
| | D1 | 32 | 55-82 |
| | D2 | 31 | 55-82 |

A second calibration procedure measures moisture change during steaming. A sheet and felt were weighed and then steamed as if for impulse drying. However, the sheet and felt were removed from the MTS and weighed again right after steaming. Five repeats were done at five platen surface temperatures, and a best fit to the data was used to determine the moisture change during steaming. Before impulse drying, the sheet moisture level was adjusted such that the sheet solids were at the target level after the steaming step, i.e., just before pressing.

Couch Trim Samples

The effect of ingoing felt moisture was tested using the Mill #1 couch trim. The A platen, R felt, and 35% ingoing solids were used (case A3). The steaming time used was 15s at a temperature of 61-71°C. Results are listed in Table 11, and the raw data are in Appendix A. Felt moisture was observed to make a difference, and it was decided to use 16% for the remainder of the experiments.

Table 11. Results of felt moisture variation impulse drying trials.

| Case | Platen Temperature (°C) | Ingoing Felt Moisture (%) | 95% Conf. Interval | Ingoing Sheet Solids (%) | 95% Conf. Interval | Outgoing Sheet Solids (%) | 95% Conf. Interval |
|--------|-------------------------|---------------------------|--------------------|--------------------------|--------------------|---------------------------|--------------------|
| A3-PR1 | 200 | 16.1 | 0.2 | 37.5 | 3.3 | 42.9 | 3.6 |
| A3-PR1 | 200 | 34.3 | 15.9 ^a | 37.2 | 2.8 | 36.1 | 9.4 |
| A3-PR1 | 250 | 16.6 | 3.4 | 36.3 | 2.4 | 44.9 | 1.0 |
| A3-PR1 | 250 | 32.7 | 2.5 | 33.9 | 2.1 | 38.6 | 3.6 |

a) The high variation for this case was the result of moisture migration within a stack of wet felts while waiting to perform the experiment.

Critical temperatures were determined from the specific elastic modulus, %CV of SEM, and from visual observations. All of this data are shown in Appendix C. An explanation of the delamination codes is at the beginning of Appendix A. The following procedure was used to determine the critical temperatures.

- 1) Determine the temperature at which the %CV of SEM exceeds a value of 15-20%. In most cases, there was a sharp increase in %CV when delamination first occurred.
- 2) Determine the temperature at which the SEM values peak.
- 3) Determine the highest temperature at which there were no visible delaminations observed.
- 4) If two or more of the above determined temperatures agree, then that was the critical temperature.
- 5) If none of the above temperatures agree, then determine if the density data peak at one of the possible temperatures. For these cases, the critical temperature was the temperature that agrees with the majority of data.
- 6) If all else fails, the critical temperature was determined from the visual observations.

- 7) Round off the temperature to the nearest 5°C.
- 8) Identify any anomalies.

Previous experiments have shown that above the critical temperature, the SEM (and other strength properties) drops. Conversely, the %CV of the SEM rises just above the critical temperature. Therefore, the above procedure will determine a lower limit for the critical temperature for most cases. To determine the upper and lower uncertainties for the critical temperature, the following procedure was used.

- 1) The upper limit was the next higher temperature for which there were data if there was no visible delamination. If there were any visible delaminations, then the upper limit was zero.
- 2) If there was a large jump in the %CV of SEM value at the upper limit (~10 to 40+), then the lower limit was 10°C less than the critical temperature; otherwise, the lower limit was next lower temperature for which there were data.
- 3) If the SEM data do not show a peak at the critical temperature, then the lower limit was the next lower temperature for which there were data.
- 4) The lower limit cannot be less than 100°C (otherwise, it would not be impulse drying).
- 5) Uncertainties are the difference between the critical temperatures and the limits rounded to the nearest 5°C.

Additional Mill #1 couch trim sheets were impulse dried to determine the critical temperature and water removal. Figures 30 through 33 show the data used to determine the critical temperature. For temperatures of 150°C and below, severe sticking affected the results, and these data were ignored when determining the critical temperature. The critical temperature was 255°C, plus zero, minus 55°C. In Figure 32, the observed delamination value of six at 200°C may have been an anomaly.

Figures 34 and 35 show the outgoing solids and felt water gain results. The higher sheet outgoing solids and lower felt water gain at temperatures of 150° and below are a result of sheet sticking. Because sticking was also a problem at high temperatures, the felt water gain was lower than the typical values of 70-90%.

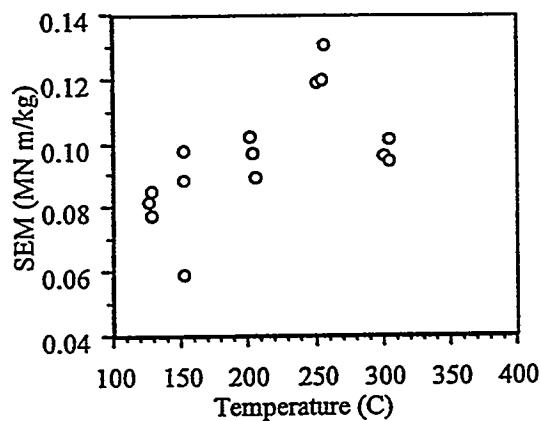


Figure 30. Specific elastic modulus.

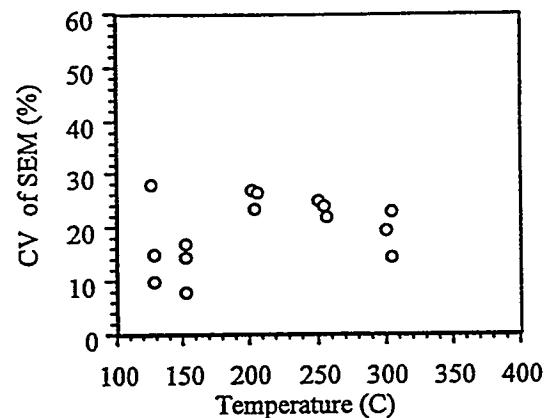


Figure 31. Coefficient of variation of SEM.

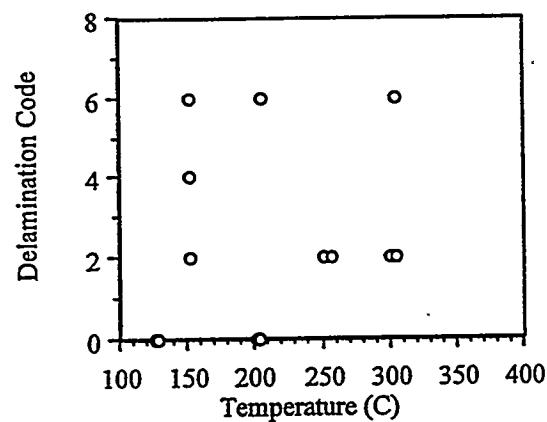


Figure 32. Visual delamination observations. See Appendix A for codes.

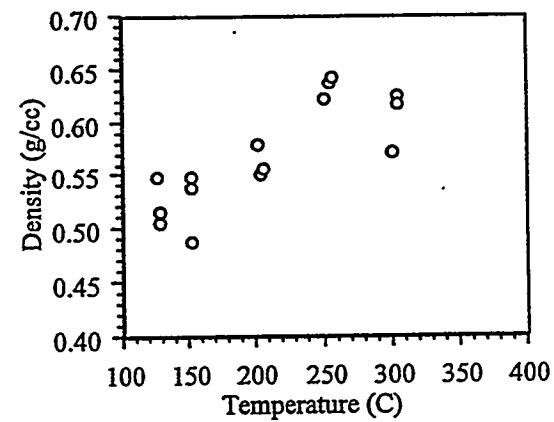


Figure 33. Ultrasonic sheet density.

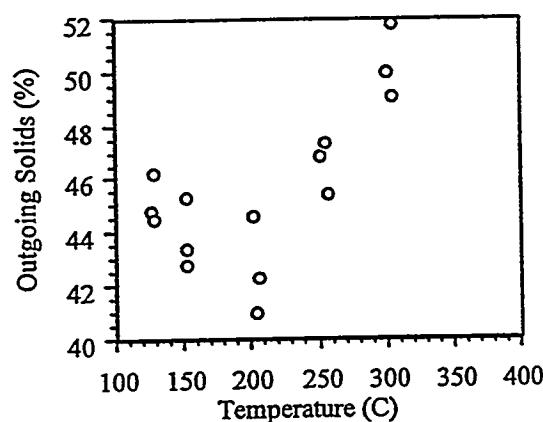


Figure 34. Outgoing sheet solids.

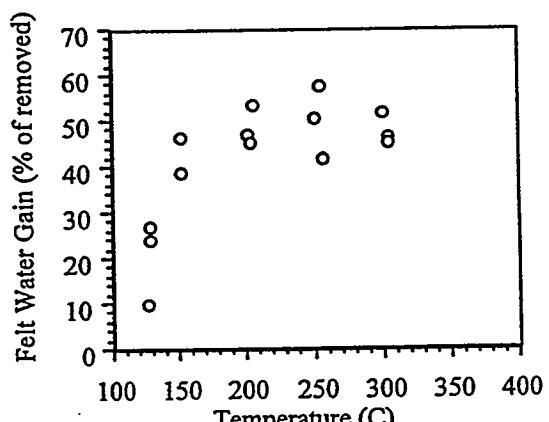


Figure 35. Felt gain of water removed.

Beloit also performed some tests using the Mill #1 and Mill #2 couch trim sheets. Ingoing solids were 36%; the "A" roll coating, "R" felt, and presteaming were used. The results at the critical temperature are tabulated in Table 12 for comparison.

Table 12. Results of Beloit impulse drying tests of couch trim.

| Test | Simulator | Mill #1 | Mill #2 |
|------------------------------------|---------------------|---------|---------|
| Critical Temperature (°C) | MTS ^a | 177 | 149 |
| | HRP ^b | 204 | 177 |
| Outgoing Solids (%) | MTS | 46.5 | 50.5 |
| | HRP | 51.9 | 52.9 |
| | DF ENP ^c | 47.7 | 47.8 |
| TAPPI Density (g/cm ³) | MTS | - | - |
| | HRP | 0.620 | 0.626 |
| | DF ENP | 0.605 | 0.574 |
| GM STFI Index (Nm/g) | MTS | - | - |
| | HRP | 27.2 | 27.5 |
| | DF ENP | 25.3 | 25.8 |
| Top Side Bendtsen Rough. (ml/min) | MTS | - | - |
| | HRP | 1650 | 790 |
| | DF ENP | 2330 | 1840 |

a) MTS = Beloit MTS.

b) HRP = Beloit impulse drying pilot roll press.

c) DF ENP = Beloit double-felted pilot extended-nip press.

Prepared Handsheets

Extensive IPST impulse drying trials were conducted for furnishes W1 and W5. A presteam temperature of ~65°C, and an ingoing felt moisture of 16% were used. Before analysis, the impulse drying data were filtered for a basis weight of $177 \pm 10 \text{ g/m}^2$ (OD), an ingoing solids of 32,35,40 or $42 \pm 1.0\%$, and an impulse of $0.1379 \pm 0.0034 \text{ MPa}\cdot\text{s}$. Data used for further analysis are listed in Appendix A. Rejected data are listed in Appendix B.

Table 13 lists the experimental conditions used for impulse drying and the critical temperatures obtained. SEM, %CV of SEM, visible delamination codes, and some of the density data that were used to determine the critical temperatures are listed in Appendix C.

Table 13. Impulse drying critical temperatures.

| Furnish ID IPST | U. C. | Case | Felt | Specific Sur. (m ² /g) | 95% C.I. | Critical Temp. (°C) | Uncertainty | |
|--------------------|-------|------|------|--------------------------------------|-------------|------------------------|-------------|-----|
| W1 | 2P1 | A1 | B | 7.35 | 0.98 | 170 | +15 | -10 |
| W1 | 2P1 | A2 | B | 5.24 | 0.58 | 160 | +10 | -10 |
| W1 | 2P1 | A3 | R | 7.35 | 0.98 | 155 | +10 | -10 |
| W1 | 2P1 | A4 | R | 5.24 | 0.58 | 160 | +10 | -15 |
| W1 | 2P1 | C1 | B | 7.35 | 0.98 | 205 | +∞ | -10 |
| W1 | 2P1 | C2 | B | 5.24 | 0.58 | 190 | +∞ | -10 |
| W5 | 2P3 | A1 | B | 6.00 | 1.94 | 175 | +10 | -10 |
| W5 | 2P3 | A2 | B | 5.24 | 0.77 | 205 | +10 | -10 |
| W5 | 2P3 | A3 | R | 6.00 | 1.94 | 160 | +10 | -15 |
| W5 | 2P3 | A4 | R | 5.24 | 0.77 | 170 | +15 | -25 |
| W5 | 2P3 | C1 | B | 6.00 | 1.94 | 230 | +10 | -20 |
| W5 | 2P3 | C2 | B | 5.24 | 0.77 | 230 | +20 | -20 |

Other physical properties at the critical temperature are listed in Tables 14 and 15, and are shown in Figures 36 through 39.

Table 14. Impulse drying water removal data at the critical temperature.

| Furnish | Case | Ingoing Solids (%) | Outgoing Solids (%) | 95% Conf. Interval | Moisture Ratio Change | 95% Conf. Interval |
|---------|-------|-----------------------|------------------------|-----------------------|--------------------------|-----------------------|
| W1 | A1 | 32 | 46.6 | 1.4 | 0.97 | 0.25 |
| W1 | A2 | 40 | 50.0 | 1.0 | 0.54 | 0.09 |
| W1 | A3 | 32 | 43.4 | 1.5 | 0.85 | 0.03 |
| W1 | A4 | 40 | 47.6 | 2.2 | 0.44 | 0.05 |
| W1 | C1 | 35 | 46.5 | 1.4 | 0.70 | 1.02 |
| W1 | C2 | 42 | 50.3 | 0.2 | 0.37 | 0.37 |
| W1 | D1 | 35 | 41.6 | 0.5 | 0.48 | 0.06 |
| W1 | D2/40 | 40 | 44.7 | 1.4 | 0.22 | 0.10 |
| W1 | D2/42 | 42 | 44.9 | 3.6 | 0.17 | 0.12 |
| W5 | A1 | 32 | 46.6 | 0.7 | 0.96 | 0.05 |
| W5 | A2 | 40 | 51.6 | 0.5 | 0.58 | 0.07 |
| W5 | A3 | 32 | 45.6 | 1.3 | 0.92 | 0.16 |
| W5 | A4 | 40 | 47.6 | 11.3 | 0.42 | 0.07 |
| W5 | C1 | 35 | 46.7 | 1.7 | 0.69 | 0.09 |
| W5 | C2 | 42 | 51.5 | 1.4 | 0.45 | 0.09 |
| W5 | D1 | 35 | 41.3 | 0.14 | 0.43 | 0.04 |
| W5 | D2/40 | 40 | 43.6 | ∞ | 0.19 | ∞ |
| W5 | D2/42 | 42 | 44.3 | ∞ | 0.13 | ∞ |

Table 15. Impulse drying physical property data at the critical temperature.

| Furnish | Case | Density (g/cm ³) | 95% Conf. Interval | STFI Index (N·m/g) | 95% Conf. Interval | SEM (MN·m/kg) | 95% Conf. Interval |
|---------|-------|---------------------------------|-----------------------|-----------------------|-----------------------|------------------|-----------------------|
| W1 | A1 | 0.683 | 0.029 | 30.19 | 0.06 | 0.186 | 0.005 |
| W1 | A2 | 0.722 | 0.072 | - | - | 0.172 | 0.020 |
| W1 | A3 | 0.665 | 0.076 | 30.06 | 2.80 | 0.154 | 0.028 |
| W1 | A4 | 0.678 | 0.066 | 29.47 | ∞ | 0.148 | 0.044 |
| W1 | C1 | 0.670 | 0.070 | 29.21 | 13.59 | 0.165 | 0.038 |
| W1 | C2 | 0.699 | 0.006 | 29.12 | 1.67 | 0.166 | 0.013 |
| W1 | D1 | 0.614 | 0.020 | 29.15 | 0.80 | 0.133 | 0.015 |
| W1 | D2/40 | 0.660 | 0.047 | 29.19 | 3.16 | 0.143 | 0.013 |
| W1 | D2/42 | 0.653 | 0.241 | 29.74 | 6.68 | 0.144 | 0.019 |
| W5 | A1 | 0.710 | 0.016 | 31.03 | 1.46 | 0.168 | 0.009 |
| W5 | A2 | 0.734 | 0.008 | 29.44 | ∞ | 0.176 | 0.012 |
| W5 | A3 | 0.699 | 0.029 | 31.61 | 3.46 | 0.158 | 0.018 |
| W5 | A4 | 0.722 | 0.051 | 31.96 | ∞ | 0.151 | 0.057 |
| W5 | C1 | 0.711 | 0.007 | 30.70 | 1.41 | 0.165 | 0.017 |
| W5 | C2 | 0.728 | 0.014 | 29.77 | 2.03 | 0.160 | 0.013 |
| W5 | D1 | 0.640 | 0.028 | 30.95 | 0.62 | 0.142 | 0.010 |
| W5 | D2/40 | 0.670 | ∞ | 32.98 | ∞ | 0.140 | ∞ |
| W5 | D2/42 | 0.643 | ∞ | 32.50 | ∞ | 0.149 | ∞ |

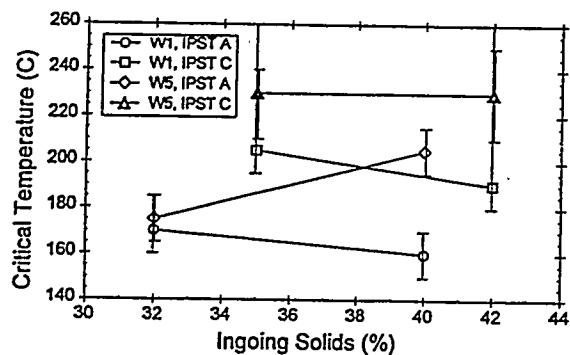


Figure 36. Critical temperatures for B felt.

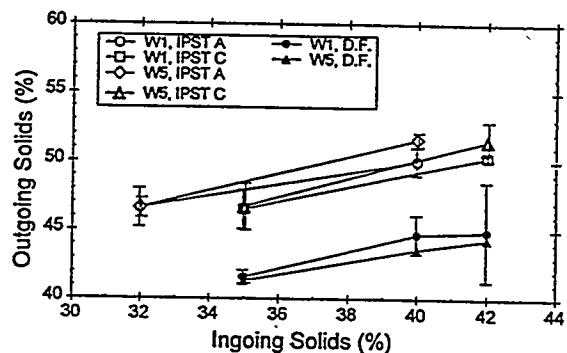


Figure 37. Outgoing solids for B felt.

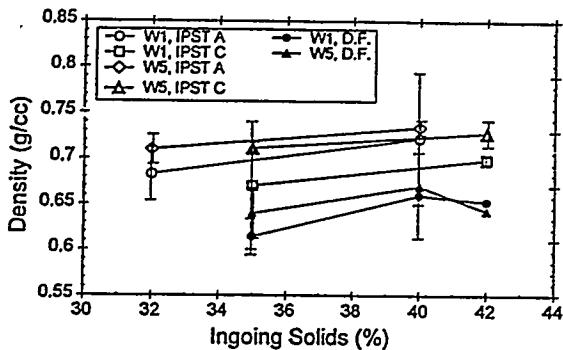


Figure 38. Density for B felt.

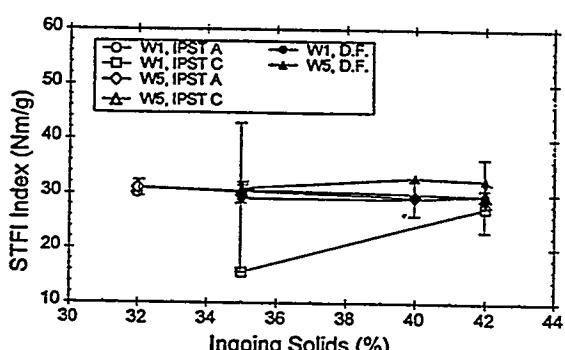


Figure 39. STFI index for B felt.

The following data, obtained by Beloit, are shown in Table 16 for comparison. The roll surface was "A" and the R felt used. The Beloit MTS impulse was 0.16 MPa·s; presteaming was used; and the felts were air dried. Presteaming was also used for the HRP and HTP impulse drying cases. The control case was prepressed and finish dried. The commercial case was prepressed and then run through a three-nip single-felted roll press at 500, 800, and 1200 pli. All physical property data reported were at the critical temperatures.

Table 16. Comparison of IPST and Beloit impulse drying results at the critical temperature.

| Test | Furnish | Nominal Ingoing Solids (%) | Cont ^d | Com ^e | IPST MTS | Beloit MTS | Beloit HRP | Beloit ENP HTP | Beloit ENP DF |
|-----------------------------------|----------|----------------------------|-------------------|------------------|----------|------------|------------|----------------|---------------|
| Critical Temp. (°C) | W1 (2P1) | 36 | - | - | 155 | 177 | <177 | 177 | - |
| | W1 (2P1) | 42 | - | - | 160 | 177 | <177 | 177 | - |
| | W5 (2P3) | 36 | - | - | 160 | 204 | 177 | 204 | - |
| | W5 (2P3) | 42 | - | - | 170 | 204 | 177 | 204 | - |
| Outgoing Solids (%) | W1 (2P1) | 36 | - | 38.0 | 43.4 | 48.8 | 49.7 | 48.0 | 46.3 |
| | W1 (2P1) | 42 | - | - | 47.6 | 51.7 | 51.3 | 49.2 | 48.3 |
| | W5 (2P3) | 36 | - | 37.4 | 45.6 | 49.4 | 48.8 | 46.9 | 45.6 |
| | W5 (2P3) | 42 | - | - | 47.6 | 50.8 | 51.2 | 50.6 | 48.2 |
| IPC Density ^b (g/cc) | W1 (2P1) | 36 | 0.615 | 0.686 | 0.665 | 0.775 | 0.825 | 0.815 | 0.800 |
| | W1 (2P1) | 42 | 0.705 | - | 0.678 | 0.805 | 0.845 | 0.825 | 0.815 |
| | W5 (2P3) | 36 | 0.617 | 0.708 | 0.699 | 0.825 | 0.820 | 0.870 | 0.860 |
| | W5 (2P3) | 42 | 0.785 | - | 0.722 | 0.840 | 0.835 | 0.835 | 0.815 |
| GM STFI Index ^a (Nm/g) | W1 (2P1) | 36 | 26.1 | 26.4 | 30.1 | 27.8 | 28.0 | 25.4 | 29.3 |
| | W1 (2P1) | 42 | - | - | 29.5 | 27.2 | 30.0 | 26.9 | 29.3 |
| | W5 (2P3) | 36 | 25.7 | 28.7 | 31.6 | 30.9 | 29.8 | 30.0 | 32.5 |
| | W5 (2P3) | 42 | 28.6 | - | 32.0 | 30.2 | 30.3 | 30.8 | 31.0 |
| MD Ring Crush Index (Nm/g) | W1 (2P1) | 36 | 13.7 | 14.3 | - | - | 13.4 | 13.4 | 15.6 |
| | W1 (2P1) | 42 | - | - | - | - | 15.0 | 12.9 | 16.4 |
| | W5 (2P3) | 36 | 12.1 | 14.4 | - | - | 14.0 | 13.8 | - |
| | W5 (2P3) | 42 | 13.6 | - | - | - | 11.8 | 15.2 | 12.9 |
| CD Ring Crush Index (Nm/g) | W1 (2P1) | 36 | 7.4 | 8.4 | - | - | 10.7 | 9.6 | 11.2 |
| | W1 (2P1) | 42 | - | - | - | - | 10.6 | 8.6 | 11.2 |
| | W5 (2P3) | 36 | 7.2 | 9.2 | - | - | 11.5 | 11.0 | - |
| | W5 (2P3) | 42 | 8.3 | - | - | - | 9.9 | 11.5 | 9.8 |
| Top Side Bendtsen Rough. (ml/min) | W1 (2P1) | 36 | 1120 | 1580 | - | 1780 | 960 | 1080 | 1680 |
| | W1 (2P1) | 42 | 2460 | - | - | 1570 | 920 | 1180 | 1750 |
| | W5 (2P3) | 36 | 1450 | 1550 | - | 1460 | 880 | 1000 | 2020 |
| | W5 (2P3) | 42 | 1730 | - | - | 1410 | 910 | 1120 | 1830 |

a) The IPST STFI results are not a geometric mean (the sheets were hand-formed).

b) The IPST densities are from the ultrasonic tests.

c) Beloit pilot ENP press operated as an impulse dryer.

d) Cont = Control case, ingoing conditions.

e) Com = Commercial case, three-nip roll press.

STEAMING TEMPERATURE PROFILES

The objective of this part of the experiments was to try to induce a temperature gradient within the sheet during prestreaming. This would enable the MTS to better simulate actual commercial machine conditions.

After preparing the sheets with thermocouples, the sheets were steamed in the MTS nip. The B felt and heat shield were used, and the platen temperature was set at 200°C. Data collection was started, and then the steam was turned on. The first set of results is shown in Figures 40 through 44. One of the thermocouples failed during the embedding process; therefore, some of the temperatures show a flat line.

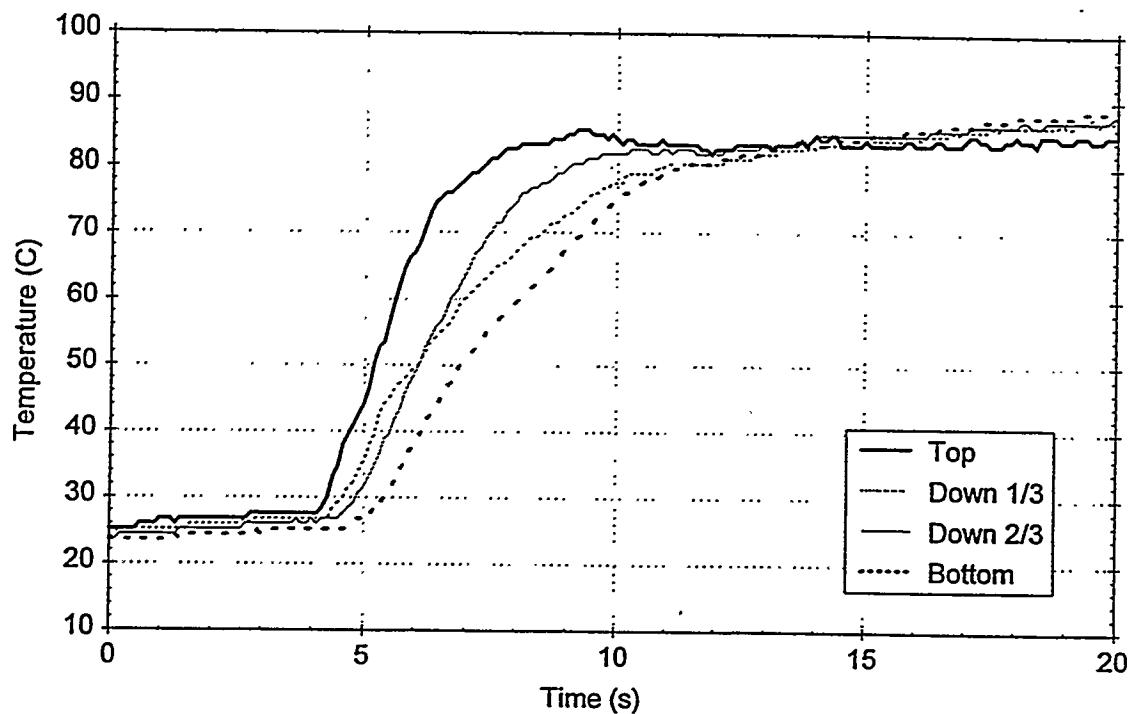


Figure 40. Furnish W13, 35% solids, repeat 1.

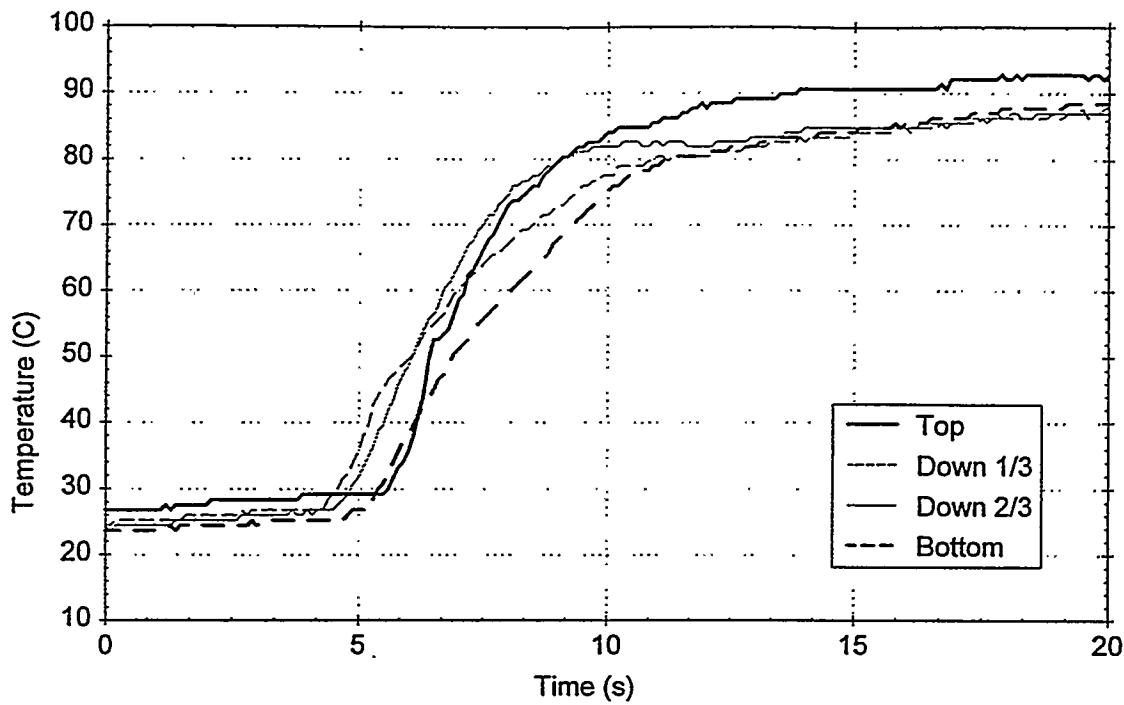


Figure 41. Furnish W13, 35% solids, repeat 2.

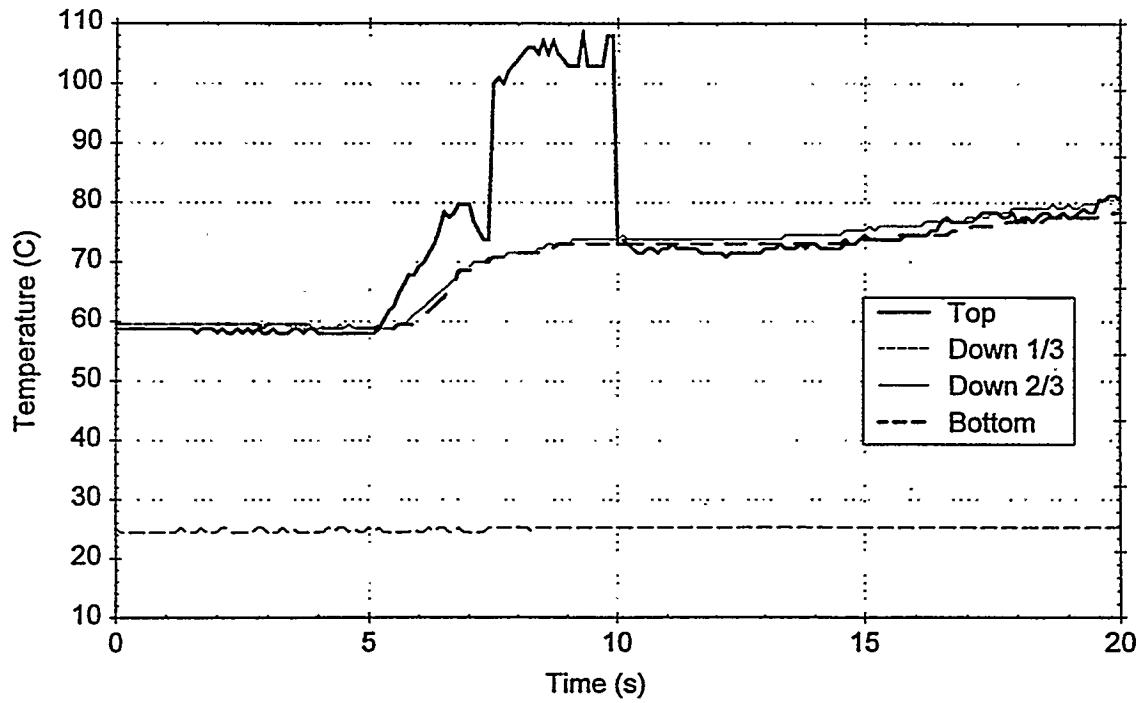


Figure 42. Furnish W14, 35% solids, repeat 1.

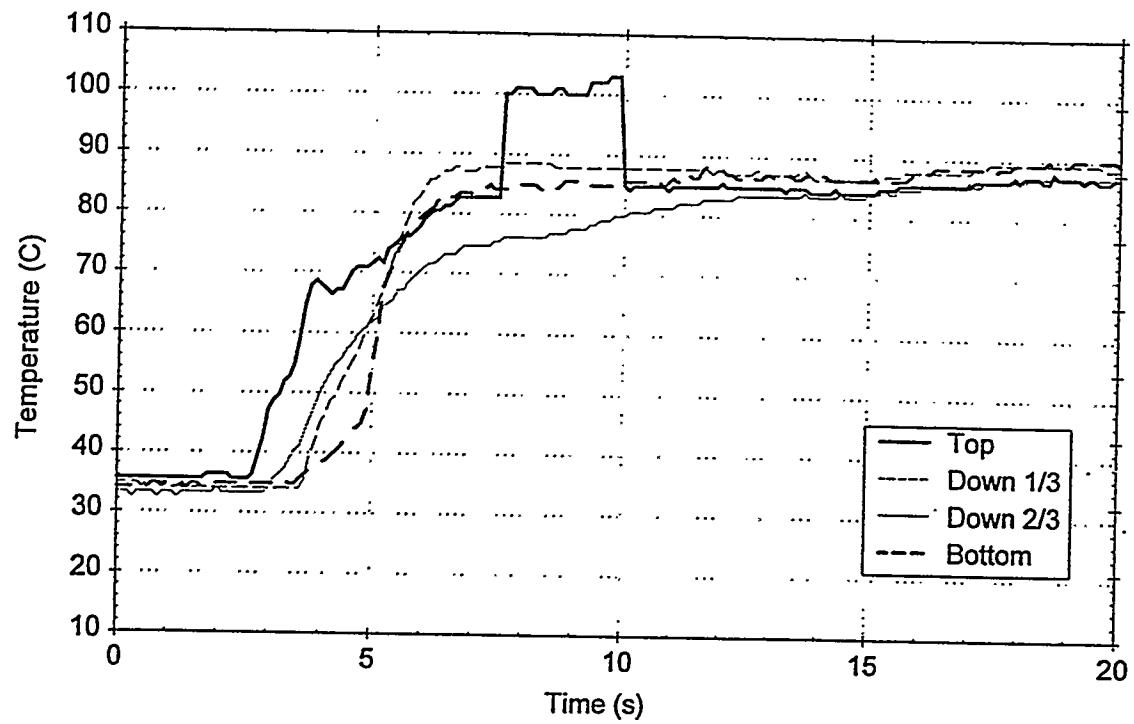


Figure 43. Furnish W14, 35% solids, repeat 2.

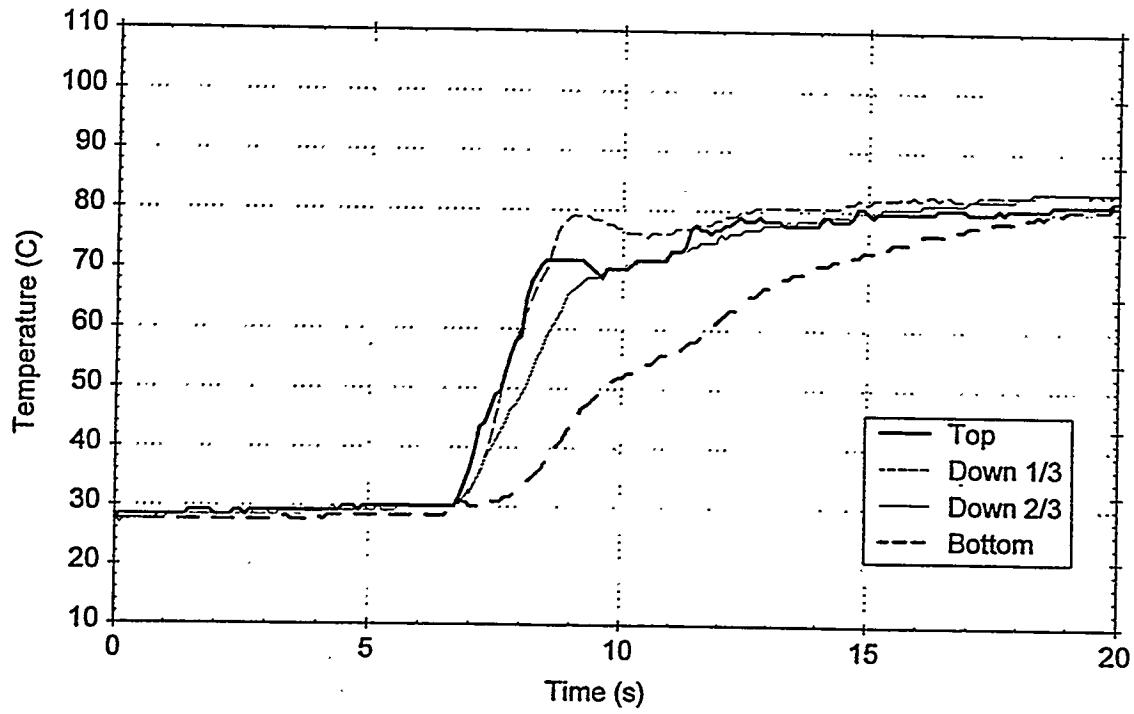


Figure 44. Furnish W14, 35% solids, repeat 3.

From the above results, it was observed that the top thermocouple was lifting from the sheet resulting in inaccurate temperature measurements. Because the felts have a curl, it is possible that enough steam was hitting the bottom of the sheet, reducing the

possible temperature gradient. For the next set of tests, the sheet was taped to the felt to prevent steaming from the bottom. Also, the top thermocouple was taped to the sheet with porous tape.

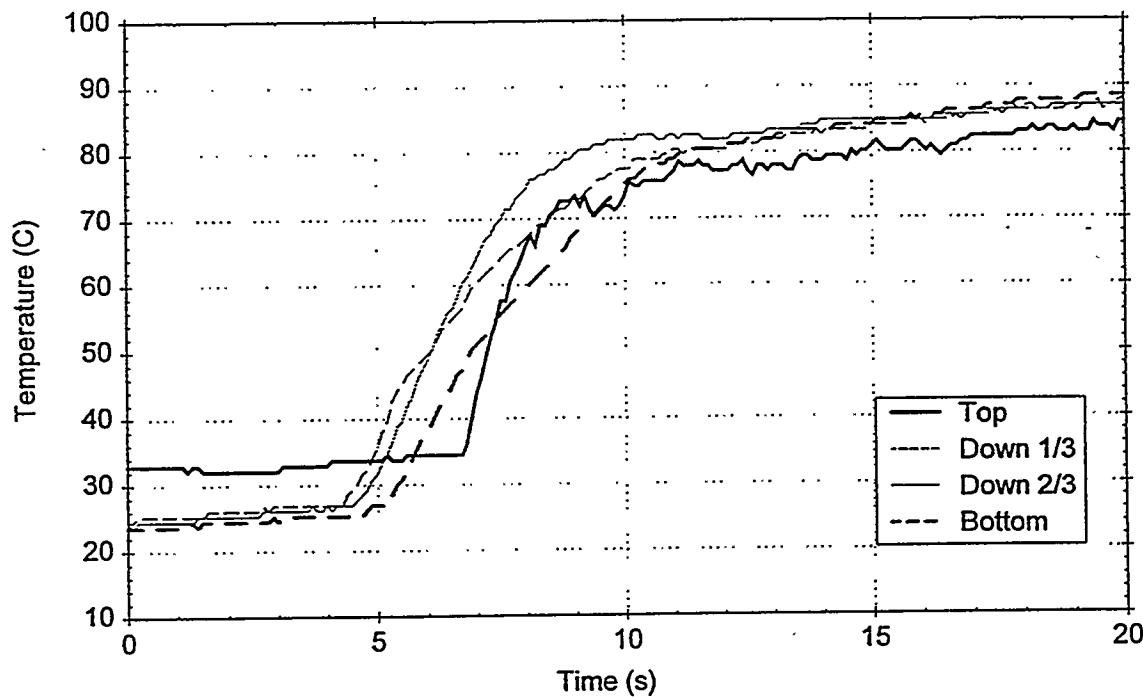


Figure 45. Furnish W13, 35% solids, sheet taped to felt, repeat 1.

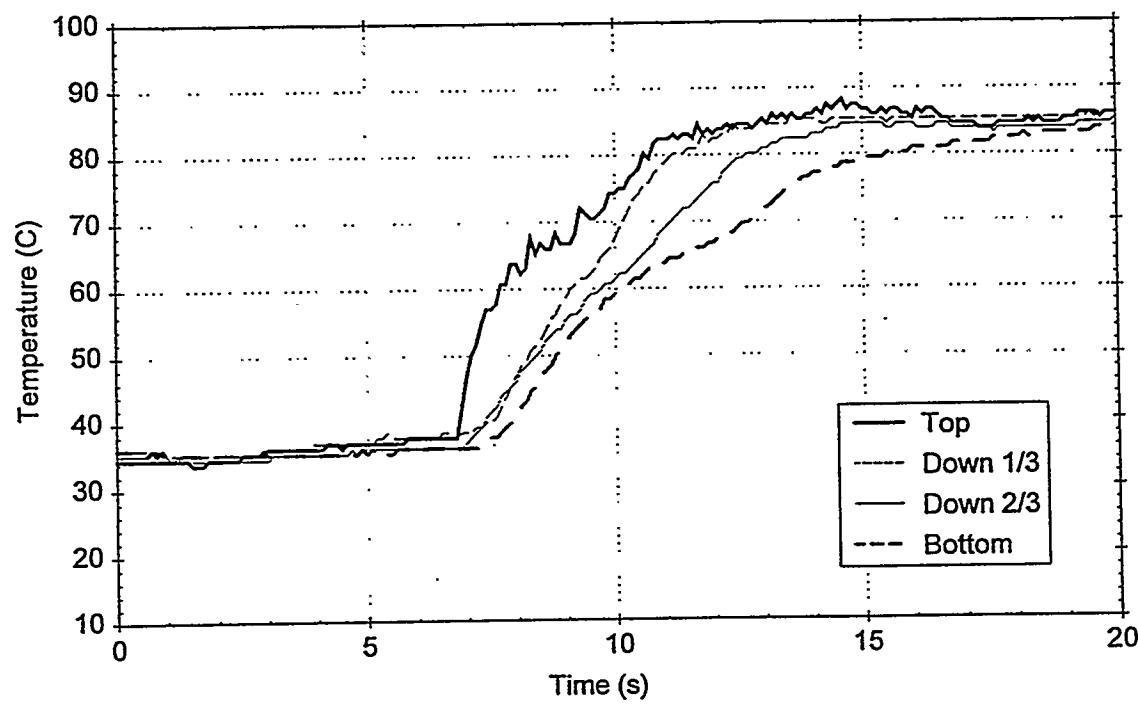


Figure 46. Furnish W13, 35% solids, sheet taped to felt, repeat 2.

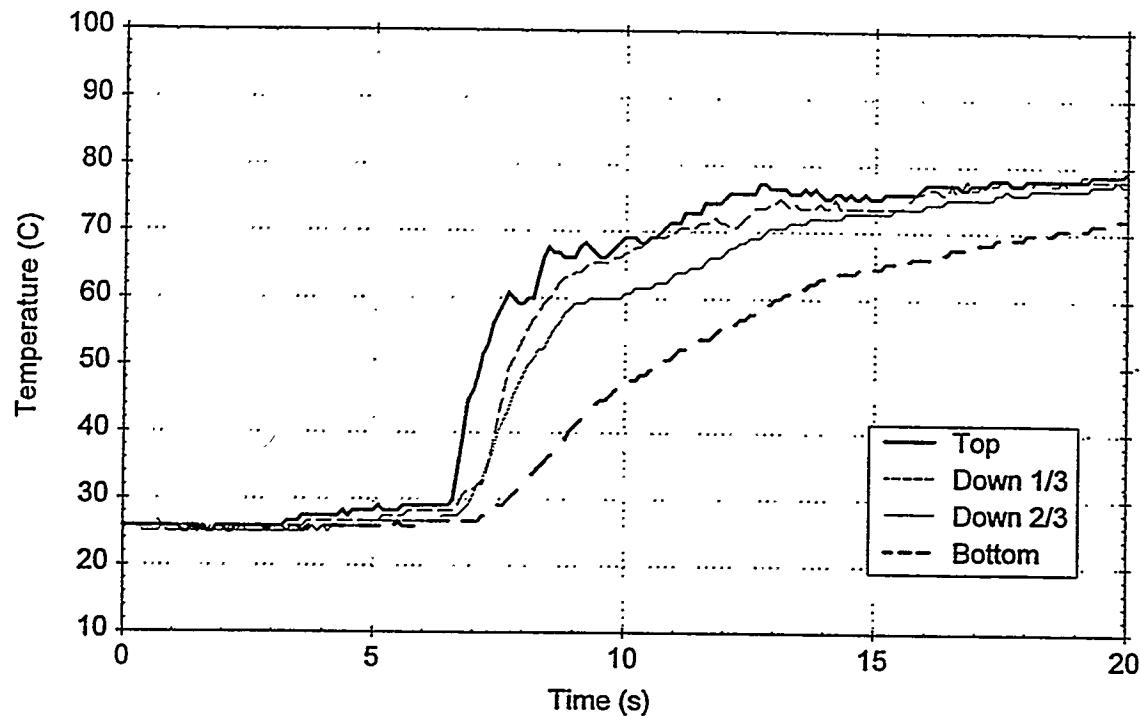


Figure 47. Furnish W14, 35% solids, sheet taped to felt, repeat 1.

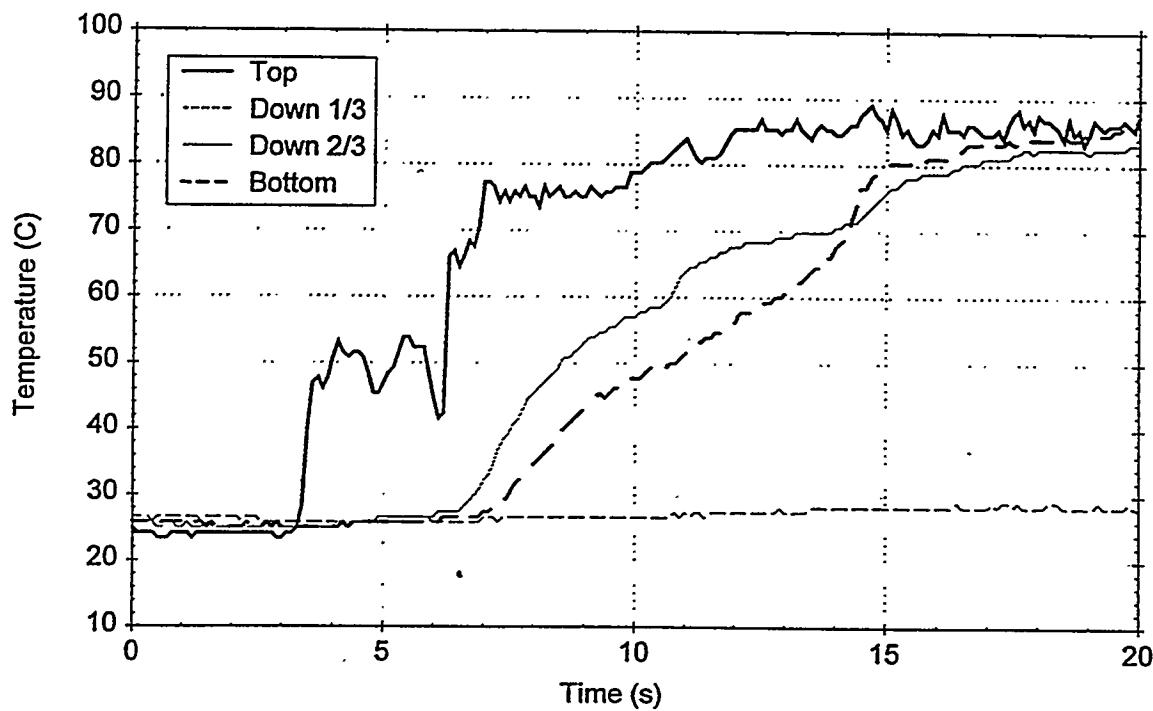


Figure 48. Furnish W14, 35% solids, sheet taped to felt, repeat 2.

For the last trial, a maximum gradient was formed by steaming only until the top surface reached 75°C. The result is shown in Figure 49.

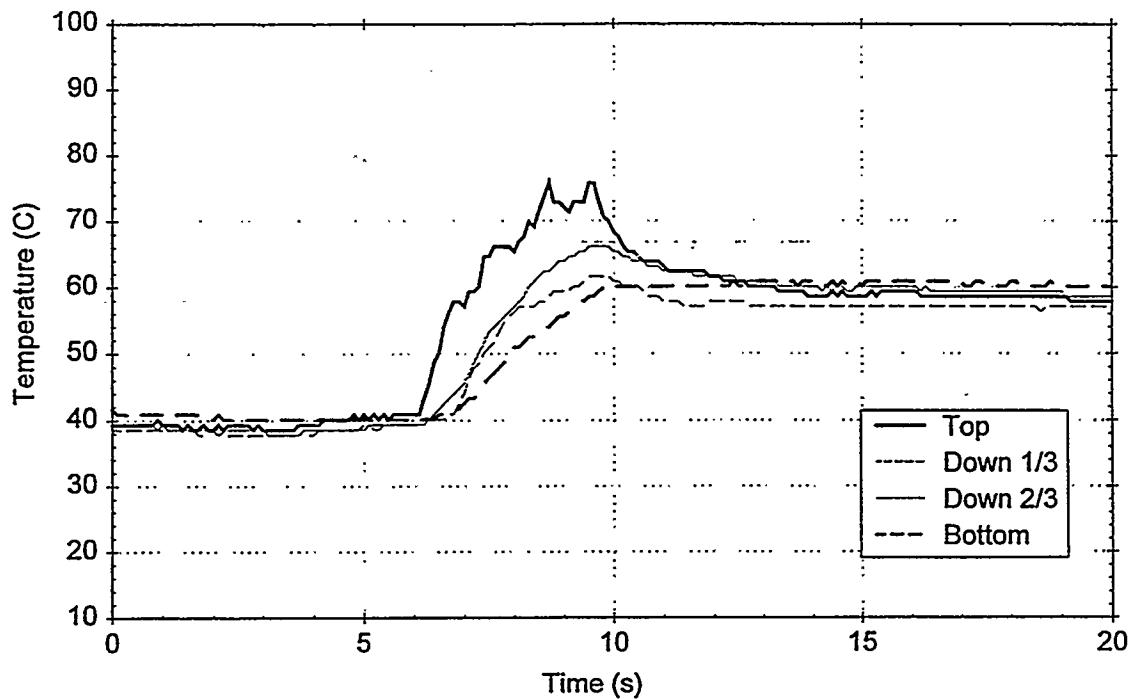


Figure 49. Furnish W14, 35% solids, sheet taped to felt, repeat 3.

Although a temperature gradient does exist during MTS steaming, the sheets reach equilibrium within two to three seconds after turning off the steam. Since it takes nine seconds for the MTS head to close during a hit, any temperature gradient will disappear before a hit can be made. It may be possible to reduce the closure time to about two seconds, but this is still too slow to test a significant temperature gradient.

CONCLUSIONS

The following conclusions can be drawn from this work.

- 1) There is no observable difference between mill-refined pulp and machine-formed paper, and laboratory-prepared pulp and laboratory-formed handsheets in regards to water permeability and impulse drying. Observed differences can be attributed to process variables such as refining level and prepressing.
- 2) As reported in previous experiments, specific surface can be minimized by minimally refining the pulp and prepressing the sheet as much as possible. Under the same processing conditions, pine has a lower specific surface than hardwood.
- 3) Permeability results are highly dependent on sheet preparation and preprocessing. For consistent results, it is important that preparation techniques be standardized and followed rigorously. An aging effect was observed that increases as the furnish becomes more closed.
- 4) IPST impulse drying results were consistent with previous experiments showing an increase in outgoing solids of 2-8 percentage points for the A platen and 5-7 percentage points for the C platen compared to double-felted pressing for 40-42% ingoing solids. STFI index values showed an increase of up to 3.5%. However, for 35% ingoing solids, impulse drying was no better than double-felted pressing.
- 5) Beloit impulse drying results had a less dramatic improvement in water removal (up to 3.8 percentage points) compared to double-felted pressing. They also had up to 15% improvement in ring crush and up to 56% decrease in Bendtsen roughness compared to double-felted pressing.
- 6) Although there was a bias in the results between IPST and Beloit, the trends were consistent, with the IPST results being the most conservative. Some of the differences may be a result of different testing conditions between laboratories.
- 7) Felt type and moisture levels have an observable effect on water removal, rewet, and sheet sticking. The best combination was the B felt at 16% moisture or less.
- 8) Present laboratory equipment cannot recreate expected machine presteaming temperature profiles in the sheet. Additional experiments are needed to determine the effect of different presteaming temperatures on impulse drying efficiency.

RECOMMENDATIONS FOR FUTURE WORK

This work was based on furnishes that simulated presently utilized commercial furnishes and a conservative nip loading. Therefore, the results indicate what could be achieved in a worst case scenario. The next phase of impulse drying work should use a less refined top ply to improve the sheet permeability. Also, recycled fiber should be evaluated.

It is not possible to directly test the effect of sheet temperature gradients on impulse drying with the MTS. The next set of experiments should look at the effect of different levels of presteam sheet temperature on impulse drying.

ACKNOWLEDGMENTS

The work reported was supported by the U.S. Department of Energy, Office of Industrial Programs, through Grant No. DE-FGO2-85CE40738. Its support is gratefully acknowledged.

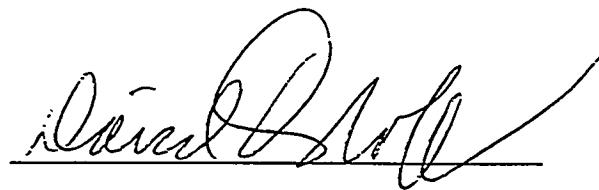
David White of Union Camp Corporation and Jere Crouse of Beloit Corporation were instrumental in the planning and execution of the experiments. Without their support, the experiments would not have been possible, and the authors are most grateful. The authors would also like to thank Andy Krause, Thomas Bales, Tim Patterson, and Barry Hojjatie of IPST for their assistance in performing the data acquisition and testing.

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APPENDIX A

The following tables contain the data that were used for analysis. The coded comments are explained below.

Delamination Codes

- 0: None
- 1: Small Blisters ($\leq 1\text{mm}$) < half the sheet
- 2: Medium Blisters (1mm to 1cm) < half the sheet
- 3: Small Blisters \geq half the sheet
- 4: Large Blisters ($> 1\text{cm}$) < half the sheet
- 5: Medium Blisters \geq half the sheet
- 6: Large Blisters \geq half the sheet
- 7: Split Sheet
- 9: Other (explain in Comments)

Rewet Codes

- 10: None
- 11: Slight Edge Rewet, < half the edge
- 12: Moderate Edge Rewet, \geq half the edge
- 13: Slight Rewet, < 1/3 of sheet
- 14: Moderate Rewet, 1/3 to 2/3 of sheet
- 15: Severe Rewet, > 2/3 of sheet
- 19: Other (explain in Comments)

Stick Codes

- 20: None
- 21: Slight Picking (surface disturbed)
- 22: Moderate Picking (a few fibers stuck to platen)
- 23: Severe Picking (many fibers stuck to platen)
- 25: Slight Sticking (sheet lifted, but released immediately, no picking)
- 26: Moderate Sticking (sheet stuck, but released on its own, may have picking)
- 27: Severe Sticking (sheet stuck, but could be easily peeled off, may have picking)
- 28: Extreme Sticking (sheet stuck, difficult to peel off)
- 29: Other (explain in Comments)

Table A1. Data with the IPST A platen and the Mill #1 couch trim.

| PLATEN SURFACE TEMP (C) | SAMPLE ID | SEM (MN/mkg) | SEM SEM (%CV) | IMPULSE (Mfa.s) | OD BASIS WEIGHT (g/m ²) | SHEET SOLIDS (%) | SHEET OUT (%) | FELT MOISTURE (%) | FELT MOISTURE (%) | FELT IN (%) | FELT OUT (%) | FELT GAIN/LOSS (%) | WATER REMOVED (Kg/m ²) | WATER REMOVED (%) | AVERAGE STFI INDEX (Nm/g) | US DENSITY (g/cm ³) | 95% C.I. (Nm/g) | DEFAM CODE | REWET CODE | STICK/PICK CODE | COMMENTS |
|-------------------------|-----------|--------------|---------------|-----------------|-------------------------------------|------------------|---------------|-------------------|-------------------|-------------|--------------|--------------------|------------------------------------|-------------------|---------------------------|---------------------------------|-----------------|------------|------------|-----------------|----------|
| | | | | | | | | | | | | | | | | | | | | | |
| A3PR11 | 127 | 0.078 | 10.26 | 0.145 | 179.8 | 34.9 | 46.3 | 0.702 | 16.9 | 19.1 | 27.0 | 0.126 | 0.507 | 0 | 10 | 28 | | | | | |
| A3PR12 | 127 | 0.085 | 15.29 | 0.142 | 186.4 | 44.5 | 44.6 | 0.488 | 16.4 | 17.8 | 24.2 | 0.091 | 0.517 | 0 | 10 | 27 | | | | | |
| A3PR13 | 126 | 0.082 | 28.05 | 0.141 | 174.0 | 38.7 | 44.8 | 0.490 | 17.5 | 18.0 | 10.2 | 0.085 | 0.548 | 0 | 10 | 28 | | | | | |
| A3PR14 | 162 | 0.059 | 16.95 | 0.138 | 175.5 | 34.3 | 45.3 | 0.708 | 11.0 | 15.1 | 46.3 | 0.124 | 0.489 | 6 | 10 | 28 | | | | | |
| A3PR15 | 162 | 0.098 | 8.16 | 0.140 | 177.7 | 34.8 | 42.8 | 0.537 | 16.0 | 18.4 | 38.8 | 0.096 | 0.639 | 2 | 10 | 27 | | | | | |
| A3PR16 | 151 | 0.089 | 14.61 | 0.144 | 177.9 | 35.2 | 43.4 | 0.539 | 17.2 | 20.0 | 46.4 | 0.098 | 0.549 | 4 | 10 | 27 | | | | | |
| A3PR17 | 206 | 0.090 | 26.67 | 0.137 | 183.5 | 34.6 | 42.3 | 0.524 | 16.6 | 19.9 | 53.3 | 0.096 | 0.556 | 6 | 13 | 20 | | | | | |
| A3PR18 | 202 | 0.102 | 27.45 | 0.138 | 184.6 | 36.2 | 44.6 | 0.520 | 16.9 | 19.8 | 46.9 | 0.096 | 0.578 | 0 | 13 | 20 | | | | | |
| A3PR19 | 203 | 0.097 | 23.71 | 0.138 | 173.0 | 34.1 | 41.0 | 0.498 | 19.7 | 22.1 | 45.4 | 0.086 | 0.550 | 0 | 14 | 20 | | | | | |
| A3PR10 | 301 | 0.098 | 19.79 | 0.134 | 180.6 | 35.5 | 50.0 | 0.813 | 17.1 | 21.7 | 51.5 | 0.147 | 0.572 | 2 | 10 | 26 | | | | | |
| A3PR11 | 304 | 0.101 | 14.85 | 0.131 | 183.7 | 38.3 | 49.1 | 0.724 | 16.8 | 20.8 | 46.5 | 0.133 | 0.625 | 2 | 13 | 26 | | | | | |
| A3PR12 | 304 | 0.095 | 23.16 | 0.131 | 183.1 | 37.1 | 51.8 | 0.767 | 17.2 | 21.2 | 45.1 | 0.140 | 0.616 | 6 | 12 | 20 | | | | | |
| A3PR13 | 288 | 0.131 | 22.14 | 0.133 | 188.7 | 35.8 | 45.4 | 0.580 | 17.3 | 20.2 | 41.6 | 0.111 | 0.643 | 2 | 13 | 27 | | | | | |
| A3PR14 | 254 | 0.120 | 24.17 | 0.142 | 185.8 | 36.5 | 47.4 | 0.629 | 17.7 | 21.9 | 57.5 | 0.117 | 0.636 | 9 | 13 | 20 | | | | | |
| A3PR15 | 251 | 0.119 | 25.21 | 0.138 | 183.5 | 36.0 | 46.9 | 0.644 | 13.2 | 17.3 | 50.4 | 0.118 | 0.622 | 2 | 13 | 20 | | | | | |

Table A2. Data with the IPST A platen.

| PLATEN ID | SAMPLE ID | SURFACE TEMP (C) | SEM (Mm/mg) | SEM %CV | OD BASIS IMPULSE (MPa.s) | OD BASIS WEIGHT (g/m ²) | SHEET SOLIDS IN (%) | | | SHEET MOISTURE OUT (%) | | | FELT MOISTURE OUT (%) | | | AVERAGE STFI INDEX (Nm/g) | | | STICK/PICK CODE COMMENTS | | |
|------------------------------------|-----------|------------------|-------------|---------|--------------------------|-------------------------------------|----------------------|---------------------------|--------|------------------------|---------|---|---------------------------------|------------|-----------------|---------------------------|------------|------------------|--------------------------|--|--|
| | | | | | | | SHEET SOLIDS OUT (%) | MOISTURE RATIO CHANGE (%) | IN (%) | MOISTURE IN (%) | OUT (%) | WATER REMOVED DENSITY (kg/cm ³) | US DENSITY (kg/m ²) | STFI INDEX | 95% C.I. (Nm/g) | DELAM CODE | REWET CODE | STICK/PICK CODE | COMMENTS | | |
| At Critical Temperature | | | | | | | | | | | | | | | | | | | | | |
| WIA1T16 | WIA1T16 | 170.5 | 0.186 | 11.29 | 0.1357 | 179.6 | 33.0 | 46.0 | 0.855 | 17.7 | 21.8 | 67.2 | 0.154 | 0.684 | 0 | 10 | 20 | | | | |
| WIA1T17 | WIA1T17 | 168.7 | 0.184 | 11.41 | 0.1367 | 174.0 | 31.6 | 46.8 | 1.024 | 17.5 | 22.8 | 72.9 | 0.176 | 0.671 | 30.185 | 1.769 | 0 | 10 | 20 | | |
| WIA1T19 | WIA1T19 | 165.8 | 0.188 | 10.64 | 0.1394 | 173.8 | 31.7 | 47.0 | 1.029 | 17.5 | 23.0 | 72.1 | 0.179 | 0.694 | 30.194 | 1.411 | 0 | 10 | 20 | | |
| Not At Critical Temperature | | | | | | | | | | | | | | | | | | | | | |
| WIA1T20 | WIA1T20 | 168.3 | 0.184 | 9.78 | 0.1367 | 176.9 | 32.3 | 47.9 | 1.011 | 16.8 | 21.8 | 65.4 | 0.179 | 0.696 | 0 | 10 | 20 | NO TRANSERA DATA | | | |
| WIA1T21 | WIA1T21 | 212.1 | 0.207 | 11.11 | 0.1384 | 173.4 | 31.8 | 49.4 | 1.120 | 16.8 | 22.7 | 71.6 | 0.194 | 0.723 | 0 | 10 | 20 | | | | |
| WIA1T24 | WIA1T24 | 212.1 | 0.184 | 4.89 | 0.1395 | 175.3 | 32.0 | 49.2 | 1.095 | 17.3 | 22.6 | 64.8 | 0.192 | 0.699 | 0 | 10 | 20 | | | | |
| WIA1T28 | WIA1T28 | 359.8 | 0.195 | 4.10 | 0.1353 | 176.9 | 32.3 | 52.9 | 1.203 | 17.1 | 20.5 | 36.5 | 0.213 | 0.691 | 0 | 10 | 20 | | | | |
| WIA1T39 | WIA1T39 | 358.9 | 0.199 | 3.02 | 0.1394 | 176.1 | 31.9 | 54.6 | 1.299 | 16.7 | 20.8 | 43.3 | 0.229 | 0.692 | 0 | 10 | 20 | | | | |
| WIA1T40 | WIA1T40 | 357.2 | 0.208 | 3.85 | 0.1406 | 180.8 | 32.8 | 53.5 | 1.181 | 16.8 | 20.7 | 45.4 | 0.214 | 0.699 | 0 | 10 | 20 | | | | |
| WIA1T44 | WIA1T44 | 207.0 | 0.186 | 4.84 | 0.1350 | 170.3 | 31.1 | 47.4 | 1.108 | 17.2 | 22.7 | 68.9 | 0.189 | 0.656 | 0 | 10 | 20 | STUCK ON CORNER | | | |
| WIA1T50 | WIA1T50 | 188.6 | 0.182 | 6.59 | 0.1395 | 173.0 | 31.5 | 47.7 | 1.080 | 16.8 | 22.7 | 74.8 | 0.187 | 0.703 | 0 | 10 | 20 | | | | |
| Delaminated | | | | | | | | | | | | | | | | | | | | | |
| WIA1T06 | WIA1T06 | 189.2 | 0.109 | 22.94 | 0.1411 | 170.3 | 31.1 | 47.5 | 1.108 | 16.7 | 22.6 | 72.3 | 0.189 | 0.845 | 6 | 10 | 29 | STUCK ON EDGE | | | |
| WIA1T08 | WIA1T08 | 188.3 | 0.162 | 9.88 | 0.1351 | 172.8 | 31.5 | 47.5 | 1.071 | 17.3 | 23.1 | 76.6 | 0.185 | 0.623 | 1 | 10 | 20 | | | | |
| WIA1T15 | WIA1T15 | 182.0 | 0.170 | 10.00 | 0.1405 | 172.8 | 31.6 | 48.0 | 0.988 | 16.5 | 21.4 | 68.7 | 0.171 | 0.668 | 2 | 10 | 20 | | | | |
| WIA1T29 | WIA1T29 | 212.9 | 0.194 | 9.28 | 0.1369 | 175.7 | 31.9 | 49.3 | 1.108 | 16.8 | 22.5 | 72.5 | 0.195 | 0.683 | 1 | 10 | 20 | | | | |
| WIA1T28 | WIA1T28 | 230.8 | 0.181 | 2.76 | 0.1383 | 171.9 | 31.1 | 50.2 | 1.219 | 16.8 | 23.1 | 70.9 | 0.210 | 0.712 | 2 | 10 | 20 | | | | |
| WIA1T29 | WIA1T29 | 232.5 | 0.183 | 15.85 | 0.1397 | 177.7 | 32.2 | 50.4 | 1.124 | 16.7 | 22.7 | 72.8 | 0.209 | 0.701 | 1 | 10 | 20 | | | | |
| WIA1T33 | WIA1T33 | 249.4 | 0.176 | 3.98 | 0.1381 | 171.7 | 31.2 | 50.5 | 1.222 | 16.2 | 22.8 | 69.0 | 0.188 | 0.686 | 1 | 10 | 20 | STUCK ON CORNER | | | |
| WIA1T42 | WIA1T42 | 212.1 | 0.129 | 27.91 | 0.1410 | 179.6 | 32.7 | 49.0 | 1.020 | 17.2 | 22.8 | 74.1 | 0.183 | 0.648 | 6 | 10 | 29 | STUCK ON CORNER | | | |
| WIA1T47 | WIA1T47 | 169.2 | 0.160 | 11.67 | 0.1374 | 173.4 | 31.8 | 48.3 | 1.080 | 17.3 | 23.0 | 76.7 | 0.187 | 0.703 | 2 | 10 | 20 | | | | |
| WIA1T48 | WIA1T48 | 180.3 | 0.172 | 8.72 | 0.1381 | 171.3 | 31.2 | 48.2 | 1.131 | 17.0 | 22.9 | 74.3 | 0.194 | 0.693 | 2 | 10 | 20 | | | | |
| WIA1T56 | WIA1T56 | 145.0 | 0.134 | 11.94 | 0.1379 | 177.5 | 32.3 | 48.7 | 0.950 | 17.0 | 22.7 | 78.5 | 0.169 | 0.678 | 27.256 | 0.844 | 0 | 10 | 20 | | |
| WIA1T65 | WIA1T65 | 169.7 | 0.118 | 31.36 | 0.1355 | 178.4 | 32.6 | 47.1 | 0.946 | 16.9 | 22.3 | 74.3 | 0.170 | 0.656 | 27.308 | 0.498 | 7 | 10 | 20 | | |
| WIA1T66 | WIA1T66 | 171.4 | 0.131 | 24.43 | 0.1366 | 171.9 | 31.3 | 48.7 | 1.051 | 17.2 | 23.1 | 76.0 | 0.181 | 0.662 | 25.182 | 0.978 | 6 | 10 | 20 | | |
| WIA1T67 | WIA1T67 | 170.5 | 0.112 | 32.14 | 0.1388 | 176.1 | 32.2 | 47.6 | 1.006 | 17.1 | 22.9 | 76.4 | 0.177 | 0.670 | 28.203 | 1.765 | 7 | 10 | 20 | | |
| At Critical Temperature | | | | | | | | | | | | | | | | | | | | | |
| WIA2T14 | WIA2T14 | 162.0 | 0.170 | 7.08 | 0.1380 | 177.1 | 39.0 | 50.4 | 0.576 | 16.7 | 19.3 | 59.2 | 0.102 | 0.690 | 0 | 10 | 20 | STEAMED 21 SEC | | | |
| WIA2T18 | WIA2T18 | 170.5 | 0.181 | 10.60 | 0.1371 | 181.0 | 39.6 | 49.6 | 0.508 | 17.4 | 19.7 | 68.6 | 0.092 | 0.729 | 0 | 10 | 20 | | | | |
| WIA2T20 | WIA2T20 | 170.5 | 0.165 | 4.85 | 0.1374 | 181.5 | 39.7 | 50.2 | 0.525 | 17.3 | 19.5 | 53.1 | 0.095 | 0.747 | 0 | 10 | 20 | | | | |
| Not At Critical Temperature | | | | | | | | | | | | | | | | | | | | | |
| WIA2T25 | WIA2T25 | 212.9 | 0.178 | 8.43 | 0.1376 | 188.0 | 40.9 | 52.3 | 0.530 | 17.2 | 19.4 | 52.8 | 0.059 | 0.731 | 0 | 10 | 20 | | | | |
| WIA2T26 | WIA2T26 | 228.2 | 0.184 | 8.15 | 0.1380 | 185.0 | 40.4 | 53.1 | 0.593 | 17.4 | 20.3 | 69.9 | 0.110 | 0.751 | 0 | 10 | 20 | | | | |
| WIA2T28 | WIA2T28 | 230.8 | 0.181 | 4.97 | 0.1368 | 184.1 | 40.1 | 53.0 | 0.508 | 17.1 | 19.9 | 59.7 | 0.112 | 0.717 | 0 | 10 | 20 | | | | |
| WIA2T33 | WIA2T33 | 254.5 | 0.180 | 3.68 | 0.1381 | 183.3 | 39.5 | 54.0 | 0.876 | 17.2 | 20.0 | 52.3 | 0.124 | 0.739 | 0 | 10 | 20 | | | | |
| WIA2T43 | WIA2T43 | 357.2 | 0.180 | 4.44 | 0.1372 | 180.0 | 39.2 | 57.4 | 0.907 | 16.9 | 20.1 | 51.4 | 0.145 | 0.745 | 0 | 10 | 20 | | | | |
| WIA2T48 | WIA2T48 | 144.2 | 0.155 | 7.10 | 0.1393 | 184.1 | 40.3 | 48.8 | 0.433 | 16.8 | 18.6 | 50.6 | 0.080 | 0.693 | 31.042 | 1.490 | 0 | 10 | 26 | | |
| WIA2T50 | WIA2T50 | 144.2 | 0.150 | 14.67 | 0.1375 | 181.5 | 39.8 | 48.6 | 0.456 | 17.5 | 19.5 | 58.1 | 0.083 | 0.699 | 0 | 10 | 29 | | | | |
| WIA2T56 | WIA2T56 | 173.1 | 0.167 | 8.38 | 0.1387 | 178.8 | 39.8 | 50.0 | 0.514 | 16.9 | 19.2 | 58.0 | 0.092 | 0.707 | 0 | 10 | 20 | | | | |
| Delaminated | | | | | | | | | | | | | | | | | | | | | |
| WIA2T07 | WIA2T07 | 188.3 | 0.135 | 28.89 | 0.1383 | 183.3 | 40.1 | 50.6 | 0.521 | 17.0 | 18.6 | 61.8 | 0.095 | 0.667 | 4 | 10 | 20 | | | | |
| WIA2T08 | WIA2T08 | 188.3 | 0.102 | 33.33 | 0.1388 | 180.8 | 39.6 | 50.3 | 0.538 | 17.1 | 19.7 | 61.9 | 0.097 | 0.648 | 6 | 10 | 20 | | | | |
| WIA2T10 | WIA2T10 | 187.5 | 0.117 | 13.37 | 0.1402 | 180.2 | 39.3 | 52.3 | 0.571 | 17.5 | 20.1 | 57.6 | 0.105 | 0.669 | 6 | 10 | 20 | | | | |
| WIA2T23 | WIA2T23 | 214.6 | 0.187 | 13.37 | 0.1402 | 180.4 | 40.1 | 52.1 | 0.641 | 17.3 | 20.4 | 63.0 | 0.116 | 0.744 | 2 | 10 | 20 | | | | |
| WIA2T29 | WIA2T29 | 230.8 | 0.174 | 13.22 | 0.1375 | 182.7 | 40.0 | 52.4 | 0.591 | 16.7 | 19.5 | 59.5 | 0.108 | 0.726 | 4 | 10 | 20 | | | | |
| WIA2T32 | WIA2T32 | 257.9 | 0.180 | 14.44 | 0.1384 | 184.1 | 40.1 | 53.7 | 0.634 | 17.1 | 19.9 | 54.9 | 0.117 | 0.724 | 2 | 10 | 20 | | | | |
| WIA2T38 | WIA2T38 | 292.7 | 0.204 | 2.94 | 0.1384 | 180.6 | 39.1 | 64.8 | 0.733 | 16.7 | 20.1 | 59.8 | 0.132 | 0.751 | 1 | 10 | 20 | | | | |
| WIA2T39 | WIA2T39 | 281.9 | 0.189 | 11.11 | 0.1390 | 183.9 | 39.8 | 55.1 | 0.694 | 16.8 | 19.9 | 54.0 | 0.128 | 0.749 | 1 | 10 | 20 | | | | |
| WIA2T44 | WIA2T44 | 355.5 | 0.186 | 5.91 | 0.1389 | 179.6 | 39.0 | 58.6 | 0.802 | 16.6 | 19.9 | 53.0 | 0.144 | 0.741 | 4 | 10 | 20 | | | | |
| WIA2T45 | WIA2T45 | 358.1 | 0.177 | 7.91 | 0.1389 | 179.0 | 39.5 | 58.5 | 0.823 | 16.8 | 19.8 | 48.6 | 0.147 | 0.727 | 1 | 10 | 20 | | | | |
| WIA2T52 | WIA2T52 | 187.5 | 0.162 | 12.35 | 0.1391 | 180.4 | 40.1 | 52.1 | 0.576 | 17.0 | 20.0 | 64.0 | 0.104 | 0.730 | 4 | 10 | 20 | | | | |
| WIA2T53 | WIA2T53 | 186.6 | 0.145 | 18.62 | 0.1394 | 180.2 | 39.8 | 51.1 | 0.556 | 16.7 | 19.3 | 59.2 | 0.100 | 0.716 | 4 | 10 | 20 | | | | |
| WIA2T54 | WIA2T54 | 179.8 | 0.163 | 11.04 | 0.1380 | 177.3 | 39.0 | 50.5 | 0.567 | 16.5 | 19.5 | 59.6 | 0.132 | 0.751 | 4 | 10 | 20 | | | | |
| WIA2T55 | WIA2T55 | 175.6 | 0.157 | 21.02 | 0.1377 | 181.7 | 40.4 | 51.0 | 0.515 | 16.9 | 19.9 | 54.0 | 0.128 | 0.749 | 6 | 10 | 20 | | | | |
| WIA2T57 | WIA2T57 | 173.1 | 0.171 | 7.02 | 0.1383 | 184.3 | 40.6 | 50.1 | 0.468 | 17.4 | 19.7 | 63.5 | 0.086 | 0.710 | 1 | 10 | 20 | | | | |
| WIA2T58 | WIA2T58 | 171.4 | 0.175 | 6.29 | 0.1372 | 178.4 | 39.5 | 50.0 | 0.532 | 17.1 | 19.7 | 61.5</td | | | | | | | | | |

Table A2 Continued. Data with the IPST A platen.

| PLATEN SAMPLE ID | SURFACE TEMP (C) | SEM (μm thick) | SEM %CV | IMPULSE (MPa.s) | OD BASIS WEIGHT (g/m ²) | SHEET SOLIDS IN OUT (%) | SHEET MOISTURE RATIO CHANGE (%) | FELT MOISTURE IN OUT (%) | FELT MOISTURE IN OUT (%) | WATER REMOVED (kg/m ²) | US DENSITY (g/cm ³) | AVERAGE STIFI INDEX (N/mm) | 95% C.I. CODE | REWET CODE | STICK/ PICK CODE | COMMENTS | | |
|------------------------------------|------------------------|-------------------|------------|--------------------|--|-------------------------------------|---|--------------------------------------|--------------------------------------|--|---------------------------------------|-------------------------------------|------------------|---------------|------------------------|----------|----|----|
| | | | | | | | | | | | | | | | | | | |
| WIA2T61 | 200.2 | 0.147 | 10.88 | 0.1379 | 180.0 | 39.8 | 52.0 | 0.987 | 17.2 | 20.0 | 60.9 | 0.106 | 0.724 | 6 | 10 | 20 | | |
| WIA2T62 | 200.2 | 0.178 | 8.38 | 0.1387 | 179.0 | 39.3 | 52.0 | 0.918 | 17.0 | 19.7 | 57.8 | 0.111 | 0.718 | 5 | 10 | 20 | | |
| WIA2T63 | 199.4 | 0.182 | 6.59 | 0.1394 | 180.4 | 39.6 | 51.7 | 0.950 | 17.4 | 20.2 | 59.8 | 0.107 | 0.707 | 2 | 10 | 20 | | |
| WIA2T64 | 201.1 | 0.130 | 24.62 | 0.1382 | 182.7 | 40.0 | 52.0 | 0.976 | 16.8 | 19.5 | 60.0 | 0.105 | 0.686 | 6 | 10 | 20 | | |
| WIA2T65 | 200.2 | 0.164 | 27.27 | 0.1381 | 179.8 | 39.6 | 52.0 | 0.901 | 16.7 | 19.5 | 60.2 | 0.108 | 0.703 | 4 | 10 | 20 | | |
| WIA2T66 | 162.9 | 0.142 | 14.79 | 0.1401 | 179.4 | 39.0 | 50.8 | 0.997 | 17.1 | 19.9 | 61.6 | 0.107 | 0.702 | 27.549 | 4 | 10 | 20 | |
| WIA2T68 | 162.0 | 0.137 | 27.74 | 0.1381 | 179.4 | 39.4 | 49.7 | 0.928 | 16.9 | 20.1 | 79.0 | 0.095 | 0.695 | 26.055 | 1.116 | 7 | 10 | 20 |
| WIA2T69 | 162.0 | 0.131 | 21.37 | 0.1385 | 179.2 | 39.3 | 51.2 | 0.989 | 17.0 | 20.1 | 68.4 | 0.108 | 0.663 | 25.810 | 2.249 | 4 | 10 | 20 |
| WIA2T72 | 162.7 | 0.162 | 10.49 | 0.1359 | 182.7 | 40.6 | 49.5 | 0.442 | 16.6 | 19.1 | 70.3 | 0.081 | 0.664 | 29.842 | 2.018 | 2 | 10 | 20 |
| At Critical Temperature | | | | | | | | | | | | | | | | | | |
| A3WIT05 | 144.2 | 0.136 | 8.82 | 0.1354 | 171.9 | 31.2 | 42.2 | 0.935 | 17.1 | 21.7 | 79.8 | 0.144 | 0.699 | 0 | 13 | 20 | | |
| WIA3T38 | 145.9 | 0.177 | 11.30 | 0.1418 | 173.6 | 31.5 | 43.2 | 0.957 | 17.5 | 21.8 | 72.4 | 0.149 | 0.711 | 31.176 | 1.844 | 0 | 13 | 20 |
| WIA3T39 | 144.2 | 0.155 | 18.06 | 0.1382 | 173.4 | 31.9 | 44.3 | 0.978 | 18.7 | 22.4 | 90.6 | 0.155 | 0.686 | 30.076 | 1.588 | 0 | 13 | 20 |
| WIA3T40 | 144.2 | 0.146 | 11.64 | 0.1384 | 173.8 | 32.2 | 43.8 | 0.930 | 17.2 | 21.7 | 76.2 | 0.144 | 0.662 | 28.921 | 1.576 | 0 | 10 | 20 |
| Delaminated | | | | | | | | | | | | | | | | | | |
| A3WIT06 | 188.6 | 0.131 | 23.66 | 0.1350 | 171.9 | 31.2 | 45.7 | 0.915 | 15.2 | 20.8 | 77.8 | 0.175 | 0.658 | 4 | 13 | 20 | | |
| A3WIT03 | 188.3 | 0.117 | 38.46 | 0.1380 | 177.1 | 32.0 | 44.9 | 0.986 | 17.7 | 22.2 | 73.3 | 0.169 | 0.659 | 0.575 | 6 | 13 | 20 | |
| A3WIT11 | 205.3 | 0.111 | 38.74 | 0.1393 | 173.4 | 31.4 | 45.7 | 0.998 | 17.1 | 22.8 | 83.6 | 0.173 | 0.627 | 6 | 14 | 20 | | |
| A3WIT12 | 203.6 | 0.127 | 26.77 | 0.1373 | 178.3 | 31.8 | 49.0 | 0.918 | 17.4 | 22.0 | 71.3 | 0.162 | 0.611 | 6 | 13 | 20 | | |
| A3WIT14 | 203.6 | 0.098 | 50.00 | 0.1387 | 176.9 | 31.9 | 46.1 | 0.963 | 15.4 | 20.7 | 78.0 | 0.170 | 0.571 | 6 | 13 | 20 | | |
| A3WIT15 | 202.8 | 0.093 | 47.31 | 0.1392 | 177.9 | 32.5 | 48.4 | 0.923 | 16.8 | 21.4 | 72.2 | 0.164 | 0.572 | 6 | 13 | 20 | | |
| A3WIT16 | 169.7 | 0.144 | 21.53 | 0.1356 | 171.5 | 31.0 | 42.6 | 0.982 | 17.3 | 22.0 | 79.0 | 0.151 | 0.629 | 4 | 13 | 20 | | |
| A3WIT17 | 169.7 | 0.140 | 8.57 | 0.1357 | 175.3 | 31.8 | 44.8 | 0.920 | 16.6 | 21.6 | 75.7 | 0.161 | 0.640 | 4 | 13 | 20 | | |
| A3WIT18 | 171.4 | 0.129 | 27.13 | 0.1371 | 181.0 | 32.7 | 43.0 | 0.932 | 17.3 | 21.4 | 75.6 | 0.133 | 0.606 | 4 | 13 | 20 | | |
| A3WIT20 | 173.1 | 0.116 | 30.17 | 0.1378 | 179.0 | 32.3 | 43.7 | 0.911 | 17.1 | 21.5 | 75.1 | 0.145 | 0.599 | 4 | 13 | 20 | | |
| A3WIT21 | 162.0 | 0.174 | 13.22 | 0.1357 | 171.7 | 31.0 | 43.8 | 0.943 | 16.9 | 22.1 | 81.3 | 0.162 | 0.691 | 4 | 13 | 20 | | |
| A3WIT23 | 162.0 | 0.146 | 19.86 | 0.1395 | 172.8 | 31.2 | 42.4 | 0.952 | 17.5 | 21.8 | 74.2 | 0.147 | 0.643 | 4 | 13 | 20 | | |
| A3WIT24 | 162.9 | 0.141 | 16.31 | 0.1354 | 179.8 | 32.4 | 43.8 | 0.902 | 16.0 | 20.6 | 75.9 | 0.144 | 0.629 | 4 | 13 | 20 | | |
| A3WIT25 | 164.6 | 0.150 | 19.33 | 0.1391 | 173.4 | 31.3 | 42.3 | 0.928 | 17.5 | 21.9 | 78.0 | 0.144 | 0.681 | 4 | 14 | 20 | | |
| A3WIT27 | 158.1 | 0.153 | 16.34 | 0.1388 | 172.2 | 31.2 | 42.4 | 0.924 | 16.8 | 21.1 | 77.4 | 0.145 | 0.629 | 1 | 13 | 20 | | |
| A3WIT29 | 154.4 | 0.163 | 9.20 | 0.1370 | 177.1 | 32.0 | 43.3 | 0.817 | 16.8 | 21.1 | 74.6 | 0.145 | 0.644 | 1 | 13 | 20 | | |
| A3WIT30 | 155.2 | 0.145 | 15.17 | 0.1375 | 161.2 | 32.8 | 41.5 | 0.843 | 17.1 | 20.5 | 69.8 | 0.117 | 0.619 | 2 | 13 | 20 | | |
| At Critical Temperature | | | | | | | | | | | | | | | | | | |
| A4WIT02 | 145.0 | 0.128 | 8.59 | 0.1372 | 178.6 | 39.0 | 46.6 | 0.947 | 17.5 | 19.5 | 62.8 | 0.074 | 0.647 | 0 | 10 | 20 | | |
| A4WIT21 | 160.3 | 0.162 | 9.26 | 0.1406 | 178.8 | 39.5 | 47.7 | 0.939 | 17.5 | 19.8 | 73.0 | 0.076 | 0.694 | 0 | 13 | 20 | | |
| WIA4T34 | 145.0 | 0.154 | 7.14 | 0.1416 | 182.1 | 39.7 | 48.4 | 0.956 | 17.5 | 20.0 | 76.8 | 0.083 | 0.692 | 29.468 | 1.389 | 0 | 10 | 20 |
| Not At Critical Temperature | | | | | | | | | | | | | | | | | | |
| A4WIT15 | 170.5 | 0.157 | 10.83 | 0.1389 | 182.3 | 39.6 | 47.7 | 0.949 | 17.1 | 19.3 | 68.6 | 0.076 | 0.662 | 0 | 10 | 20 | | |
| A4WIT16 | 173.1 | 0.145 | 8.28 | 0.1392 | 178.6 | 39.0 | 48.0 | 0.944 | 17.1 | 19.6 | 72.2 | 0.086 | 0.647 | 0 | 13 | 20 | | |
| WIA4T27 | 128.9 | 0.142 | 7.75 | 0.1374 | 180.8 | 39.4 | 47.6 | 0.936 | 17.2 | 20.7 | 111.0 | 0.079 | 0.709 | 28.955 | 1.213 | 0 | 10 | 20 |
| Delaminated | | | | | | | | | | | | | | | | | | |
| A4WIT05 | 188.6 | 0.128 | 40.31 | 0.1381 | 182.5 | 39.7 | 49.1 | 0.941 | 17.3 | 19.1 | 48.4 | 0.088 | 0.643 | 4 | 13 | 20 | | |
| A4WIT08 | 188.6 | 0.094 | 58.51 | 0.1387 | 180.6 | 39.4 | 49.6 | 0.954 | 18.1 | 20.7 | 67.6 | 0.095 | 0.598 | 6 | 13 | 20 | | |
| A4WIT07 | 188.6 | 0.101 | 55.45 | 0.1386 | 182.5 | 39.5 | 49.5 | 0.912 | 17.0 | 19.4 | 63.0 | 0.093 | 0.607 | 6 | 13 | 20 | | |
| A4WIT13 | 208.2 | 0.080 | 55.00 | 0.1391 | 180.0 | 39.0 | 50.2 | 0.974 | 18.6 | 19.6 | 64.1 | 0.103 | 0.598 | 6 | 13 | 20 | | |
| A4WIT17 | 173.1 | 0.161 | 15.63 | 0.1385 | 184.1 | 40.0 | 48.2 | 0.948 | 17.2 | 19.5 | 70.6 | 0.079 | 0.658 | 2 | 13 | 20 | | |
| A4WIT24 | 162.0 | 0.144 | 7.64 | 0.1389 | 181.0 | 40.8 | 49.4 | 0.942 | 17.2 | 19.6 | 66.4 | 0.085 | 0.681 | 1 | 13 | 20 | | |
| WIA4T37 | 161.2 | 0.104 | 15.38 | 0.1353 | 188.6 | 40.8 | 50.4 | 0.947 | 17.6 | 20.3 | 76.0 | 0.087 | 0.694 | 27.378 | 1.397 | 7 | 10 | 20 |
| WIA4T40 | 161.2 | 0.129 | 17.05 | 0.1369 | 180.6 | 39.5 | 49.0 | 0.949 | 17.3 | 19.5 | 33.3 | 0.088 | 0.683 | 4 | 12.5 | 20 | | |
| WIA4T41 | 161.2 | 0.096 | 31.25 | 0.1372 | 182.3 | 39.8 | 49.1 | 0.947 | 16.7 | 19.3 | 71.0 | 0.087 | 0.653 | 5 | 10 | 20 | | |
| WIA4T42 | 175.6 | 0.110 | 26.36 | 0.1401 | 183.9 | 40.1 | 50.5 | 0.913 | 16.4 | 19.7 | 83.3 | 0.094 | 0.696 | 7 | 10 | 20 | | |
| WIA4T43 | 176.5 | 0.101 | 34.95 | 0.1403 | 179.4 | 39.0 | 49.3 | 0.954 | 17.2 | 18.7 | 38.8 | 0.096 | 0.658 | 7 | 10 | 20 | | |
| WIA4T44 | 175.6 | 0.090 | 28.89 | 0.1344 | 181.2 | 39.5 | 49.3 | 0.960 | 17.0 | 18.8 | 50.7 | 0.091 | 0.657 | 25.560 | 1.401 | 7 | 10 | 20 |
| WIA4T45 | 174.8 | 0.090 | 38.89 | 0.1384 | 181.7 | 39.9 | 49.6 | 0.949 | 17.1 | 19.6 | 68.5 | 0.089 | 0.660 | 25.351 | 1.770 | 7 | 10 | 20 |
| At Critical Temperature | | | | | | | | | | | | | | | | | | |
| WSA1T33 | 174.8 | 0.162 | 8.64 | 0.1380 | 174.2 | 31.8 | 47.9 | 1.060 | 17.8 | 23.2 | 73.0 | 0.185 | 0.732 | 0 | 10 | 20 | | |
| WSA1T34 | 173.9 | 0.180 | 7.78 | 0.1383 | 176.9 | 32.4 | 46.8 | 0.951 | 16.9 | 22.1 | 70.6 | 0.168 | 0.742 | 0 | 10 | 20 | | |
| WSA1T38 | 174.8 | 0.179 | 7.82 | 0.1372 | 177.7 | 32.2 | 45.9 | 0.924 | 17.4 | 22.2 | 70.8 | 0.164 | 0.734 | 0 | 10 | 20 | | |

Table A2 Continued. Data with the IPST A platen.

| PLATEN ID | SAMPLE ID | PLATEN SURFACE TEMP (C) | SEM (MN/m²g) | SEM %GCV | OD BASIS IMPULSE (MPa.s) | SHEET SOLIDS (%) | SHEET MOISTURE OUT (%) | FELT MOISTURE IN (%) | FELT GAIN/LOSS (%) | AVERAGE STFI INDEX | WATER REMOVED (kg/m²) | US DENSITY (kg/cm³) | 95% C.I. DELAM CODE | REVET CODE | STICKY PICK CODE | COMMENTS |
|-----------------------------|-----------|-------------------------|--------------|----------|--------------------------|------------------|------------------------|----------------------|--------------------|--------------------|-----------------------|---------------------|---------------------|------------|------------------|----------|
| | | | | | | | | | | | | | | | | |
| W5A1T44 | 167.1 | 0.139 | 12.23 | 0.1387 | 174.2 | 31.6 | 47.5 | 1.060 | 17.5 | 23.4 | 79.9 | 0.185 | 0.687 | 29.621 | 2.603 | 0 |
| W5A1T45 | 168.3 | 0.171 | 12.28 | 0.1385 | 179.4 | 32.7 | 45.7 | 0.667 | 17.6 | 22.7 | 77.0 | 0.156 | 0.693 | 30.775 | 2.404 | 0 |
| W5A1T46 | 165.4 | 0.169 | 14.79 | 0.1371 | 180.0 | 32.8 | 46.1 | 0.881 | 17.4 | 22.3 | 71.9 | 0.159 | 0.691 | 32.728 | 3.052 | 0 |
| W5A1T47 | 174.8 | 0.172 | 8.72 | 0.1404 | 180.2 | 32.8 | 47.5 | 0.947 | 17.0 | 22.6 | 80.6 | 0.171 | 0.712 | 30.987 | 1.289 | 0 |
| W5A1T49 | 174.8 | 0.168 | 7.14 | 0.1380 | 174.4 | 31.8 | 45.9 | 0.987 | 16.8 | 21.9 | 73.0 | 0.169 | 0.694 | 32.584 | 1.481 | 0 |
| W5A1T50 | 174.8 | 0.168 | 7.14 | 0.1386 | 174.8 | 31.9 | 45.9 | 0.961 | 17.0 | 22.3 | 74.0 | 0.168 | 0.702 | 29.497 | 0.923 | 0 |
| Not At Critical Temperature | | | | | | | | | | | | | | | | |
| A1W5T04 | 226.9 | 0.178 | 8.43 | 0.1388 | 180.6 | 32.9 | 49.4 | 1.016 | 16.9 | 22.1 | 67.5 | 0.184 | 0.705 | 0 | 0 | 10 |
| W5A1T11 | 188.3 | 0.178 | 7.87 | 0.1345 | 170.9 | 31.2 | 47.9 | 1.121 | 17.3 | 23.1 | 73.7 | 0.192 | 0.725 | 0 | 0 | 10 |
| W5A1T14 | 188.3 | 0.163 | 7.98 | 0.1371 | 171.7 | 31.3 | 47.3 | 1.081 | 16.2 | 21.8 | 72.5 | 0.188 | 0.691 | 0 | 0 | 10 |
| W5A1T15 | 187.5 | 0.164 | 4.88 | 0.1370 | 174.0 | 31.6 | 47.1 | 1.039 | 17.1 | 22.4 | 68.8 | 0.181 | 0.686 | 0 | 0 | 10 |
| W5A1T16 | 211.3 | 0.185 | 8.65 | 0.1389 | 175.0 | 31.8 | 48.2 | 1.076 | 16.1 | 21.8 | 72.3 | 0.188 | 0.720 | 0 | 0 | 10 |
| W5A1T18 | 211.3 | 0.178 | 3.93 | 0.1383 | 172.8 | 31.4 | 48.0 | 1.101 | 17.1 | 22.6 | 69.3 | 0.180 | 0.700 | 0 | 0 | 10 |
| W5A1T17 | 211.3 | 0.182 | 7.14 | 0.1384 | 178.1 | 32.4 | 48.2 | 1.018 | 17.2 | 22.3 | 69.0 | 0.181 | 0.711 | 0 | 0 | 10 |
| W5A1T19 | 358.1 | 0.183 | 2.73 | 0.1361 | 177.9 | 32.5 | 53.0 | 1.193 | 17.3 | 21.0 | 40.3 | 0.212 | 0.735 | 0 | 0 | 10 |
| W5A1T28 | 358.1 | 0.149 | 8.05 | 0.1380 | 181.7 | 33.0 | 46.0 | 0.853 | 17.0 | 21.4 | 69.4 | 0.155 | 0.686 | 32.097 | 1.678 | 0 |
| W5A1T30 | 145.0 | 0.174 | 11.49 | 0.1377 | 177.1 | 32.2 | 46.8 | 0.975 | 17.3 | 22.8 | 75.4 | 0.173 | 0.708 | 29.841 | 0.663 | 0 |
| W5A1T66 | 188.3 | 0.174 | Definitiated | 0.162 | 6.17 | 0.1391 | 179.4 | 32.7 | 49.0 | 1.017 | 17.1 | 22.4 | 67.3 | 0.183 | 0.710 | 1 |
| A1W5T03 | 229.9 | 0.162 | 6.17 | 0.1391 | 179.4 | 32.7 | 49.0 | 1.005 | 16.8 | 21.9 | 64.9 | 0.182 | 0.694 | 1 | 1 | 10 |
| A1W5T05 | 229.1 | 0.157 | 8.28 | 0.1389 | 180.6 | 32.9 | 49.0 | 1.152 | 17.2 | 22.8 | 68.1 | 0.189 | 0.701 | 2 | 2 | 10 |
| W5A1T24 | 260.5 | 0.172 | 3.49 | 0.1381 | 172.8 | 31.6 | 49.7 | 1.058 | 18.9 | 22.4 | 68.5 | 0.193 | 0.707 | 2 | 2 | 10 |
| W5A1T25 | 257.9 | 0.191 | 3.14 | 0.1362 | 178.1 | 32.7 | 50.5 | 1.081 | 18.9 | 23.0 | 72.5 | 0.183 | 0.734 | 2 | 2 | 10 |
| W5A1T32 | 174.8 | 0.168 | 12.05 | 0.1389 | 170.6 | 31.2 | 47.0 | 1.075 | 17.5 | 23.0 | 71.2 | 0.188 | 0.726 | 4 | 4 | 10 |
| W5A1T38 | 201.9 | 0.171 | 19.30 | 0.1376 | 177.5 | 32.2 | 49.0 | 1.061 | 17.6 | 23.1 | 69.9 | 0.180 | 0.708 | 2 | 10 | 20 |
| W5A1T39 | 201.1 | 0.161 | 13.04 | 0.1380 | 170.5 | 31.2 | 47.9 | 1.114 | 17.6 | 22.4 | 78.0 | 0.173 | 0.721 | 31.751 | 2.170 | 4 |
| W5A1T52 | 187.5 | 0.168 | 8.33 | 0.1382 | 177.5 | 32.3 | 47.2 | 0.974 | 16.6 | 22.9 | 78.3 | 0.170 | 0.706 | 31.976 | 0.947 | 2 |
| W5A1T54 | 187.5 | 0.161 | 8.70 | 0.1393 | 177.1 | 32.2 | 46.5 | 0.958 | 17.4 | 23.2 | 78.7 | 0.173 | 0.694 | 28.255 | 4.518 | 4 |
| W5A1T55 | 188.6 | 0.148 | 27.03 | 0.1383 | 179.2 | 32.7 | 47.8 | 0.966 | 17.6 | 23.2 | 78.7 | 0.173 | 0 | 0 | 0 | 20 |
| At Critical Temperature | | | | | | | | | | | | | | | | |
| A2W5T54 | 212.1 | 0.192 | 5.21 | 0.1396 | 185.8 | 39.4 | 51.7 | 0.605 | 17.4 | 19.7 | 67.3 | 0.094 | 0.738 | 0 | 0 | 10 |
| W5A2T55 | 213.8 | 0.177 | 9.04 | 0.1378 | 180.8 | 39.4 | 51.7 | 0.606 | 17.0 | 20.2 | 65.7 | 0.110 | 0.729 | 0 | 0 | 10 |
| W5A2T56 | 209.8 | 0.173 | 8.09 | 0.1369 | 185.2 | 40.1 | 51.7 | 0.558 | 17.3 | 20.0 | 60.6 | 0.103 | 0.729 | 0 | 0 | 10 |
| W5A2T62 | 204.6 | 0.172 | 6.98 | 0.1384 | 184.3 | 40.0 | 51.4 | 0.651 | 16.4 | 19.4 | 63.5 | 0.113 | 0.730 | 0 | 0 | 10 |
| W5A2T78 | 198.0 | 0.168 | 6.63 | 0.1391 | 178.4 | 39.0 | 52.2 | 0.651 | 16.7 | 19.9 | 64.3 | 0.116 | 0.743 | 0 | 0 | 10 |
| W5A2T79 | 198.0 | 0.168 | 10.86 | 0.1365 | 186.0 | 40.8 | 52.2 | 0.535 | 17.3 | 19.9 | 60.4 | 0.100 | 0.750 | 0 | 0 | 10 |
| A2W5T01 | 231.6 | 0.175 | 10.86 | 0.1365 | 186.0 | 40.1 | 52.0 | 0.571 | 16.4 | 19.1 | 57.8 | 0.104 | 0.748 | 0 | 0 | 10 |
| A2W5T55 | 229.1 | 0.168 | 5.73 | 0.1375 | 182.7 | 39.2 | 61.5 | 0.611 | 16.6 | 19.2 | 54.4 | 0.109 | 0.720 | 0 | 0 | 10 |
| A2W5T05 | 230.8 | 0.167 | 5.73 | 0.1375 | 185.2 | 40.1 | 51.7 | 0.433 | 17.2 | 19.2 | 58.9 | 0.080 | 0.678 | 0 | 0 | 10 |
| W5A2T09 | 162.9 | 0.138 | 8.70 | 0.1378 | 183.7 | 40.2 | 48.7 | 0.406 | 16.8 | 19.7 | 53.8 | 0.075 | 0.693 | 0 | 0 | 10 |
| W5A2T10 | 162.0 | 0.162 | 5.68 | 0.1365 | 188.0 | 40.6 | 50.2 | 0.519 | 17.1 | 19.7 | 60.6 | 0.094 | 0.693 | 0 | 0 | 10 |
| W5A2T12 | 188.3 | 0.165 | 7.74 | 0.1386 | 181.9 | 39.8 | 50.2 | 0.549 | 16.6 | 19.2 | 64.9 | 0.110 | 0.739 | 0 | 0 | 10 |
| W5A2T19 | 254.6 | 0.201 | 5.97 | 0.1372 | 185.2 | 40.3 | 52.9 | 0.593 | 16.9 | 20.0 | 56.0 | 0.125 | 0.718 | 0 | 0 | 10 |
| W5A2T22 | 272.4 | 0.185 | 3.24 | 0.1383 | 177.7 | 39.0 | 53.9 | 0.705 | 16.9 | 20.1 | 68.5 | 0.118 | 0.727 | 0 | 0 | 10 |
| W5A2T24 | 272.4 | 0.198 | 3.03 | 0.1380 | 180.0 | 39.4 | 53.0 | 0.651 | 17.2 | 20.1 | 65.5 | 0.115 | 0.765 | 0 | 0 | 10 |
| W5A2T25 | 299.5 | 0.184 | 7.07 | 0.1406 | 185.4 | 40.5 | 54.1 | 0.623 | 16.9 | 19.2 | 47.6 | 0.128 | 0.735 | 0 | 0 | 10 |
| W5A2T29 | 287.0 | 0.177 | 3.95 | 0.1373 | 180.8 | 39.5 | 54.8 | 0.710 | 16.6 | 19.7 | 55.1 | 0.128 | 0.736 | 0 | 0 | 10 |
| W5A2T30 | 322.4 | 0.168 | 18.27 | 0.1403 | 184.8 | 40.4 | 54.7 | 0.645 | 16.9 | 19.3 | 47.9 | 0.119 | 0.708 | 0 | 0 | 10 |
| W5A2T32 | 322.4 | 0.182 | 0.32 | 0.1389 | 182.7 | 39.9 | 56.3 | 0.732 | 16.3 | 18.9 | 44.1 | 0.134 | 0.737 | 0 | 0 | 10 |
| W5A2T37 | 355.6 | 0.185 | 4.21 | 0.1382 | 178.8 | 39.8 | 56.7 | 0.748 | 17.0 | 19.4 | 42.4 | 0.135 | 0.732 | 0 | 0 | 10 |
| W5A2T38 | 350.4 | 0.192 | 6.21 | 0.1382 | 178.2 | 39.8 | 56.7 | 0.743 | 16.6 | 19.3 | 46.2 | 0.133 | 0.747 | 0 | 0 | 10 |
| W5A2T39 | 358.9 | 0.185 | 2.68 | 0.1392 | 178.6 | 39.3 | 55.5 | 0.743 | 16.6 | 19.2 | 50.7 | 0.079 | 0.752 | 33.056 | 2.048 | 0 |
| W5A2T40 | 358.9 | 0.197 | 13.79 | 0.1392 | 182.9 | 39.9 | 48.5 | 0.445 | 17.3 | 19.3 | 54.4 | 0.081 | 0.744 | 0 | 0 | 10 |
| W5A2T41 | 145.9 | 0.174 | 4.73 | 0.1359 | 180.4 | 38.7 | 48.4 | 0.453 | 17.5 | 19.6 | 60.1 | 0.082 | 0.720 | 34.815 | 2.376 | 0 |
| W5A2T43 | 144.2 | 0.169 | 4.73 | 0.1359 | 180.4 | 38.7 | 48.4 | 0.453 | 17.5 | 19.6 | 60.1 | 0.082 | 0.720 | 31.554 | 1.531 | 0 |
| W5A2T47 | 175.6 | 0.170 | 8.82 | 0.1378 | 178.0 | 39.3 | 49.6 | 0.527 | 17.4 | 20.1 | 63.9 | 0.094 | 0.718 | 0 | 0 | 10 |
| W5A2T68 | 145.0 | 0.142 | 10.58 | 0.1378 | 180.5 | 39.5 | 48.2 | 0.454 | 17.0 | 19.4 | 59.5 | 0.075 | 0.682 | 0 | 0 | 10 |
| W5A2T70 | 145.9 | 0.160 | 11.25 | 0.1385 | 183.7 | 40.4 | 48.5 | 0.411 | 17.3 | 19.2 | 59.5 | 0.075 | 0.685 | 33.524 | 0.743 | 0 |
| W5A2T71 | 171.4 | 0.197 | 4.57 | 0.1368 | 183.9 | 40.5 | 49.0 | 0.431 | 17.1 | 18.9 | 50.7 | 0.079 | 0.752 | 33.650 | 1.947 | 0 |
| W5A2T72 | 169.7 | 0.188 | 7.53 | 0.1370 | 179.6 | 39.6 | 48.7 | 0.470 | 17.1 | 19.2 | 57.1 | 0.084 | 0.721 | 32.611 | 2.376 | 0 |
| W5A2T73 | 170.6 | 0.172 | 6.82 | 0.1376 | 177.5 | 39.1 | 49.1 | 0.522 | 17.1 | 19.8 | 68.4 | 0.093 | 0.721 | 31.554 | 1.531 | 0 |
| W5A2T74 | 171.4 | 0.163 | 9.82 | 0.1402 | 180.2 | 39.6 | 51.1 | 0.570 | 16.3 | 19.5 | 69.2 | 0.103 | 0.701 | 29.731 | 2.042 | 0 |
| W5A2T77 | 188.3 | 0.152 | 11.84 | 0.1385 | 185.4 | 40.5 | 50.9 | 0.503 | 17.0 | 19.6 | 65.3 | 0.093 | 0.719 | 30.665 | 1.375 | 0 |
| W5A2T87 | | | | | | | | | | | | | | | | |

Table A2 Continued. Data with the IPST A platen.

| PLATEN ID | SURFACE TEMP (C) | SEM (MN/m²) | SEM %CV | IMPULSE (NPsq) | OD BASIS WEIGHT (g/m²) | SHEET SOLIDS IN (%) | SHEET MOISTURE OUT (%) | FELT MOISTURE IN (%) | FELT MOISTURE OUT (%) | WATER REMOVED (kg/m²) | US DENSITY (g/cm³) | AVERAGE STFI INDEX (Nm/g) | 95% C.I. DELAM CODE | REWET CODE | STICK/PICK CODE | COMMENTS |
|-----------------------------|------------------|-------------|---------|----------------|------------------------|---------------------|------------------------|----------------------|-----------------------|-----------------------|--------------------|---------------------------|---------------------|------------|-----------------|----------|
| | | | | | | | | | | | | | | | | |
| W542T68 | 187.5 | 0.186 | 12.37 | 0.1407 | 186.4 | 40.7 | 49.7 | 0.446 | 16.9 | 19.1 | 61.9 | 0.083 | 0.739 | 32.365 | 2.552 | 0 |
| Delaminated | | | | | | | | | | | | | | | | |
| W542T53 | 212.9 | 0.170 | 11.76 | 0.1404 | 179.0 | 39.1 | 51.1 | 0.602 | 17.1 | 20.1 | 67.1 | 0.108 | 0.735 | 2 | 10 | 20 |
| W542T60 | 207.9 | 0.163 | 14.11 | 0.1383 | 183.5 | 40.0 | 50.9 | 0.535 | 16.9 | 19.4 | 58.3 | 0.098 | 0.731 | 4 | 10 | 20 |
| W542T63 | 219.7 | 0.172 | 16.12 | 0.1398 | 176.9 | 39.3 | 52.0 | 0.617 | 17.3 | 19.7 | 52.3 | 0.109 | 0.738 | 4 | 10 | 20 |
| W542T81 | 205.3 | 0.174 | 9.77 | 0.1381 | 178.8 | 39.1 | 49.9 | 0.556 | 17.2 | 19.7 | 59.4 | 0.099 | 0.744 | 31.020 | 2.371 | 4 |
| W542T82 | 205.3 | 0.175 | 8.57 | 0.1378 | 181.0 | 39.7 | 50.7 | 0.550 | 16.9 | 19.7 | 65.3 | 0.100 | 0.719 | 31.540 | 1.199 | 2 |
| At Critical Temperature | | | | | | | | | | | | | | | | |
| W543T31 | 145.0 | 0.150 | 8.67 | 0.1354 | 179.0 | 32.4 | 45.2 | 0.871 | 16.9 | 23.0 | 99.8 | 0.156 | 0.686 | 0.690 | 0 | 10 |
| W543T52 | 161.2 | 0.162 | 14.81 | 0.1358 | 177.9 | 32.3 | 45.4 | 0.890 | 17.0 | 22.6 | 99.4 | 0.158 | 0.705 | 33.191 | 0.896 | 0 |
| W543T54 | 162.9 | 0.163 | 11.04 | 0.1395 | 174.8 | 31.7 | 46.2 | 0.993 | 17.1 | 22.9 | 83.4 | 0.174 | 0.707 | 31.065 | 1.742 | 0 |
| Not At Critical Temperature | | | | | | | | | | | | | | | | |
| A3W5T09 | 171.4 | 0.154 | 11.69 | 0.1368 | 180.6 | 32.8 | 42.6 | 0.718 | 17.2 | 21.3 | 79.6 | 0.130 | 0.685 | 0 | 13 | 20 |
| A3W5T12 | 189.2 | 0.158 | 11.39 | 0.1359 | 177.3 | 32.2 | 43.3 | 0.794 | 16.7 | 21.1 | 78.7 | 0.141 | 0.676 | 0 | 13 | 20 |
| A3W5T15 | 188.3 | 0.167 | 13.77 | 0.1376 | 175.0 | 31.8 | 44.3 | 0.893 | 16.1 | 21.1 | 77.5 | 0.158 | 0.688 | 0 | 13 | 20 |
| A3W5T16 | 205.3 | 0.173 | 10.98 | 0.1390 | 175.7 | 32.2 | 43.4 | 0.804 | 17.0 | 21.9 | 87.7 | 0.141 | 0.686 | 0 | 14 | 20 |
| A3W5T17 | 206.2 | 0.161 | 9.94 | 0.1382 | 177.9 | 32.4 | 43.8 | 0.807 | 17.0 | 21.6 | 78.3 | 0.144 | 0.682 | 0 | 13 | 20 |
| A3W5T19 | 208.2 | 0.167 | 15.57 | 0.1377 | 180.4 | 32.7 | 44.3 | 0.798 | 16.8 | 21.3 | 78.7 | 0.144 | 0.687 | 0 | 13 | 20 |
| A3W5T20 | 207.0 | 0.166 | 16.03 | 0.1378 | 178.1 | 31.9 | 43.5 | 0.839 | 16.9 | 20.8 | 64.5 | 0.148 | 0.672 | 0 | 13 | 20 |
| A3W5T25 | 229.9 | 0.162 | 11.54 | 0.1394 | 177.5 | 32.4 | 45.9 | 0.910 | 17.6 | 22.3 | 72.5 | 0.161 | 0.677 | 0 | 13 | 20 |
| Delaminated | | | | | | | | | | | | | | | | |
| A3W5T18 | 205.3 | 0.168 | 13.25 | 0.1369 | 178.8 | 32.6 | 45.1 | 0.856 | 17.1 | 22.0 | 81.6 | 0.153 | 0.684 | 2 | 13 | 20 |
| A3W5T22 | 227.4 | 0.181 | 6.08 | 0.1378 | 179.8 | 33.0 | 47.1 | 0.909 | 15.6 | 20.6 | 72.6 | 0.163 | 0.687 | 1 | 13 | 20 |
| A3W5T23 | 229.1 | 0.163 | 7.38 | 0.1359 | 180.9 | 32.9 | 46.4 | 0.887 | 14.6 | 19.7 | 73.7 | 0.160 | 0.671 | 1 | 10 | 29 |
| W543T38 | 188.3 | 0.106 | 31.13 | 0.1364 | 173.4 | 31.5 | 47.8 | 1.089 | 16.7 | 22.7 | 80.4 | 0.189 | 0.659 | 26.391 | 1.485 | 7 |
| W543T38 | 187.5 | 0.093 | 23.66 | 0.1411 | 181.2 | 32.8 | 48.4 | 0.984 | 17.2 | 22.7 | 79.8 | 0.178 | 0.677 | 26.847 | 1.376 | 7 |
| W543T39 | 186.6 | 0.081 | 24.89 | 0.1372 | 174.8 | 31.8 | 48.5 | 1.102 | 17.1 | 23.3 | 82.8 | 0.183 | 0.681 | 1.305 | 7 | 10 |
| W543T40 | 188.6 | 0.082 | 31.71 | 0.1378 | 173.4 | 31.4 | 48.8 | 1.138 | 16.8 | 23.1 | 81.1 | 0.197 | 0.653 | 26.033 | 1.919 | 7 |
| W543T46 | 162.0 | 0.116 | 23.28 | 0.1408 | 177.7 | 32.1 | 45.9 | 0.939 | 17.4 | 23.4 | 91.5 | 0.167 | 0.684 | 30.058 | 0.871 | 6 |
| W543T53 | 162.0 | 0.145 | 17.93 | 0.1392 | 172.2 | 31.2 | 45.6 | 1.014 | 17.2 | 23.9 | 97.8 | 0.175 | 0.688 | 31.662 | 2.633 | 4 |
| W543T58 | 169.7 | 0.114 | 42.11 | 0.1378 | 176.8 | 31.9 | 45.4 | 0.929 | 16.8 | 22.7 | 92.7 | 0.184 | 0.685 | 27.487 | 1.010 | 7 |
| W543T59 | 170.5 | 0.142 | 17.61 | 0.1400 | 173.8 | 31.3 | 46.3 | 1.038 | 16.8 | 23.5 | 93.5 | 0.180 | 0.682 | 32.158 | 1.232 | 4 |
| At Critical Temperature | | | | | | | | | | | | | | | | |
| AAW5T01 | 145.0 | 0.146 | 12.33 | 0.1395 | 178.1 | 39.0 | 46.7 | 0.424 | 17.8 | 19.8 | 65.5 | 0.076 | 0.718 | 0.718 | 0 | 13 |
| W544T32 | 145.9 | 0.155 | 18.71 | 0.1402 | 187.0 | 40.4 | 48.5 | 0.414 | 16.8 | 19.7 | 88.4 | 0.077 | 0.726 | 31.955 | 0.908 | 0 |
| Not At Critical Temperature | | | | | | | | | | | | | | | | |
| AAW5T18 | 205.3 | 0.165 | 7.88 | 0.1369 | 181.2 | 39.4 | 48.6 | 0.479 | 16.8 | 19.3 | 67.5 | 0.087 | 0.691 | 0 | 13 | 20 |
| AAW5T19 | 205.3 | 0.167 | 8.98 | 0.1358 | 180.0 | 39.2 | 48.0 | 0.471 | 17.1 | 19.4 | 65.3 | 0.085 | 0.689 | 0 | 19 | 20 |
| AAW5T24 | 226.5 | 0.170 | 7.06 | 0.1361 | 185.6 | 40.5 | 50.6 | 0.493 | 17.2 | 19.6 | 64.6 | 0.091 | 0.709 | 0 | 10 | 20 |
| Delaminated | | | | | | | | | | | | | | | | |
| AAW5T15 | 188.3 | 0.145 | 12.41 | 0.1376 | 182.3 | 39.7 | 47.8 | 0.425 | 17.2 | 19.5 | 73.7 | 0.078 | 0.684 | 1 | 13 | 20 |
| AAW5T16 | 204.5 | 0.165 | 12.12 | 0.1391 | 179.0 | 39.1 | 48.8 | 0.508 | 17.2 | 20.1 | 79.9 | 0.091 | 0.707 | 27.489 | 2.303 | 1 |
| W544T07 | 175.6 | 0.135 | 23.70 | 0.1365 | 185.4 | 40.3 | 50.5 | 0.500 | 16.9 | 20.1 | 85.3 | 0.093 | 0.715 | 29.789 | 1.664 | 4 |
| W544T40 | 174.8 | 0.131 | 22.90 | 0.1385 | 185.8 | 40.6 | 49.7 | 0.452 | 17.4 | 20.1 | 79.9 | 0.085 | 0.707 | 29.789 | 1.664 | 6 |

Table A3. Data with the IPST C platen.

| PLATEN SAMPLE ID | SURFACE TEMP (C) | SEM (MN/m²g) | SEM %CV | OD BASIS WEIGHT (g/m²) | SHEET SOLIDS IN (%) | IMPULSE (MPa.s) | SHEET SOLIDS OUT (%) | FELT MOISTURE RATIO CHANGE (%) | FELT MOISTURE OUT (%) | FELT GAIN/ LOSS (%) | WATER REMOVED (kg/m²) | US DENSITY (g/cm³) | AVERAGE STI INDEX (Nm/g) | 95% C.I. CODE | DELAM CODE | REWET CODE | STICK/ PICK CODE | COMMENTS |
|-----------------------------|------------------------|-----------------|------------|---------------------------------|------------------------------|--------------------|-------------------------------|--|--------------------------------|------------------------------|-----------------------------|--------------------------|-----------------------------------|------------------|---------------|---------------|------------------------|----------|
| | | | | | | | | | | | | | | | | | | |
| W1C1T08 | 194.4 | 0.168 | 8.33 | 0.1397 | 122.2 | 34.2 | 46.6 | 0.781 | 16.6 | 20.4 | 65.3 | 0.134 | 0.675 | 30.279 | 1.666 | 0 | 10 | 20 |
| W1C1T12 | 206.7 | 0.162 | 10.49 | 0.1363 | 181.7 | 36.0 | 46.4 | 0.620 | 17.2 | 20.1 | 59.3 | 0.113 | 0.664 | 28.140 | 1.519 | 0 | 10 | 20 |
| Net At Critical Temperature | | | | | | | | | | | | | | | | | | |
| W1C1T10 | 192.5 | 0.175 | 8.00 | 0.1360 | 173.8 | 34.7 | 46.3 | 0.723 | 16.9 | 20.1 | 59.8 | 0.126 | 0.677 | 30.014 | 0.854 | 0 | 10 | 20 |
| W1C1T18 | 183.1 | 0.155 | 4.52 | 0.1360 | 177.9 | 35.4 | 45.5 | 0.627 | 17.3 | 20.3 | 62.3 | 0.111 | 0.665 | 30.898 | 1.470 | 0 | 10 | 20 |
| W1C1T19 | 184.0 | 0.170 | 9.41 | 0.1393 | 178.4 | 35.3 | 45.4 | 0.632 | 17.1 | 19.7 | 54.6 | 0.113 | 0.659 | 30.830 | 1.110 | 0 | 10 | 20 |
| W1C1T20 | 184.9 | 0.162 | 8.64 | 0.1385 | 174.4 | 34.6 | 45.1 | 0.678 | 16.7 | 19.8 | 58.2 | 0.118 | 0.652 | 30.798 | 1.032 | 0 | 10 | 20 |
| W1C1T23 | 169.8 | 0.155 | 12.80 | 0.1362 | 181.0 | 35.8 | 44.8 | 0.560 | 16.9 | 19.5 | 56.2 | 0.101 | 0.629 | 28.542 | 0.881 | 0 | 10 | 20 |
| W1C1T25 | 168.9 | 0.160 | 11.25 | 0.1393 | 177.3 | 35.2 | 45.7 | 0.648 | 17.1 | 20.3 | 68.7 | 0.115 | 0.633 | 28.367 | 0.453 | 0 | 10 | 20 |
| Delaminated | | | | | | | | | | | | | | | | | | |
| W1C1T15 | 207.6 | 0.145 | 15.86 | 0.1973 | 179.8 | 35.5 | 47.1 | 0.694 | 16.4 | 19.8 | 63.6 | 0.125 | 0.675 | 28.153 | 3.015 | 6 | 10 | 20 |
| At Critical Temperature | | | | | | | | | | | | | | | | | | |
| W1C2T16 | 183.1 | 0.165 | 8.48 | 0.1356 | 176.5 | 41.9 | 50.4 | 0.399 | 17.2 | 18.9 | 57.5 | 0.070 | 0.699 | 29.255 | 0.694 | 0 | 10 | 20 |
| W1C2T18 | 183.1 | 0.167 | 10.18 | 0.1385 | 180.2 | 42.9 | 50.3 | 0.341 | 17.5 | 18.9 | 51.7 | 0.061 | 0.698 | 28.892 | 1.355 | 0 | 10 | 20 |
| Not At Critical Temperature | | | | | | | | | | | | | | | | | | |
| W1C2T22 | 147.2 | 0.174 | 8.05 | 0.1405 | 178.2 | 42.7 | 48.8 | 0.295 | 17.1 | 18.5 | 56.8 | 0.053 | 0.700 | 31.425 | 1.620 | 0 | 10 | 20 |
| Delaminated | | | | | | | | | | | | | | | | | | |
| W1C2T07 | 192.5 | 0.162 | 18.52 | 0.1394 | 177.9 | 42.6 | 50.3 | 0.359 | 17.2 | 18.7 | 50.2 | 0.084 | 0.700 | 30.055 | 1.543 | 1 | 10 | 20 |
| W1C2T08 | 192.5 | 0.147 | 16.33 | 0.1412 | 174.4 | 41.4 | 50.9 | 0.453 | 17.6 | 19.3 | 52.9 | 0.079 | 0.692 | 28.799 | 3.260 | 4 | 10 | 20 |
| At Critical Temperature | | | | | | | | | | | | | | | | | | |
| W5C1T11 | 212.3 | 0.175 | 13.71 | 0.1372 | 177.7 | 35.3 | 46.3 | 0.671 | 16.4 | 19.6 | 61.0 | 0.119 | 0.716 | 29.475 | 1.752 | 0 | 10 | 20 |
| W5C1T12 | 213.3 | 0.168 | 11.31 | 0.1382 | 180.8 | 36.0 | 46.2 | 0.619 | 16.9 | 19.9 | 63.5 | 0.112 | 0.706 | 31.259 | 0.604 | 0 | 10 | 20 |
| W5C1T13 | 211.4 | 0.165 | 10.30 | 0.1378 | 175.0 | 34.7 | 46.1 | 0.711 | 17.1 | 20.4 | 61.8 | 0.125 | 0.710 | 31.432 | 1.564 | 0 | 10 | 20 |
| W5C1T20 | 230.3 | 0.150 | 12.00 | 0.1406 | 178.8 | 35.5 | 48.3 | 0.750 | 16.8 | 20.9 | 72.0 | 0.134 | 0.710 | 30.851 | 1.571 | 0 | 10 | 20 |
| Net At Critical Temperature | | | | | | | | | | | | | | | | | | |
| W5C1T04 | 147.2 | 0.138 | 12.32 | 0.1394 | 180.8 | 36.0 | 44.2 | 0.517 | 17.0 | 19.4 | 58.2 | 0.093 | 0.684 | 29.305 | 1.237 | 0 | 10 | 20 |
| W5C1T05 | 147.2 | 0.139 | 9.35 | 0.1371 | 172.4 | 34.4 | 43.8 | 0.619 | 16.9 | 19.8 | 66.3 | 0.107 | 0.671 | 32.916 | 1.355 | 0 | 10 | 20 |
| W5C1T08 | 193.4 | 0.156 | 9.62 | 0.1401 | 177.9 | 35.3 | 46.3 | 0.672 | 17.4 | 20.6 | 62.9 | 0.120 | 0.683 | 31.201 | 0.767 | 0 | 10 | 20 |
| W5C1T09 | 193.4 | 0.160 | 10.63 | 0.1379 | 178.8 | 35.9 | 46.5 | 0.637 | 17.4 | 20.3 | 58.3 | 0.114 | 0.692 | 31.113 | 0.960 | 0 | 10 | 20 |
| W5C1T10 | 193.4 | 0.156 | 12.18 | 0.1374 | 180.0 | 35.6 | 47.2 | 0.693 | 17.3 | 20.9 | 66.5 | 0.125 | 0.687 | 30.514 | 1.109 | 0 | 10 | 20 |
| Delaminated | | | | | | | | | | | | | | | | | | |
| W5C1T17 | 230.3 | 0.139 | 16.55 | 0.1373 | 177.7 | 35.2 | 46.9 | 0.707 | 17.2 | 20.6 | 63.9 | 0.126 | 0.706 | 30.157 | 2.141 | 2 | 10 | 20 |
| W5C1T21 | 239.7 | 0.134 | 19.40 | 0.1408 | 171.3 | 34.0 | 48.1 | 0.866 | 18.0 | 22.5 | 73.9 | 0.148 | 0.726 | 30.954 | 0.702 | 4 | 10 | 20 |
| At Critical Temperature | | | | | | | | | | | | | | | | | | |
| W5C2T11 | 212.3 | 0.161 | 4.97 | 0.1390 | 180.4 | 43.0 | 51.3 | 0.376 | 16.8 | 19.5 | 58.0 | 0.068 | 0.739 | 30.558 | 2.938 | 0 | 10 | 20 |
| W5C2T12 | 213.3 | 0.149 | 6.72 | 0.1387 | 173.2 | 41.1 | 50.3 | 0.447 | 17.4 | 19.2 | 55.3 | 0.077 | 0.729 | 28.563 | 0.837 | 0 | 10 | 20 |
| W5C2T18 | 231.2 | 0.161 | 5.59 | 0.1374 | 177.3 | 41.9 | 52.4 | 0.476 | 17.2 | 19.1 | 50.8 | 0.084 | 0.718 | 28.863 | 1.367 | 0 | 10 | 20 |
| W5C2T21 | 249.2 | 0.169 | 8.88 | 0.1376 | 173.8 | 41.3 | 52.0 | 0.499 | 17.0 | 19.4 | 63.7 | 0.087 | 0.725 | 31.144 | 1.969 | 0 | 10 | 20 |
| Net At Critical Temperature | | | | | | | | | | | | | | | | | | |
| W5C2T05 | 147.2 | 0.140 | 7.86 | 0.1379 | 174.4 | 41.5 | 50.1 | 0.321 | 17.7 | 18.8 | 45.2 | 0.058 | 0.698 | 30.985 | 1.846 | 0 | 10 | 20 |
| W5C2T06 | 194.4 | 0.157 | 6.28 | 0.1357 | 179.6 | 42.8 | 49.5 | 0.353 | 17.1 | 18.4 | 46.4 | 0.063 | 0.728 | 29.683 | 1.506 | 0 | 10 | 20 |
| W5C2T07 | 194.4 | 0.176 | 6.82 | 0.1372 | 180.2 | 42.7 | 49.5 | 0.324 | 17.7 | 18.8 | 43.6 | 0.058 | 0.737 | 32.613 | 1.339 | 0 | 10 | 20 |
| W5C2T10 | 192.5 | 0.150 | 5.33 | 0.1405 | 172.2 | 41.0 | 49.3 | 0.414 | 17.5 | 18.9 | 45.2 | 0.071 | 0.725 | 27.874 | 3.208 | 0 | 10 | 20 |
| W5C2T25 | 250.1 | 0.145 | 10.34 | 0.1379 | 180.4 | 43.0 | 53.5 | 0.458 | 17.6 | 19.6 | 56.3 | 0.083 | 0.703 | 1.351 | 0 | 10 | 20 | |
| W5C2T28 | 268.0 | 0.202 | 6.44 | 0.1389 | 176.7 | 42.2 | 52.1 | 0.450 | 16.8 | 18.8 | 57.2 | 0.080 | 0.767 | 32.889 | 0.780 | 0 | 10 | 20 |
| W5C2T27 | 269.9 | 0.218 | 5.05 | 0.1400 | 179.4 | 42.8 | 51.7 | 0.399 | 16.9 | 18.5 | 60.8 | 0.072 | 0.774 | 33.894 | 0.897 | 0 | 10 | 20 |
| W5C2T28 | 268.1 | 0.172 | 8.72 | 0.1380 | 178.1 | 42.3 | 52.0 | 0.441 | 17.5 | 19.3 | 51.8 | 0.079 | 0.729 | 28.995 | 0.929 | 0 | 10 | 20 |
| W5C2T32 | 286.9 | 0.165 | 9.09 | 0.1402 | 176.7 | 41.8 | 53.6 | 0.528 | 17.1 | 18.7 | 39.1 | 0.083 | 0.728 | 30.545 | 1.788 | 0 | 10 | 20 |
| Delaminated | | | | | | | | | | | | | | | | | | |
| W5C2T16 | 232.2 | 0.185 | 7.03 | 0.1398 | 176.1 | 42.0 | 50.8 | 0.411 | 17.1 | 19.0 | 58.1 | 0.072 | 0.760 | 31.666 | 3.344 | 1 | 10 | 20 |

Table A4. Data for the double-felted pressing control cases.

| PLATEN SURFACE SAMPLE ID | TEMP (C) | SEM (MN/mm²) | SEM %CV | OD BASIS WEIGHT (g/m²) | SHEET SOLIDS IN (%) | SHEET SOLIDS OUT (%) | FELT MOISTURE RATIO (%) | FELT MOISTURE IN (%) | FELT MOISTURE OUT (%) | FELT GAIN/LOSS (%) | WATER REMOVED (%) | US DENSITY (kg/m³) | AVERAGE STFI INDEX (Nm/g) | 95% C.I. CODE | REWET CODE | STICK/PICK CODE | COMMENTS |
|--------------------------|----------|--------------|---------|------------------------|---------------------|----------------------|-------------------------|----------------------|-----------------------|--------------------|-------------------|--------------------|---------------------------|---------------|------------|-----------------|----------|
| | | | | | | | | | | | | | | | | | |
| WID1T04 | 99.0 | 0.141 | 23.40 | 0.1349 | 174.6 | 34.6 | 41.2 | 0.469 | 17.8 | 19.7 | 68.3 | 0.082 | 0.611 | 28.616 | 1.219 | 0 | 10 |
| WID1T04 | 99.0 | 0.119 | 19.33 | 0.1415 | 180.4 | 35.9 | 41.9 | 0.404 | 16.8 | 18.4 | 44.2 | 0.073 | 0.604 | 28.234 | 0.845 | 0 | 10 |
| WID1T05 | 98.1 | 0.145 | 11.72 | 0.1378 | 173.4 | 40.8 | 44.7 | 0.216 | 18.1 | 18.7 | 36.5 | 0.037 | 0.664 | 30.455 | 0.998 | 0 | 10 |
| WID1T05 | 99.0 | 0.137 | 18.98 | 0.1356 | 170.5 | 40.7 | 44.1 | 0.188 | 18.3 | 18.8 | 31.8 | 0.032 | 0.640 | 27.910 | 2.274 | 0 | 10 |
| WID2T09 | 98.1 | 0.142 | 11.97 | 0.1395 | 176.5 | 41.7 | 45.1 | 0.161 | 18.3 | 18.7 | 39.9 | 0.029 | 0.672 | 29.217 | 0.773 | 0 | 10 |
| WID2T09 | 99.0 | 0.145 | 24.14 | 0.1354 | 177.1 | 41.6 | 44.6 | 0.180 | 16.7 | 17.0 | 24.3 | 0.032 | 0.634 | 30.287 | 1.087 | 0 | 10 |
| WID2T05 | 99.0 | 0.142 | 21.99 | 0.1339 | 172.2 | 34.2 | 41.2 | 0.495 | 18.0 | 20.0 | 57.2 | 0.085 | 0.649 | 30.926 | 2.928 | 0 | 10 |
| WID2T10 | 98.1 | 0.141 | 17.73 | 0.1375 | 178.8 | 35.4 | 41.2 | 0.401 | 18.3 | 17.9 | 50.1 | 0.072 | 0.648 | 32.004 | 1.173 | 0 | 10 |
| WSD1T01 | 99.0 | 0.139 | 15.11 | 0.1393 | 176.5 | 35.1 | 41.3 | 0.429 | 18.0 | 18.8 | 57.9 | 0.076 | 0.651 | 31.030 | 1.867 | 0 | 10 |
| WSD1T03 | 99.0 | 0.141 | 23.62 | 0.1399 | 175.3 | 35.0 | 41.5 | 0.443 | 17.1 | 18.7 | 48.9 | 0.078 | 0.629 | 30.565 | 3.076 | 0 | 10 |
| WSD1T03 | 99.0 | 0.144 | 22.92 | 0.1401 | 180.2 | 35.6 | 41.5 | 0.398 | 17.7 | 18.3 | 28.7 | 0.072 | 0.591 | 30.275 | 0.712 | 0 | 10 |
| WSD1T04 | 99.0 | 0.158 | 12.66 | 0.1382 | 177.5 | 35.0 | 41.3 | 0.434 | 18.1 | 16.5 | 58.7 | 0.077 | 0.670 | 30.910 | 1.237 | 0 | 10 |
| WSD1T04 | 99.0 | 0.140 | 10.71 | 0.1377 | 168.8 | 40.3 | 43.6 | 0.191 | 18.4 | 18.7 | 25.5 | 0.032 | 0.670 | 32.984 | 2.178 | 0 | 13 |
| WSD2T09 | 99.0 | 0.149 | 13.42 | 0.1383 | 174.2 | 41.9 | 44.3 | 0.133 | 18.3 | 18.9 | 60.5 | 0.023 | 0.643 | 32.503 | 0.457 | 0 | 10 |
| At 40% Solids | 99.0 | | | | | | | | | | | | | | | | |
| At 42% Solids | 99.0 | | | | | | | | | | | | | | | | |
| WSD2T05 | 99.0 | | | | | | | | | | | | | | | | |
| WSD2T05 | 99.0 | | | | | | | | | | | | | | | | |

APPENDIX B

The following tables contain the data that were not used for analysis. Data were not used if the ingoing solids or basis weight were out of the established range. Also rejected were data where the sheet stuck to the platen (except at the corner) or showed any other anomalous behavior.

Table B1. Data with the IPST A platen.

| PLATEN SURFACE | SAMPLE ID | TEMP (C) | SEM (MN/m²) | SEM %ACV | IMPULSE (MPa.s) | OD BASIS WEIGHT (g/m²) | SHEET SOLIDS IN OUT (%) | | | FELT MOISTURE IN OUT (%) | | | WATER REMOVED DENSITY (kg/m³) | | | AVERAGE STIFF INDEX (Nm²) | | | STICK/PICK CODE COMMENTS | | |
|----------------|-----------|----------|-------------|----------|-----------------|------------------------|-------------------------|--------|---------------------|--------------------------|----------|--------|-------------------------------|----------|---------|---------------------------|------------|----------|--------------------------|------------|-----------------|
| | | | | | | | SHEET | SOLIDS | MOISTURE CHANGE (%) | FELT | MOISTURE | IN (%) | FELT | MOISTURE | OUT (%) | WATER | US DENSITY | 95% C.I. | DELM CODE | REWET CODE | STICK/PICK CODE |
| WIA1T01 | 145.9 | 0.149 | 10.74 | 0.140 | 6.43 | 0.1260 | 178.0 | 32.6 | 46.1 | 0.895 | 17.2 | 21.8 | 70.6 | 0.160 | 0.649 | 0.000 | 0.000 | 0 | 0 | 0 | 27 |
| WIA1T02 | 145.0 | 0.140 | 6.43 | 0.1300 | 178.8 | 32.6 | 45.6 | 0.868 | 17.3 | 21.9 | 70.0 | 0.155 | 0.623 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 27 |
| WIA1T03 | 144.2 | 0.162 | 7.89 | 0.1225 | 177.3 | 32.4 | 45.1 | 0.870 | 17.4 | 22.2 | 75.8 | 0.164 | 0.628 | 29.532 | 1.516 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T04 | 144.2 | 0.164 | 8.54 | 0.1299 | 171.9 | 31.3 | 45.0 | 0.868 | 17.2 | 22.5 | 75.2 | 0.166 | 0.635 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T05 | 145.0 | 0.138 | 7.97 | 0.1352 | 170.5 | 31.0 | 57.6 | 1.486 | 17.2 | 22.0 | 45.6 | 0.253 | 0.633 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T06 | 145.0 | 0.093 | 37.63 | 0.1367 | 167.4 | 30.5 | 47.1 | 1.151 | 16.1 | 22.3 | 74.2 | 0.193 | 0.612 | 0.000 | 0.000 | 6 | 0 | 0 | 10 | 0 | 28 |
| WIA1T07 | 189.2 | 0.093 | 7.97 | 0.1352 | 163.7 | 30.5 | 47.1 | 1.151 | 16.1 | 22.3 | 74.2 | 0.193 | 0.612 | 0.000 | 0.000 | 6 | 0 | 0 | 10 | 0 | 28 |
| WIA1T08 | 197.5 | 0.088 | 27.03 | 0.1367 | 163.8 | 30.5 | 47.1 | 1.151 | 16.1 | 22.3 | 74.2 | 0.193 | 0.612 | 0.000 | 0.000 | 6 | 0 | 0 | 10 | 0 | 28 |
| WIA1T09 | 187.5 | 0.098 | 31.63 | 0.1382 | 189.7 | 34.6 | 47.4 | 0.856 | 16.7 | 21.5 | 72.8 | 0.158 | 0.595 | 0.000 | 0.000 | 6 | 0 | 0 | 10 | 0 | 28 |
| WIA1T10 | 187.5 | 0.098 | 31.63 | 0.1382 | 189.7 | 34.6 | 47.4 | 0.798 | 16.9 | 21.4 | 73.6 | 0.151 | 0.589 | 0.000 | 0.000 | 6 | 0 | 0 | 10 | 0 | 28 |
| WIA1T11 | 182.0 | 0.168 | 12.50 | 0.1120 | 186.8 | 34.2 | 45.3 | 0.716 | 17.3 | 21.1 | 64.4 | 0.134 | 0.659 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T12 | 162.0 | 0.160 | 9.38 | 0.1256 | 180.2 | 33.0 | 46.2 | 0.865 | 17.2 | 21.5 | 65.7 | 0.156 | 0.652 | 28.728 | 1.274 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T13 | 162.9 | 0.179 | 7.26 | 0.1357 | 166.3 | 30.5 | 48.5 | 1.127 | 17.3 | 23.1 | 75.6 | 0.188 | 0.676 | 28.792 | 2.032 | 1 | 0 | 25 | 10 | 0 | 28 |
| WIA1T14 | 163.7 | 0.177 | 6.21 | 0.1415 | 173.4 | 31.6 | 47.0 | 1.035 | 17.8 | 23.1 | 71.6 | 0.180 | 0.675 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T15 | 179.0 | 0.180 | 9.47 | 0.1372 | 181.9 | 33.1 | 47.0 | 0.900 | 17.4 | 22.3 | 69.4 | 0.164 | 0.633 | 30.283 | 0.957 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T16 | 212.9 | 0.179 | 10.61 | 0.1382 | 175.9 | 32.3 | 50.4 | 1.112 | 16.9 | 22.4 | 67.7 | 0.196 | 0.701 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T17 | 212.9 | 0.149 | 20.81 | 0.1380 | 181.9 | 33.2 | 49.7 | 1.003 | 17.3 | 22.5 | 69.6 | 0.182 | 0.685 | 0.000 | 0.000 | 2 | 0 | 0 | 10 | 0 | 28 |
| WIA1T18 | 437.9 | 0.160 | 9.38 | 0.1446 | 169.1 | 31.1 | 55.4 | 1.416 | 16.3 | 19.7 | 31.7 | 0.239 | 0.658 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T19 | 232.5 | 0.168 | 4.82 | 0.1357 | 169.7 | 30.8 | 53.8 | 1.382 | 17.2 | 23.0 | 59.8 | 0.234 | 0.708 | 0.000 | 0.000 | 1 | 0 | 0 | 10 | 0 | 28 |
| WIA1T20 | 231.6 | 0.182 | 9.34 | 0.1390 | 169.9 | 30.8 | 50.1 | 1.255 | 16.8 | 22.6 | 66.3 | 0.213 | 0.634 | 0.000 | 0.000 | 2 | 0 | 0 | 10 | 0 | 28 |
| WIA1T21 | 228.9 | 0.180 | 4.21 | 0.1383 | 169.7 | 30.8 | 50.5 | 1.289 | 16.9 | 23.5 | 71.3 | 0.215 | 0.638 | 0.000 | 0.000 | 1 | 0 | 0 | 10 | 0 | 28 |
| WIA1T22 | 212.9 | 0.179 | 9.50 | 0.1393 | 175.0 | 31.9 | 55.5 | 1.334 | 16.2 | 21.8 | 57.5 | 0.233 | 0.692 | 0.000 | 0.000 | 1 | 0 | 0 | 10 | 0 | 28 |
| WIA1T23 | 252.0 | 0.193 | 4.68 | 0.1377 | 174.6 | 31.9 | 51.5 | 1.189 | 17.0 | 22.7 | 66.6 | 0.208 | 0.668 | 0.000 | 0.000 | 1 | 0 | 0 | 10 | 0 | 28 |
| WIA1T24 | 249.4 | 0.191 | 8.28 | 0.1382 | 170.3 | 31.1 | 50.6 | 1.237 | 16.8 | 22.8 | 68.3 | 0.211 | 0.679 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T25 | 252.0 | 0.175 | 13.71 | 0.1372 | 181.0 | 33.2 | 52.4 | 1.104 | 17.2 | 22.6 | 63.8 | 0.200 | 0.635 | 0.000 | 0.000 | 1 | 0 | 0 | 10 | 0 | 28 |
| WIA1T26 | 358.1 | 0.201 | 4.48 | 0.1351 | 168.8 | 30.4 | 53.8 | 1.432 | 16.9 | 21.0 | 39.6 | 0.239 | 0.720 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T27 | 212.1 | 0.181 | 12.71 | 0.1294 | 184.3 | 33.6 | 48.8 | 0.929 | 16.9 | 22.5 | 78.0 | 0.171 | 0.632 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T28 | 214.6 | 0.142 | 33.10 | 0.1377 | 183.3 | 33.4 | 49.0 | 0.951 | 17.1 | 22.6 | 73.2 | 0.174 | 0.847 | 0.000 | 0.000 | 5 | 0 | 0 | 10 | 0 | 28 |
| WIA1T29 | 204.5 | 0.180 | 7.78 | 0.1352 | 167.9 | 30.6 | 53.0 | 1.383 | 17.0 | 23.5 | 68.7 | 0.232 | 0.851 | 0.000 | 0.000 | 2 | 0 | 0 | 10 | 0 | 28 |
| WIA1T30 | 189.2 | 0.183 | 10.38 | 0.1380 | 186.1 | 30.9 | 47.0 | 1.110 | 17.1 | 22.7 | 72.2 | 0.188 | 0.676 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T31 | 188.6 | 0.183 | 5.62 | 0.1372 | 185.4 | 33.6 | 48.7 | 0.934 | 17.2 | 22.4 | 74.0 | 0.173 | 0.694 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T32 | 179.0 | 0.178 | 7.87 | 0.1379 | 166.2 | 30.4 | 47.3 | 1.180 | 17.1 | 22.8 | 67.5 | 0.198 | 0.877 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T33 | 145.0 | 0.164 | 10.39 | 0.1374 | 182.9 | 33.7 | 45.6 | 0.788 | 17.2 | 21.7 | 78.4 | 0.141 | 0.673 | 32.166 | 1.297 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T34 | 214.6 | 0.145 | 13.10 | 0.1315 | 178.3 | 32.5 | 45.4 | 0.873 | 17.1 | 22.0 | 73.8 | 0.154 | 0.847 | 0.000 | 0.000 | 5 | 0 | 0 | 10 | 0 | 28 |
| WIA1T35 | 145.0 | 0.146 | 6.76 | 0.1363 | 182.9 | 33.8 | 46.2 | 0.810 | 17.5 | 22.2 | 74.0 | 0.148 | 0.683 | 28.908 | 0.813 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T36 | 145.0 | 0.144 | 9.03 | 0.1395 | 184.9 | 30.4 | 48.4 | 1.227 | 17.3 | 22.9 | 68.0 | 0.202 | 0.681 | 0.000 | 0.000 | 1 | 0 | 0 | 10 | 0 | 28 |
| WIA1T37 | 178.1 | 0.173 | 6.94 | 0.1399 | 189.3 | 31.2 | 50.3 | 1.215 | 16.9 | 22.3 | 63.6 | 0.206 | 0.699 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T38 | 178.1 | 0.167 | 12.57 | 0.1422 | 160.0 | 29.5 | 48.0 | 1.299 | 16.7 | 22.7 | 70.6 | 0.208 | 0.674 | 0.000 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T39 | 145.0 | 0.161 | 7.95 | 0.1377 | 174.4 | 31.8 | 49.8 | 1.128 | 17.1 | 22.3 | 63.9 | 0.197 | 0.683 | 30.332 | 1.632 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T40 | 145.0 | 0.150 | 13.33 | 0.1398 | 173.2 | 31.5 | 47.0 | 1.047 | 17.4 | 23.3 | 80.1 | 0.181 | 0.676 | 30.102 | 2.137 | 2 | 0 | 0 | 10 | 0 | 28 |
| WIA1T41 | 144.2 | 0.163 | 6.54 | 0.1395 | 177.3 | 32.3 | 46.6 | 0.942 | 16.9 | 22.2 | 77.5 | 0.187 | 0.658 | 29.946 | 2.398 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T42 | 144.2 | 0.164 | 8.44 | 0.1374 | 175.3 | 32.0 | 46.5 | 0.977 | 17.4 | 22.8 | 72.8 | 0.171 | 0.675 | 28.374 | 1.716 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T43 | 170.5 | 0.127 | 33.07 | 0.1376 | 183.1 | 33.4 | 47.0 | 0.868 | 16.7 | 21.9 | 77.8 | 0.159 | 0.671 | 27.124 | 2.202 | 7 | 0 | 0 | 10 | 0 | 28 |
| WIA1T44 | 169.7 | 0.114 | 28.95 | 0.1394 | 170.3 | 31.1 | 47.7 | 1.122 | 17.0 | 22.3 | 75.6 | 0.160 | 0.680 | 26.185 | 1.477 | 7 | 0 | 0 | 10 | 0 | 28 |
| WIA1T45 | 162.0 | 0.127 | 22.83 | 0.1405 | 171.5 | 30.9 | 47.4 | 1.123 | 16.7 | 23.5 | 88.6 | 0.193 | 0.695 | 26.354 | 2.238 | 7 | 0 | 0 | 10 | 0 | 28 |
| WIA1T46 | 150.0 | 0.150 | 14.00 | 0.1385 | 172.4 | 31.2 | 48.7 | 1.064 | 17.2 | 23.2 | 81.1 | 0.183 | 0.663 | 29.431 | 1.774 | 2 | 0 | 0 | 10 | 0 | 28 |
| WIA1T47 | 152.7 | 0.166 | 12.18 | 0.1345 | 183.9 | 33.4 | 46.9 | 0.886 | 16.9 | 21.7 | 73.3 | 0.159 | 0.655 | 28.815 | 2.100 | 0 | 0 | 0 | 10 | 0 | 28 |
| WIA1T48 | 152.7 | 0.153 | 23.53 | 0.1382 | 173.2 | 31.4 | 45.2 | 0.970 | 17.5 | 23.0 | 76.8 | 0.169 | 0.644 | 30.414 | 4.247 | 4 | 0 | 0 | 10 | 0 | 28 |
| WIA1T49 | 153.5 | 0.160 | 12.50 | 0.1384 | 174.8 | 31.8 | 46.4 | 0.894 | 16.8 | 22.4 | 77.4 | 0.172 | 0.686 | 28.848 | 1.827 | 2 | 0 | 0 | 10 | 0 | 28 |
| WIA1T50 | 154.4 | 0.141 | 15.60 | 0.1373 | 183.1 | 33.4 | 47.5 | 0.892 | 17.9 | 22.9 | 74.3 | 0.163 | 0.647 | 29.382 | 1.336 | 2 | 0 | 0 | 10 | 0 | 28 |
| WIA2T01 | 145.9 | 0.157 | 10.19 | 0.1442 | 190.3 | 41.7 | 49.3 | 0.374 | 17.0 | 18.7 | 54.8 | 0.071 | 0.686 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 | |
| WIA2T02 | 145.0 | 0.172 | 3.49 | 0.1459 | 173.4 | 37.8 | 51.9 | 0.716 | 17.1 | 19.3 | 41.2 | 0.124 | 0.663 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 | |
| WIA2T03 | 145.9 | 0.153 | 11.11 | 0.1394 | 179.0 | 39.4 | 53.5 | 0.525 | 16.5 | 18.3 | 44.8 | 0.124 | 0.663 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 | |
| WIA2T04 | 145.0 | 0.164 | 7.93 | 0.1562 | 180.0 | 39.3 | 49.5 | 0.526 | 17.2 | 19.6 | 57.1 | 0.095 | 0.664 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 | |
| WIA2T05 | 145.0 | 0.128 | 32.61 | 0.1429 | 182.5 | 40.0 | 50.1 | 0.504 | 17.3 | 19.9 | 64.2 | 0.092 | 0.688 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 | |
| WIA2T06 | 187.5 | 0.108 | 34.26 | 0.1382 | 175.6 | 38.5 | 49.5 | 0.406 | 17.1 | 20.0 | 60.3 | 0.109 | 0.679 | 0.000 | 0 | 0 | 0 | 10 | 0 | 28 | |
| WIA2T07 | 187.5 | 0.127 | 7.26 | 0.1386 | 174.0 | 31.4 | 45.2 | 0.970 | 17.5 | 23.0 | 76.8 | 0.169 | 0.644 | 30.414 | 4.247 | 4 | 0 | 0 | 10 | 0 | 28 |
| WIA2T08 | 162.9 | 0.179 | 8.19 | 0.1371 | | | | | | | | | | | | | | | | | |

Table B1 Continued. Data with the IPST A platen.

| PLATEN SURFACE ID | TEMP (C) | SEM (MN/m²g) | SEM %CV | OB BASIS WEIGHT (g/m²) | IMPULSE (MPa.s) | SHEET SOLIDS IN (%) | MOISTURE CHANGE (%) | FELT MOISTURE IN (%) | FELT MOISTURE OUT (%) | WATER LOSS (%) | US REMOVED DENSITY (KG/m³) | AVERAGE STFI INDEX | 95% C.I. (Nm/g) | DELAM CODE | REWET CODE | PICK CODE | STICK COMMENTS | | |
|-------------------|----------|--------------|---------|------------------------|-----------------|---------------------|---------------------|----------------------|-----------------------|----------------|----------------------------|--------------------|-----------------|------------|------------|-----------|----------------|---|---|
| | | | | | | | | | | | | | | | | | | | |
| W1A2T18 | 169.7 | 0.169 | 11.24 | 0.1376 | 193.0 | 42.3 | 50.8 | 0.938 | 16.8 | 18.5 | 48.9 | 0.077 | 0.707 | 0 | 0 | 0 | 0 | | |
| W1A2T19 | 171.4 | 0.174 | 11.49 | 0.1380 | 178.8 | 38.8 | 52.0 | 0.859 | 17.1 | 20.0 | 58.4 | 0.118 | 0.720 | 0 | 0 | 0 | 0 | | |
| W1A2T21 | 212.1 | 0.176 | 6.82 | 0.1444 | 198.2 | 43.3 | 54.8 | 0.487 | 16.6 | 19.9 | 61.1 | 0.122 | 0.735 | 0 | 0 | 0 | 0 | | |
| W1A2T22 | 213.8 | 0.190 | 7.37 | 0.1392 | 176.1 | 38.7 | 52.8 | 0.687 | 17.6 | 19.2 | 54.0 | 0.101 | 0.728 | 0 | 0 | 0 | 0 | | |
| W1A2T24 | 213.8 | 0.176 | 11.36 | 0.1387 | 188.5 | 41.1 | 52.7 | 0.535 | 16.8 | 19.2 | 60.6 | 0.101 | 0.728 | 0 | 0 | 0 | 0 | | |
| W1A2T27 | 229.1 | 0.184 | 4.89 | 0.1398 | 171.5 | 37.7 | 52.8 | 0.754 | 17.2 | 20.9 | 65.2 | 0.129 | 0.727 | 0 | 0 | 0 | 0 | | |
| W1A2T30 | 229.9 | 0.186 | 4.30 | 0.1397 | 174.6 | 38.1 | 52.0 | 0.705 | 16.6 | 20.2 | 68.4 | 0.123 | 0.740 | 0 | 0 | 0 | 0 | | |
| W1A2T31 | 258.2 | 0.173 | 15.81 | 0.1350 | 198.2 | 43.3 | 54.8 | 0.487 | 16.4 | 18.3 | 44.6 | 0.097 | 0.740 | 0 | 0 | 0 | 0 | | |
| W1A2T34 | 255.4 | 0.193 | 3.11 | 0.1388 | 179.6 | 38.9 | 54.7 | 0.745 | 16.8 | 20.1 | 57.6 | 0.134 | 0.735 | 0 | 0 | 0 | 0 | | |
| W1A2T35 | 257.1 | 0.188 | 2.69 | 0.1368 | 174.8 | 38.1 | 54.2 | 0.782 | 16.8 | 20.4 | 60.6 | 0.137 | 0.739 | 0 | 0 | 0 | 0 | | |
| W1A2T36 | 283.6 | 0.204 | 2.94 | 0.1403 | 174.6 | 37.8 | 55.1 | 0.830 | 17.0 | 20.7 | 69.3 | 0.145 | 0.753 | 0 | 0 | 0 | 0 | | |
| W1A2T37 | 284.4 | 0.200 | 5.00 | 0.1381 | 175.9 | 38.1 | 64.8 | 0.799 | 16.9 | 20.4 | 56.8 | 0.141 | 0.742 | 0 | 0 | 0 | 0 | | |
| W1A2T40 | 285.3 | 0.208 | 5.34 | 0.1402 | 171.7 | 37.5 | 54.9 | 0.846 | 16.7 | 20.4 | 60.2 | 0.145 | 0.755 | 0 | 0 | 0 | 0 | | |
| W1A2T41 | 356.4 | 0.176 | 4.55 | 0.1440 | 180.0 | 39.9 | 59.0 | 0.814 | 16.3 | 19.6 | 51.4 | 0.147 | 0.737 | 0 | 0 | 0 | 0 | | |
| W1A2T42 | 358.9 | 0.179 | 6.16 | 0.1414 | 185.0 | 40.4 | 57.1 | 0.723 | 16.6 | 19.4 | 47.5 | 0.134 | 0.741 | 0 | 0 | 0 | 0 | | |
| W1A2T45 | 145.0 | 0.169 | 11.95 | 0.1350 | 178.6 | 39.7 | 50.6 | 0.544 | 16.5 | 18.0 | 35.4 | 0.097 | 0.685 | 31.007 | 0.902 | 0 | 0 | | |
| W1A2T47 | 144.2 | 0.160 | 15.83 | 0.1377 | 197.2 | 43.6 | 49.7 | 0.283 | 17.0 | 20.7 | 47.9 | 0.056 | 0.701 | 28.518 | 1.147 | 0 | 0 | | |
| W1A2T49 | 145.8 | 0.152 | 11.18 | 0.1371 | 186.0 | 41.2 | 49.2 | 0.398 | 17.3 | 19.2 | 61.1 | 0.074 | 0.683 | 30.190 | 2.194 | 0 | 0 | | |
| W1A2T51 | 168.3 | 0.143 | 15.38 | 0.1391 | 186.8 | 41.3 | 51.7 | 0.487 | 17.3 | 20.0 | 70.5 | 0.091 | 0.737 | 0 | 0 | 0 | 0 | | |
| W1A2T67 | 162.9 | 0.147 | 21.77 | 0.1359 | 188.7 | 40.9 | 50.5 | 0.465 | 16.9 | 18.7 | 44.8 | 0.088 | 0.681 | 27.863 | 1.498 | 0 | 0 | | |
| W1A2T70 | 162.0 | 0.164 | 12.80 | 0.1386 | 176.5 | 38.5 | 49.5 | 0.578 | 16.2 | 19.4 | 71.6 | 0.102 | 0.677 | 28.500 | 3.684 | 0 | 0 | | |
| W1A2T71 | 152.7 | 0.175 | 7.43 | 0.1362 | 177.5 | 38.9 | 49.6 | 0.553 | 16.8 | 20.1 | 79.5 | 0.098 | 0.659 | 30.591 | 0.753 | 0 | 0 | | |
| W1A2T73 | 162.7 | 0.146 | 9.59 | 0.1423 | 174.4 | 38.3 | 53.5 | 0.743 | 17.0 | 20.5 | 64.5 | 0.130 | 0.658 | 28.608 | 1.538 | 0 | 0 | | |
| W1A2T74 | 154.4 | 0.150 | 9.57 | 0.1386 | 170.7 | 37.3 | 49.4 | 0.657 | 16.5 | 20.2 | 74.2 | 0.112 | 0.650 | 28.664 | 2.761 | 0 | 0 | | |
| W1A2T75 | 152.7 | 0.173 | 7.51 | 0.1386 | 196.1 | 42.8 | 50.6 | 0.360 | 17.3 | 18.8 | 50.6 | 0.071 | 0.657 | 27.941 | 1.795 | 0 | 0 | | |
| A3W1T01 | 145.0 | 0.121 | 22.31 | 0.1240 | 167.8 | 30.4 | 42.7 | 0.951 | 16.8 | 22.2 | 84.5 | 0.160 | 0.581 | 0 | 0 | 0 | 0 | | |
| A3W1T02 | 145.9 | 0.120 | 17.50 | 0.1174 | 171.3 | 31.2 | 42.5 | 0.849 | 17.3 | 21.7 | 75.9 | 0.146 | 0.581 | 0 | 0 | 0 | 0 | | |
| A3W1T03 | 145.0 | 0.116 | 12.93 | 0.1191 | 180.4 | 32.6 | 42.1 | 0.689 | 17.0 | 20.9 | 76.7 | 0.124 | 0.691 | 0 | 0 | 0 | 0 | | |
| A3W1T04 | 144.2 | 0.126 | 8.73 | 0.1249 | 180.6 | 32.7 | 42.4 | 0.700 | 18.2 | 22.0 | 77.0 | 0.126 | 0.693 | 0 | 0 | 0 | 0 | | |
| A3W1T07 | 187.5 | 0.104 | 38.54 | 0.1352 | 187.7 | 34.1 | 45.4 | 0.732 | 15.9 | 19.9 | 71.7 | 0.137 | 0.654 | 0 | 0 | 0 | 0 | | |
| A3W1T09 | 188.3 | 0.117 | 41.88 | 0.1352 | 171.5 | 31.1 | 43.9 | 0.936 | 18.3 | 21.3 | 78.7 | 0.161 | 0.555 | 0 | 0 | 0 | 0 | | |
| A3W1T10 | 189.2 | 0.102 | 44.12 | 0.1412 | 174.0 | 31.4 | 43.4 | 0.678 | 17.8 | 22.2 | 72.7 | 0.153 | 0.578 | 0 | 0 | 0 | 0 | | |
| A3W1T13 | 209.3 | 0.103 | 33.98 | 0.1394 | 170.1 | 30.6 | 43.7 | 0.975 | 19.0 | 23.8 | 73.8 | 0.168 | 0.581 | 0 | 0 | 0 | 0 | | |
| A3W1T19 | 171.4 | 0.148 | 10.14 | 0.1343 | 182.1 | 32.9 | 43.7 | 0.754 | 17.3 | 21.1 | 68.3 | 0.137 | 0.646 | 0 | 0 | 0 | 0 | | |
| A3W1T22 | 164.6 | 0.147 | 17.01 | 0.1366 | 167.6 | 30.2 | 42.1 | 0.929 | 17.0 | 22.1 | 80.7 | 0.156 | 0.638 | 0 | 0 | 0 | 0 | | |
| A3W1T26 | 154.4 | 0.163 | 13.60 | 0.1378 | 160.8 | 29.3 | 42.5 | 0.688 | 15.9 | 21.4 | 79.5 | 0.171 | 0.652 | 0 | 0 | 0 | 0 | | |
| A3W1T28 | 165.2 | 0.155 | 9.68 | 0.1379 | 183.7 | 33.2 | 42.6 | 0.686 | 17.4 | 20.9 | 71.9 | 0.122 | 0.650 | 0 | 0 | 0 | 0 | | |
| W1A3T31 | 128.1 | 0.162 | 11.11 | 0.1323 | 173.0 | 31.3 | 44.1 | 0.926 | 16.8 | 20.7 | 73.2 | 0.160 | 0.634 | 0 | 0 | 0 | 0 | | |
| W1A3T32 | 128.1 | 0.140 | 27.14 | 0.1307 | 188.7 | 34.2 | 44.0 | 0.649 | 16.9 | 18.9 | 60.9 | 0.123 | 0.645 | 28.347 | 0.634 | 0 | 0 | | |
| W1A3T33 | 128.1 | 0.135 | 20.74 | 0.1351 | 178.5 | 32.4 | 43.9 | 0.841 | 19.0 | 23.0 | 90.9 | 0.145 | 0.653 | 28.241 | 0.642 | 0 | 0 | | |
| W1A3T34 | 128.1 | 0.165 | 10.97 | 0.1382 | 174.8 | 31.7 | 50.1 | 1.162 | 22.6 | 68.9 | 0.203 | 0.678 | 29.716 | 2.864 | 0 | 0 | 0 | 0 | |
| W1A3T35 | 128.1 | 0.146 | 11.64 | 0.1406 | 175.9 | 31.8 | 44.0 | 0.869 | 17.2 | 22.0 | 79.7 | 0.153 | 0.654 | 30.516 | 1.208 | 0 | 0 | 0 | 0 |
| W1A3T36 | 145.9 | 0.162 | 13.58 | 0.1408 | 170.1 | 30.8 | 44.4 | 0.692 | 17.9 | 23.4 | 82.8 | 0.169 | 0.706 | 0 | 0 | 0 | 0 | | |
| W1A3T37 | 145.0 | 0.186 | 7.23 | 0.1386 | 184.1 | 33.9 | 45.4 | 0.748 | 15.6 | 20.7 | 80.8 | 0.137 | 0.658 | 30.325 | 1.633 | 0 | 0 | 0 | 0 |
| W1A3T41 | 163.5 | 0.168 | 12.03 | 0.0985 | 178.7 | 32.1 | 44.0 | 0.841 | 16.9 | 22.5 | 93.6 | 0.149 | 0.683 | 30.134 | 0.668 | 0 | 0 | 0 | 0 |
| W1A3T42 | 164.4 | 0.146 | 20.65 | 0.1109 | 177.1 | 32.1 | 44.5 | 0.864 | 17.4 | 23.0 | 92.0 | 0.163 | 0.650 | 28.125 | 1.081 | 0 | 0 | 0 | 0 |
| W1A3T43 | 162.7 | 0.134 | 15.87 | 0.1188 | 162.0 | 29.4 | 45.6 | 1.201 | 16.8 | 23.2 | 94.5 | 0.185 | 0.653 | 28.275 | 2.712 | 0 | 0 | 0 | 0 |
| W1A3T44 | 163.5 | 0.111 | 33.83 | 0.1242 | 163.1 | 29.8 | 44.8 | 1.142 | 17.8 | 23.4 | 76.7 | 0.188 | 0.631 | 25.504 | 4.028 | 0 | 0 | 0 | 0 |
| W1A3T45 | 163.6 | 0.131 | 20.61 | 0.1286 | 179.4 | 32.7 | 45.7 | 0.885 | 16.7 | 21.7 | 78.8 | 0.155 | 0.658 | 26.762 | 1.242 | 0 | 0 | 0 | 0 |
| A3W1T01 | 144.2 | 0.134 | 6.72 | 0.1374 | 176.1 | 38.2 | 46.3 | 0.458 | 16.6 | 18.8 | 68.2 | 0.080 | 0.671 | 0 | 0 | 0 | 0 | 0 | 0 |
| A3W1T03 | 144.2 | 0.137 | 11.68 | 0.1368 | 178.3 | 38.4 | 46.9 | 0.469 | 18.8 | 19.1 | 68.2 | 0.083 | 0.653 | 0 | 0 | 0 | 0 | 0 | 0 |
| A3W1T04 | 148.4 | 0.131 | 8.87 | 0.1353 | 176.5 | 38.5 | 46.3 | 0.439 | 17.0 | 19.4 | 73.8 | 0.078 | 0.640 | 0 | 0 | 0 | 0 | 0 | 0 |
| A3W1T08 | 187.5 | 0.135 | 37.78 | 0.1367 | 178.8 | 38.7 | 49.2 | 0.549 | 16.5 | 19.5 | 67.2 | 0.098 | 0.629 | 0 | 0 | 0 | 0 | 0 | 0 |
| A3W1T09 | 188.6 | 0.116 | 37.07 | 0.1378 | 176.1 | 38.2 | 48.9 | 0.575 | 18.4 | 21.3 | 72.6 | 0.101 | 0.607 | 0 | 0 | 0 | 0 | 0 | 0 |
| A3W1T10 | 204.6 | 0.161 | 8.07 | 0.1385 | 180.2 | 38.9 | 51.8 | 0.638 | 17.2 | 20.3 | 68.4 | 0.115 | 0.687 | 0 | 0 | 0 | 0 | 0 | 0 |
| A3W1T11 | 205.3 | 0.168 | 26.92 | 0.1402 | 167.1 | 36.5 | 49.5 | 0.721 | 17.4 | 20.9 | 73.3 | 0.121 | 0.672 | 0 | 0 | 0 | 0 | 0 | 0 |
| A3W1T12 | 203.6 | 0.107 | 57.94 | 0.1386 | 178.4 | 38.6 | 50.2 | 0.599 | 17.5 | 20.4 | 67.7 | 0.107 | 0.629 | 0 | 0 | 0 | 0 | 0 | 0 |
| A3W1T14 | 205.3 | 0.098 | 47.47 | 0.1408 | 175.3 | 38.0 | 49.2 | 0.604 | 17.0 | 20.1 | 71.7 | 0.108 | 0.601 | 0 | 0 | 0 | 0 | 0 | 0 |
| A3W1T15 | 205.3 | 0.153 | 8.23 | 0.1375 | 178.8 | 38.8 | 47.9 | 0.468 | 17.3 | 20.2 | 78.6 | 0.087 | 0 | 0 | 0 | 0 | 0 | 0 | |

Table B1 Continued. Data with the IPST A platen.

| PLATEN SURFACE TEMP (C) | SAMPLE ID | SEM (MV/mkg) | OD BASIS WEIGHT (g/m ²) | SHEET SOLIDS IN (%) | SHEET SOLIDS OUT (%) | SHEET MOISTURE CHANGE (%) | FELT MOISTURE IN (%) | FELT MOISTURE OUT (%) | FELT GAIN/LOSS (%) | WATER REMOVED (kg/m ²) | US DENSITY (g/cm ³) | AVERAGE STFI INDEX (Nm/g) | 95% C.I. DELAM CODE | REWET CODE | STICK/PICK CODE | COMMENTS |
|-------------------------|-----------|--------------|-------------------------------------|---------------------|----------------------|---------------------------|----------------------|-----------------------|--------------------|------------------------------------|---------------------------------|---------------------------|---------------------|------------|-----------------|----------|
| | | | | | | | | | | | | | | | | |
| A4WT19 | 171.4 | 0.156 | 11.39 | 0.1389 | 172.8 | 37.4 | 48.4 | 0.007 | 17.2 | 19.1 | 77.8 | 0.105 | 0.662 | 0 | 13 | 20 |
| A4WT20 | 161.2 | 0.156 | 9.62 | 0.1423 | 182.3 | 40.0 | 47.2 | 0.035 | 17.2 | 19.4 | 62.6 | 0.070 | 0.681 | 4 | 13 | 20 |
| A4WT22 | 161.2 | 0.164 | 13.41 | 0.1407 | 168.8 | 36.7 | 47.6 | 0.027 | 17.4 | 20.3 | 70.3 | 0.108 | 0.692 | 2 | 13 | 20 |
| A4WT23 | 160.3 | 0.173 | 8.67 | 0.1358 | 162.4 | 36.5 | 47.1 | 0.031 | 17.1 | 19.7 | 63.0 | 0.102 | 0.688 | 0 | 13 | 20 |
| A4WT25 | 160.3 | 0.135 | 12.59 | 0.1356 | 137.8 | 36.9 | 48.1 | 0.028 | 17.4 | 19.7 | 65.9 | 0.087 | 0.666 | 0 | 13 | 20 |
| A4WT26 | 161.2 | 0.148 | 10.98 | 0.1405 | 139.5 | 37.8 | 49.1 | 0.007 | 17.2 | 19.4 | 64.8 | 0.095 | 0.693 | 0 | 19 | 20 |
| W1A1T26 | 128.9 | 0.139 | 11.51 | 0.1349 | 177.9 | 38.7 | 48.4 | 0.428 | 17.3 | 20.9 | 113.6 | 0.076 | 0.690 | 28.264 | 1.790 | 20 |
| W1A1T28 | 128.9 | 0.139 | 9.51 | 0.1384 | 174.4 | 37.8 | 46.9 | 0.372 | 17.7 | 20.9 | 90.1 | 0.090 | 0.690 | 29.823 | 1.707 | 20 |
| W1A1T29 | 128.1 | 0.162 | 11.18 | 0.1357 | 176.9 | 38.2 | 48.2 | 0.044 | 17.6 | 20.6 | 79.2 | 0.058 | 0.673 | 30.353 | 1.104 | 27 |
| W1A1T30 | 128.1 | 0.144 | 9.03 | 0.1367 | 174.0 | 37.9 | 50.4 | 0.653 | 16.9 | 19.2 | 49.1 | 0.114 | 0.695 | 29.354 | 2.583 | 28 |
| W1A1T31 | 128.1 | 0.165 | 10.97 | 0.1393 | 178.4 | 38.7 | 48.0 | 0.499 | 16.8 | 19.8 | 74.4 | 0.089 | 0.701 | 30.213 | 2.566 | 20 |
| W1A1T32 | 145.0 | 0.150 | 12.67 | 0.1392 | 177.7 | 38.8 | 48.3 | 0.507 | 16.8 | 19.4 | 68.5 | 0.080 | 0.688 | 30.724 | 1.510 | 20 |
| W1A1T33 | 145.0 | 0.114 | 9.85 | 0.1370 | 184.7 | 42.6 | 50.8 | 0.372 | 18.9 | 19.2 | 74.5 | 0.072 | 0.653 | 28.149 | 1.184 | 20 |
| W1A1T35 | 144.2 | 0.138 | 7.97 | 0.1389 | 176.6 | 38.5 | 48.2 | 0.619 | 17.4 | 18.8 | 35.2 | 0.092 | 0.672 | 28.319 | 1.709 | 27 |
| W1A1T38 | 182.0 | 0.103 | 27.18 | 0.1367 | 178.8 | 38.8 | 48.7 | 0.522 | 17.0 | 19.6 | 87.9 | 0.093 | 0.673 | 28.515 | 1.620 | 20 |
| W1A1T39 | 182.0 | 0.129 | 22.48 | 0.1404 | 179.0 | 38.9 | 51.6 | 0.633 | 17.0 | 18.6 | 32.113 | 0.683 | 0.751 | 27.581 | 1.742 | 20 |
| W1A1T43 | 174.8 | 0.102 | 24.51 | 0.1388 | 179.4 | 38.9 | 49.1 | 0.536 | 17.0 | 19.8 | 64.8 | 0.098 | 0.655 | 25.754 | 0.425 | 10 |
| W1A1T46 | 174.8 | 0.174 | 12.07 | 0.1337 | 167.2 | 30.6 | 48.9 | 1.226 | 16.3 | 22.5 | 71.8 | 0.205 | 0.734 | 1 | 10 | 25 |
| A1W5T01 | 229.1 | 0.165 | 4.52 | 0.1384 | 169.5 | 30.9 | 49.6 | 1.220 | 17.2 | 23.1 | 69.2 | 0.207 | 0.710 | 1 | 10 | 26 |
| A1W5T02 | 229.9 | 0.111 | 28.13 | 0.1481 | 176.7 | 32.1 | 44.8 | 0.981 | 17.1 | 21.6 | 66.3 | 0.158 | 0.679 | 1 | 10 | 26 |
| A1W5T08 | 144.2 | 0.142 | 23.89 | 0.1382 | 179.0 | 32.8 | 48.4 | 0.974 | 16.7 | 20.4 | 49.0 | 0.175 | 0.633 | 2 | 10 | 28 |
| A1W5T07 | 146.7 | 0.113 | 28.13 | 0.1373 | 182.7 | 33.1 | 68.7 | 1.265 | 17.0 | 19.7 | 27.0 | 0.229 | 0.609 | 1 | 10 | 28 |
| A1W5T09 | 145.0 | 0.155 | 14.19 | 0.1692 | 180.6 | 33.1 | 47.0 | 0.893 | 17.3 | 22.4 | 78.4 | 0.161 | 0.708 | 1 | 10 | 20 |
| A1W5T10 | 162.9 | 0.142 | 21.13 | 0.1255 | 188.4 | 34.0 | 45.0 | 0.720 | 17.5 | 21.0 | 60.8 | 0.134 | 0.688 | 0 | 10 | 20 |
| A1W5T12 | 188.3 | 0.170 | 13.53 | 0.1373 | 188.6 | 30.4 | 47.5 | 1.185 | 17.1 | 22.9 | 70.9 | 0.197 | 0.698 | 0 | 10 | 20 |
| W5A1T12 | 188.3 | 0.153 | 8.50 | 0.1387 | 169.1 | 30.8 | 48.3 | 1.218 | 17.3 | 23.3 | 72.8 | 0.208 | 0.697 | 0 | 10 | 20 |
| W5A1T13 | 211.3 | 0.174 | 5.17 | 0.1391 | 188.2 | 30.6 | 48.6 | 1.213 | 17.2 | 23.0 | 70.0 | 0.204 | 0.712 | 0 | 10 | 20 |
| W5A1T18 | 211.3 | 0.179 | 8.38 | 0.1372 | 165.4 | 28.2 | 48.4 | 1.476 | 17.1 | 23.7 | 71.1 | 0.229 | 0.708 | 1 | 10 | 20 |
| W5A1T20 | 249.4 | 0.192 | 2.80 | 0.1393 | 188.0 | 33.9 | 49.5 | 0.933 | 17.0 | 21.7 | 61.4 | 0.174 | 0.740 | 0 | 10 | 20 |
| W5A1T21 | 252.0 | 0.178 | 6.18 | 0.1392 | 181.7 | 33.2 | 49.8 | 1.001 | 18.9 | 22.0 | 65.6 | 0.182 | 0.697 | 1 | 10 | 20 |
| W5A1T22 | 252.8 | 0.185 | 3.24 | 0.1401 | 181.9 | 33.2 | 50.6 | 1.033 | 17.1 | 22.3 | 68.1 | 0.198 | 0.708 | 2 | 10 | 20 |
| W5A1T27 | 145.9 | 0.155 | 13.55 | 0.1283 | 173.4 | 31.5 | 50.2 | 1.179 | 17.3 | 22.5 | 62.4 | 0.204 | 0.698 | 30.974 | 2.384 | 0 |
| W5A1T28 | 145.9 | 0.139 | 15.11 | 0.1366 | 179.0 | 32.4 | 48.8 | 1.037 | 17.5 | 23.3 | 74.3 | 0.186 | 0.668 | 28.533 | 3.068 | 0 |
| W5A1T29 | 145.0 | 0.146 | 10.27 | 0.1370 | 173.0 | 31.4 | 48.0 | 1.011 | 17.8 | 22.9 | 71.2 | 0.176 | 0.687 | 30.705 | 1.651 | 0 |
| W5A1T31 | 144.2 | 0.149 | 10.07 | 0.1369 | 187.0 | 30.2 | 45.6 | 1.110 | 17.3 | 23.0 | 75.0 | 0.185 | 0.691 | 31.472 | 3.533 | 0 |
| W5A1T35 | 175.6 | 0.169 | 7.10 | 0.1387 | 184.3 | 33.6 | 46.9 | 0.840 | 17.4 | 22.1 | 71.5 | 0.155 | 0.720 | 0 | 10 | 20 |
| W5A1T37 | 204.5 | 0.167 | 12.57 | 0.1385 | 170.3 | 30.9 | 48.2 | 1.184 | 17.2 | 23.5 | 75.4 | 0.188 | 0.739 | 4 | 10 | 20 |
| W5A1T40 | 209.2 | 0.181 | 12.15 | 0.1366 | 183.5 | 33.6 | 49.0 | 1.030 | 17.2 | 22.4 | 71.9 | 0.171 | 0.732 | 1 | 10 | 20 |
| W5A1T42 | 199.4 | 0.171 | 9.84 | 0.1352 | 180.4 | 33.3 | 48.0 | 0.919 | 17.4 | 22.2 | 69.8 | 0.168 | 0.719 | 0 | 10 | 20 |
| W5A1T43 | 167.1 | 0.179 | 11.17 | 0.1375 | 183.9 | 33.5 | 48.6 | 0.844 | 18.0 | 23.0 | 78.9 | 0.165 | 0.726 | 32.193 | 2.113 | 0 |
| W5A1T46 | 188.3 | 0.163 | 12.88 | 0.1385 | 181.7 | 33.2 | 46.2 | 0.854 | 17.8 | 22.6 | 77.4 | 0.155 | 0.709 | 32.115 | 1.524 | 0 |
| W5A1T48 | 175.6 | 0.165 | 18.97 | 0.1374 | 181.7 | 33.1 | 48.8 | 0.888 | 17.5 | 22.7 | 79.2 | 0.161 | 0.698 | 28.377 | 3.004 | 4 |
| W5A1T51 | 175.6 | 0.165 | 5.45 | 0.1385 | 180.6 | 29.3 | 46.6 | 1.270 | 17.1 | 23.6 | 78.2 | 0.204 | 0.741 | 32.086 | 1.446 | 0 |
| W5A1T53 | 188.3 | 0.161 | 11.80 | 0.1390 | 188.9 | 34.4 | 49.9 | 0.902 | 17.2 | 22.6 | 77.5 | 0.170 | 0.701 | 29.135 | 0.701 | 10 |
| A2W5T02 | 229.1 | 0.168 | 5.42 | 0.1379 | 178.7 | 38.9 | 51.8 | 0.638 | 18.3 | 19.1 | 57.7 | 0.113 | 0.724 | 0 | 10 | 20 |
| A2W5T03 | 230.8 | 0.154 | 4.55 | 0.1373 | 176.1 | 38.7 | 51.9 | 0.659 | 18.8 | 19.7 | 59.9 | 0.118 | 0.717 | 0 | 10 | 20 |
| W5A2T03 | 162.9 | 0.153 | 7.09 | 0.1335 | 183.1 | 40.3 | 49.0 | 0.438 | 17.2 | 19.1 | 54.6 | 0.080 | 0.689 | 0 | 10 | 20 |
| W5A2T07 | 162.9 | 0.168 | 6.63 | 0.1352 | 198.8 | 37.5 | 48.7 | 0.613 | 17.1 | 20.0 | 64.3 | 0.105 | 0.691 | 0 | 10 | 20 |
| W5A2T11 | 257.1 | 0.183 | 7.65 | 0.1422 | 185.6 | 40.5 | 53.3 | 0.270 | 17.0 | 18.1 | 47.6 | 0.054 | 0.707 | 0 | 10 | 20 |
| W5A2T12 | 255.4 | 0.197 | 5.08 | 0.1405 | 186.2 | 40.7 | 50.0 | 0.433 | 18.4 | 20.9 | 52.7 | 0.081 | 0.722 | 0 | 10 | 20 |
| W5A2T13 | 188.3 | 0.163 | 5.52 | 0.1396 | 182.7 | 35.4 | 49.6 | 0.811 | 17.1 | 20.9 | 66.3 | 0.132 | 0.688 | 0 | 10 | 20 |
| W5A2T14 | 188.3 | 0.163 | 5.52 | 0.1403 | 167.8 | 36.8 | 48.9 | 0.873 | 17.0 | 20.2 | 68.4 | 0.113 | 0.698 | 0 | 10 | 20 |
| W5A2T15 | 187.5 | 0.172 | 8.14 | 0.1356 | 193.4 | 42.2 | 49.9 | 0.363 | 17.1 | 18.6 | 49.3 | 0.070 | 0.702 | 0 | 10 | 20 |
| W5A2T16 | 254.5 | 0.193 | 5.18 | 0.1502 | 177.9 | 39.0 | 53.5 | 0.638 | 18.0 | 19.8 | 69.8 | 0.124 | 0.751 | 0 | 10 | 20 |
| W5A2T17 | 257.1 | 0.147 | 7.65 | 0.1422 | 185.6 | 40.5 | 53.3 | 0.594 | 18.9 | 20.0 | 63.3 | 0.110 | 0.751 | 0 | 10 | 20 |
| W5A2T18 | 255.4 | 0.205 | 5.08 | 0.1436 | 186.2 | 40.7 | 53.5 | 0.591 | 18.5 | 19.5 | 62.8 | 0.110 | 0.731 | 0 | 10 | 20 |
| W5A2T20 | 217.2 | 0.174 | 7.47 | 0.1370 | 180.9 | 37.3 | 52.7 | 0.784 | 18.0 | 20.9 | 65.4 | 0.134 | 0.737 | 0 | 10 | 20 |
| W5A2T22 | 272.4 | 0.191 | 4.71 | 0.1405 | 175.3 | 38.3 | 53.7 | 0.750 | 18.7 | 19.8 | 54.7 | 0.131 | 0.729 | 0 | 10 | 20 |

Table B1 Continued. Data with the IPST A platen.

| PLATEN ID | SAMPLE ID | SURFACE TEMP (C) | SEM (MN/m²) | SEM %CV | OD BASIS WEIGHT (g/m²) | IMPULSE (NPa.s) | SHEET SOLIDS IN (%) | SHEET SOLIDS OUT (%) | FELT MOISTURE CHANGE (%) | FELT MOISTURE IN (%) | FELT MOISTURE OUT (%) | WATER REMOVED (%) | US DENSITY (kg/m³) | AVERAGE STFI INDEX | 95% C.I. (Nm/g) | DELAM CODE | REWET CODE | STICK PICK CODE | COMMENTS |
|-----------|-----------|------------------|-------------|---------|------------------------|-----------------|---------------------|----------------------|--------------------------|----------------------|-----------------------|-------------------|--------------------|--------------------|-----------------|------------|------------|-----------------|-----------------|
| | | | | | | | | | | | | | | | | | | | |
| W5A2T24 | 2/3/2 | 0.177 | 6.21 | 0.13956 | 187.4 | 41.0 | 53.5 | 0.587 | 16.3 | 18.7 | 52.3 | 0.106 | 0.717 | 1 | 10 | 20 | 20 | 20 | STUCK ON CORNER |
| W5A2T25 | 297.0 | 0.161 | 6.21 | 0.1406 | 190.8 | 41.7 | 54.5 | 0.563 | 17.6 | 19.9 | 49.8 | 0.107 | 0.733 | 0 | 0 | 10 | 20 | 20 | |
| W5A2T27 | 298.7 | 0.181 | 6.08 | 0.1425 | 184.3 | 40.2 | 54.0 | 0.632 | 16.7 | 19.4 | 52.6 | 0.117 | 0.724 | 0 | 0 | 10 | 20 | 20 | |
| W5A2T28 | 296.1 | 0.178 | 4.49 | 0.1383 | 176.5 | 38.5 | 53.7 | 0.736 | 17.1 | 20.0 | 54.5 | 0.130 | 0.720 | 0 | 0 | 10 | 20 | 20 | |
| W5A2T31 | 321.6 | 0.167 | 6.59 | 0.1398 | 177.5 | 39.8 | 57.0 | 0.822 | 16.6 | 19.7 | 50.9 | 0.148 | 0.725 | 0 | 0 | 10 | 20 | 20 | |
| W5A2T32 | 322.4 | 0.179 | 7.26 | 0.1407 | 187.7 | 41.2 | 55.1 | 0.616 | 16.8 | 19.1 | 43.2 | 0.116 | 0.696 | 0 | 0 | 10 | 20 | 20 | |
| W5A2T33 | 322.4 | 0.194 | 4.12 | 0.1421 | 189.9 | 41.7 | 54.7 | 0.573 | 16.9 | 19.9 | 43.3 | 0.109 | 0.718 | 0 | 0 | 10 | 20 | 20 | |
| W5A2T34 | 322.4 | 0.191 | 6.81 | 0.1417 | 199.4 | 43.7 | 55.8 | 0.498 | 16.9 | 18.5 | 38.3 | 0.099 | 0.707 | 0 | 0 | 10 | 20 | 20 | |
| W5A2T35 | 321.6 | 0.171 | 2.92 | 0.1419 | 181.2 | 39.7 | 56.2 | 0.739 | 16.3 | 18.9 | 42.9 | 0.134 | 0.743 | 0 | 0 | 10 | 20 | 20 | |
| W5A2T36 | 357.2 | 0.174 | 3.45 | 0.1378 | 171.5 | 37.7 | 66.5 | 0.861 | 16.8 | 19.4 | 40.3 | 0.151 | 0.737 | 0 | 0 | 10 | 20 | 20 | |
| W5A2T40 | 145.0 | 0.162 | 8.64 | 0.1432 | 178.6 | 38.9 | 47.8 | 0.478 | 17.2 | 19.1 | 50.6 | 0.085 | 0.714 | 33.692 | 1.217 | 0 | 10 | 20 | |
| W5A2T42 | 145.0 | 0.160 | 11.88 | 0.1371 | 176.3 | 38.5 | 48.0 | 0.519 | 16.8 | 19.3 | 61.4 | 0.091 | 0.707 | 31.974 | 1.353 | 0 | 10 | 20 | |
| W5A2T44 | 144.2 | 0.167 | 16.77 | 0.1359 | 187.9 | 41.0 | 51.6 | 0.503 | 16.7 | 19.0 | 57.3 | 0.094 | 0.757 | 32.321 | 4.815 | 0 | 10 | 20 | |
| W5A2T45 | 145.8 | 0.157 | 8.92 | 0.1384 | 158.9 | 38.0 | 47.5 | 0.872 | 17.3 | 20.6 | 71.2 | 0.107 | 0.752 | 32.321 | 4.815 | 0 | 10 | 20 | |
| W5A2T46 | 174.8 | 0.179 | 5.59 | 0.1413 | 169.1 | 37.1 | 49.5 | 0.877 | 17.1 | 20.3 | 65.8 | 0.114 | 0.760 | 31.525 | 1.701 | 0 | 10 | 20 | |
| W5A2T48 | 174.8 | 0.171 | 9.38 | 0.1375 | 172.2 | 37.8 | 49.3 | 0.813 | 17.2 | 20.2 | 63.9 | 0.106 | 0.723 | 0 | 0 | 10 | 20 | 20 | |
| W5A2T49 | 175.6 | 0.170 | 12.94 | 0.1384 | 173.4 | 38.3 | 51.7 | 0.679 | 17.2 | 20.4 | 64.1 | 0.118 | 0.706 | 31.608 | 1.606 | 0 | 10 | 20 | |
| W5A2T50 | 174.8 | 0.168 | 4.22 | 0.1374 | 162.6 | 38.3 | 49.6 | 0.734 | 17.4 | 20.8 | 68.7 | 0.119 | 0.757 | 32.861 | 2.108 | 0 | 10 | 20 | |
| W5A2T51 | 212.9 | 0.167 | 16.77 | 0.1359 | 187.9 | 41.0 | 51.6 | 0.503 | 16.7 | 19.0 | 57.3 | 0.094 | 0.757 | 6 | 10 | 20 | 20 | 20 | |
| W5A2T52 | 212.9 | 0.163 | 9.20 | 0.1387 | 179.8 | 38.9 | 51.5 | 0.630 | 16.7 | 18.9 | 60.5 | 0.113 | 0.741 | 0 | 0 | 10 | 20 | 20 | |
| W5A2T53 | 203.6 | 0.168 | 3.61 | 0.1384 | 176.3 | 38.4 | 51.9 | 0.852 | 16.9 | 20.8 | 72.9 | 0.120 | 0.722 | 34.221 | 1.689 | 0 | 10 | 20 | |
| W5A2T55 | 202.8 | 0.176 | 7.95 | 0.1385 | 170.7 | 38.6 | 52.9 | 0.703 | 17.3 | 20.3 | 58.7 | 0.120 | 0.744 | 32.164 | 4.519 | 0 | 10 | 20 | |
| W5A2T56 | 210.4 | 0.157 | 4.46 | 0.1380 | 169.7 | 37.4 | 53.1 | 0.792 | 17.1 | 21.1 | 70.7 | 0.134 | 0.753 | 30.773 | 1.422 | 0 | 10 | 20 | |
| W5A2T59 | 209.6 | 0.190 | 4.74 | 0.1382 | 168.4 | 37.9 | 51.4 | 0.654 | 17.5 | 20.7 | 63.2 | 0.117 | 0.757 | 31.292 | 1.456 | 0 | 10 | 20 | |
| W5A2T61 | 219.7 | 0.178 | 10.11 | 0.1376 | 170.7 | 38.1 | 51.6 | 0.686 | 17.3 | 20.7 | 68.2 | 0.117 | 0.733 | 0 | 0 | 10 | 20 | 20 | |
| W5A2T65 | 220.6 | 0.170 | 9.41 | 0.1383 | 177.7 | 38.7 | 52.2 | 0.898 | 17.2 | 20.3 | 63.1 | 0.118 | 0.719 | 0 | 0 | 10 | 20 | 20 | |
| W5A2T66 | 145.0 | 0.142 | 9.15 | 0.1346 | 177.7 | 39.1 | 51.9 | 0.655 | 17.4 | 19.8 | 48.7 | 0.120 | 0.737 | 0 | 0 | 10 | 20 | 20 | |
| W5A2T67 | 145.0 | 0.176 | 15.91 | 0.1375 | 189.7 | 41.2 | 48.2 | 0.358 | 17.6 | 19.2 | 58.7 | 0.068 | 0.740 | 31.692 | 1.349 | 0 | 10 | 20 | |
| W5A2T69 | 145.0 | 0.169 | 9.43 | 0.1355 | 187.2 | 40.8 | 48.1 | 0.372 | 16.4 | 18.4 | 62.6 | 0.070 | 0.704 | 31.692 | 0.895 | 0 | 10 | 20 | |
| W5A2T75 | 170.5 | 0.190 | 8.95 | 0.1392 | 169.1 | 41.5 | 49.7 | 0.398 | 16.8 | 18.7 | 58.6 | 0.075 | 0.755 | 31.616 | 1.238 | 0 | 10 | 20 | |
| W5A2T76 | 196.0 | 0.166 | 16.27 | 0.1383 | 163.1 | 35.9 | 50.8 | 0.817 | 17.0 | 21.2 | 76.3 | 0.133 | 0.767 | 30.803 | 2.369 | 4 | 10 | 20 | |
| W5A2T77 | 196.8 | 0.184 | 8.52 | 0.1384 | 172.8 | 38.2 | 51.4 | 0.676 | 16.7 | 20.3 | 71.1 | 0.117 | 0.756 | 31.776 | 1.715 | 2 | 10 | 20 | |
| W5A2T79 | 195.1 | 0.174 | 8.62 | 0.1381 | 168.6 | 37.2 | 50.1 | 0.892 | 16.8 | 20.3 | 70.2 | 0.117 | 0.741 | 29.851 | 1.069 | 0 | 10 | 20 | |
| W5A2T80 | 196.8 | 0.159 | 25.79 | 0.1404 | 175.9 | 38.6 | 50.8 | 0.622 | 16.7 | 19.9 | 68.0 | 0.109 | 0.724 | 28.369 | 1.918 | 4 | 10 | 20 | |
| W5A2T83 | 204.5 | 0.156 | 5.13 | 0.1376 | 159.3 | 35.0 | 52.8 | 0.959 | 16.8 | 21.6 | 73.7 | 0.154 | 0.726 | 31.856 | 1.529 | 0 | 10 | 20 | |
| W5A2T84 | 203.6 | 0.160 | 16.25 | 0.1383 | 169.3 | 37.2 | 53.4 | 0.813 | 16.7 | 20.8 | 69.8 | 0.138 | 0.693 | 27.425 | 2.759 | 4 | 10 | 20 | |
| W5A2T85 | 188.3 | 0.160 | 8.13 | 0.1386 | 174.8 | 37.7 | 50.4 | 0.684 | 16.5 | 20.0 | 68.0 | 0.116 | 0.724 | 32.399 | 1.456 | 0 | 10 | 20 | |
| W5A2T88 | 188.3 | 0.147 | 8.84 | 0.1355 | 175.0 | 38.1 | 50.6 | 0.651 | 17.2 | 20.8 | 74.3 | 0.114 | 0.734 | 29.642 | 0.744 | 0 | 10 | 20 | |
| W5A2T89 | 187.5 | 0.180 | 9.44 | 0.1410 | 176.9 | 38.6 | 49.4 | 0.563 | 16.5 | 19.1 | 58.2 | 0.100 | 0.734 | 33.208 | 1.353 | 0 | 10 | 20 | |
| A3W5T01 | 145.9 | 0.130 | 10.77 | 0.1421 | 168.0 | 30.5 | 42.0 | 0.892 | 16.1 | 21.7 | 92.0 | 0.150 | 0.628 | 0.000 | 0.000 | 0 | 13 | 20 | |
| A3W5T02 | 145.9 | 0.112 | 7.14 | 0.1417 | 174.2 | 31.7 | 44.0 | 0.887 | 16.7 | 22.0 | 86.7 | 0.154 | 0.611 | 0.000 | 0.000 | 0 | 13 | 20 | |
| A3W5T03 | 145.9 | 0.131 | 9.92 | 0.1377 | 157.1 | 28.5 | 40.3 | 0.930 | 16.4 | 22.0 | 85.9 | 0.182 | 0.602 | 0.000 | 0.000 | 0 | 13 | 20 | |
| A3W5T04 | 145.9 | 0.140 | 7.83 | 0.1382 | 167.8 | 30.4 | 41.7 | 0.895 | 17.0 | 21.9 | 82.3 | 0.150 | 0.616 | 0.000 | 0.000 | 0 | 13 | 20 | |
| A3W5T05 | 145.0 | 0.142 | 8.45 | 0.1375 | 163.3 | 29.4 | 41.3 | 0.893 | 16.1 | 21.6 | 84.2 | 0.161 | 0.657 | 0.000 | 0.000 | 0 | 13 | 20 | |
| A3W5T08 | 171.4 | 0.178 | 15.73 | 0.1573 | 180.0 | 32.5 | 42.2 | 0.707 | 17.0 | 21.1 | 80.6 | 0.127 | 0.698 | 0.000 | 0.000 | 0 | 13 | 20 | |
| A3W5T09 | 172.2 | 0.159 | 13.21 | 0.1327 | 181.0 | 32.8 | 43.2 | 0.737 | 16.7 | 20.9 | 79.7 | 0.133 | 0.672 | 0.000 | 0.000 | 0 | 13 | 20 | |
| A3W5T10 | 171.4 | 0.148 | 10.14 | 0.1387 | 167.0 | 30.1 | 41.6 | 0.918 | 17.2 | 22.1 | 81.0 | 0.177 | 0.687 | 0.000 | 0.000 | 0 | 13 | 20 | |
| A3W5T11 | 187.5 | 0.165 | 15.48 | 0.1372 | 169.9 | 30.8 | 42.8 | 0.809 | 16.7 | 21.0 | 88.8 | 0.154 | 0.677 | 0.000 | 0.000 | 0 | 13 | 20 | |
| A3W5T13 | 179.0 | 0.153 | 17.65 | 0.1342 | 178.1 | 32.4 | 45.7 | 0.901 | 17.0 | 22.2 | 80.7 | 0.160 | 0.664 | 0.000 | 0.000 | 0 | 13 | 20 | |
| A3W5T14 | 186.8 | 0.168 | 9.84 | 0.1363 | 169.7 | 30.7 | 42.6 | 0.899 | 16.6 | 21.5 | 79.4 | 0.154 | 0.664 | 0.000 | 0.000 | 0 | 13 | 20 | |
| A3W5T21 | 229.1 | 0.172 | 11.05 | 0.1346 | 172.4 | 31.5 | 47.7 | 1.077 | 16.1 | 20.8 | 70.6 | 0.188 | 0.697 | 0.000 | 0.000 | 0 | 10 | 20 | |
| A3W5T24 | 229.1 | 0.164 | 8.54 | 0.1378 | 175.9 | 32.0 | 47.7 | 1.035 | 17.2 | 22.4 | 74.3 | 0.182 | 0.676 | 0.000 | 0.000 | 0 | 10 | 20 | |
| W5A3T26 | 128.9 | 0.126 | 21.43 | 0.1053 | 174.8 | 31.9 | 47.0 | 1.011 | 16.8 | 21.8 | 71.5 | 0.177 | 0.638 | 28.858 | 0.652 | 0 | 10 | 20 | |
| W5A3T27 | 127.2 | 0.131 | 19.08 | 0.1284 | 184.8 | 33.4 | 44.8 | 0.781 | 17.2 | 23.2 | 108.5 | 0.141 | 0.645 | 31.767 | 1.368 | 0 | 10 | 20 | |
| W5A3T28 | 128.1 | 0.141 | 19.15 | 0.1378 | 182.5 | 32.9 | 43.5 | 0.742 | 16.9 | 22.7 | 107.9 | 0.135 | 0.649 | 29.569 | 1.009 | 0 | 10 | 20 | |
| W5A3T29 | 128.8 | 0.136 | 16.91 | 0.1375 | 184.6 | 33.3 | 46.2 | 0.837 | 17.3 | 22.3 | 82.2 | 0.154 | 0.635 | 29.961 | 2.221 | | | | |

Table B1 Continued. Data with the IPST A platen.

| PLATEN SURFACE | TEMP (C) | SEM (MN/mm²) | OD BASIS WEIGHT (g/m²) | SHEET SOLIDS IN (%) | SHEET SOLIDS OUT (%) | MOISTURE RATIO CHANGE (%) | FELT MOISTURE IN (%) | FELT MOISTURE OUT (%) | FELT GAIN/LOSS (%) | AVERAGE STFI INDEX (Nm/m²) | US DENSITY (g/cm³) | 95% C.I. DELAM CODE | STICK/PICK CODE | REWET CODE | COMMENTS |
|----------------|----------|--------------|------------------------|---------------------|----------------------|---------------------------|----------------------|-----------------------|--------------------|----------------------------|--------------------|---------------------|-----------------|------------|----------|
| W5A3T37 | 187.5 | 0.100 | 18.80 | 0.126 | 184.6 | 33.6 | 48.5 | 0.912 | 17.1 | 22.9 | 66.5 | 0.168 | 0.678 | 27.856 | 1.603 |
| W5A3T41 | 178.1 | 0.115 | 16.52 | 0.1276 | 184.3 | 33.4 | 47.6 | 0.895 | 17.3 | 21.9 | 70.2 | 0.165 | 0.658 | 29.224 | 1.063 |
| W5A3T42 | 178.1 | 0.087 | 28.74 | 0.1412 | 185.2 | 33.3 | 47.9 | 0.912 | 17.8 | 23.9 | 94.8 | 0.169 | 0.667 | 27.464 | 1.780 |
| W5A3T43 | 171.4 | 0.085 | 20.00 | 0.1381 | 177.3 | 32.0 | 50.4 | 1.135 | 16.2 | 22.0 | 71.4 | 0.201 | 0.650 | 27.259 | 1.148 |
| W5A3T44 | 171.4 | 0.102 | 28.47 | 0.1413 | 179.0 | 32.2 | 46.2 | 0.936 | 16.7 | 22.9 | 90.6 | 0.168 | 0.675 | 27.339 | 1.0 |
| W5A3T45 | 162.0 | 0.123 | 21.05 | 0.1345 | 185.8 | 33.4 | 45.9 | 0.821 | 17.0 | 23.1 | 101.0 | 0.152 | 0.705 | 31.809 | 2.636 |
| W5A3T46 | 173.5 | 0.153 | 5.88 | 0.1214 | 173.8 | 31.5 | 46.6 | 1.023 | 16.7 | 23.6 | 97.3 | 0.178 | 0.678 | 32.127 | 1.356 |
| W5A3T48 | 164.4 | 0.146 | 13.70 | 0.1277 | 178.1 | 32.4 | 45.7 | 0.900 | 16.6 | 22.8 | 98.6 | 0.160 | 0.679 | 31.461 | 0 |
| W5A3T49 | 153.5 | 0.149 | 18.79 | 0.1354 | 185.8 | 33.4 | 46.1 | 0.822 | 16.5 | 22.8 | 104.2 | 0.152 | 0.687 | 31.222 | 0.1047 |
| W5A3T50 | 162.7 | 0.155 | 14.19 | 0.1376 | 182.7 | 33.1 | 45.4 | 0.822 | 16.5 | 22.5 | 98.8 | 0.150 | 0.681 | 0.577 | 0 |
| W5A3T51 | 154.4 | 0.155 | 17.42 | 0.1340 | 178.3 | 32.2 | 44.9 | 0.883 | 16.9 | 23.0 | 99.9 | 0.158 | 0.687 | 30.684 | 0 |
| W5A3T55 | 162.9 | 0.157 | 20.38 | 0.1389 | 184.3 | 33.3 | 45.8 | 0.818 | 16.9 | 22.6 | 98.9 | 0.151 | 0.681 | 31.669 | 2.577 |
| W5A3T56 | 162.9 | 0.149 | 15.44 | 0.1394 | 188.7 | 34.0 | 46.1 | 0.769 | 16.9 | 22.6 | 99.5 | 0.145 | 0.676 | 31.414 | 0 |
| W5A3T57 | 169.7 | 0.148 | 24.32 | 0.1387 | 169.7 | 30.6 | 46.3 | 1.114 | 16.9 | 23.9 | 94.0 | 0.189 | 0.697 | 28.604 | 1.913 |
| W5A3T80 | 170.5 | 0.130 | 27.69 | 0.1334 | 178.6 | 32.3 | 45.4 | 0.890 | 16.9 | 23.1 | 98.0 | 0.159 | 0.679 | 28.144 | 2.796 |
| W5A3T81 | 171.4 | 0.152 | 19.74 | 0.1385 | 183.3 | 33.3 | 47.3 | 0.893 | 16.8 | 23.2 | 98.6 | 0.164 | 0.686 | 0.795 | 4 |
| A4W5T02 | 147.6 | 0.139 | 5.78 | 0.1411 | 157.7 | 34.8 | 48.2 | 0.713 | 17.3 | 20.7 | 75.3 | 0.112 | 0.733 | 0 | 13 |
| A4W5T03 | 144.2 | 0.143 | 7.69 | 0.1376 | 172.8 | 37.8 | 45.0 | 0.421 | 17.1 | 19.2 | 70.5 | 0.073 | 0.714 | 0 | 13 |
| A4W5T04 | 144.2 | 0.149 | 8.04 | 0.1382 | 187.3 | 36.7 | 46.2 | 0.559 | 17.8 | 20.6 | 71.6 | 0.094 | 0.725 | 0 | 13 |
| A4W5T05 | 145.9 | 0.165 | 8.67 | 0.1388 | 170.1 | 37.0 | 45.6 | 0.508 | 17.0 | 19.3 | 63.2 | 0.086 | 0.701 | 0 | 13 |
| A4W5T06 | 169.7 | 0.151 | 9.27 | 0.1394 | 188.7 | 41.1 | 47.4 | 0.324 | 17.1 | 18.7 | 62.8 | 0.061 | 0.732 | 1 | 13 |
| A4W5T07 | 169.7 | 0.163 | 7.83 | 0.1390 | 167.4 | 38.5 | 45.9 | 0.561 | 16.8 | 19.3 | 68.5 | 0.094 | 0.713 | 0 | 13 |
| A4W5T08 | 171.4 | 0.172 | 11.05 | 0.1386 | 174.2 | 37.4 | 46.8 | 0.532 | 17.1 | 20.0 | 78.8 | 0.093 | 0.704 | 0 | 19 |
| A4W5T09 | 171.4 | 0.153 | 7.19 | 0.1394 | 178.1 | 38.7 | 46.7 | 0.441 | 17.2 | 19.8 | 72.8 | 0.078 | 0.698 | 0 | 13 |
| A4W5T10 | 171.4 | 0.149 | 10.74 | 0.1400 | 188.7 | 41.3 | 47.6 | 0.318 | 16.6 | 18.2 | 60.4 | 0.060 | 0.691 | 0 | 19 |
| A4W5T11 | 168.3 | 0.177 | 9.04 | 0.1391 | 173.6 | 38.1 | 47.7 | 0.532 | 16.5 | 19.1 | 68.5 | 0.092 | 0.714 | 2 | 10 |
| A4W5T12 | 169.2 | 0.145 | 10.34 | 0.1373 | 170.7 | 37.2 | 46.8 | 0.559 | 17.2 | 20.0 | 72.6 | 0.095 | 0.673 | 1 | 13 |
| A4W5T13 | 168.3 | 0.173 | 8.09 | 0.1377 | 184.7 | 35.9 | 48.5 | 0.634 | 17.1 | 20.3 | 74.1 | 0.104 | 0.680 | 1 | 13 |
| A4W5T14 | 168.3 | 0.171 | 7.60 | 0.1385 | 157.6 | 34.5 | 48.9 | 0.765 | 16.4 | 20.1 | 75.5 | 0.120 | 0.705 | 1 | 13 |
| A4W5T17 | 207.0 | 0.167 | 10.18 | 0.1402 | 173.8 | 37.8 | 48.1 | 0.564 | 16.8 | 19.4 | 65.7 | 0.098 | 0.698 | 0 | 13 |
| A4W5T20 | 205.3 | 0.169 | 9.52 | 0.1385 | 180.4 | 38.9 | 48.8 | 0.518 | 16.0 | 18.8 | 71.7 | 0.094 | 0.692 | 0 | 19 |
| A4W5T21 | 228.1 | 0.184 | 7.32 | 0.1305 | 178.4 | 39.5 | 51.4 | 0.587 | 16.7 | 19.8 | 72.1 | 0.105 | 0.709 | 2 | 10 |
| A4W5T22 | 228.2 | 0.170 | 4.71 | 0.1310 | 178.6 | 39.4 | 52.1 | 0.619 | 16.8 | 19.7 | 61.8 | 0.111 | 0.673 | 1 | 13 |
| A4W5T23 | 228.9 | 0.191 | 5.76 | 0.1343 | 187.2 | 41.1 | 50.6 | 0.457 | 16.7 | 19.1 | 67.1 | 0.086 | 0.733 | 0 | 10 |
| A4W5T25 | 225.7 | 0.163 | 9.20 | 0.1377 | 194.5 | 42.4 | 51.8 | 0.428 | 17.3 | 19.5 | 65.7 | 0.083 | 0.718 | 0 | 13 |
| W5A4T28 | 128.1 | 0.148 | 13.70 | 0.1393 | 173.4 | 37.7 | 47.0 | 0.527 | 16.9 | 20.9 | 108.9 | 0.091 | 0.713 | 32.293 | 4.934 |
| W5A4T27 | 128.1 | 0.128 | 16.28 | 0.1429 | 178.4 | 39.0 | 48.1 | 0.483 | 17.4 | 21.2 | 111.1 | 0.087 | 0.680 | 28.509 | 1.988 |
| W5A4T28 | 128.9 | 0.126 | 13.49 | 0.1367 | 162.9 | 35.2 | 47.9 | 0.754 | 17.4 | 21.8 | 89.0 | 0.123 | 0.677 | 28.349 | 3.681 |
| W5A4T29 | 128.9 | 0.153 | 9.80 | 0.1390 | 168.2 | 34.0 | 45.9 | 0.656 | 18.0 | 22.8 | 103.4 | 0.120 | 0.693 | 32.194 | 3.918 |
| W5A4T30 | 128.1 | 0.138 | 15.94 | 0.1394 | 183.9 | 40.0 | 47.2 | 0.386 | 16.8 | 19.7 | 93.7 | 0.071 | 0.691 | 31.718 | 1.838 |
| W5A4T31 | 145.9 | 0.157 | 11.48 | 0.1366 | 179.0 | 38.9 | 47.9 | 0.486 | 17.3 | 20.5 | 92.5 | 0.087 | 0.730 | 31.707 | 1.884 |
| W5A4T33 | 145.0 | 0.148 | 9.59 | 0.1367 | 170.5 | 37.3 | 49.2 | 0.648 | 17.0 | 20.0 | 67.2 | 0.111 | 0.718 | 30.569 | 1.785 |
| W5A4T34 | 145.0 | 0.159 | 10.69 | 0.1405 | 187.7 | 40.6 | 48.5 | 0.403 | 16.7 | 18.8 | 66.3 | 0.076 | 0.714 | 31.107 | 1.035 |
| W5A4T35 | 144.2 | 0.147 | 12.24 | 0.1403 | 180.4 | 34.9 | 47.7 | 0.765 | 17.0 | 21.2 | 83.9 | 0.123 | 0.692 | 31.668 | 1.127 |
| W5A4T36 | 176.6 | 0.160 | 8.75 | 0.1368 | 171.3 | 37.2 | 49.0 | 0.647 | 16.6 | 20.6 | 87.5 | 0.111 | 0.743 | 30.635 | 1.422 |
| W5A4T38 | 175.8 | 0.145 | 8.28 | 0.1368 | 173.8 | 37.9 | 49.6 | 0.594 | 16.6 | 20.1 | 81.8 | 0.103 | 0.732 | 29.352 | 2.285 |
| W5A4T39 | 173.9 | 0.125 | 24.80 | 0.1424 | 180.6 | 39.2 | 49.0 | 0.513 | 17.3 | 20.7 | 91.4 | 0.093 | 0.710 | 27.807 | 2.768 |
| W5A4T41 | 187.5 | 0.120 | 17.50 | 0.1362 | 173.2 | 37.8 | 49.7 | 0.630 | 16.9 | 20.4 | 79.7 | 0.109 | 0.720 | 28.683 | 1.074 |
| W5A4T42 | 188.3 | 0.103 | 28.16 | 0.1408 | 172.2 | 37.6 | 49.3 | 0.628 | 16.8 | 20.5 | 85.0 | 0.108 | 0.703 | 27.723 | 1.485 |
| W5A4T43 | 187.5 | 0.118 | 25.00 | 0.1374 | 187.7 | 40.9 | 50.1 | 0.448 | 17.2 | 20.1 | 87.2 | 0.084 | 0.720 | 27.434 | 1.388 |

Table B2. Data with the IPST C plates.

| PLATEN SAMPLE ID | TEMP (C) | SEM (MN m/kg) | SEM %CV | OD IMPULSE (MPa) | BASIS WEIGHT (g/m ²) | OD SHEET SOLIDS IN OUT (%) | SHEET SOLIDS MOISTURE RATIO CHANGE (%) | FELT MOISTURE IN OUT (%) | FELT GAIN/ LOSS (%) | AVERAGE STI INDEX | US DENSITY (kg/m ³) | 95% C.I. (Nm/g) | DELAM CODE | REWET CODE | STICK/ PICK CODE | COMMENTS | | |
|---------------------|-------------|------------------|------------|------------------------|--|---|---|--------------------------------------|------------------------------|-------------------------|---------------------------------------|--------------------|---------------|---------------|------------------------|----------|----|----|
| | | | | | | | | | | | | | | | | | | |
| WIC1T01 | 147.2 | 0.159 | 11.32 | 0.1404 | 166.0 | 33.0 | 44.8 | 0.797 | 17.1 | 21.0 | 68.4 | 0.132 | 0.691 | 2.706 | 0 | 10 | 20 | |
| WIC1T02 | 147.2 | 0.157 | 10.19 | 0.1434 | 174.6 | 34.9 | 45.1 | 0.651 | 17.1 | 20.2 | 66.1 | 0.114 | 0.667 | 30.074 | 1.295 | 0 | 10 | 20 |
| WIC1T03 | 147.2 | 0.158 | 12.66 | 0.1422 | 158.7 | 31.5 | 44.7 | 0.938 | 17.0 | 21.6 | 70.6 | 0.149 | 0.685 | 26.638 | 2.853 | 0 | 10 | 20 |
| WIC1T04 | 148.1 | 0.155 | 9.03 | 0.1418 | 163.7 | 32.6 | 44.8 | 0.837 | 17.4 | 21.5 | 71.7 | 0.137 | 0.668 | 28.148 | 1.989 | 0 | 10 | 20 |
| WIC1T05 | 149.1 | 0.151 | 17.88 | 0.1376 | 189.7 | 45.4 | 45.4 | 0.459 | 17.3 | 19.7 | 60.7 | 0.087 | 0.649 | 29.566 | 1.366 | 0 | 10 | 20 |
| WIC1T06 | 193.4 | 0.168 | 11.90 | 0.1404 | 165.6 | 33.6 | 46.7 | 0.834 | 17.1 | 21.3 | 69.5 | 0.141 | 0.693 | 1.064 | 1 | 10 | 20 | |
| WIC1T07 | 192.5 | 0.157 | 9.55 | 0.1386 | 184.6 | 37.1 | 47.4 | 0.588 | 17.4 | 20.3 | 63.1 | 0.108 | 0.674 | 26.962 | 1.517 | 2 | 10 | 20 |
| WIC1T08 | 192.5 | 0.168 | 11.45 | 0.1414 | 163.1 | 32.4 | 46.7 | 0.946 | 17.5 | 21.8 | 68.8 | 0.154 | 0.846 | 3.036 | 2.2 | 0 | 10 | 20 |
| WIC1T11 | 208.6 | 0.172 | 13.37 | 0.1393 | 186.2 | 36.9 | 47.4 | 0.599 | 16.8 | 19.7 | 61.5 | 0.112 | 0.701 | 29.684 | 0.910 | 1 | 10 | 20 |
| WIC1T13 | 207.6 | 0.149 | 8.05 | 0.1395 | 162.6 | 32.2 | 48.5 | 1.043 | 17.4 | 22.5 | 73.0 | 0.170 | 0.684 | 26.179 | 1.520 | 2 | 10 | 20 |
| WIC1T14 | 206.7 | 0.135 | 23.70 | 0.1391 | 182.3 | 36.2 | 47.3 | 0.650 | 17.3 | 20.2 | 58.1 | 0.118 | 0.681 | 27.185 | 1.990 | 6 | 10 | 20 |
| WIC1T16 | 183.1 | 0.173 | 9.83 | 0.1343 | 176.1 | 35.0 | 45.3 | 0.652 | 17.2 | 20.5 | 67.0 | 0.115 | 0.689 | 29.630 | 1.064 | 0 | 10 | 20 |
| WIC1T17 | 183.1 | 0.165 | 4.24 | 0.1362 | 165.8 | 33.5 | 45.1 | 0.774 | 17.3 | 21.0 | 67.7 | 0.131 | 0.670 | 30.762 | 1.286 | 0 | 10 | 20 |
| WIC1T21 | 169.8 | 0.159 | 11.32 | 0.1349 | 186.4 | 36.8 | 45.9 | 0.541 | 17.1 | 19.5 | 55.7 | 0.101 | 0.660 | 30.252 | 1.337 | 0 | 10 | 20 |
| WIC1T22 | 168.9 | 0.158 | 19.87 | 0.1391 | 184.3 | 38.6 | 45.4 | 0.388 | 17.2 | 18.7 | 48.8 | 0.075 | 0.633 | 29.506 | 2.221 | 0 | 10 | 20 |
| WIC1T24 | 169.8 | 0.151 | 7.28 | 0.1380 | 182.5 | 36.4 | 45.3 | 0.540 | 16.8 | 19.3 | 57.9 | 0.099 | 0.625 | 29.953 | 1.346 | 0 | 10 | 20 |
| WIC2T01 | 146.2 | 0.141 | 13.48 | 0.1394 | 186.2 | 44.3 | 49.3 | 0.226 | 17.3 | 17.9 | 34.9 | 0.042 | 0.678 | 28.398 | 1.076 | 0 | 10 | 20 |
| WIC2T03 | 147.2 | 0.173 | 9.25 | 0.1390 | 187.0 | 44.6 | 49.2 | 0.207 | 17.0 | 17.7 | 38.5 | 0.039 | 0.716 | 29.734 | 2.169 | 0 | 10 | 20 |
| WIC2T04 | 147.2 | 0.175 | 8.00 | 0.1414 | 175.3 | 41.7 | 48.4 | 0.331 | 16.9 | 18.1 | 49.6 | 0.058 | 0.706 | 30.249 | 1.236 | 0 | 10 | 20 |
| WIC2T05 | 147.2 | 0.168 | 7.14 | 0.1362 | 180.4 | 43.6 | 48.6 | 0.237 | 17.3 | 18.4 | 54.8 | 0.043 | 0.708 | 30.071 | 1.162 | 0 | 10 | 20 |
| WIC2T08 | 192.5 | 0.160 | 20.00 | 0.1430 | 184.3 | 43.7 | 50.9 | 0.320 | 17.8 | 18.5 | 48.4 | 0.059 | 0.715 | 32.805 | 3.834 | 4 | 10 | 20 |
| WIC2T09 | 192.5 | 0.162 | 12.35 | 0.1385 | 181.7 | 43.2 | 50.8 | 0.342 | 17.4 | 18.8 | 49.2 | 0.062 | 0.690 | 30.331 | 1.162 | 1 | 10 | 20 |
| WIC2T10 | 194.4 | 0.157 | 8.28 | 0.1406 | 180.6 | 42.9 | 50.3 | 0.343 | 16.9 | 18.2 | 47.8 | 0.062 | 0.692 | 29.767 | 1.081 | 1 | 10 | 25 |
| WIC2T11 | 208.6 | 0.138 | 13.04 | 0.1372 | 188.4 | 44.3 | 51.4 | 0.313 | 17.1 | 17.9 | 33.2 | 0.058 | 0.701 | 28.231 | 1.438 | 4 | 10 | 20 |
| WIC2T12 | 207.8 | 0.138 | 20.29 | 0.1407 | 192.2 | 45.9 | 51.9 | 0.253 | 17.2 | 18.2 | 47.5 | 0.049 | 0.683 | 28.851 | 2.482 | 4 | 10 | 20 |
| WIC2T13 | 208.6 | 0.167 | 5.39 | 0.1391 | 188.8 | 44.7 | 51.1 | 0.281 | 17.4 | 18.3 | 41.3 | 0.052 | 0.726 | 29.082 | 1.353 | 4 | 10 | 20 |
| WIC2T14 | 208.8 | 0.149 | 19.46 | 0.1385 | 189.9 | 45.7 | 51.5 | 0.247 | 17.5 | 18.2 | 35.2 | 0.047 | 0.711 | 28.025 | 1.533 | 2 | 10 | 20 |
| WIC2T15 | 208.7 | 0.162 | 11.84 | 0.1385 | 185.4 | 44.6 | 50.2 | 0.288 | 17.6 | 18.3 | 31.0 | 0.049 | 0.695 | 30.791 | 1.490 | 0 | 10 | 20 |
| WIC2T17 | 183.1 | 0.152 | 16.45 | 0.1368 | 185.6 | 43.6 | 50.5 | 0.311 | 17.0 | 18.3 | 51.6 | 0.057 | 0.689 | 27.403 | 1.018 | 4 | 10 | 20 |
| WIC2T18 | 184.9 | 0.163 | 9.15 | 0.1377 | 180.5 | 45.4 | 51.1 | 0.244 | 17.1 | 17.8 | 33.2 | 0.046 | 0.677 | 28.620 | 1.627 | 0 | 10 | 20 |
| WIC2T20 | 184.0 | 0.172 | 6.98 | 0.1389 | 185.7 | 45.1 | 50.9 | 0.253 | 17.6 | 18.4 | 40.9 | 0.048 | 0.672 | 31.108 | 1.146 | 0 | 10 | 20 |
| WIC2T21 | 186.9 | 0.171 | 11.11 | 0.1391 | 183.3 | 43.7 | 49.9 | 0.284 | 17.1 | 17.8 | 31.0 | 0.052 | 0.728 | 30.458 | 1.228 | 0 | 10 | 20 |
| WIC2T22 | 170.8 | 0.165 | 10.26 | 0.1387 | 184.6 | 44.0 | 49.9 | 0.267 | 17.3 | 18.2 | 41.2 | 0.049 | 0.695 | 30.791 | 1.490 | 0 | 10 | 20 |
| WIC2T23 | 169.8 | 0.180 | 12.22 | 0.1370 | 189.7 | 45.1 | 50.4 | 0.233 | 17.7 | 18.1 | 24.4 | 0.044 | 0.723 | 32.131 | 1.032 | 0 | 10 | 20 |
| WIC2T24 | 168.9 | 0.161 | 16.77 | 0.1379 | 187.9 | 45.1 | 52.1 | 0.162 | 17.3 | 17.4 | 5.1 | 0.033 | 0.725 | 2.354 | 0 | 10 | 20 | |
| WIC2T25 | 169.8 | 0.160 | 8.13 | 0.1387 | 187.4 | 45.1 | 50.2 | 0.227 | 17.3 | 18.0 | 40.4 | 0.043 | 0.736 | 30.697 | 1.547 | 0 | 10 | 20 |
| W5C1T01 | 147.2 | 0.139 | 23.02 | 0.1303 | 180.2 | 35.6 | 45.3 | 0.670 | 17.1 | 20.1 | 64.8 | 0.108 | 0.692 | 30.057 | 1.931 | 0 | 10 | 20 |
| W5C1T02 | 147.2 | 0.138 | 20.29 | 0.1297 | 176.9 | 35.0 | 43.8 | 0.675 | 15.5 | 18.1 | 55.1 | 0.102 | 0.662 | 30.562 | 1.534 | 0 | 10 | 20 |
| W5C1T03 | 147.2 | 0.145 | 13.79 | 0.133 | 167.6 | 33.4 | 43.4 | 0.688 | 17.1 | 20.3 | 65.4 | 0.115 | 0.660 | 30.498 | 2.936 | 0 | 10 | 20 |
| W5C1T06 | 192.5 | 0.163 | 7.98 | 0.138 | 182.1 | 36.3 | 45.8 | 0.668 | 16.6 | 19.5 | 64.0 | 0.103 | 0.718 | 32.716 | 1.714 | 0 | 10 | 20 |
| W5C1T07 | 193.4 | 0.154 | 9.09 | 0.141 | 182.8 | 32.3 | 46.4 | 0.943 | 16.9 | 21.2 | 68.4 | 0.153 | 0.659 | 30.504 | 1.816 | 0 | 10 | 20 |
| W5C1T14 | 213.3 | 0.182 | 7.41 | 0.138 | 183.5 | 36.4 | 46.8 | 0.615 | 17.5 | 20.5 | 62.7 | 0.113 | 0.659 | 31.259 | 0.732 | 0 | 10 | 20 |
| W5C1T15 | 211.4 | 0.168 | 10.24 | 0.137 | 156.2 | 31.1 | 45.6 | 1.023 | 17.2 | 21.9 | 68.2 | 0.160 | 0.726 | 28.908 | 2.009 | 0 | 10 | 20 |
| W5C1T16 | 232.2 | 0.150 | 14.00 | 0.131 | 169.5 | 33.6 | 46.7 | 0.834 | 16.9 | 21.6 | 75.8 | 0.141 | 0.749 | 30.825 | 0 | 10 | 20 | |
| W5C1T18 | 232.2 | 0.141 | 15.80 | 0.1418 | 175.7 | 34.8 | 47.8 | 0.785 | 17.1 | 21.4 | 75.1 | 0.138 | 0.722 | 29.214 | 1.810 | 4 | 10 | 20 |
| W5C1T19 | 232.2 | 0.137 | 8.76 | 0.138 | 182.5 | 36.1 | 47.3 | 0.655 | 17.0 | 20.2 | 59.7 | 0.119 | 0.707 | 28.830 | 1.115 | 1 | 10 | 20 |
| W5C1T22 | 239.7 | 0.135 | 16.30 | 0.138 | 163.9 | 32.4 | 47.1 | 0.962 | 16.8 | 21.9 | 74.4 | 0.158 | 0.703 | 27.088 | 2.913 | 4 | 10 | 20 |
| W5C1T23 | 239.7 | 0.130 | 20.00 | 0.139 | 163.9 | 32.6 | 47.1 | 0.948 | 17.3 | 22.0 | 72.3 | 0.155 | 0.703 | 27.531 | 1.031 | 4 | 10 | 20 |
| W5C1T24 | 241.6 | 0.151 | 11.92 | 0.138 | 183.3 | 36.5 | 48.1 | 0.681 | 17.3 | 21.0 | 72.6 | 0.121 | 0.702 | 30.712 | 1.303 | 4 | 10 | 20 |
| W5C1T25 | 239.7 | 0.154 | 9.09 | 0.137 | 181.7 | 36.1 | 48.2 | 0.693 | 17.1 | 20.8 | 68.0 | 0.126 | 0.707 | 30.368 | 1.987 | 4 | 10 | 20 |
| W5C2T01 | 146.2 | 0.163 | 7.55 | 0.1297 | 175.5 | 41.7 | 47.6 | 0.297 | 16.7 | 17.8 | 45.4 | 0.052 | 0.709 | 32.429 | 1.607 | 0 | 10 | 20 |
| W5C2T02 | 147.2 | 0.138 | 8.42 | 0.132 | 182.9 | 43.7 | 48.0 | 0.203 | 17.2 | 17.5 | 20.3 | 0.037 | 0.685 | 31.208 | 0.397 | 0 | 10 | 20 |
| W5C2T03 | 146.2 | 0.146 | 10.98 | 0.135 | 182.5 | 43.7 | 48.3 | 0.219 | 17.1 | 17.4 | 40.8 | 0.040 | 0.683 | 31.290 | 1.009 | 0 | 10 | 20 |
| W5C2T04 | 148.2 | 0.162 | 11.73 | 0.135 | 184.4 | 39.7 | 46.8 | 0.382 | 17.2 | 18.5 | 45.4 | 0.063 | 0.704 | 32.501 | 2.916 | 0 | 10 | 20 |
| W5C2T08 | 194.4 | 0.168 | 8.33 | 0.1426 | 174.4 | 41.3 | 49.8 | 0.418 | 17.2 | 18.5 | 38.0 | 0.073 | 0.752 | 32.010 | 1.775 | 0 | 10 | 20 |
| W5C2T09 | 192.5 | 0.177 | 6.21 | 0.1337 | 177.1 | 41.9 | 49.1 | 0.353 | 17.6 | 18.8 | 40.4 | 0.062 | 0.738 | 32.183 | 0.933 | 0 | 10 | 20 |
| W5C2T13 | 212.3 | 0.176 | 8.09 | 0.139 | 184.8</ | | | | | | | | | | | | | |

Table B2 Continued. Data with the IPST C platen.

| PLATEN SURFACE TEMP (C) | SEM (MN m/kg) | SEM (%CV) | IMPULSE (MPa.s) | OD BASIS WEIGHT (g/m ²) | SHEET SOLIDS | | | FELT GAIN/LOSS (%) | | | AVERAGE STFI INDEX (Nm/g) | | | 95% C.I. DELAM CODE | REWET CODE | STICKY PICK CODE | COMMENTS | |
|-------------------------|---------------|-----------|-----------------|-------------------------------------|---------------|---------------|-----------------|--------------------|------------------------------------|---------------------------------|---------------------------|-------|-------|---------------------|------------|------------------|----------|----|
| | | | | | SHEET OUT (%) | SOLID OUT (%) | MOISTURE IN (%) | MOISTURE OUT (%) | WATER REMOVED (kg/m ²) | US DENSITY (g/cm ³) | | | | | | | | |
| W52T15 | 213.3 | 0.146 | 6.16 | 0.141 | 185.6 | 44.6 | 51.3 | 0.294 | 17.7 | 18.8 | 48.0 | 0.055 | 0.726 | 2.095 | 0 | 10 | 20 | |
| W52T17 | 232.2 | 0.145 | 8.21 | 0.137 | 185.4 | 44.0 | 53.0 | 0.387 | 17.5 | 19.1 | 62.3 | 0.072 | 0.724 | 29.165 | 2.171 | 0 | 10 | 20 |
| W52T19 | 231.2 | 0.201 | 8.46 | 0.135 | 168.4 | 39.6 | 50.0 | 0.525 | 17.5 | 19.6 | 53.8 | 0.087 | 0.725 | 32.575 | 1.984 | 0 | 10 | 20 |
| W52T20 | 232.2 | 0.169 | 10.65 | 0.138 | 185.2 | 44.1 | 51.2 | 0.316 | 17.2 | 18.2 | 40.5 | 0.059 | 0.726 | 30.008 | 1.560 | 0 | 10 | 20 |
| W52T22 | 249.2 | 0.184 | 4.89 | 0.139 | 180.6 | 43.4 | 52.3 | 0.389 | 17.1 | 18.8 | 45.5 | 0.070 | 0.724 | 30.354 | 1.896 | 0 | 10 | 20 |
| W52T23 | 249.2 | 0.184 | 5.43 | 0.139 | 171.3 | 40.7 | 51.1 | 0.602 | 17.8 | 19.7 | 52.6 | 0.086 | 0.738 | 32.550 | 0.567 | 0 | 10 | 20 |
| W52T24 | 251.1 | 0.183 | 7.65 | 0.138 | 162.2 | 38.7 | 51.2 | 0.630 | 17.5 | 20.0 | 57.8 | 0.102 | 0.730 | 33.076 | 3.122 | 0 | 10 | 20 |
| W52T29 | 269.9 | 0.280 | 5.00 | 0.136 | 180.2 | 43.1 | 51.9 | 0.391 | 16.8 | 18.1 | 47.6 | 0.070 | 0.740 | 31.052 | 2.005 | 0 | 10 | 20 |
| W52T30 | 267.1 | 0.190 | 6.32 | 0.139 | 189.1 | 45.2 | 52.9 | 0.320 | 17.0 | 17.7 | 24.2 | 0.060 | 0.751 | 31.528 | 2.049 | 0 | 10 | 20 |
| W52T31 | 268.8 | 0.168 | 7.83 | 0.138 | 195.3 | 46.4 | 55.5 | 0.355 | 17.5 | 18.6 | 38.5 | 0.069 | 0.731 | 28.654 | 1.112 | 0 | 10 | 20 |
| W52T33 | 278.4 | 0.183 | 4.92 | 0.139 | 188.5 | 44.5 | 54.5 | 0.415 | 17.2 | 18.0 | 60.9 | 0.078 | 0.787 | 32.895 | 1.720 | 0 | 10 | 20 |
| W52T34 | 268.6 | 0.180 | 18.67 | 0.144 | 171.1 | 40.2 | 51.7 | 0.549 | 16.7 | 18.8 | 51.3 | 0.094 | 0.755 | 30.985 | 2.461 | 4 | 10 | 20 |
| W52T35 | 259.6 | 0.168 | 10.24 | 0.141 | 167.8 | 40.0 | 53.4 | 0.828 | 17.3 | 20.1 | 64.6 | 0.105 | 0.738 | 29.882 | 2.642 | 1 | 10 | 20 |
| W52T38 | 280.5 | 0.167 | 18.17 | 0.139 | 161.0 | 38.3 | 51.6 | 0.674 | 17.2 | 20.1 | 63.1 | 0.108 | 0.759 | 32.438 | 1.798 | 4 | 10 | 20 |
| W52T37 | 259.6 | 0.165 | 11.11 | 0.138 | 184.8 | 43.9 | 53.8 | 0.416 | 17.5 | 19.2 | 46.8 | 0.077 | 0.747 | 29.855 | 1.192 | 0 | 10 | 20 |
| W52T38 | 258.6 | 0.165 | 15.76 | 0.138 | 169.9 | 40.6 | 52.2 | 0.552 | 17.5 | 19.8 | 59.2 | 0.094 | 0.745 | 29.173 | 1.357 | 2 | 10 | 20 |

Table B3. Data for the double-felted pressing control cases.

| PLATEN SURFACE TEMP (C) | SEM (MN/mkg) | SEM %CV | IMPULSE (MPa.s) | IMPULSE %CV | OD BASIS WEIGHT (g/m ²) | SHEET SOLIDS IN (%) | SHEET MOISTURE OUT (%) | FELT MOISTURE IN (%) | FELT MOISTURE OUT (%) | WATER REMOVED (%) | US DENSITY (g/cm ³) | STFI INDEX (Nm/g) | 95% C.I. CODE | DELAW CODE | REWET CODE | STICK/PICK CODE | COMMENTS | | |
|-------------------------|--------------|---------|-----------------|-------------|-------------------------------------|---------------------|------------------------|----------------------|-----------------------|-------------------|---------------------------------|-------------------|---------------|------------|------------|-----------------|----------|------------|----|
| | | | | | | | | | | | | | | | | | | | |
| WID1T01 | 99.0 | 0.136 | 19.85 | 0.116 | 189.7 | 37.6 | 41.8 | 0.288 | 17.8 | 18.9 | 45.2 | 0.051 | 0.639 | 28.923 | 1.127 | 0 | 20 | TOP BOTTOM | |
| WID1T02 | 99.0 | 0.123 | 21.14 | 0.1236 | 181.5 | 36.1 | 41.6 | 0.366 | 18.0 | 19.7 | 40.2 | 0.068 | 0.616 | 28.577 | 1.052 | 0 | 10 | 20 | |
| WID1T02 | 99.0 | 0.133 | 16.15 | 0.1324 | 175.7 | 35.0 | 41.2 | 0.434 | 18.2 | 20.0 | 59.7 | 0.076 | 0.606 | 30.247 | 1.499 | 0 | 10 | 20 | |
| WID1T03 | 99.0 | 0.130 | 16.15 | 0.1324 | 175.7 | 35.0 | 41.2 | 0.434 | 17.2 | 18.9 | 52.6 | 0.094 | 0.621 | 28.927 | 0.881 | 0 | 10 | 20 | |
| WID1T03 | 99.0 | 0.135 | 16.30 | 0.1398 | 170.7 | 33.9 | 41.7 | 0.551 | 17.7 | 20.0 | 55.9 | 0.094 | 0.617 | 29.100 | 1.787 | 0 | 10 | 20 | |
| WID1T08 | 99.0 | 0.137 | 17.52 | 0.139 | 166.6 | 33.1 | 41.2 | 0.593 | 17.6 | 19.5 | 45.6 | 0.099 | 0.617 | 29.100 | 1.787 | 0 | 10 | 20 | |
| WID1T10 | 99.0 | 0.137 | 17.52 | 0.139 | 166.6 | 33.1 | 41.2 | 0.593 | 18.9 | 18.5 | 37.3 | 0.099 | 0.617 | 29.100 | 1.787 | 0 | 10 | 20 | |
| WID1T10 | 99.0 | 0.150 | 13.33 | 0.1520 | 176.1 | 41.7 | 45.3 | 0.189 | 18.2 | 18.3 | 5.0 | 0.033 | 0.678 | 30.728 | 1.504 | 0 | 10 | 20 | |
| WID2T02 | 98.1 | 0.150 | 17.39 | 0.1439 | 177.3 | 42.0 | 45.7 | 0.193 | 17.8 | 18.5 | 44.0 | 0.034 | 0.659 | 29.040 | 1.220 | 0 | 10 | 20 | |
| WID2T03 | 99.0 | 0.138 | 12.58 | 0.1290 | 164.9 | 39.3 | 43.8 | 0.257 | 17.9 | 18.6 | 41.5 | 0.042 | 0.679 | 28.426 | 2.077 | 0 | 10 | 20 | |
| WID2T06 | 98.1 | 0.151 | 12.58 | 0.1290 | 164.9 | 39.3 | 43.8 | 0.257 | 16.6 | 17.7 | 56.8 | 0.027 | 0.662 | 32.978 | 0.450 | 0 | 10 | 20 | |
| WID2T06 | 98.1 | 0.158 | 12.03 | 0.1318 | 178.8 | 42.4 | 45.2 | 0.149 | 17.9 | 18.6 | 57.4 | 0.027 | 0.662 | 32.978 | 0.450 | 0 | 10 | 20 | |
| WID2T07 | 98.1 | 0.158 | 12.03 | 0.1318 | 178.8 | 42.4 | 45.2 | 0.149 | 16.5 | 17.0 | 44.6 | 0.026 | 0.654 | 29.216 | 0.890 | 0 | 10 | 20 | |
| WID2T08 | 98.1 | 0.153 | 18.05 | 0.1338 | 181.5 | 43.2 | 46.1 | 0.146 | 17.6 | 18.1 | 39.8 | 0.026 | 0.654 | 29.216 | 0.890 | 0 | 10 | 20 | |
| WID2T08 | 98.1 | 0.153 | 18.05 | 0.1338 | 181.5 | 43.2 | 46.1 | 0.146 | 18.9 | 17.1 | 12.1 | 0.026 | 0.654 | 29.216 | 0.890 | 0 | 10 | 20 | |
| WSD1T02 | 99.0 | 0.127 | 24.41 | 0.1381 | 187.7 | 37.3 | 42.2 | 0.314 | 18.3 | 19.7 | 60.0 | 0.059 | 0.642 | 28.894 | 1.165 | 0 | 10 | 20 | |
| WSD1T02 | 99.0 | 0.150 | 20.67 | 0.1388 | 157.9 | 31.5 | 40.3 | 0.695 | 18.0 | 19.4 | 51.8 | 0.110 | 0.656 | 30.143 | 6.476 | 0 | 10 | 20 | |
| WSD1T06 | 98.1 | 0.126 | 13.49 | 0.1368 | 165.1 | 32.9 | 40.5 | 0.576 | 16.5 | 17.7 | 24.5 | 0.095 | 0.614 | 30.130 | 1.727 | 0 | 10 | 20 | |
| WSD1T07 | 99.0 | 0.142 | 16.20 | 0.1364 | 158.1 | 31.4 | 40.4 | 0.707 | 17.8 | 18.3 | 33.7 | 0.112 | 0.630 | 28.659 | 2.667 | 0 | 10 | 20 | |
| WSD1T08 | 99.0 | 0.142 | 16.20 | 0.1364 | 158.1 | 31.4 | 40.4 | 0.707 | 16.2 | 17.9 | 36.4 | 0.112 | 0.630 | 28.659 | 2.667 | 0 | 10 | 20 | |
| WSD2T02 | 99.0 | 0.142 | 8.45 | 0.1258 | 181.7 | 44.0 | 45.8 | 0.092 | 17.8 | 18.1 | 46.6 | 0.017 | 0.702 | 31.594 | 1.263 | 0 | 10 | 20 | |
| WSD2T01 | 99.0 | 0.140 | 7.14 | 0.1369 | 183.3 | 43.8 | 45.5 | 0.083 | 18.1 | 15.9 | 48.3 | 0.015 | 0.684 | 32.040 | 1.988 | 0 | 10 | 20 | |
| WSD2T02 | 99.0 | 0.133 | 17.29 | 0.1371 | 183.9 | 43.8 | 45.4 | 0.080 | 18.0 | 16.5 | 21.0 | 0.015 | 0.610 | 30.094 | 1.539 | 0 | 10 | 20 | |
| WSD2T03 | 99.0 | 0.145 | 6.90 | 0.1387 | 182.1 | 43.7 | 45.2 | 0.078 | 18.4 | 18.7 | 46.0 | 0.014 | 0.642 | 30.782 | 1.710 | 0 | 10 | 20 | |
| WSD2T04 | 99.0 | 0.172 | 11.05 | 0.1376 | 183.9 | 43.8 | 45.4 | 0.084 | 18.2 | 15.9 | 38.5 | 0.015 | 0.720 | 33.624 | 0.909 | 0 | 10 | 20 | |
| WSD2T06 | 98.1 | 0.162 | 13.16 | 0.1385 | 183.1 | 43.7 | 45.6 | 0.094 | 18.2 | 18.3 | 21.4 | 0.017 | 0.668 | 33.063 | 1.836 | 0 | 10 | 20 | |
| WSD2T06 | 98.1 | 0.140 | 10.00 | 0.1368 | 183.9 | 44.0 | 45.2 | 0.083 | 18.4 | 18.6 | 40.6 | 0.012 | 0.682 | 31.153 | 1.164 | 0 | 10 | 20 | |
| WSD2T06 | 98.1 | 0.163 | 13.73 | 0.1385 | 181.7 | 43.3 | 44.9 | 0.080 | 17.9 | 18.6 | 52.8 | 0.014 | 0.693 | 31.058 | 2.348 | 0 | 10 | 20 | |
| WSD2T10 | 99.0 | 0.153 | 13.73 | 0.1385 | 181.7 | 43.3 | 44.9 | 0.080 | 17.9 | 18.6 | 16.8 | -2.1 | 0.014 | 0.693 | 31.058 | 2.348 | 0 | 10 | 20 |

APPENDIX C

The following figures show the specific elastic modulus, %CV of SEM, visual delamination code, and selected density plots used to determine the critical temperature.

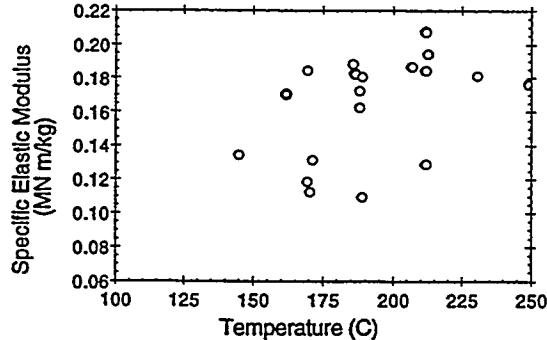


Figure C1. Case W1A1.

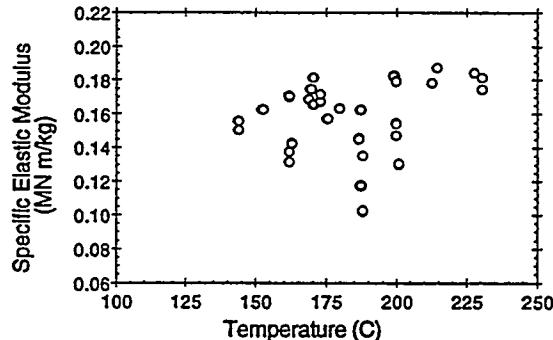


Figure C2. Case W1A2.

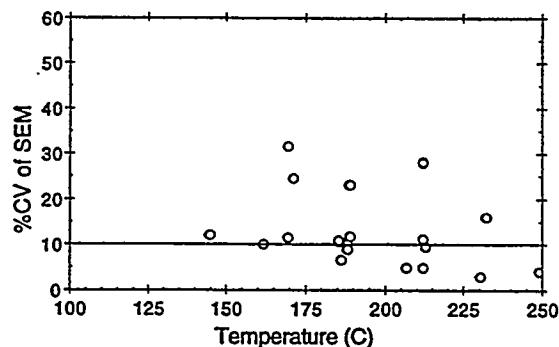


Figure C3. Case W1A1.

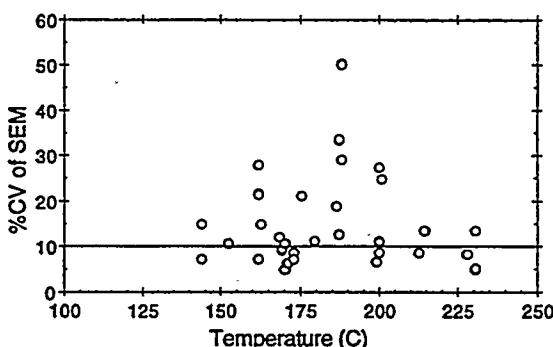


Figure C4. Case W1A2.

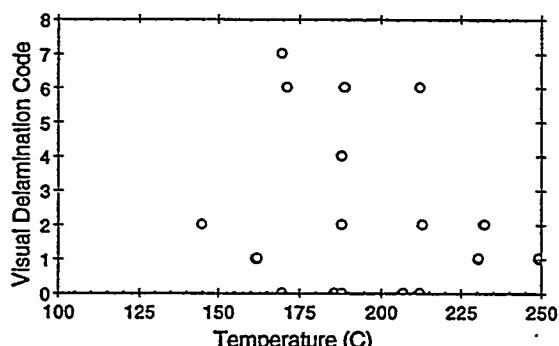


Figure C5. Case W1A1.

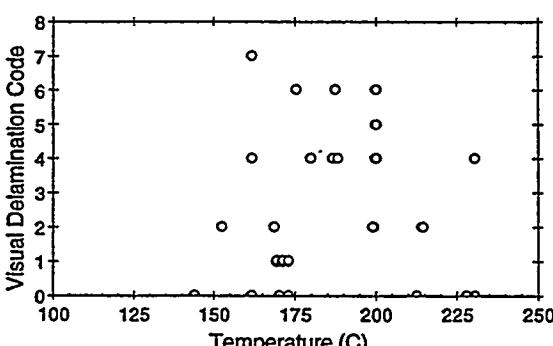


Figure C6. Case W1A2.

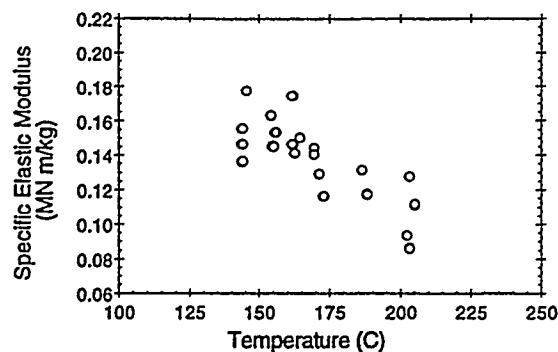


Figure C7. Case W1A3.

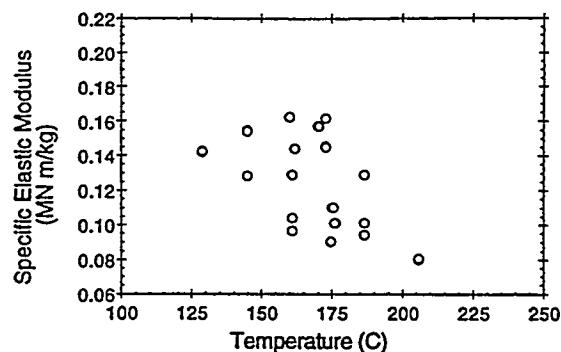


Figure C8. Case W1A4.

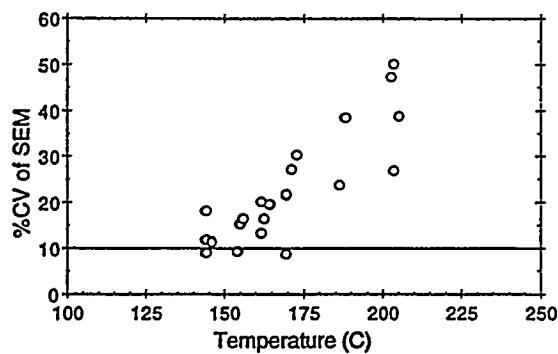


Figure C9. Case W1A3.

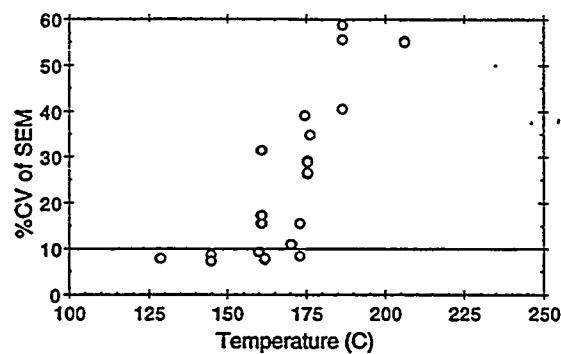


Figure C10. Case W1A4.

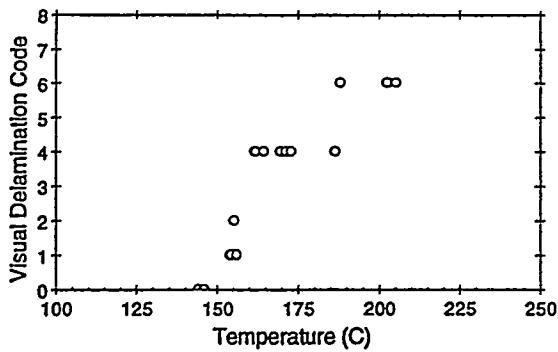


Figure C11. Case W1A3.

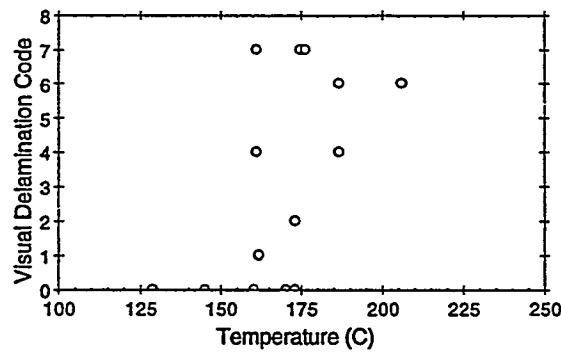


Figure C12. Case W1A4.

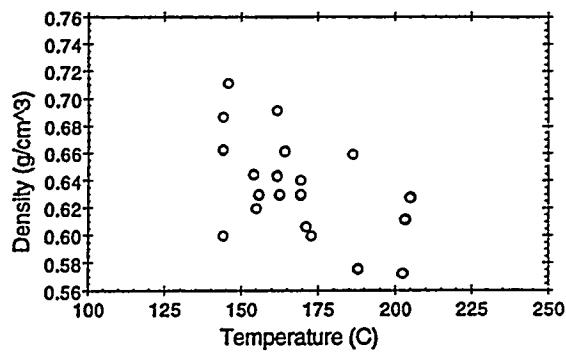


Figure C11A. Case W1A3.

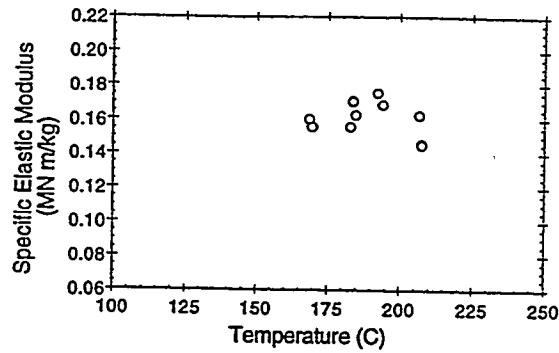


Figure C13. Case W1C1.

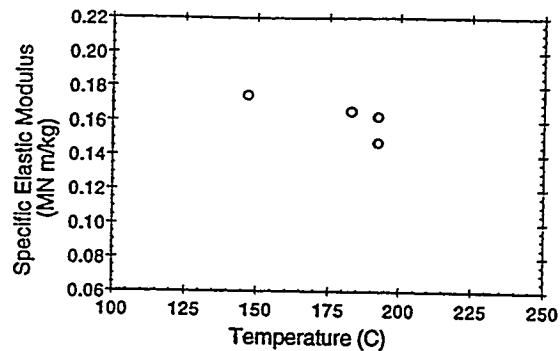


Figure C14. Case W1C2.

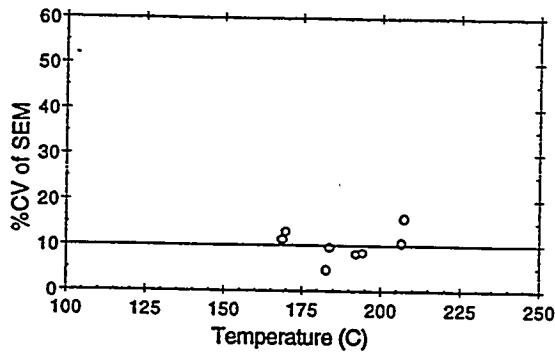


Figure C15. Case W1C1.

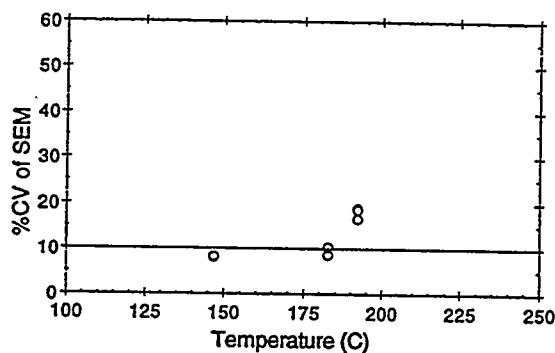


Figure C16. Case W1C2.

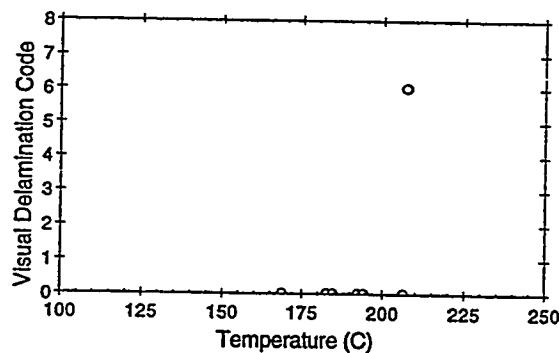


Figure C17. Case W1C1.

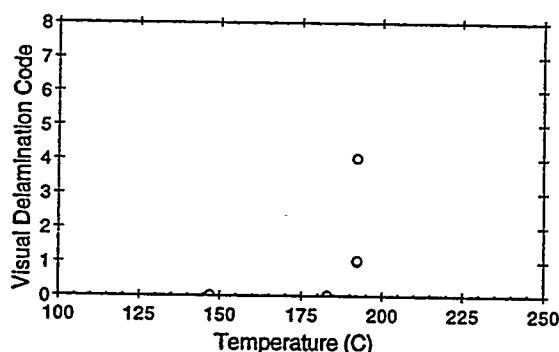


Figure C18. Case W1C2.

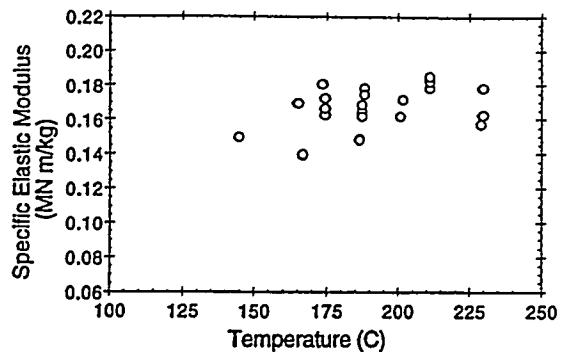


Figure C19. Case W5A1.

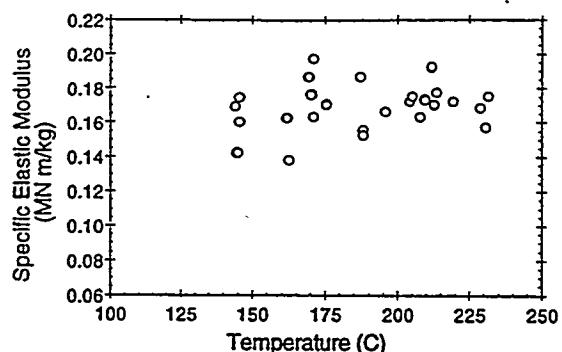


Figure C20. Case W5A2.

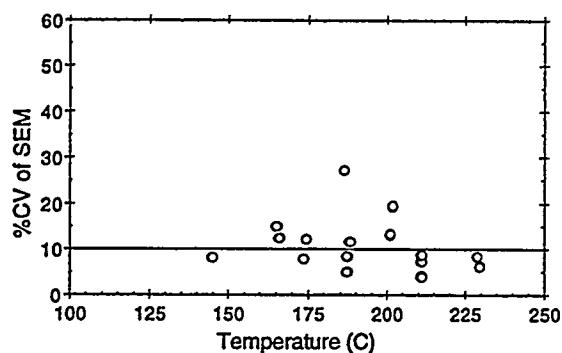


Figure C21. Case W5A1.

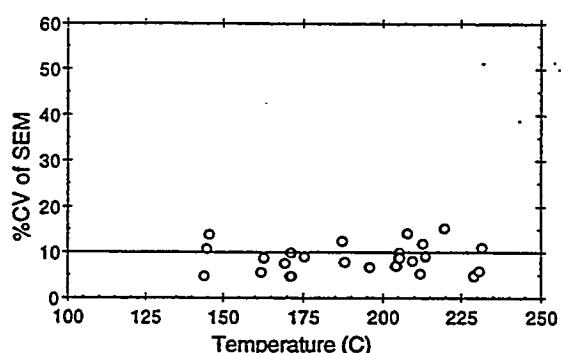


Figure C22. Case W5A2.

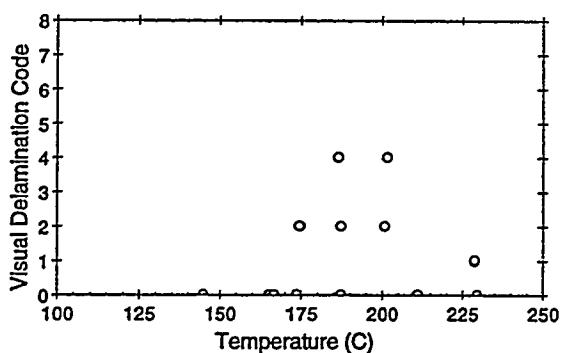


Figure C23. Case W5A1.

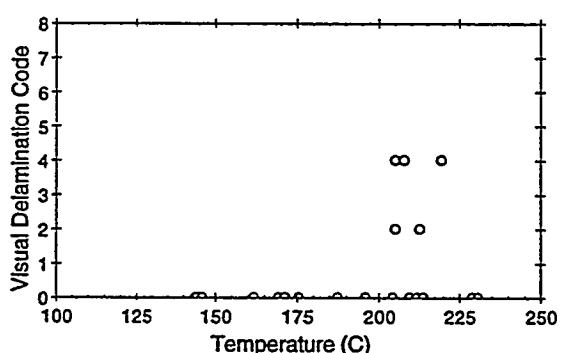


Figure C24. Case W5A2.

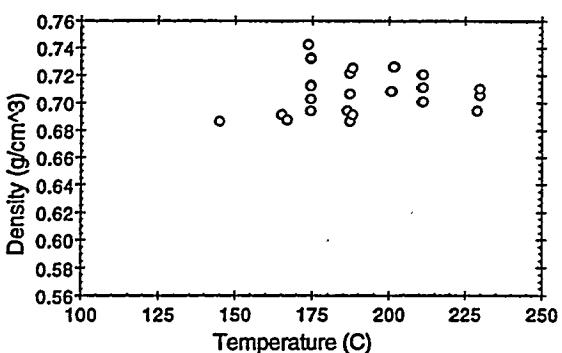


Figure C23A. Case W5A1.

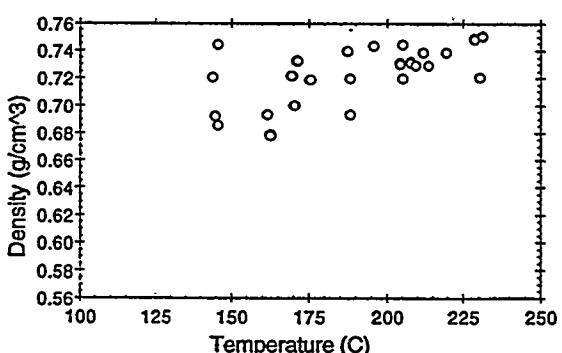


Figure C24A. Case W5A2.

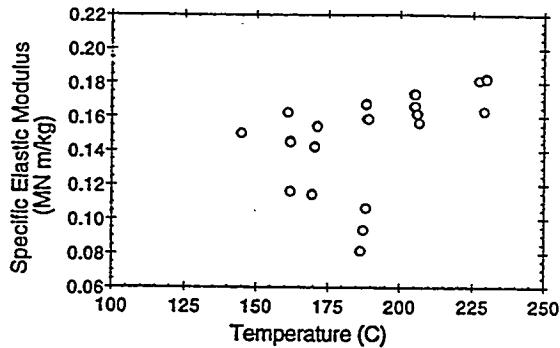


Figure C25. Case W5A3.

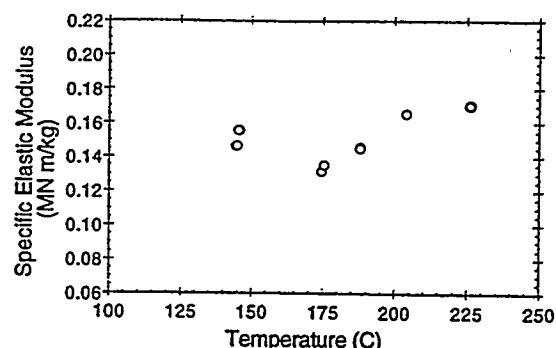


Figure C26. Case W5A4.

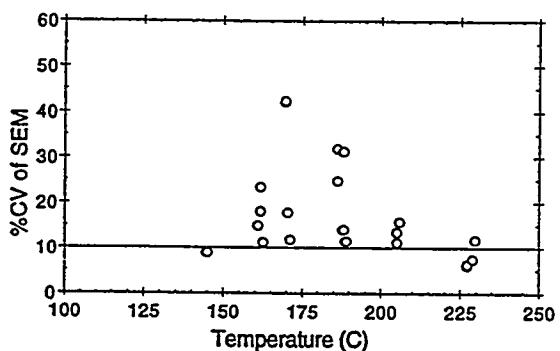


Figure C27. Case W5A3.

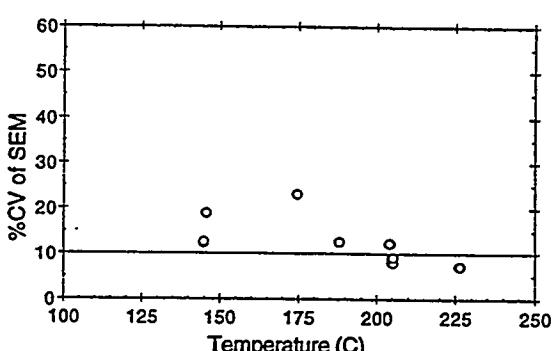


Figure C28. Case W5A4.

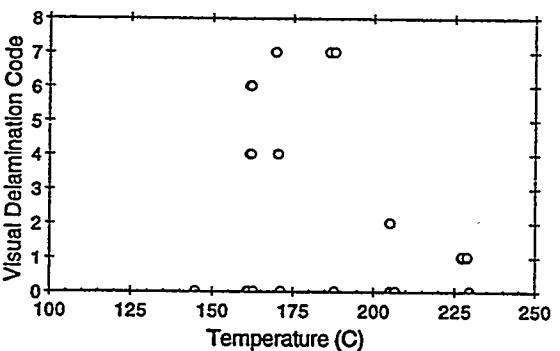


Figure C29. Case W5A3.

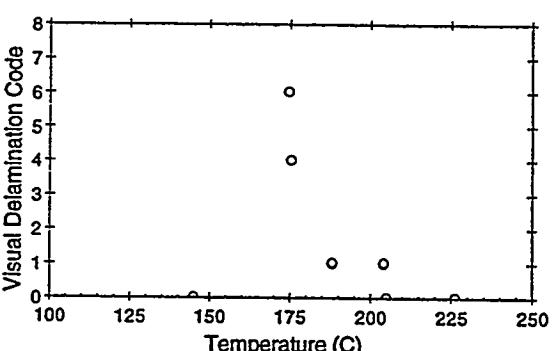


Figure C30. Case W5A4.

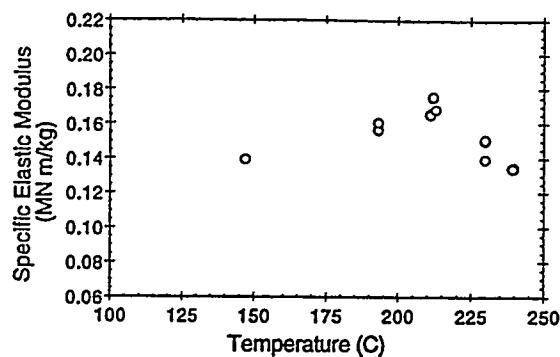


Figure C31. Case W5C1.

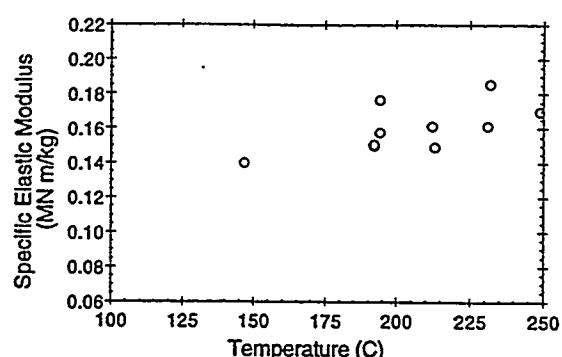


Figure C32. Case W5C2.

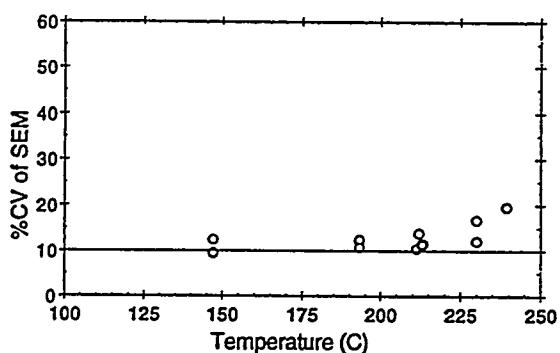


Figure C33. Case W5C1.

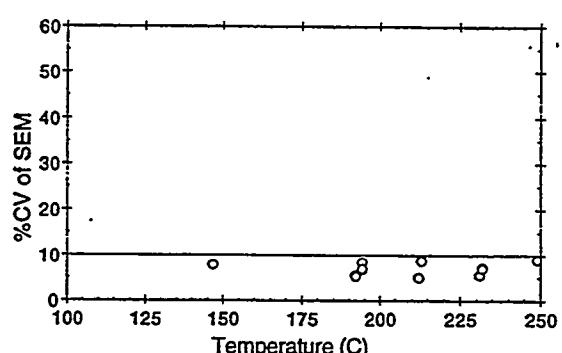


Figure C34. Case W5C2.

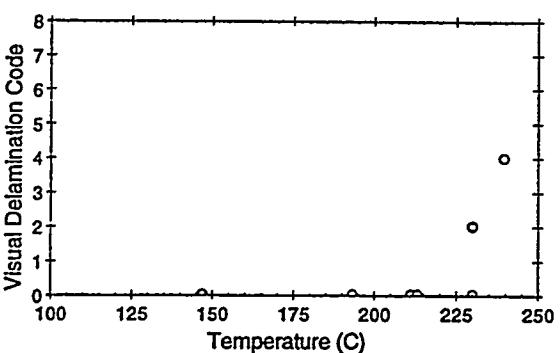


Figure C35. Case W5C1.

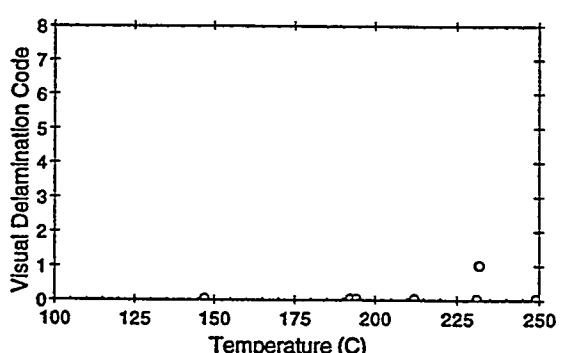


Figure C36. Case W5C2.

APPENDIX D

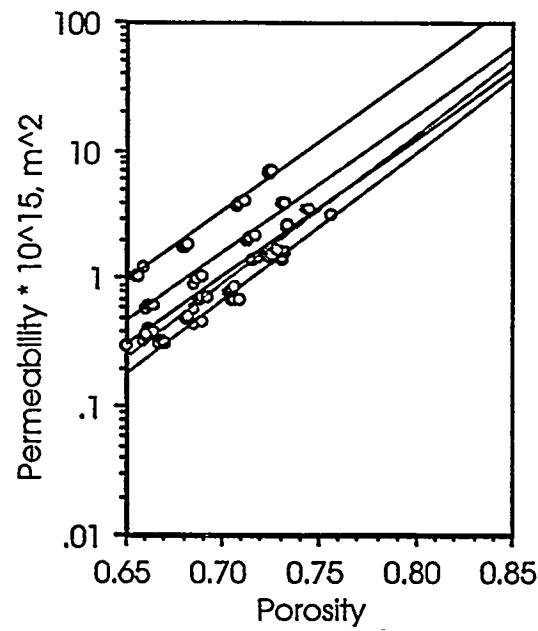


Figure D1. Mill #1 furnish, whole sheet.

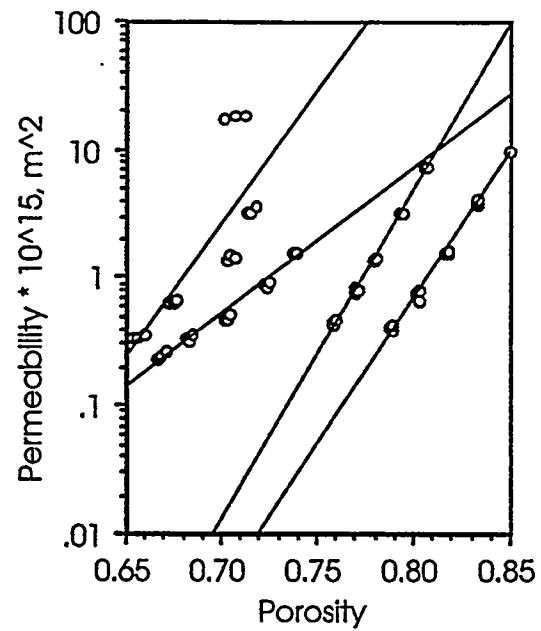


Figure D2. Mill #1 furnish, whole sheet.

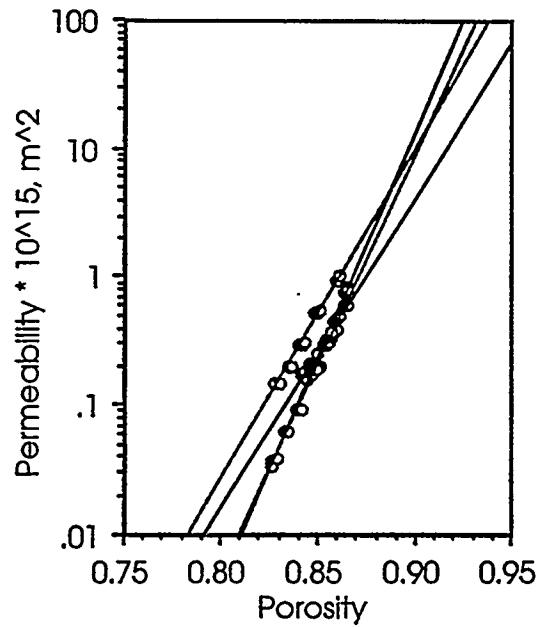


Figure D3. Mill #1 furnish, top ply.

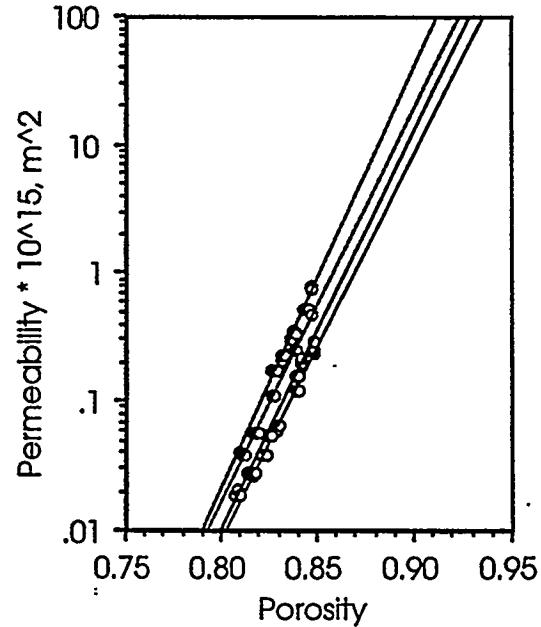


Figure D4. Mill #1 furnish, bottom ply.

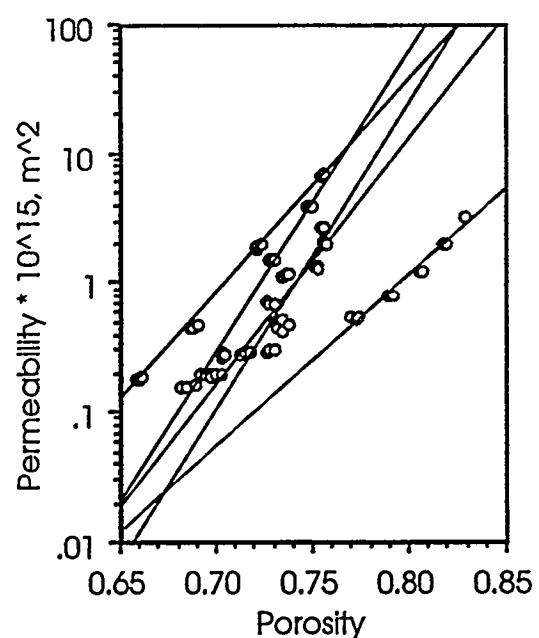


Figure D5. Mill #2 furnish, whole sheet.

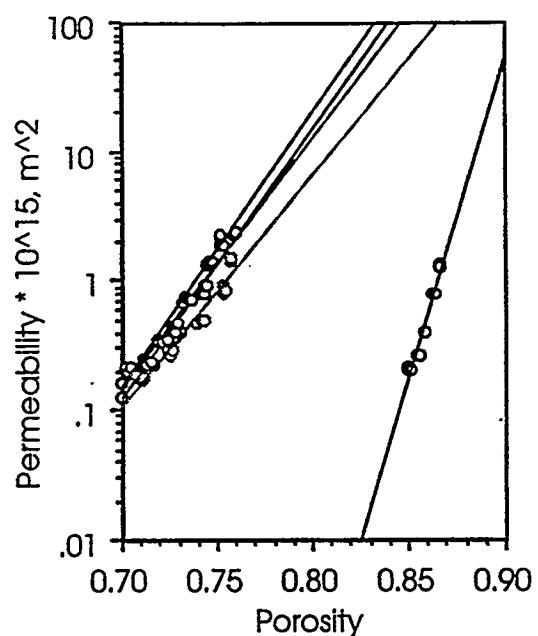


Figure D6. Mill #2 furnish, whole sheet.

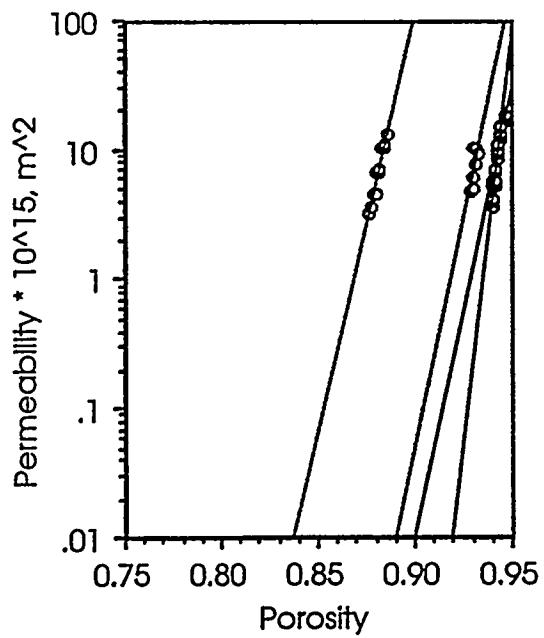


Figure D7. Mill #2 furnish, top ply.

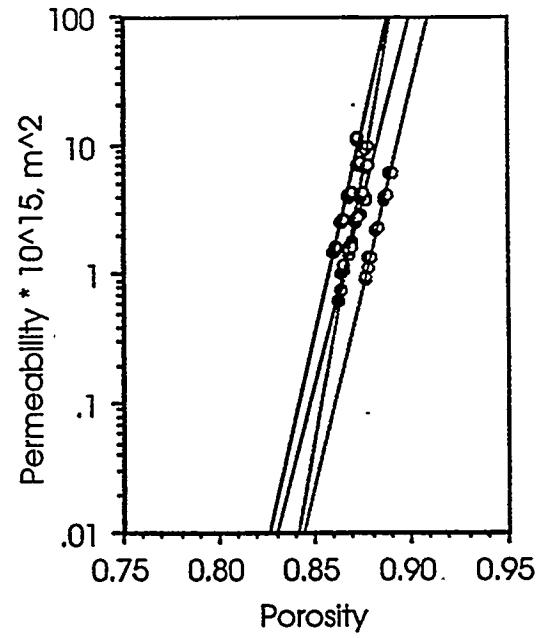


Figure D8. Mill #2 furnish, bottom ply.

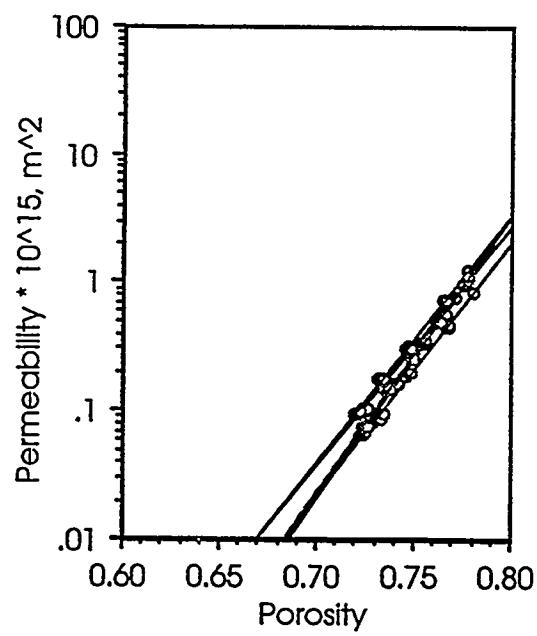


Figure D9. Furnish W1, solids 35%.

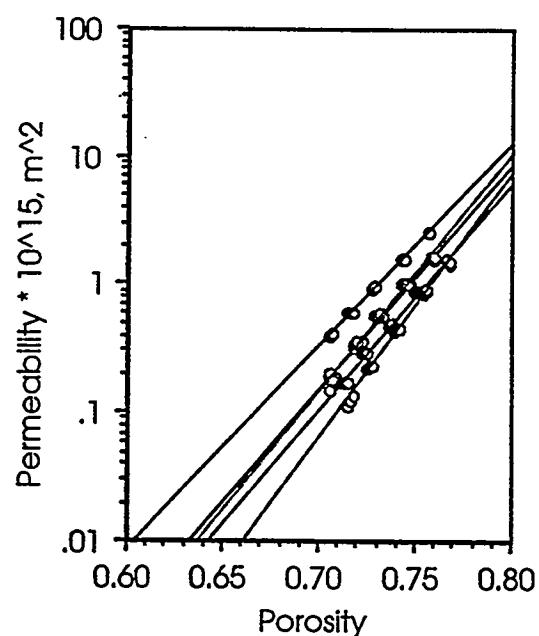


Figure D10. Furnish W1, solids 42%.

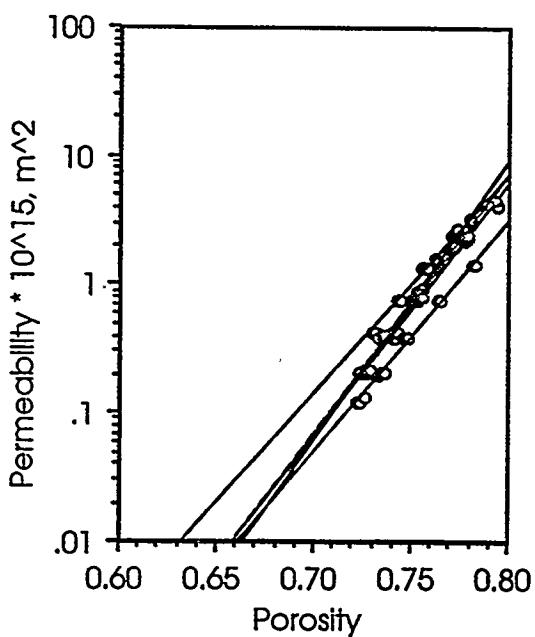


Figure D11. Furnish W2, solids 35%.

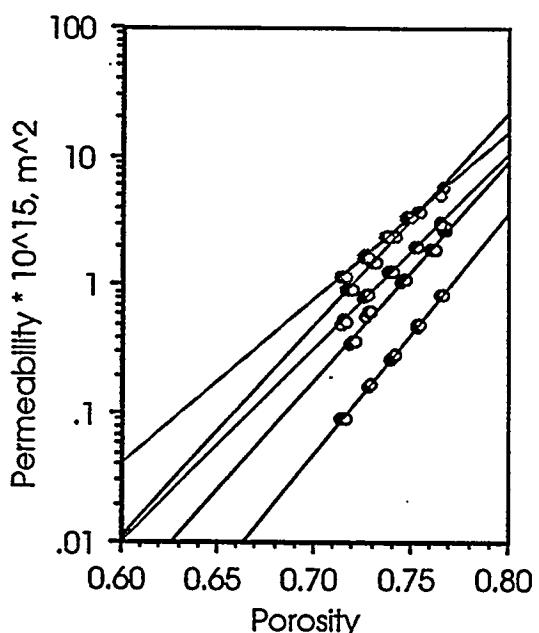


Figure D12. Furnish W2, solids 42%.

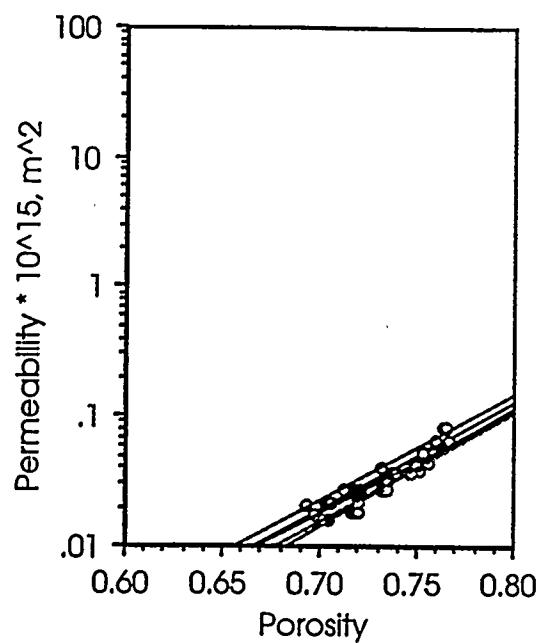


Figure D13. Furnish W3, solids 35%.

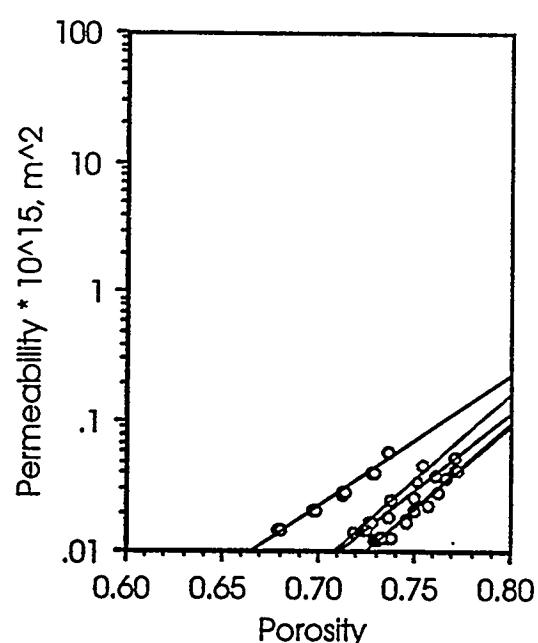


Figure D14. Furnish W3, solids 40%.

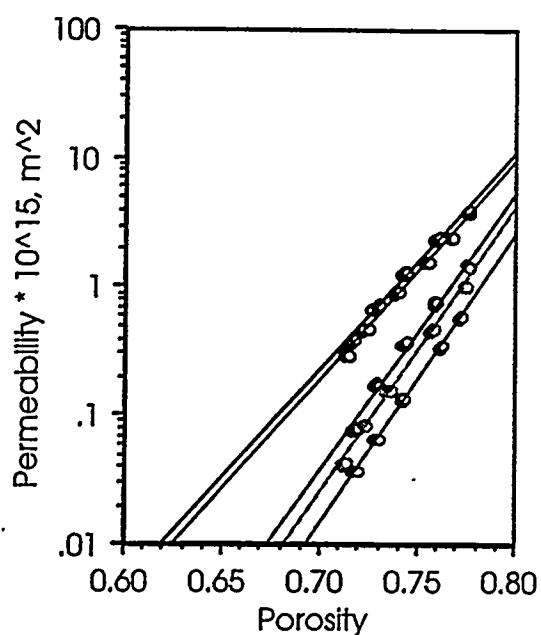


Figure D15. Furnish W5, solids 35%.

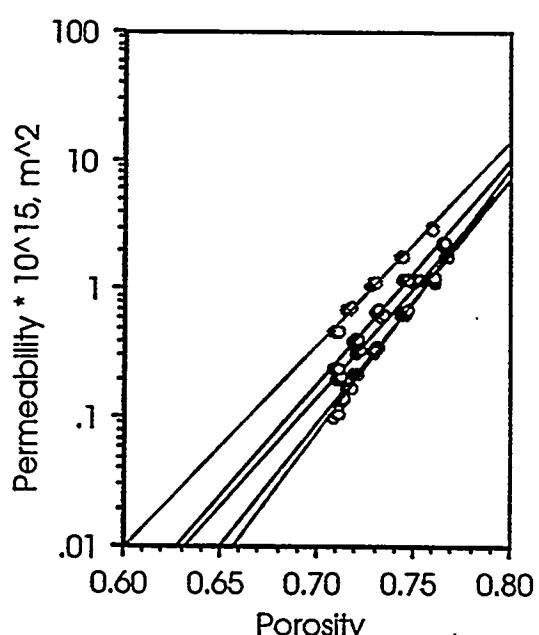


Figure D16. Furnish W5, solids 42%.

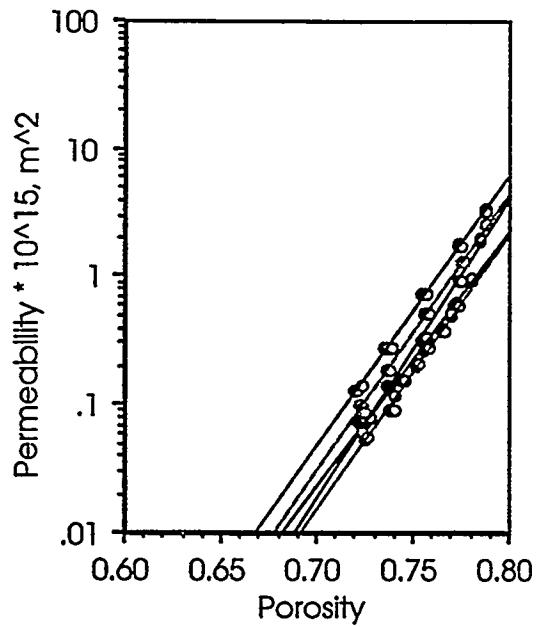


Figure D17. Furnish W6, solids 35%.

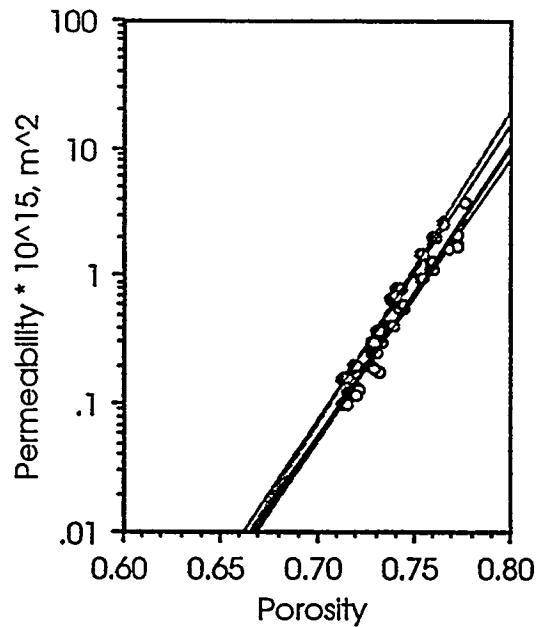


Figure D18. Furnish W6, solids 42%.

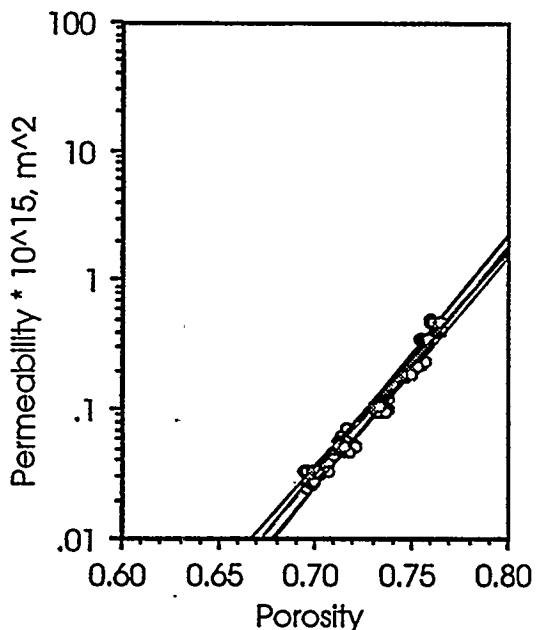


Figure D19. Furnish W7, solids 35%.

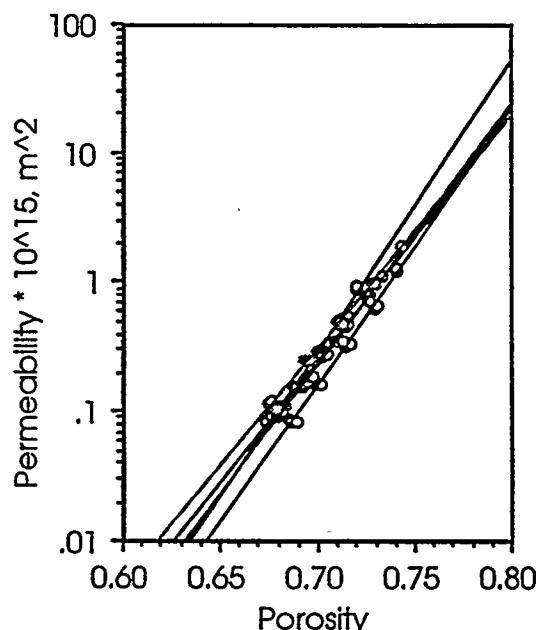


Figure D20. Furnish W7, solids 42%.

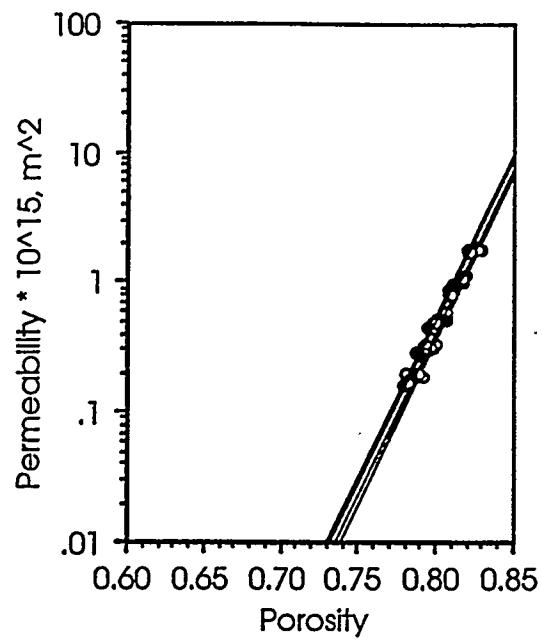


Figure D21. Furnish W8, solids 35%.

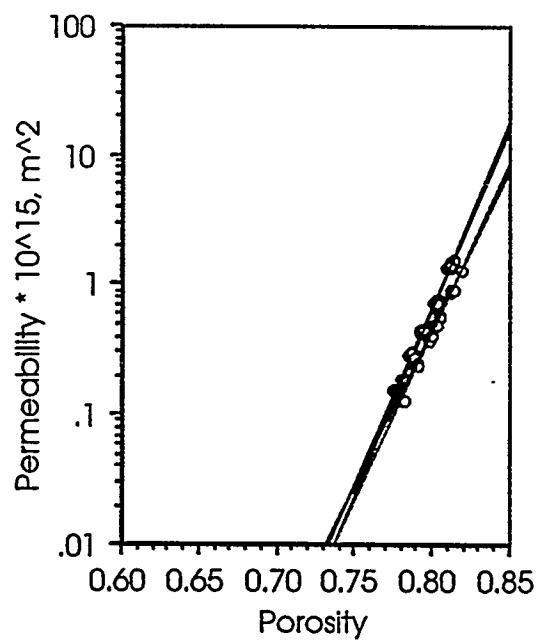


Figure D22. Furnish W8, solids 42%.

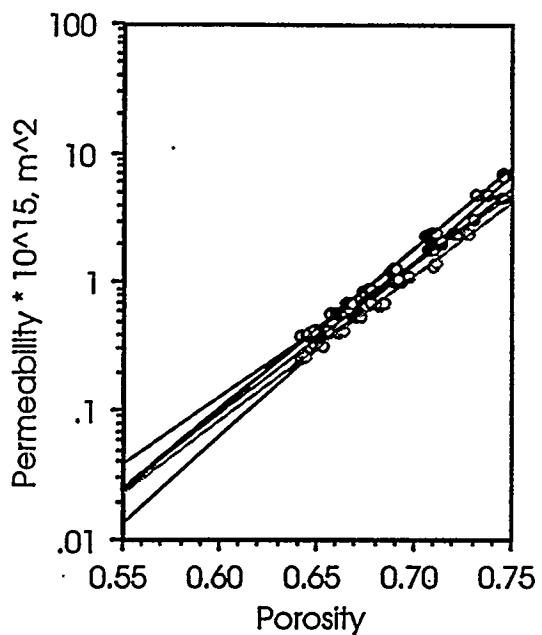


Figure D23. Furnish W9, press condition P1.

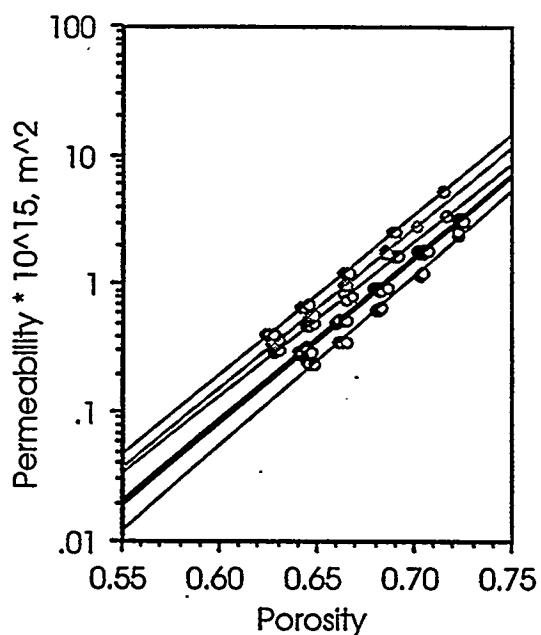


Figure D24. Furnish W9, press condition P2.

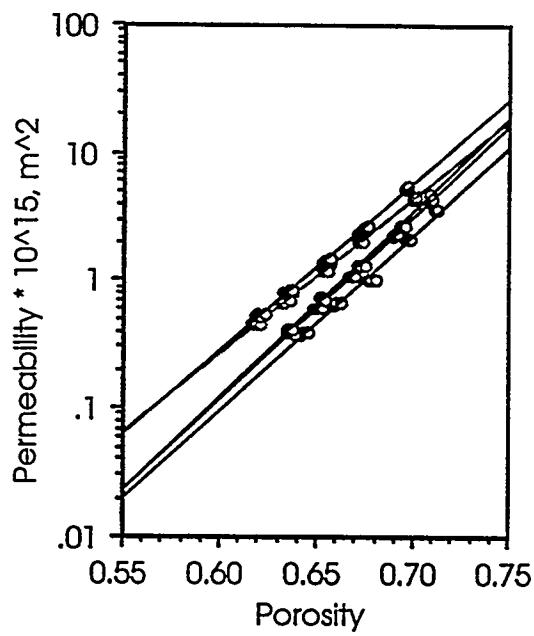


Figure D25. Furnish W9, press condition P3.

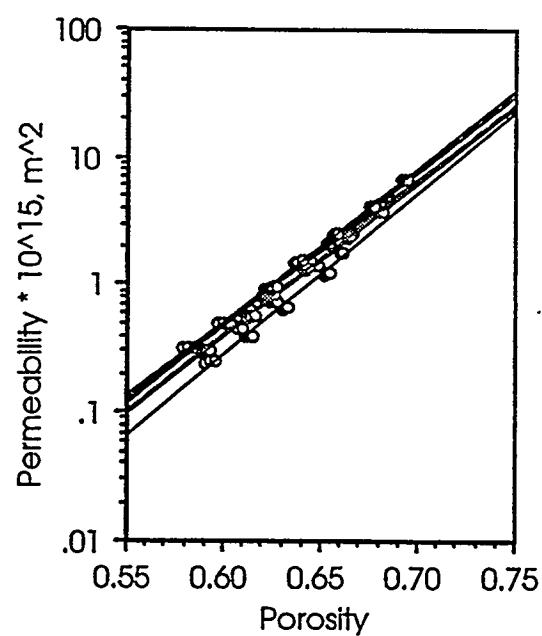


Figure D26. Furnish W9, press condition P4.

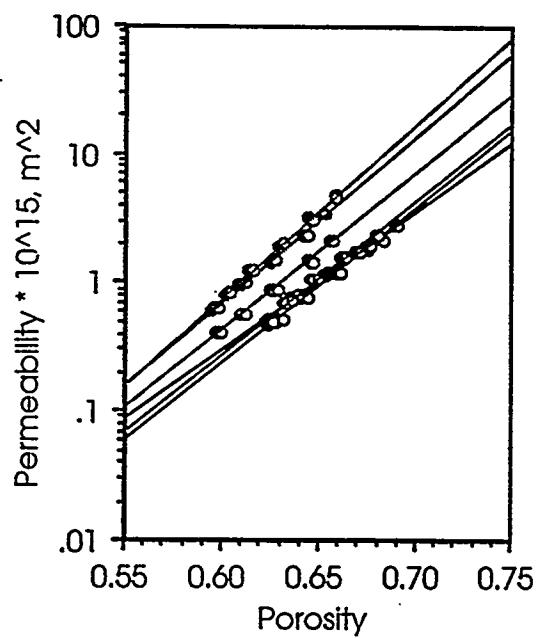


Figure D27. Furnish W9, press condition P5.

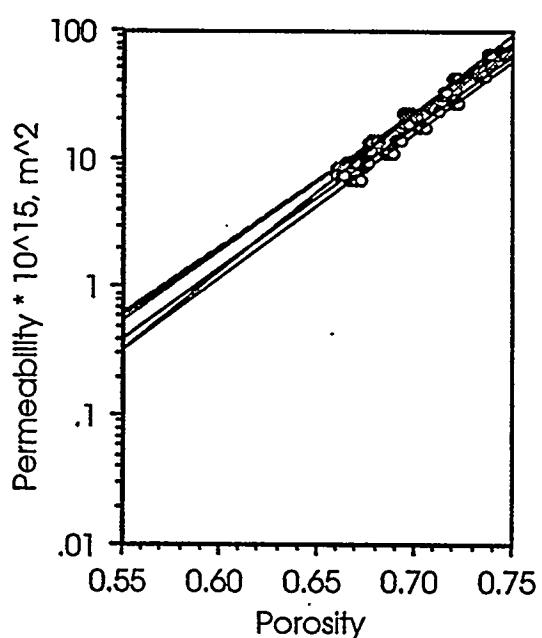


Figure D28. Furnish W10, press condition P1.

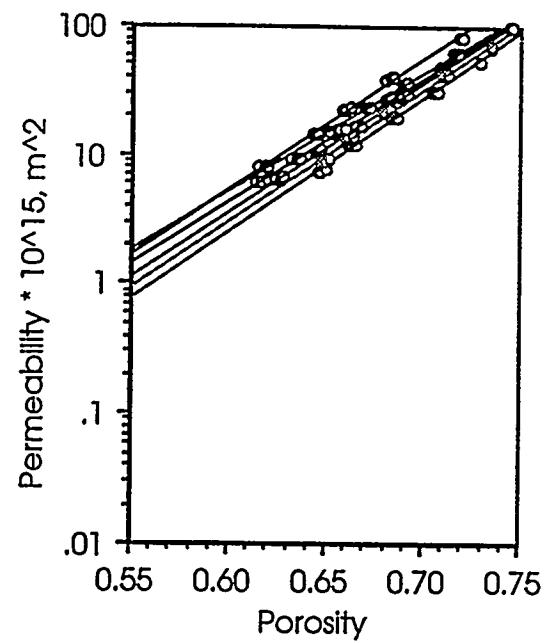


Figure D29. Furnish W10, press condition P2.

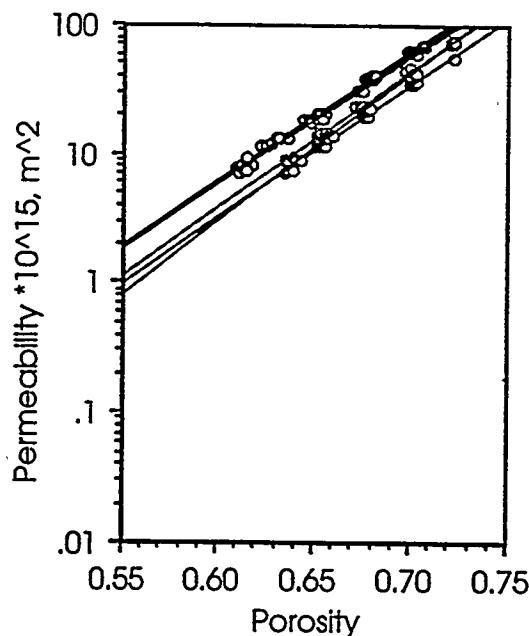


Figure D30. Furnish W10, press condition P3.

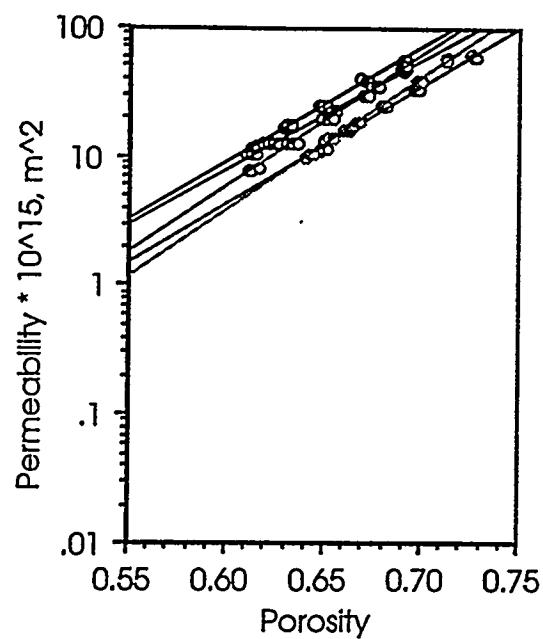


Figure D31. Furnish W10, press condition P4.

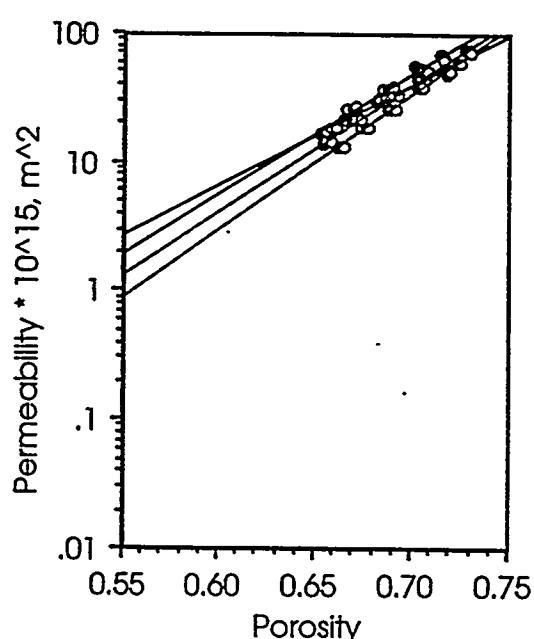


Figure D32. Furnish W10, press condition P5.

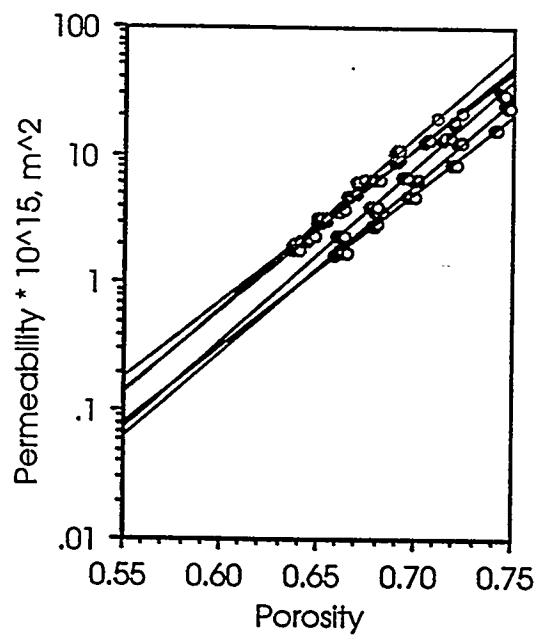


Figure D33. Furnish W11, press condition P1.

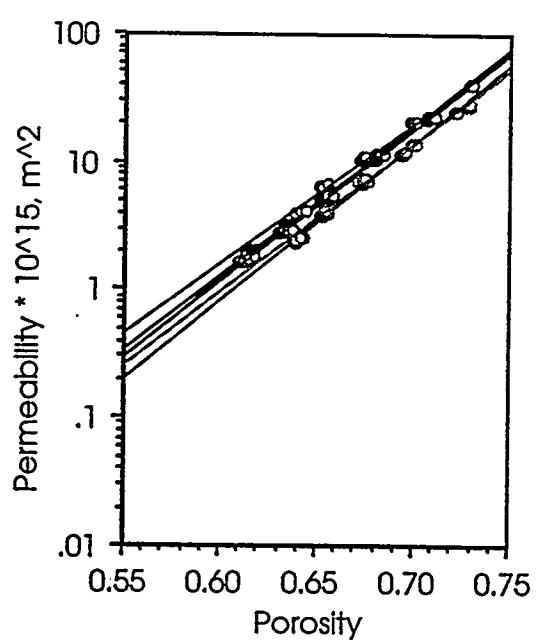


Figure D34. Furnish W11, press condition P2.

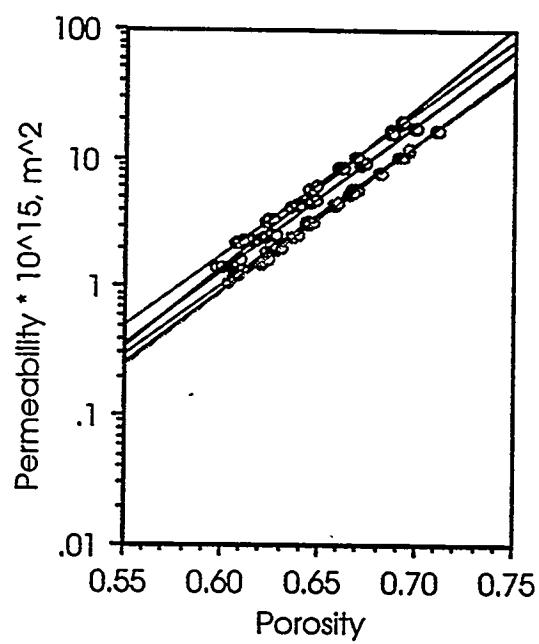


Figure D35. Furnish W11, press condition P3.

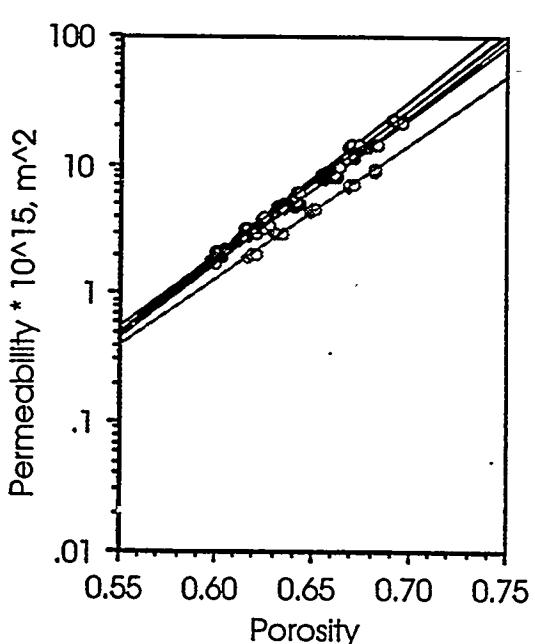


Figure D36. Furnish W11, press condition P4.

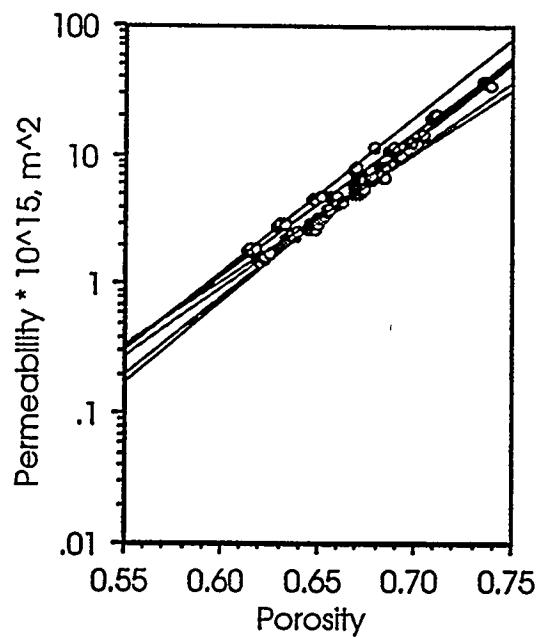


Figure D15. Furnish W37, press condition P5.

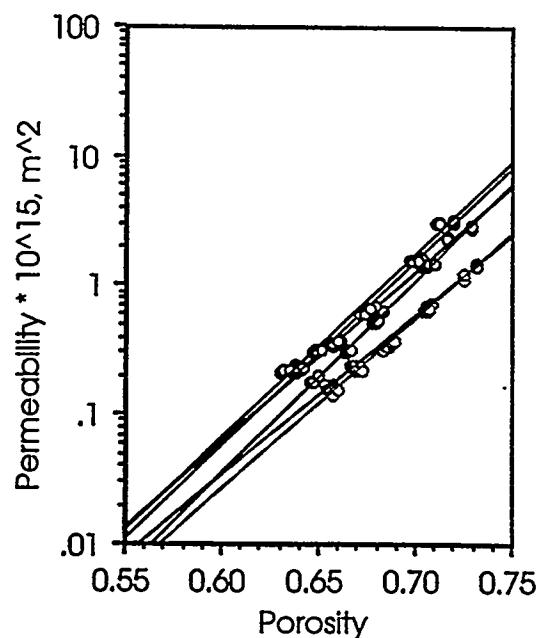


Figure D38. Furnish W12, press condition P1.

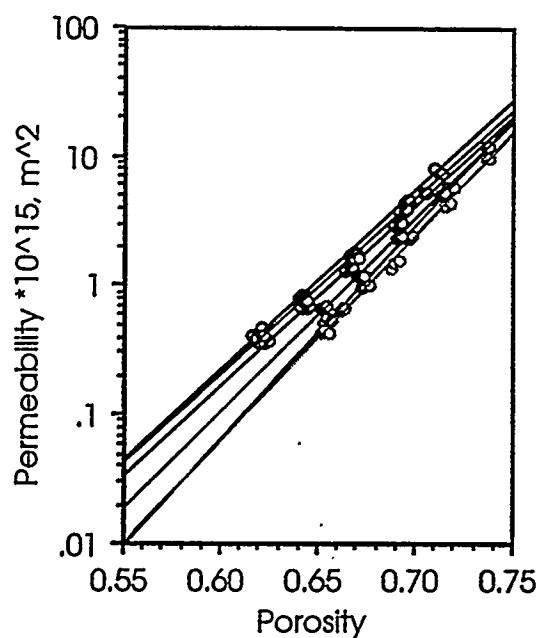


Figure D39. Furnish W12, press condition P2.

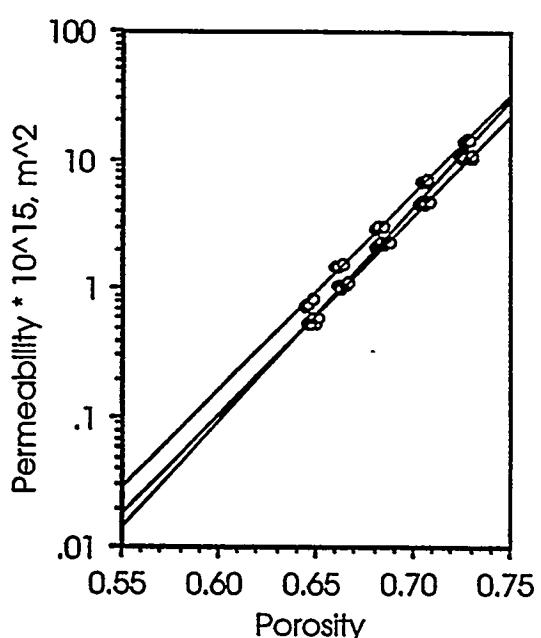


Figure D40. Furnish W12, press condition P3.

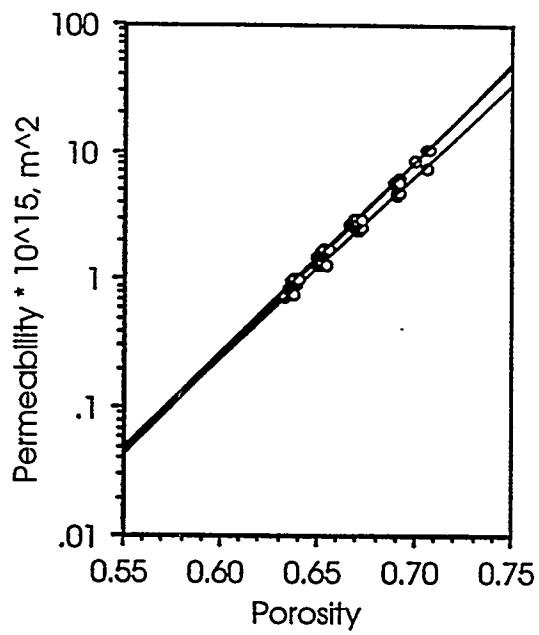


Figure D41. Furnish W12, press condition P4.

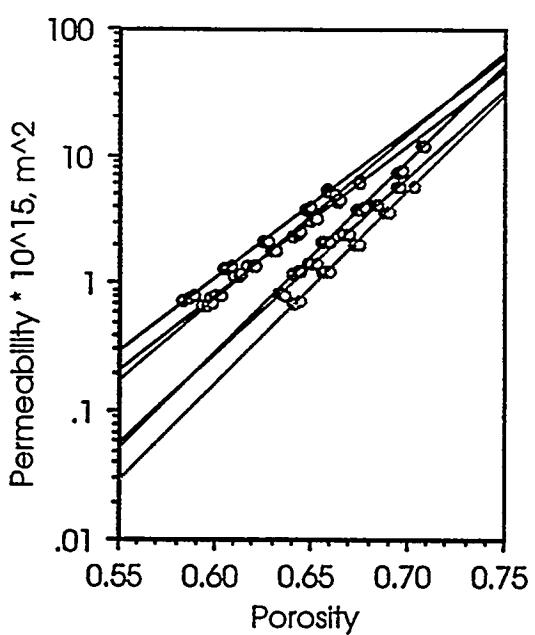


Figure D42. Furnish W12, press condition P5.

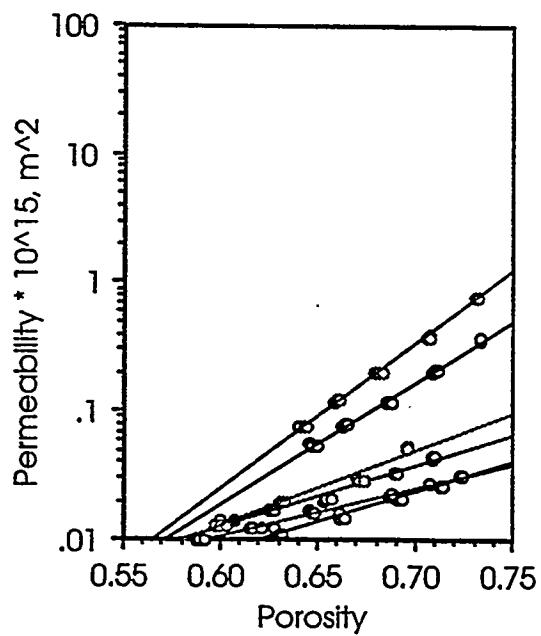


Figure D43. Furnish W15, press condition P2.

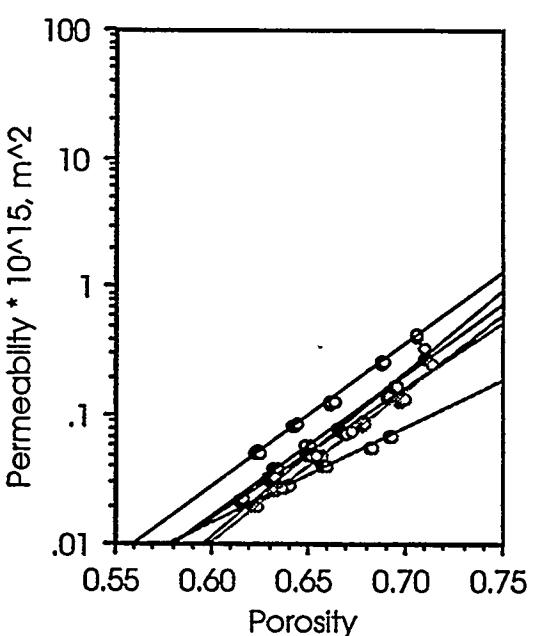


Figure D44. Furnish W15, press condition P3.

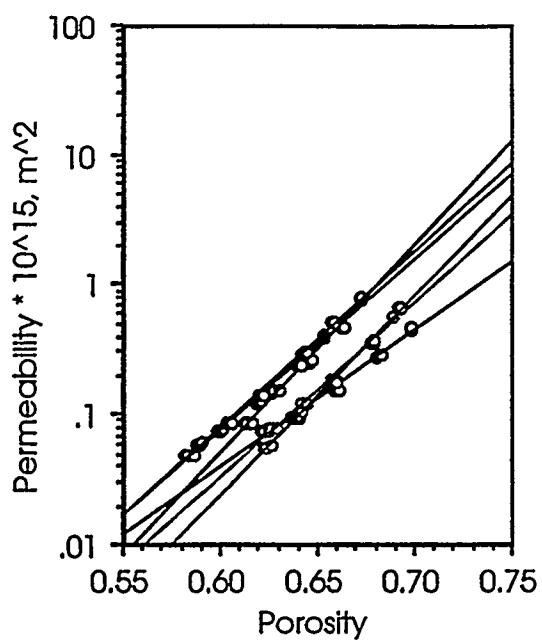


Figure D45. Furnish W15, press condition P4.

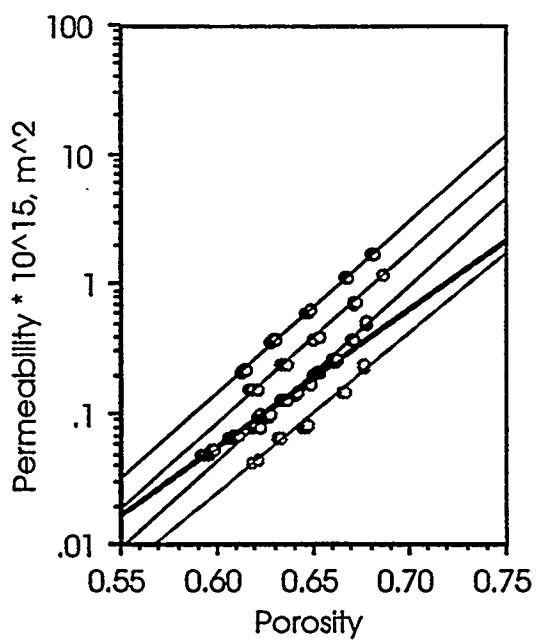


Figure D46. Furnish W15, press condition P5.

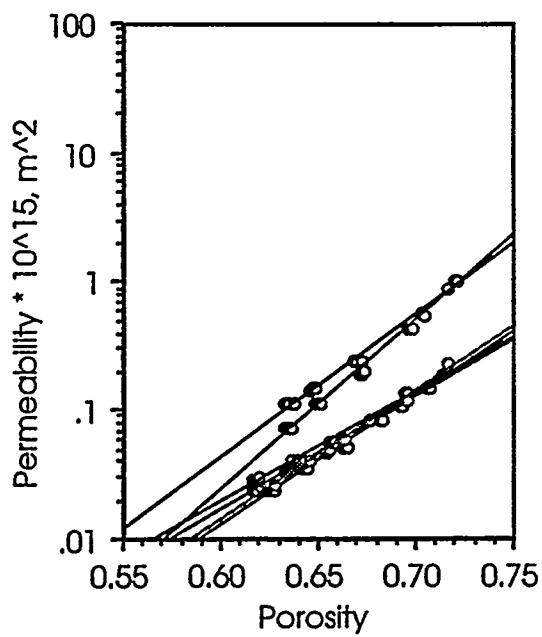


Figure D47. Furnish W16, press condition P2.

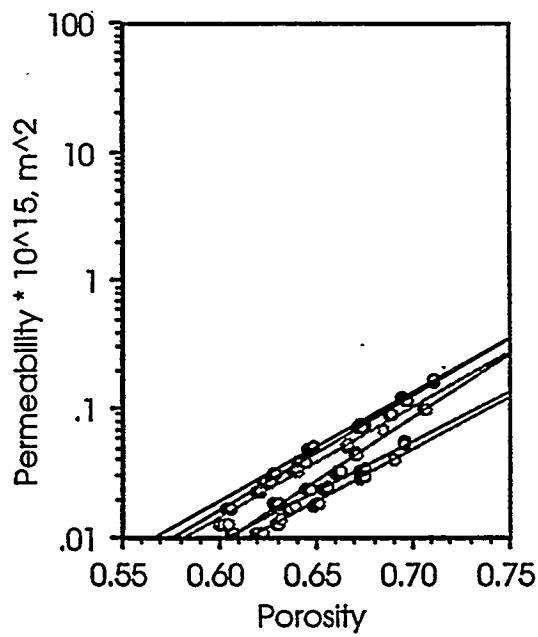


Figure D48. Furnish W16, press condition P3.

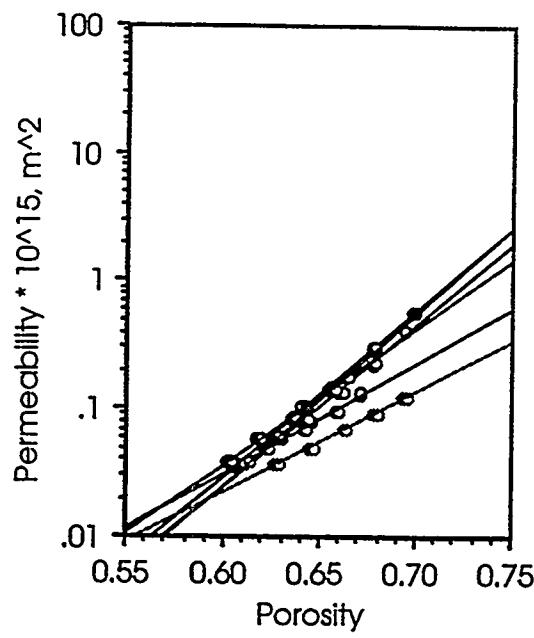


Figure D49. Furnish W16, press condition P4.

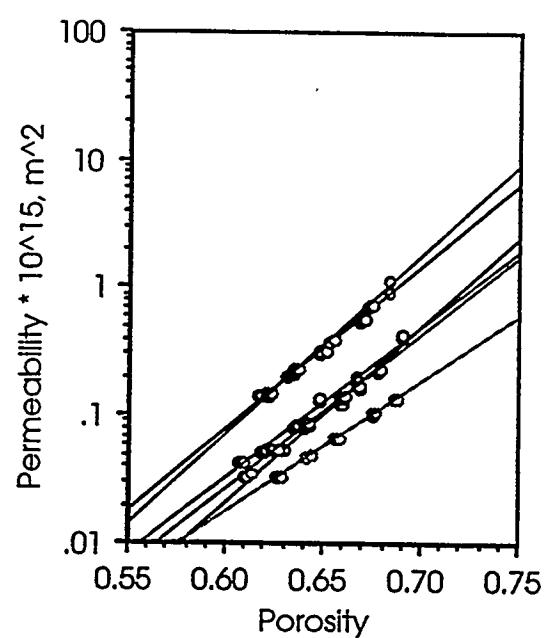


Figure D50. Furnish W16, press condition P5.

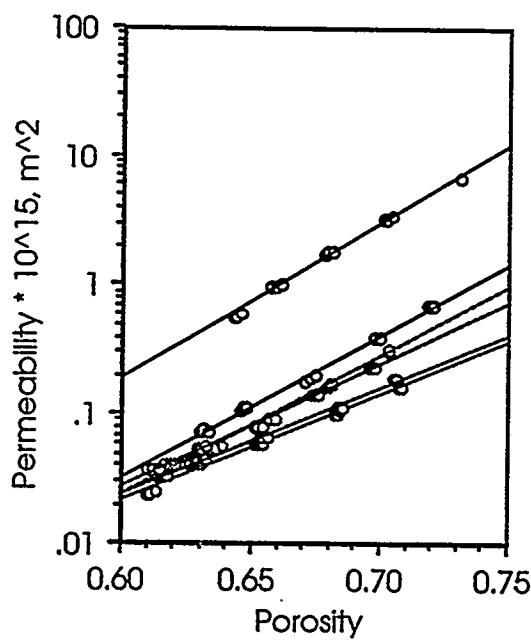


Figure D51. Furnish W17, press condition P1.

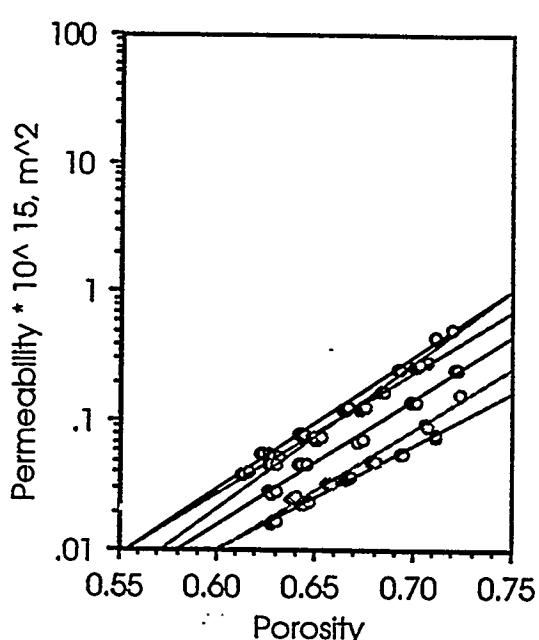


Figure D52. Furnish W17, press condition P2.

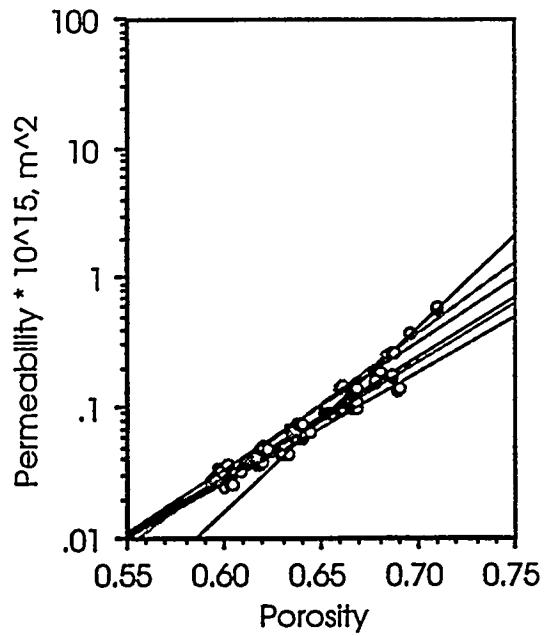


Figure D53. Furnish W17, press condition P3.

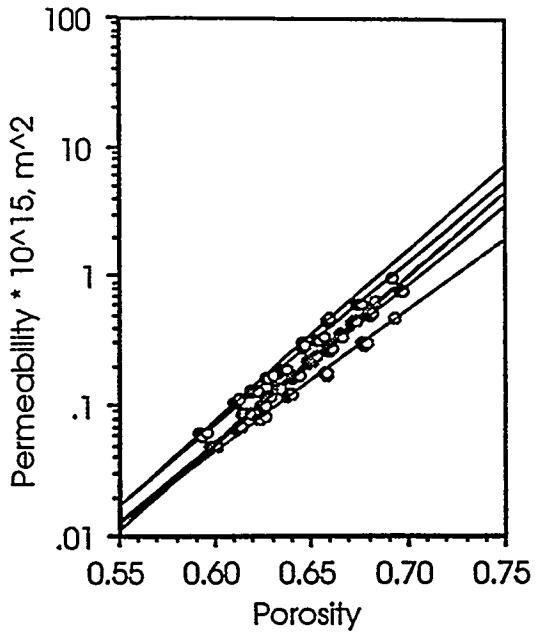


Figure D54. Furnish W17, press condition P4.

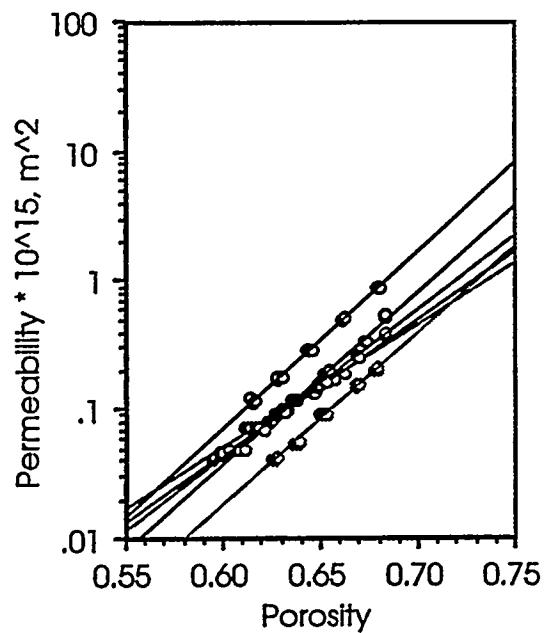


Figure D55. Furnish W17, press condition P5.

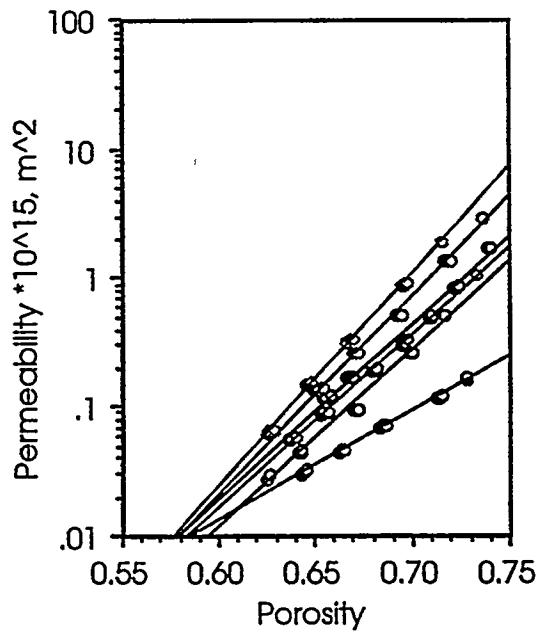


Figure D56. Furnish W18, press condition P1.

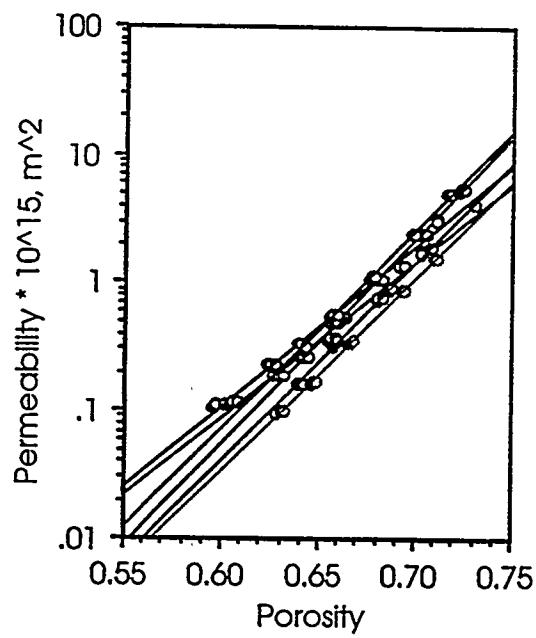


Figure D57. Furnish W18, press condition P2.

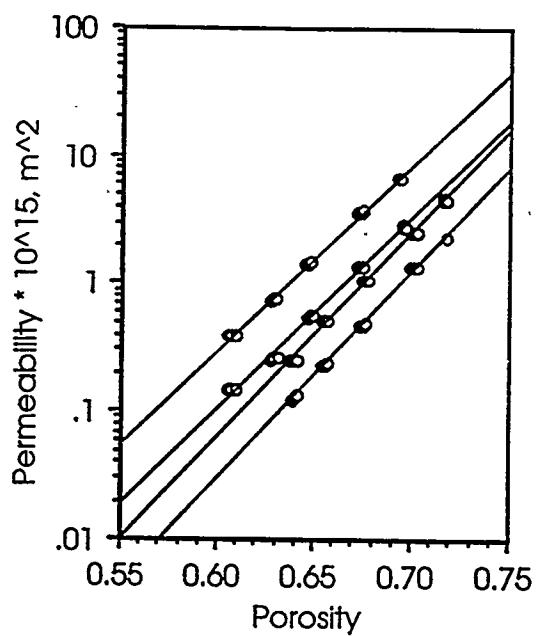


Figure D58. Furnish W18, press condition P3.

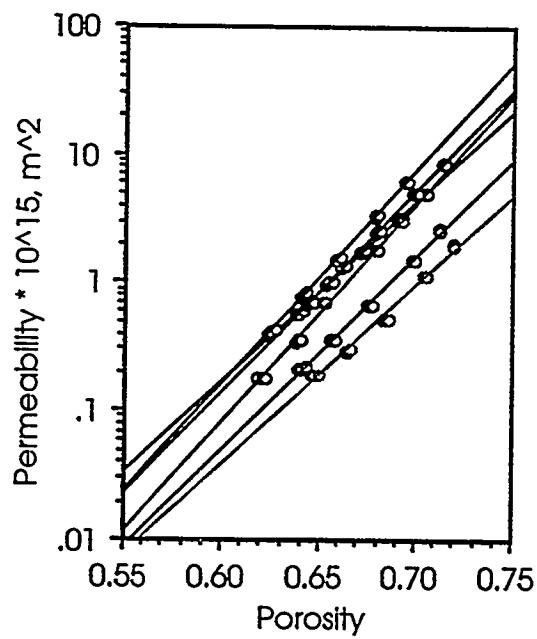


Figure D59. Furnish W18, press condition P4.

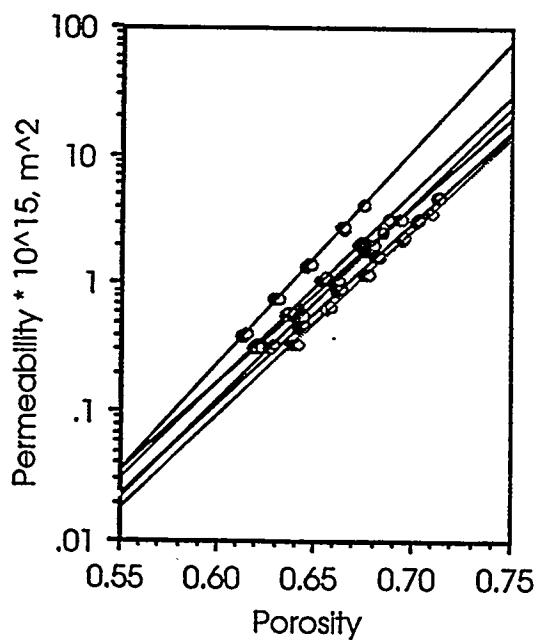


Figure D60. Furnish W18, press condition P5.

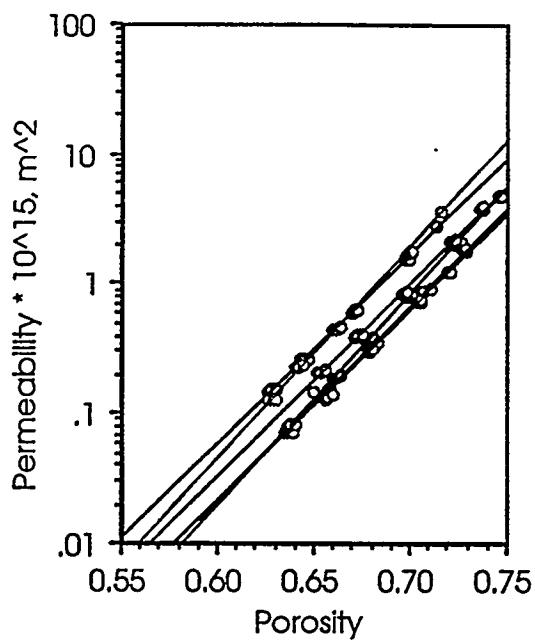


Figure D61. Furnish W19, press condition P1.

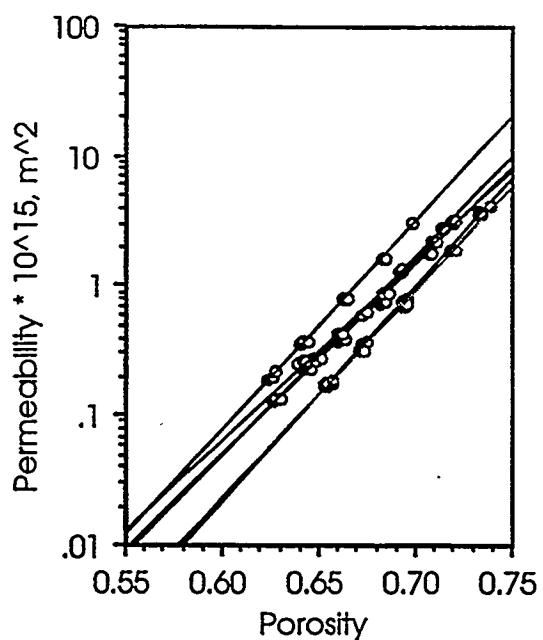


Figure D62. Furnish W19, press condition P2.

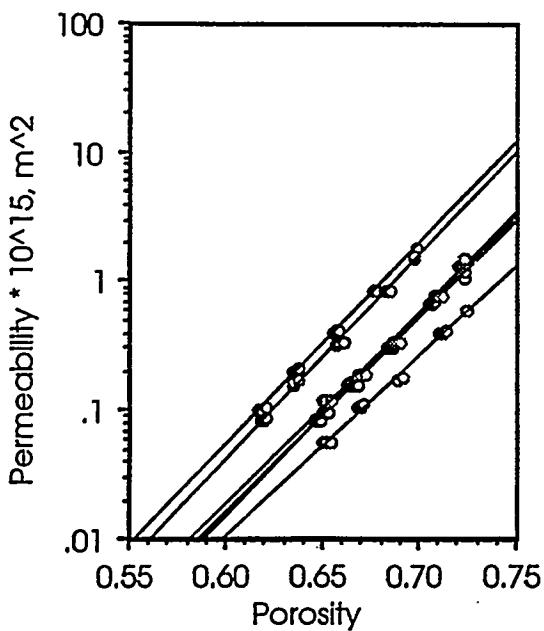


Figure D63. Furnish W19, press condition P3.

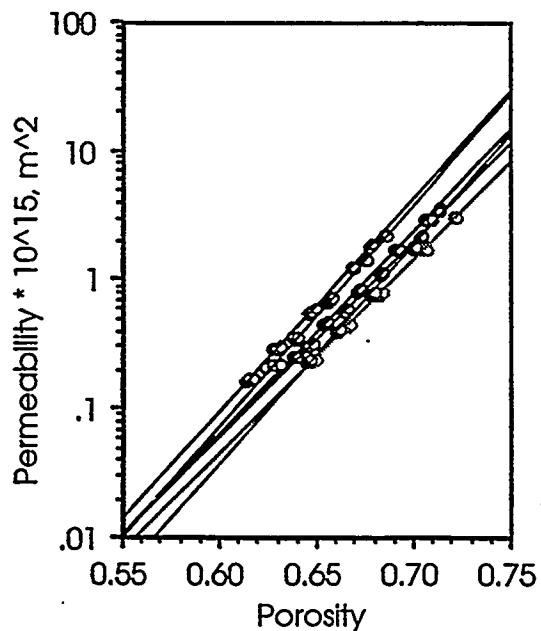


Figure D64. Furnish W19, press condition P4.

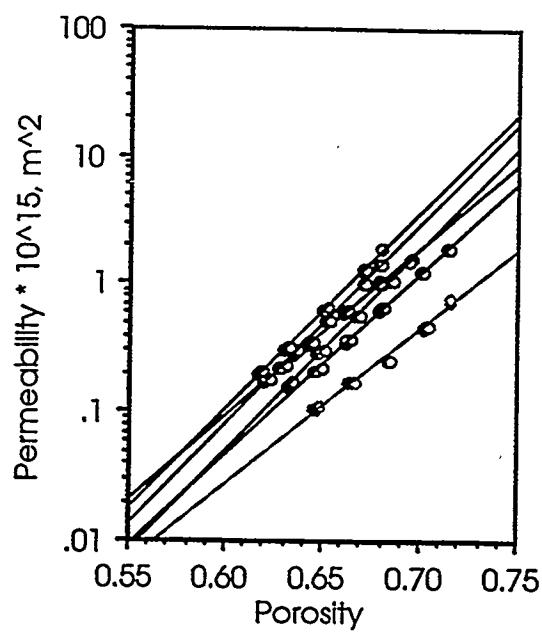


Figure D65. Furnish W19, press condition P5.

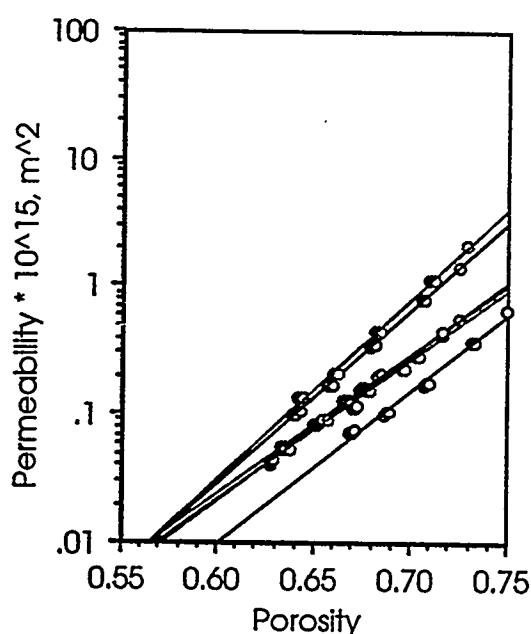


Figure D66. Furnish W20, press condition P1.

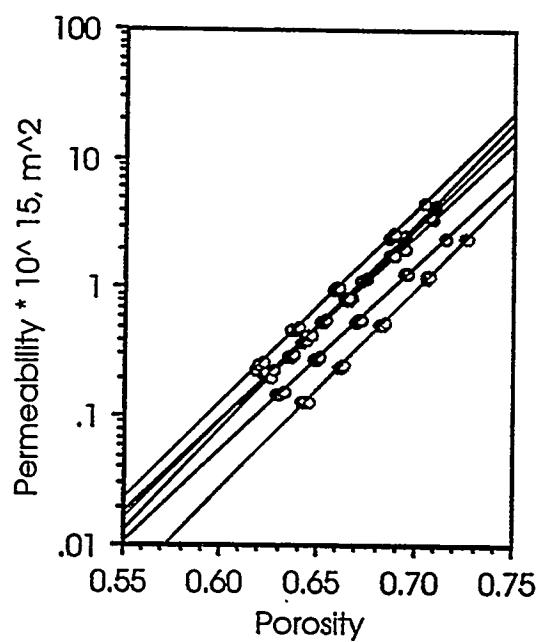


Figure D67. Furnish W20, press condition P2.

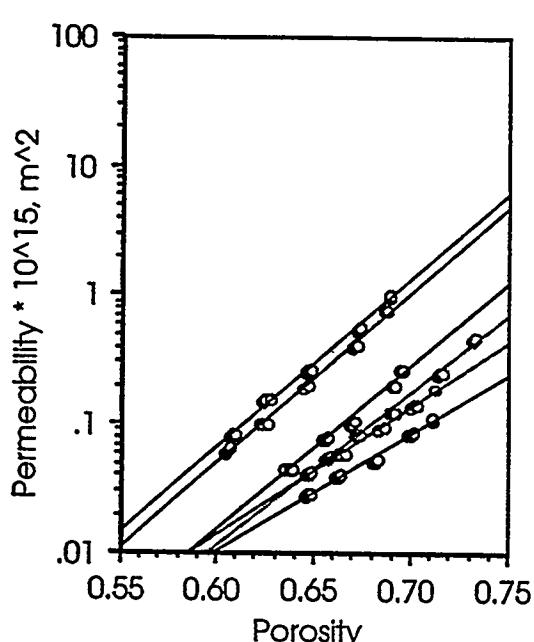


Figure D68. Furnish W20, press condition P3.

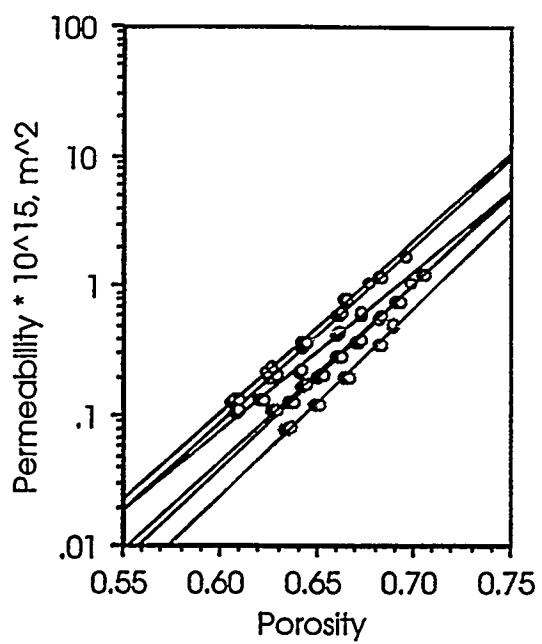


Figure D69. Furnish W20, press condition P4.

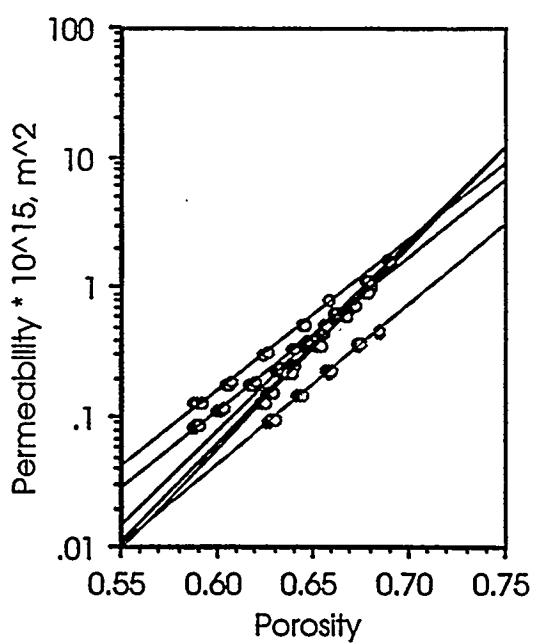


Figure D70. Furnish W20, press condition P5.

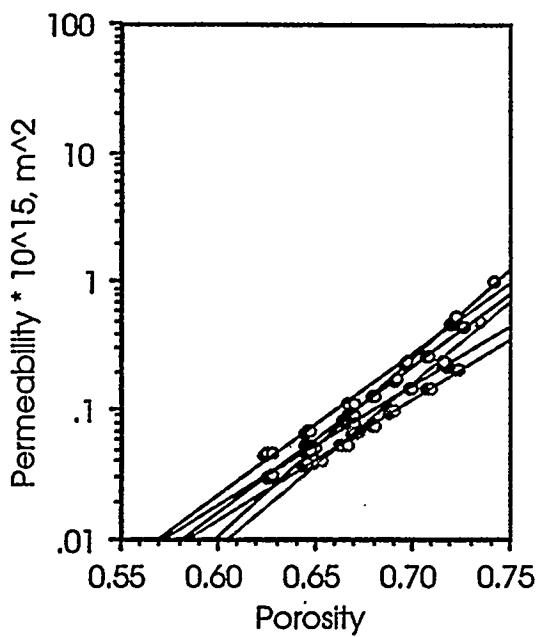


Figure D71. Furnish W21, press condition P1.

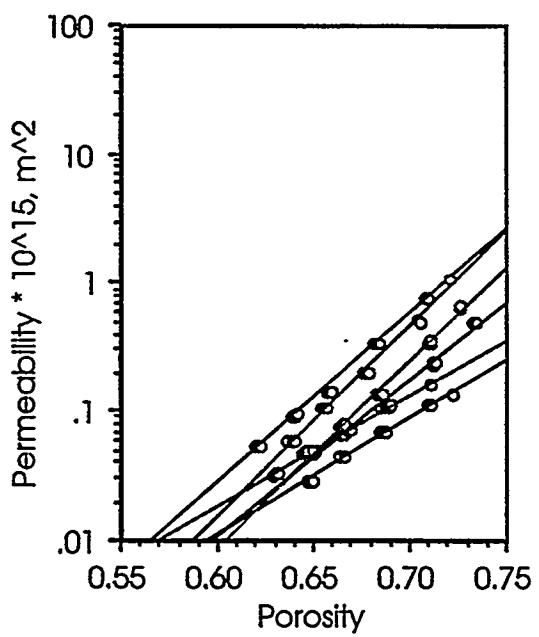


Figure D72. Furnish W21, press condition P2.

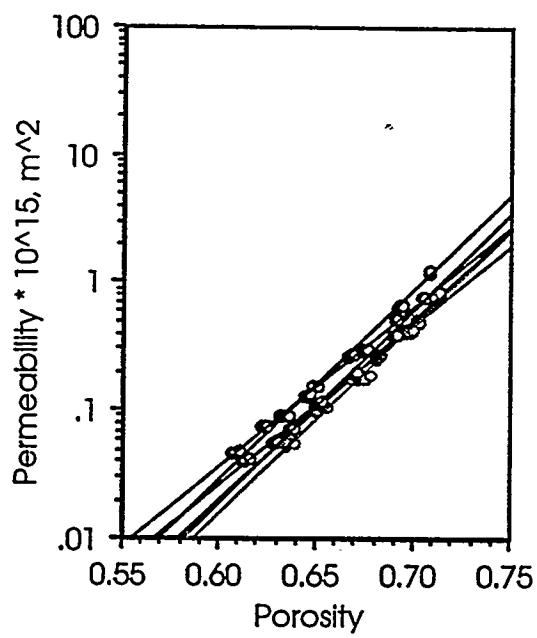


Figure D73. Furnish W21, press condition P3.

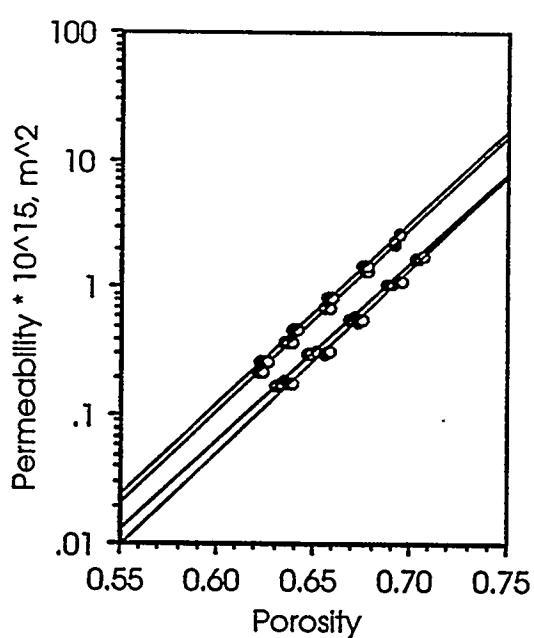


Figure D74. Furnish W21, press condition P4.

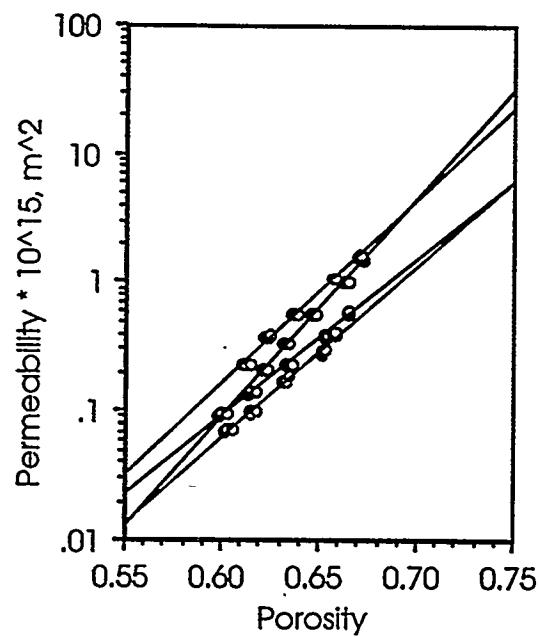


Figure D75. Furnish W21, press condition P5.

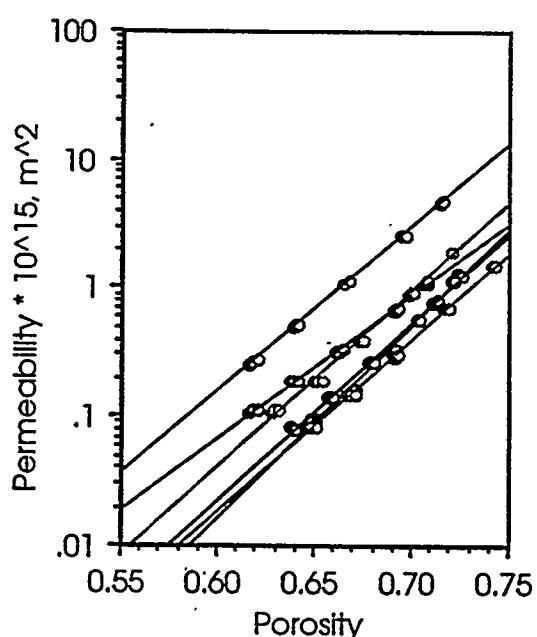


Figure D76. Furnish W22, press condition P1.

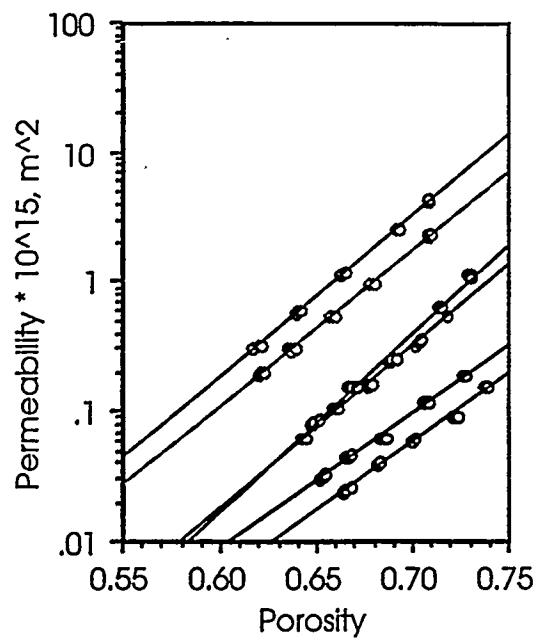


Figure D77. Furnish W22, press condition P2.

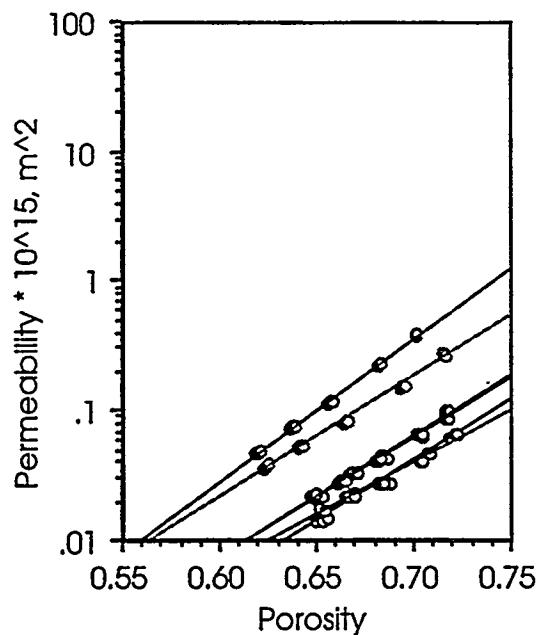


Figure D78. Furnish W22, press condition P3.

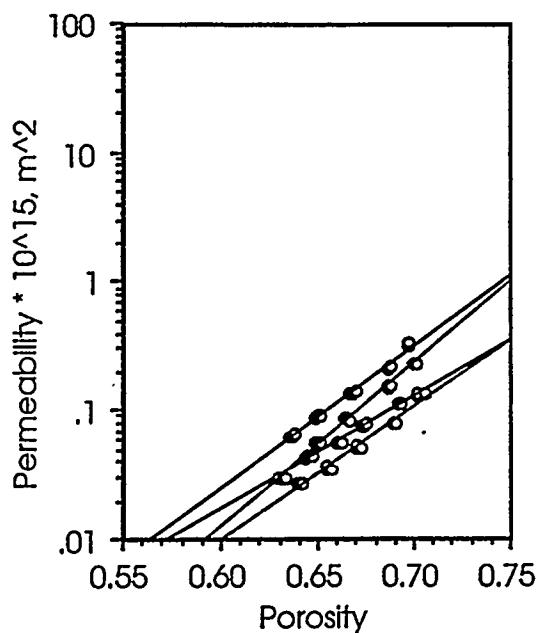


Figure D79. Furnish W22, press condition P4.

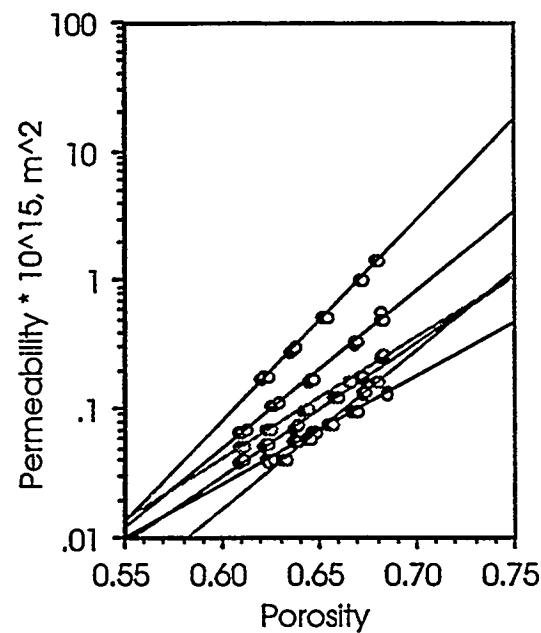


Figure D80. Furnish W22, press condition P5.

APPENDIX E

The following figures show the temperatures recorded during presteaming. Time zero is when the steam is first turned on. The steaming time was set to the time when the lowest temperature exceeded 55°C.

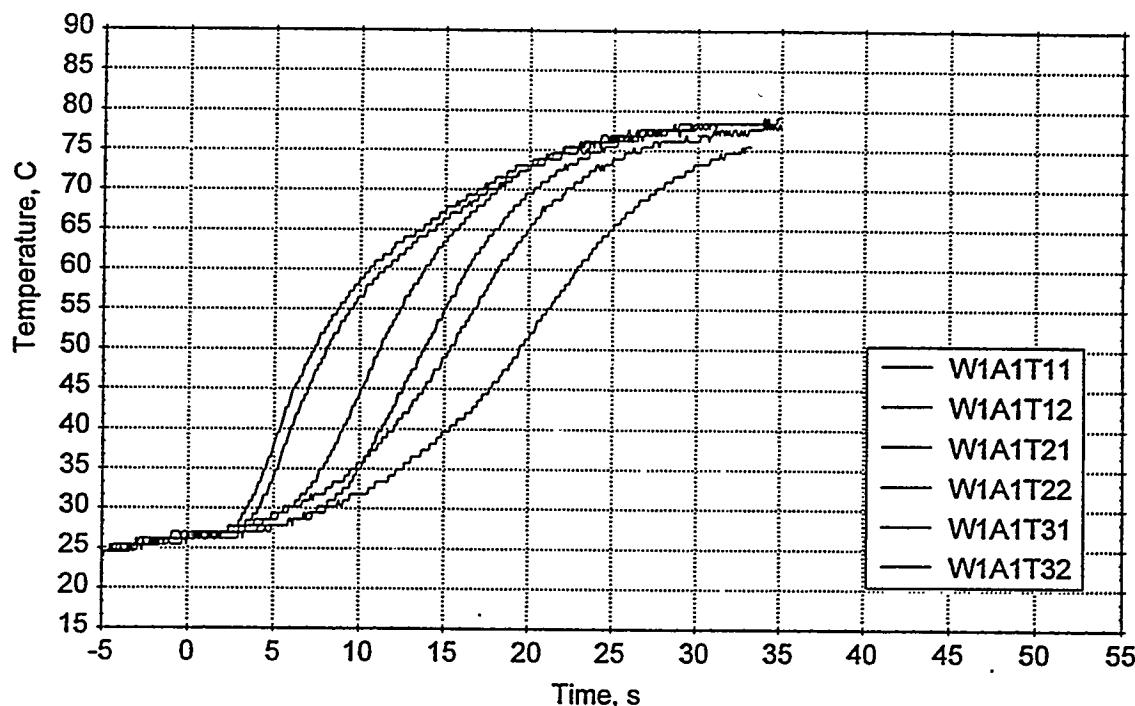


Figure E1. Furnish W1 (2P1), A platen, B felt, 35% sheet solids.

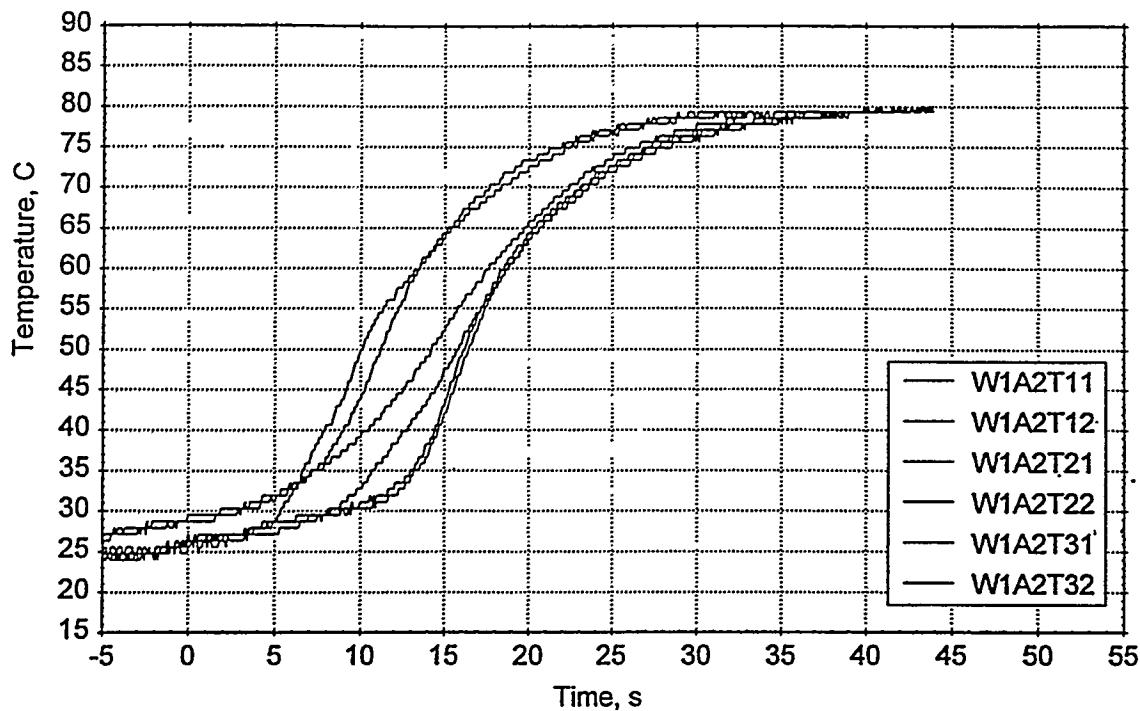


Figure E2. Furnish W1 (2P1), A platen, B felt, 42% sheet solids.

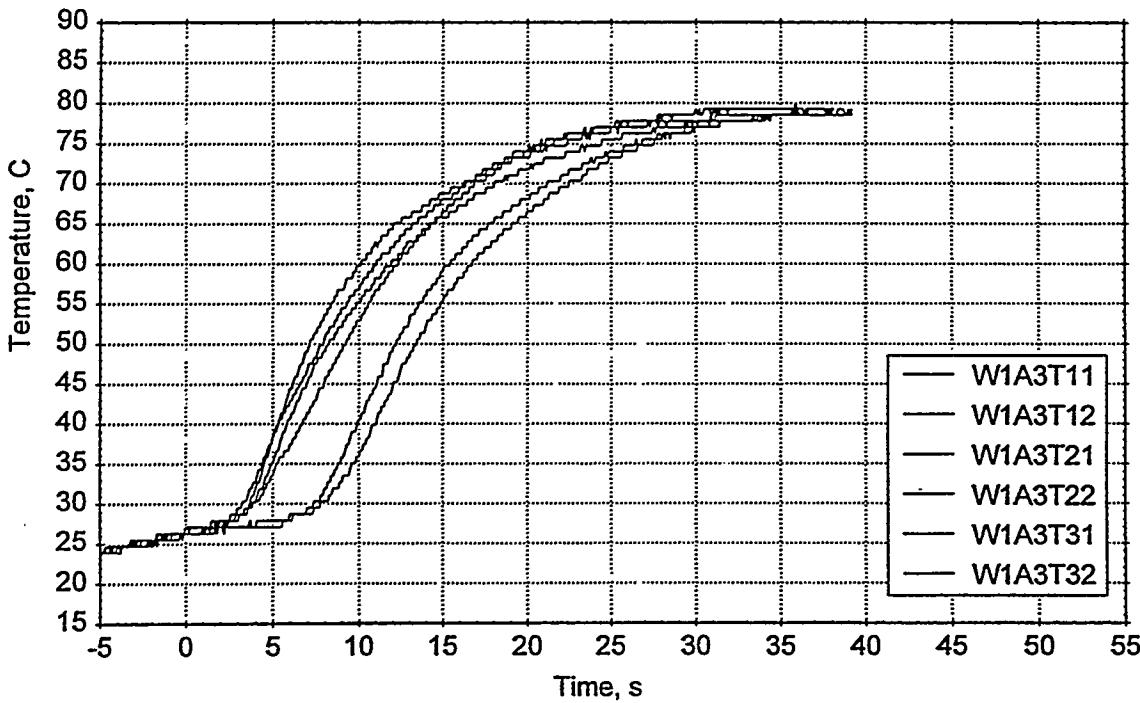


Figure E3. Furnish W1 (2P1), A platen, R felt, 35% sheet solids.

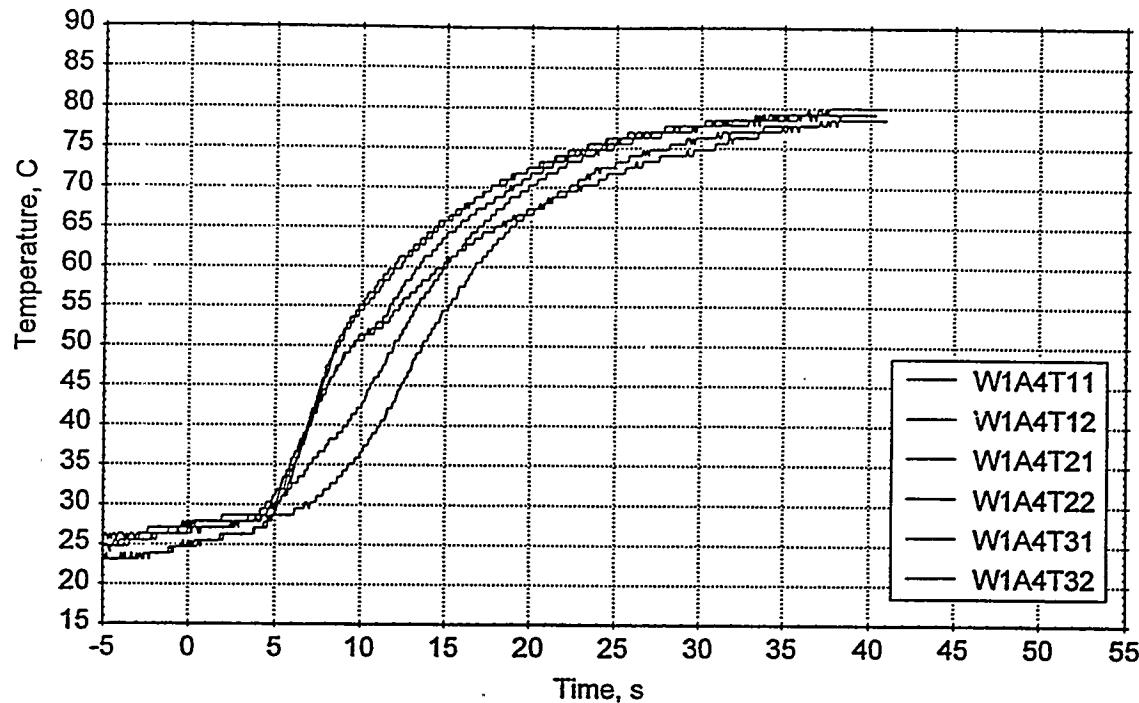


Figure E4. Furnish W1 (2P1), A platen, R felt, 42% sheet solids.

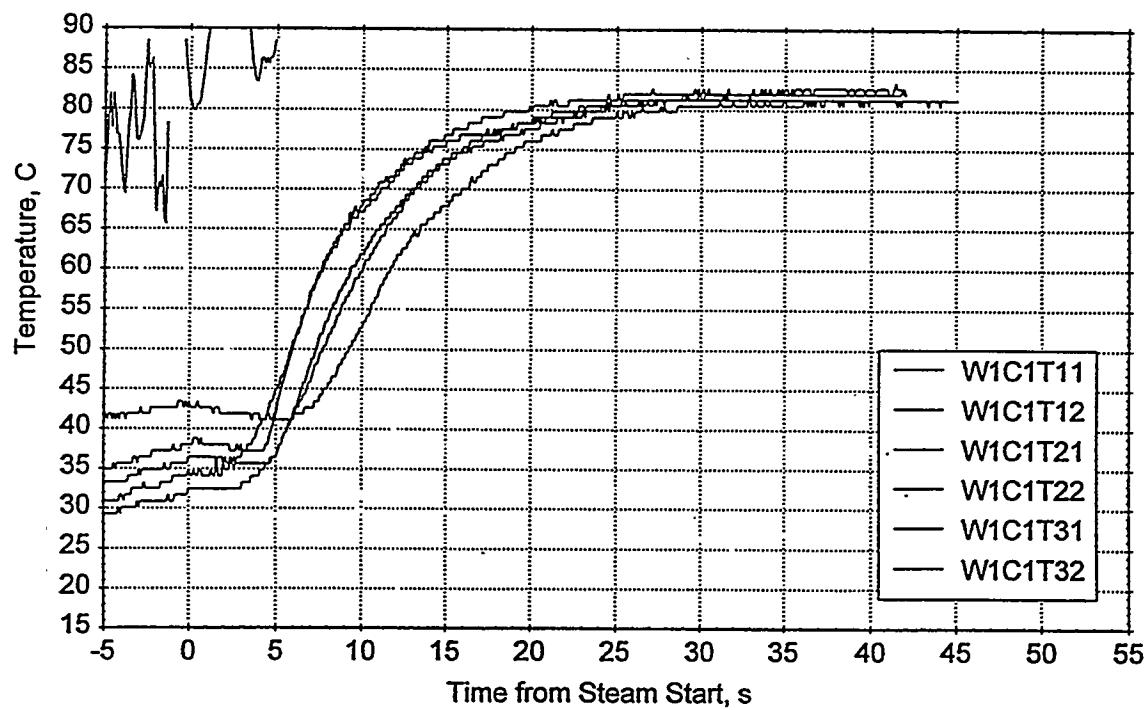


Figure E5. Furnish W1 (2P1), C platen, B felt, 35% sheet solids.

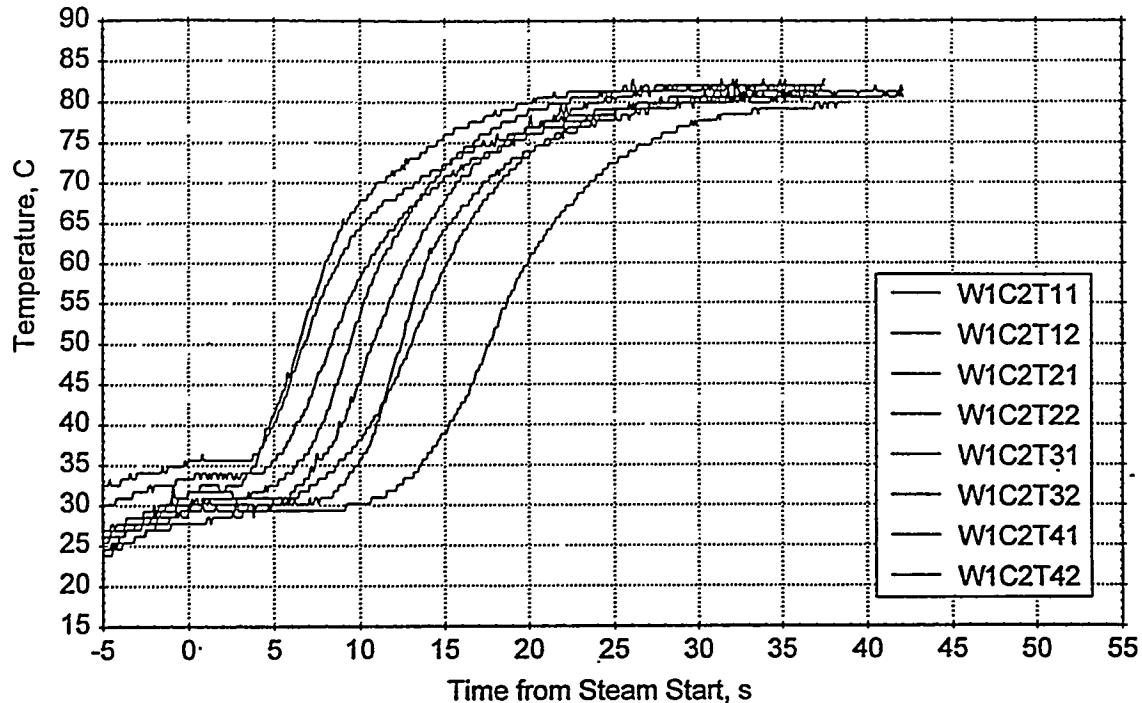


Figure E6. Furnish W1 (2P1), C platen, B felt, 42% sheet solids.

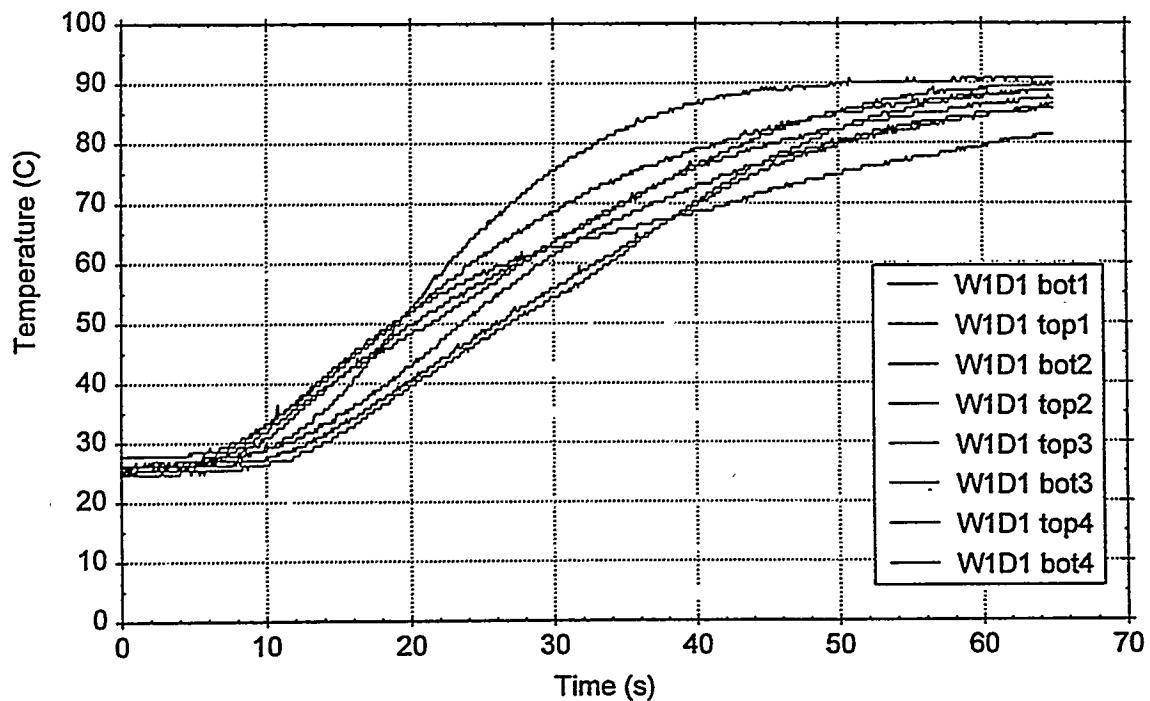


Figure E7. Furnish W1 (2P1), double-felted pressing, B felt, 35% sheet solids.

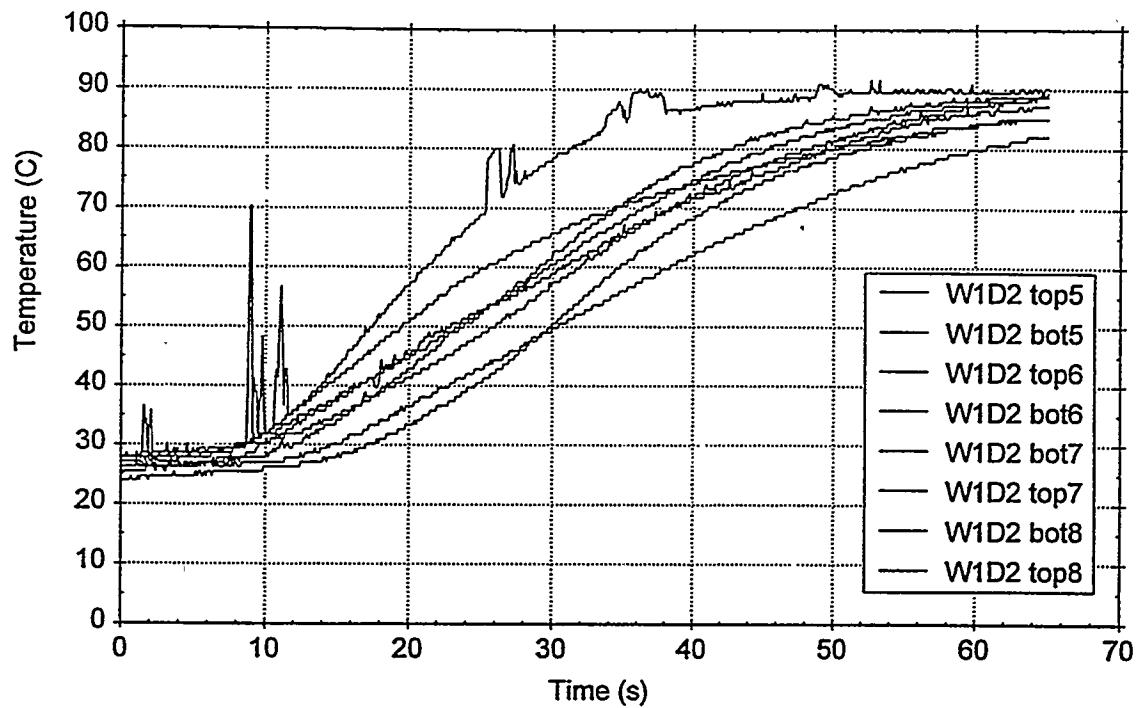


Figure E8. Furnish W1 (2P1), double-felted pressing, B felt, 42% sheet solids.

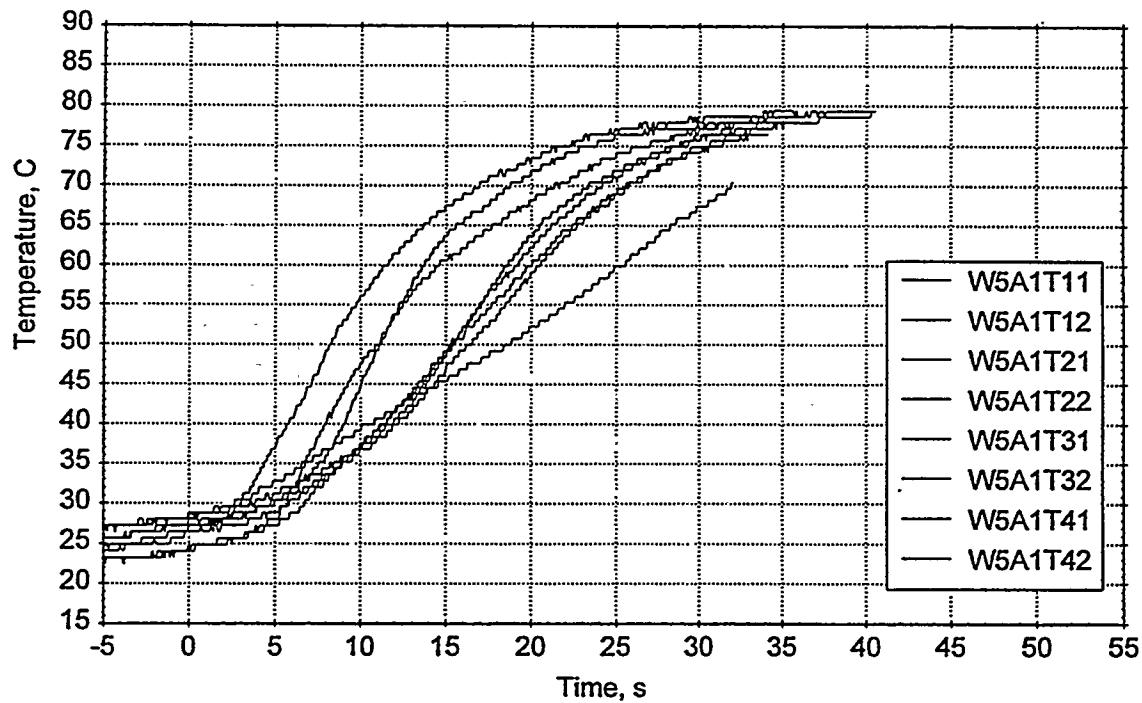


Figure E9. Furnish W5 (2P3), A platen, B felt, 35% sheet solids.

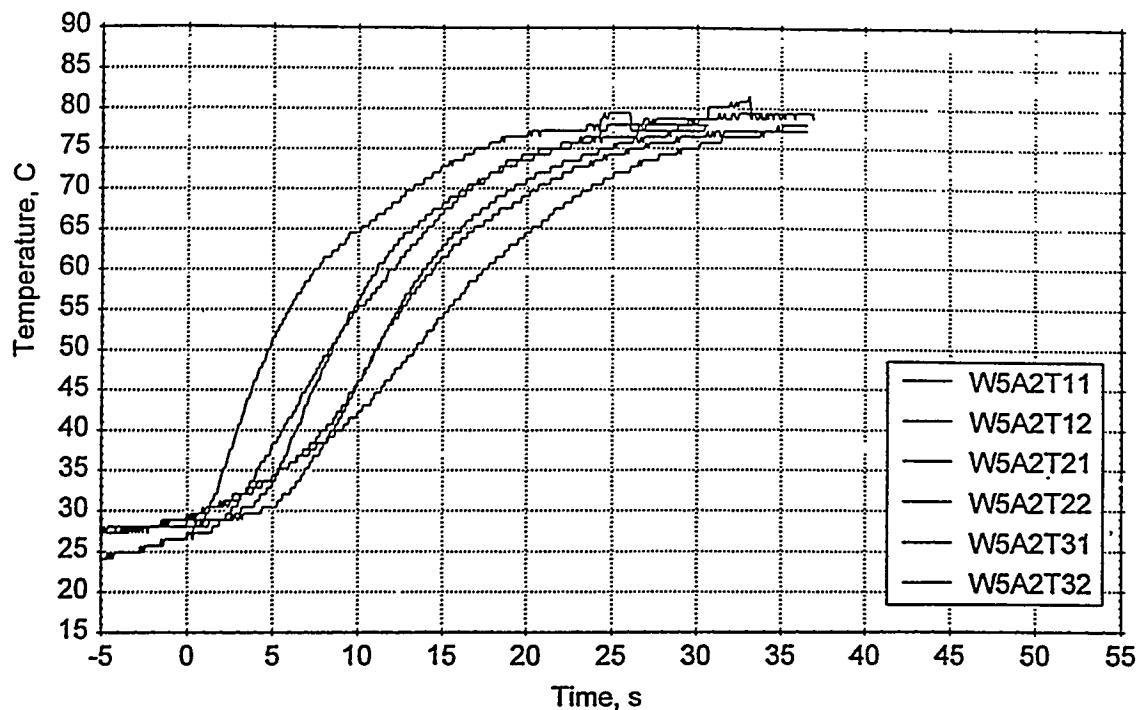


Figure E10. Furnish W5 (2P3), A platen, B felt, 42% sheet solids.

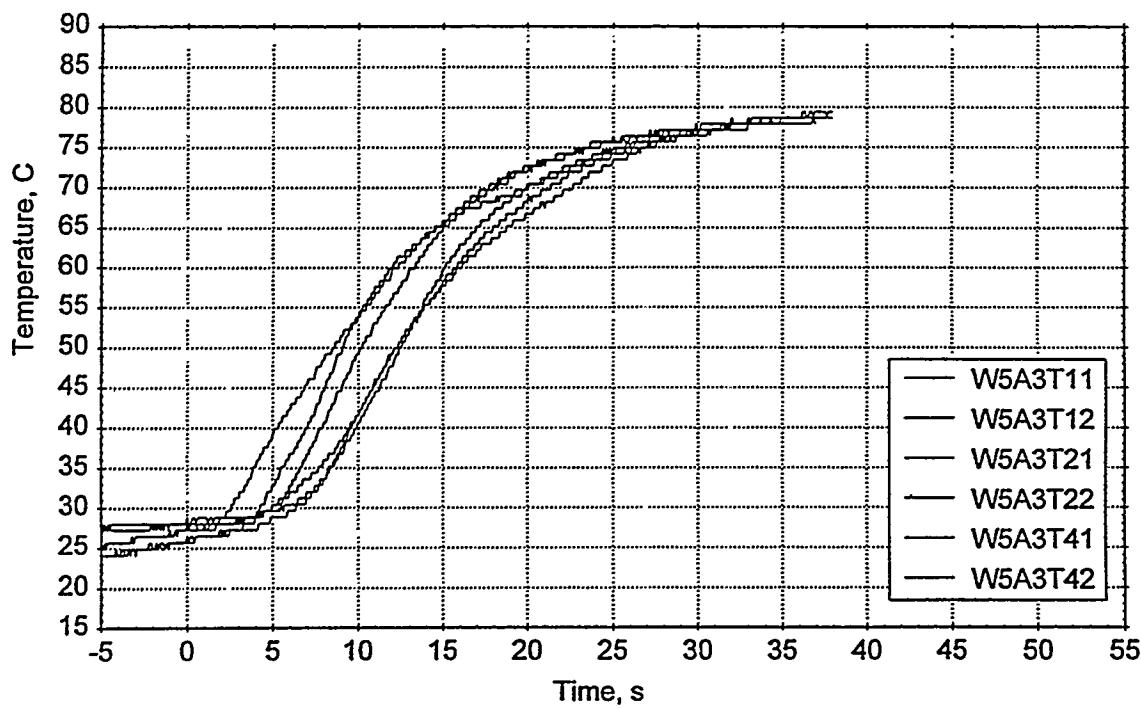


Figure E11. Furnish W5 (2P3), A platen, R felt, 35% sheet solids.

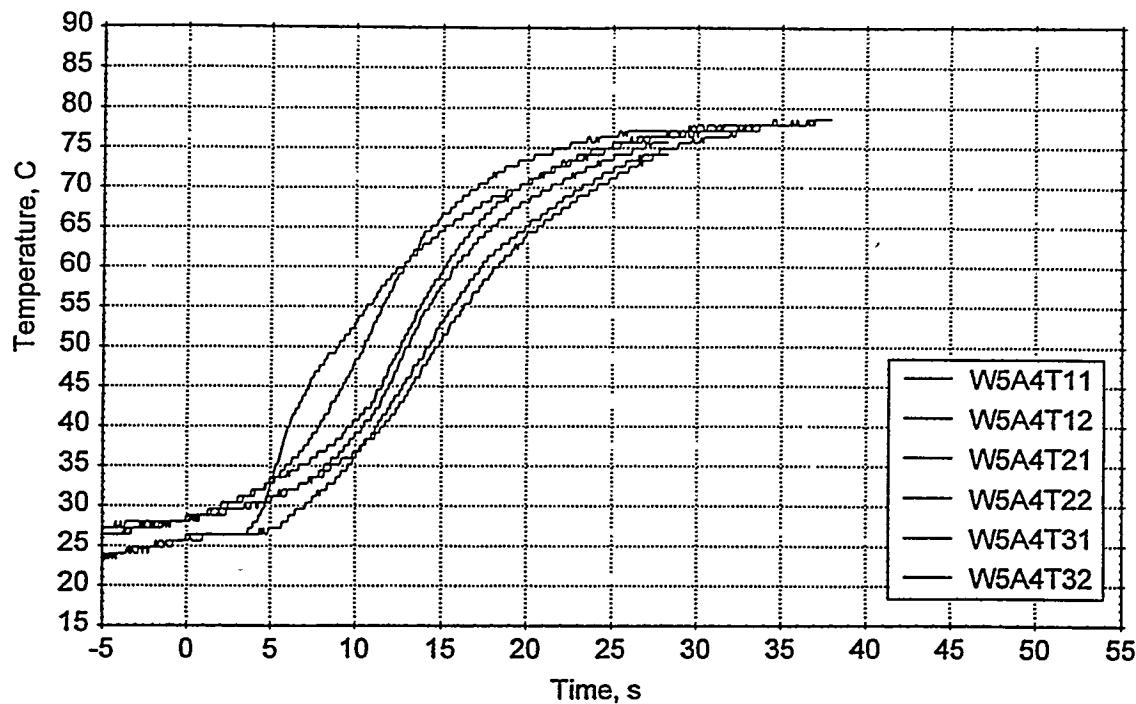


Figure E12. Furnish W5 (2P3), A platen, R felt, 42% sheet solids.

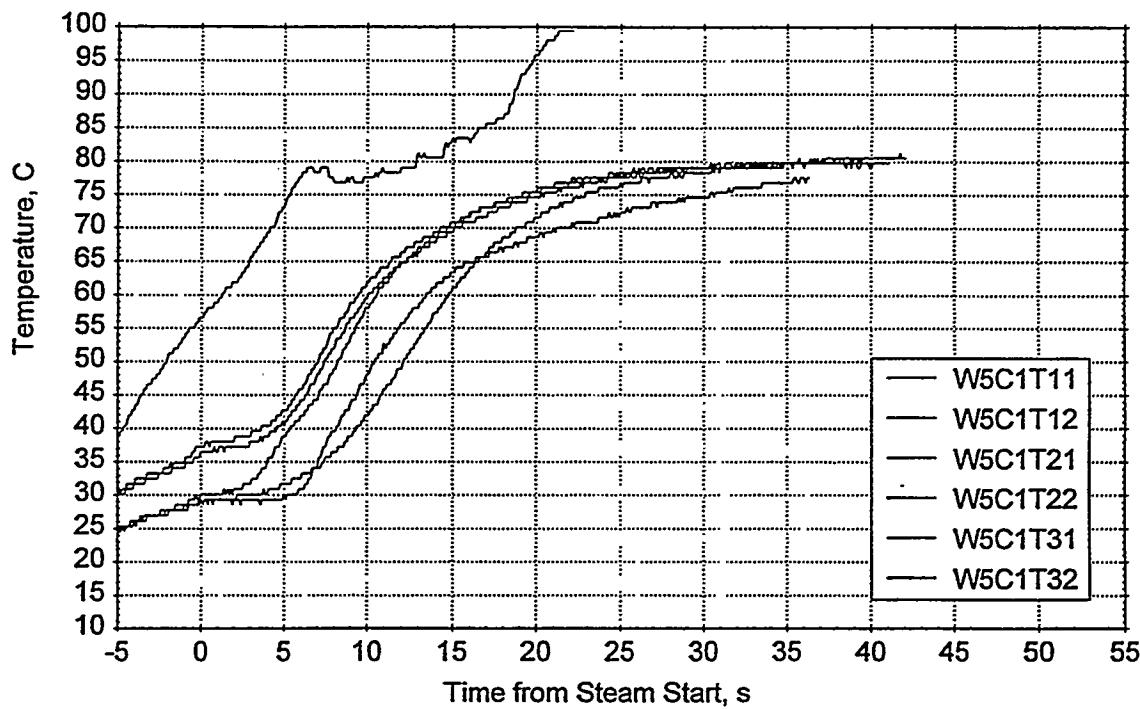


Figure E13. Furnish W5 (2P3), C platen, B felt, 35% sheet solids.

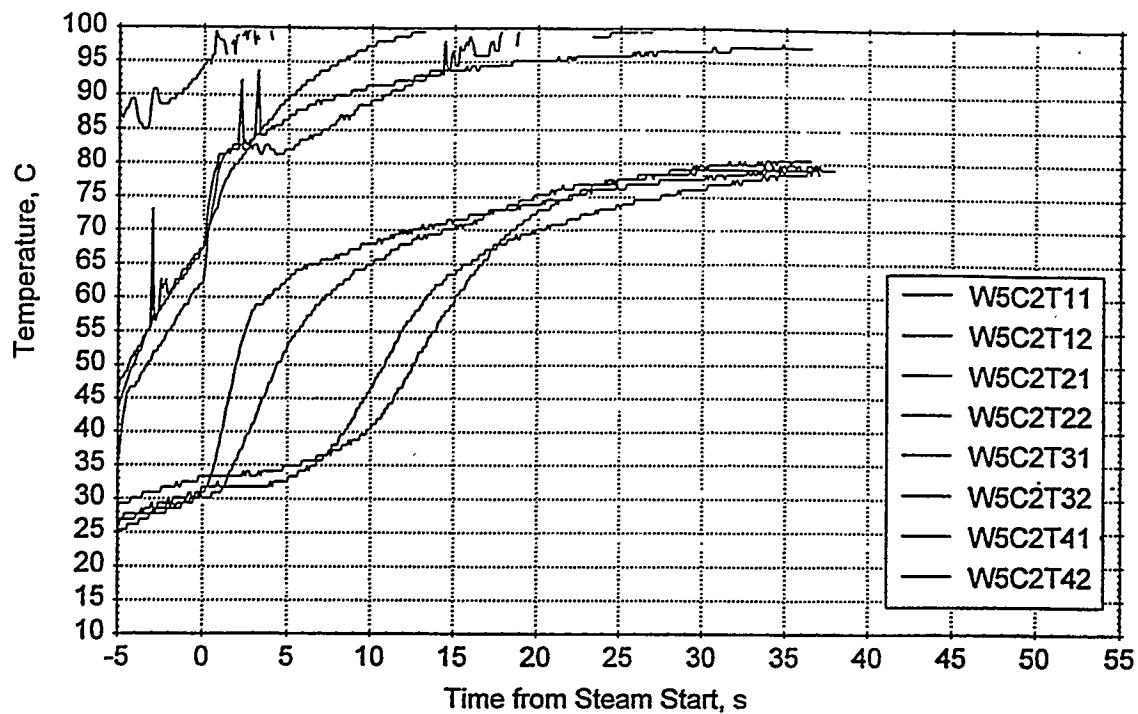


Figure E14. Furnish W5 (2P3), C platen, B felt, 42% sheet solids.

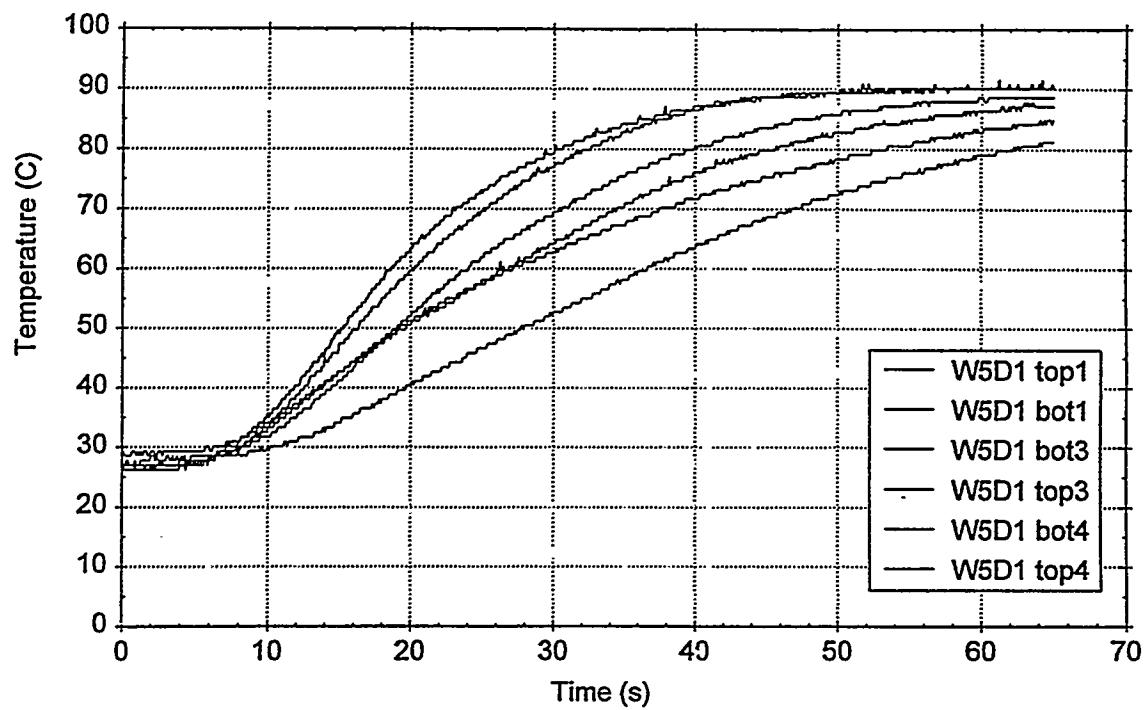


Figure E15. Furnish W5 (2P3), double-felted pressing, B felt, 35% sheet solids.

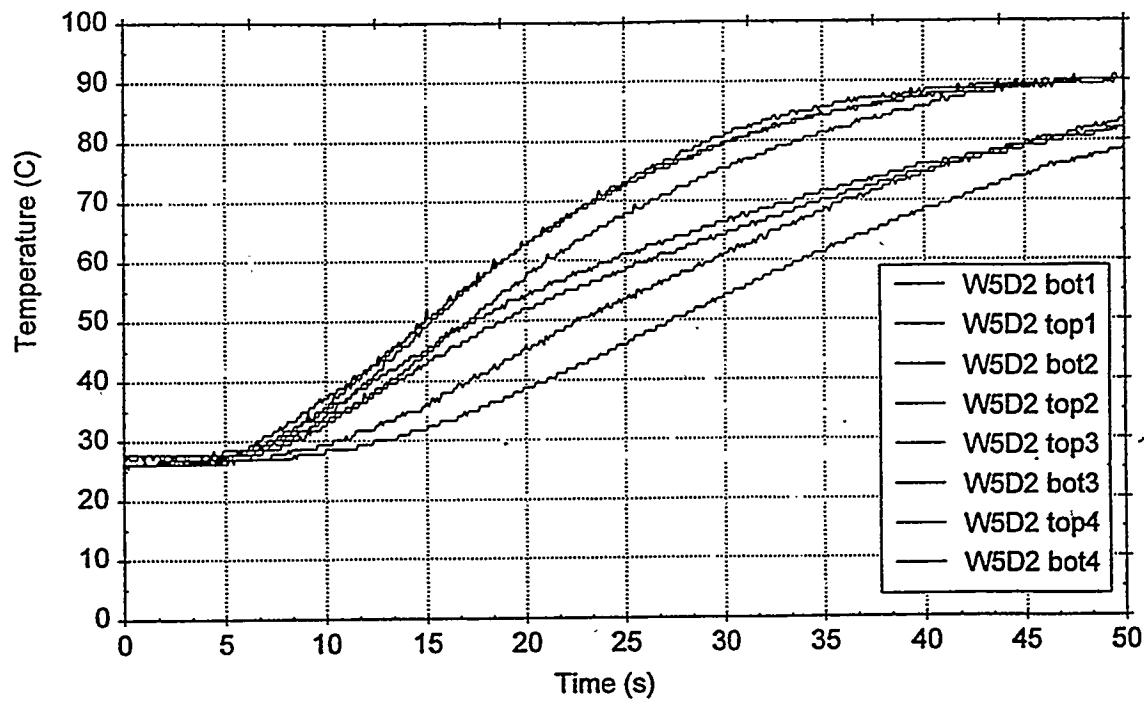
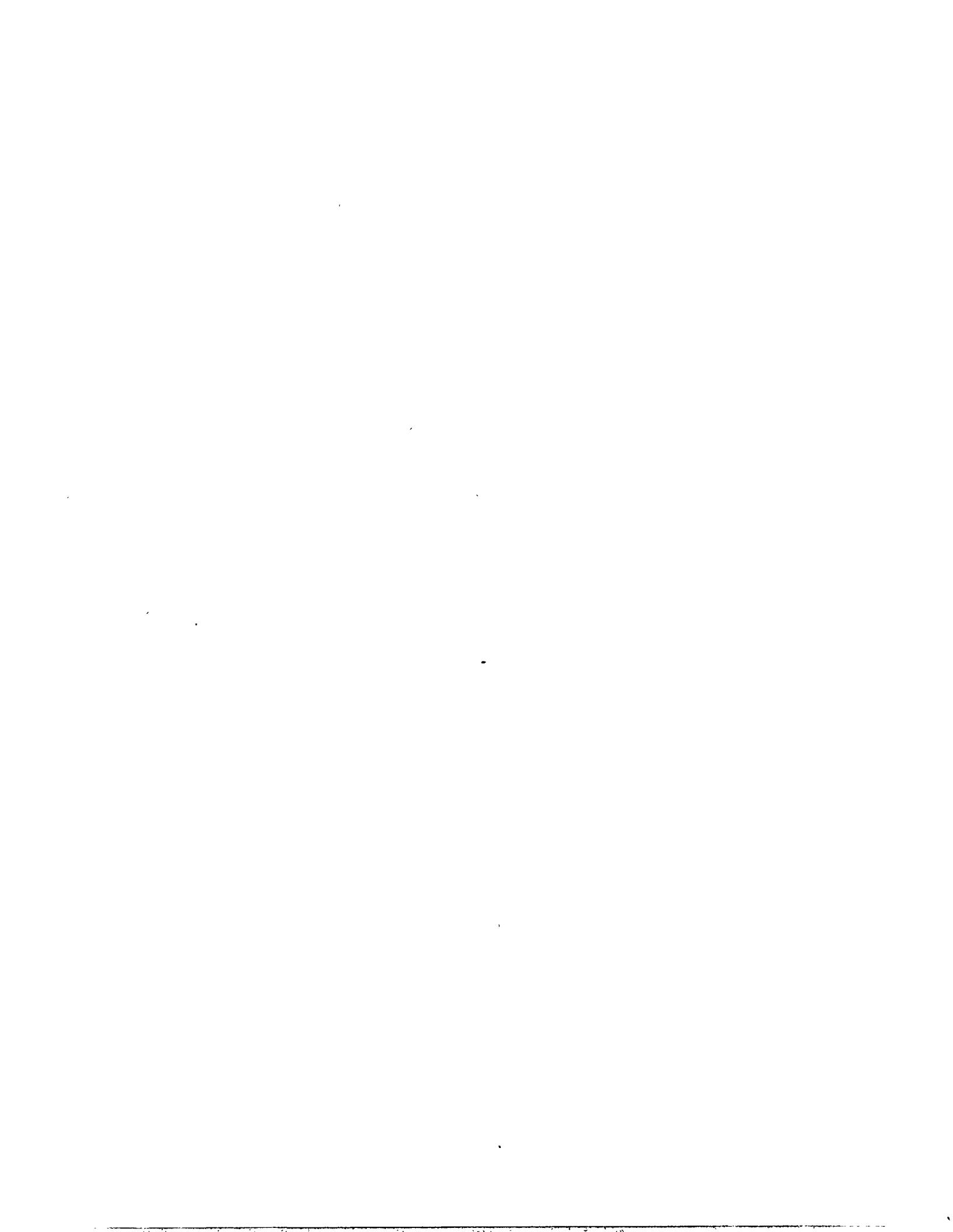


Figure E16. Furnish W5 (2P3), double-felted pressing, B felt, 42% sheet solids.



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